

An optimal control approach to the problem of the longest self-supporting structure

Giacomo Vecchiato¹, Michele Palladino^{1,2}, and Pierangelo Marcati¹

¹Gran Sasso Science Institute, L'Aquila, Italy

²DISIM, Department of Information Engineering, Computer Science and Mathematics, University of L'Aquila, Via Vetoio - 67100 L'Aquila, Italy

June 21, 2023

Abstract

The characterisation of the self-supporting slender structure with the furthest length is of interest both from a mechanical and biological point of view. Indeed, from a mechanical perspective, this classical problem was developed and studied with different methods, for example using similarity solutions and stable manifolds. However, none of them led to a complete analytical solution. On the other hand, plant structures such as tree branches or searcher shoots in climbing plants can be considered elastic cantilevered beams. In this paper, we formulate the problem as a non-convex optimisation problem with mixed state constraints. The problem is solved by analyzing the corresponding relaxation. With this method, it is possible to obtain an analytical characterization of the cross-section

1 Introduction

In the last decades, there has been an increasing interest in plant modelling. Indeed, recent studies on how plants perceive and react to the external environment (see [1, 2, 3, 4] for instance) led to a deeper insight into the plant growth mechanism. Current models consider proprioception [2], internal fluxes of hormones [5] or memory in the elaboration of the external cues [4]. Plant self-supporting structures are modelled like morphoelastic rods, whose curvatures change in time accordingly to the plant sensing activity. Furthermore, plants exhibit a great variability of the biomechanical properties *intra* and *inter* species [6]. In particular, climbing plants are a clear example of this structural variety. Consider the species *Condylocarpon guianense*, a common liana widely found in the flora of French Guyana. *C. guianense* is a twining climbing plant, which means that it reaches the canopy of the forest by twining around the branches and the trunks of its hosts. Several studies on its structure (see [7, 6, 8] for instance) have revealed that in different growth stages, it changes the

thickness and the nature of the layers that form its stem and consequently, it changes its stiffness. More specifically, the plant is stiffer when and where is developing a self-supporting state, while it displays a less dense material and a thicker compliant cortex when attached to a support.

Thanks to their wide adaptability, plants became a source of inspiration for new technologies and robots [9, 10]. For instance, the movement of the roots into the ground has inspired the development of new ways for soil exploration [11]. And again, the efficient strategies to attach their bodies to external supports have led to the development of a robot that imitates in essence the wrapping movement and the stem stiffening of tendrils [12]. In this framework, mathematical models based on an optimal control approach are a valuable resource to understand better the mechanisms used by plants to interact with the external environment.

In this paper, we are interested in modelling the self-supporting structures developed by climbing plants. These structures are called *searcher shoots* and are generated by the plant in order to explore and find support. The mechanics of the searcher shoots is an interesting and challenging study [13] because they exhibit both active and passive movements and must find a compromise between rigidity and flexibility to explore the surrounding environment and navigate obstacles and supports. In particular, we want to use the tools of optimal control theory to better understand how the mass is distributed along a searcher shoot. More precisely, for a given amount of mass, we want to find the best way to distribute it so as to maximize the length of the shoot and not exceed a given amount of mechanical stress. To achieve this goal, we formulate an optimal control problem for a time (length) maximization subject to mixed-state constraints. This optimization problem belongs to a classical category of problems on beam buckling. In particular, in 1960 J. B. Keller [14] investigated the shape of the column that has the largest buckling load. From that work, further studies and methods were developed to solve the problem of the tallest column. Of particular note in this line of research are the works of Y. Farjoun and J. Neu [15], and Z. Wei et al. [16]. In the former work, a symmetry of the dynamical system is employed to solve the boundary value problem related to maximizing height. In the latter work, the same technique is used to solve the problem of the tree branch with the furthest reach. In that work, the problem's solution is studied analytically towards the tip, while the whole behaviour is displayed only via numerical simulations. Here, the problem is slightly different, since we look for a *length* maximization. Moreover, we employ a deeper study of the necessary conditions for the solution optimality to characterize analytically the optimal radius of the cross-section.

This work is structured in the following way. In section 2, we use the theory of elastic rods to derive the differential equation of the mechanics for the searching shoot. Then, we couple this equation with the boundary and stress constraints, and a cost function. In this way, we state the optimal control problem on length maximization. In section 3, we extend the dynamic by convexification of the velocities set. This relaxation of the problem allows us to prove an optimal solution's existence. In section 4, we reformulate the opti-

mal control problem and we find a set of necessary conditions for the optimal trajectory. Then, in section 5 we study the corresponding adjoint system and obtain a feedback formula for the optimal control u^* . Finally, in section 6, we make some numerical simulations for the optimal trajectory and the adjoint arcs based on experimental data. In the last sections, we discuss the results of these simulations and the analytical optimal solution.

2 Derivation of the Model

{sec:DerOfMod}

We model the searcher shoot as an inextensible and unshearable elastic rod whose centerline is confined in a plane. Let be $\{e_1, e_2, e_3\}$ an orthonormal base for \mathbb{R}^3 . Then we represent the centerline of the rod with a curve $r \in C^2([0, L] \rightarrow \mathbb{R}^3)$ of length L . We parametrize the curve with its arc-length parameter $s \in [0, L]$ and we assume that $r \in \text{span}\{e_1, e_3\}$. For the rod cross-section, we consider as generalized frame [17] the Frenet mobile system $\{\nu, \beta, \tau\}$, formed respectively by the normal, binormal and tangent vectors. Naming $\theta(s)$ the angle between $\tau(s)$ and e_2 (that is, the vertical line), the curvature $\kappa(s)$ is simply

$$\theta'(s) = \kappa(s),$$

where “ $'$ ” denotes the derivative with respect to s . Since r is confined in the plane, it is entirely described by its initial point $r(0)$, initial inclination $\theta(0)$ and its curvature κ .

We want to account for the gravity force acting on the rod r , $\{\nu, \beta, \tau\}$. To achieve this aim, we consider another configuration \hat{r} , $\{\hat{\nu}, \hat{\beta}, \hat{\tau}\}$ confined in $\{e_1, e_3\}$. We refer to this latter configuration as *intrinsic* configuration, and it represents the shape that the rod would have in the absence of gravity. Instead, we refer to the former configuration as the *current* configuration. In response to the gravity force, the rod generates an internal force n and an internal moment (of force) m . Assuming that the gravity force is oriented along $-e_3$ and that it is balanced by the rod’s response, we get the following set of equations:

$$\begin{cases} n' - e_3 g \rho = 0 \\ m' + r' \times n = 0, \end{cases} \quad (1) \quad \{\text{eq:Balance}\}$$

where g is the gravity acceleration constant and ρ is the density per unit of length of the rod. We refer to ρ as *linear density*. To close the set of differential equations, we need a constitutive relationship between the internal moment and the difference between the intrinsic and the current curvature. The Euler-Bernoulli law provides a classical relationship of this kind, which in the planar case reads the following form

$$m = EI(\kappa - \hat{\kappa}). \quad (2) \quad \{\text{eq:ConstRel}\}$$

In this equation, the quantity E is the Young’s modulus and it measures the stiffness of the rod. Furthermore, the quantity I is the second moment of area of

the cross-section along the direction given by the normal vector n . Considering together system (1) and equation (2), we obtain

$$(E(s)I(s)(\hat{\kappa} - \theta'(s)))' = \sin \theta(s) g \int_s^L \rho(\sigma) d\sigma, \quad (3) \quad \{\text{eq:e1_rod0}\}$$

where we are also assuming that there is not any external load at the rod's tip. This means that $n(L) = 0$.

2.1 Stress Threshold

As expressed by equations (1), when an elastic rod is subject to external forces, the material generates the internal moment m in response [18]. This moment causes the deflection of the rod. The internal pressure that generates m is called (bending) *stress* and we name it σ . Let $\mathcal{S}(s)$ be the cross-section of the rod r at $r(s)$. We define

$$\mathcal{S}(s, z) = \{w \in \mathbb{R} : r(s) + z\nu(s) + w\beta(s) \in \mathcal{S}(s)\}.$$

Then the maximal stress $\sigma_m(s)$ acting on $\mathcal{S}(s)$ is [18]

$$\sigma_m(s) = \max\{z : \in \mathcal{S}(s) \neq \emptyset\} \cdot E|\kappa(s) - \theta'(s)|.$$

We assume that the maximal stress σ_m exerted on the bar cannot cross a certain fixed threshold $\bar{\sigma}$.

2.2 Formulation of the problem

We analyse the case of an elastic rod with a circular cross-section of radius R . In this situation, we have

$$I = \frac{\pi}{4} R^4.$$

So, the norm of the maximal stress is

$$\sigma_m = |\theta' - \hat{\kappa}|RE.$$

The mass of the shoot is represented by the linear density ρ of the main stem, which is related to the density per unit of volume ρ_3 and the radius R by the equation

$$\rho = \rho_3 \pi R^2.$$

To formulate our problem, we consider the volume density ρ_3 and the Young's modulus E constant along the shoot. Furthermore, we assume that the main stem does not have any secondary branches or leaves. Then, we represent the optimal control problem of the shoot length maximization with the following

system:

$$\begin{cases} \max_{(R,L) \in \mathcal{U}} L \\ \text{subject to} \\ (-R^4(\theta'(s) - \hat{\kappa}(s)))' = \tilde{c}_1 \sin \theta(s) \left[\int_s^L \rho_3 \pi R^2(\sigma) d\sigma \right] \\ \theta(0) = \theta_0 \\ \theta'(L) = \hat{u}_1(L) \\ \int_0^L \pi \rho_3 R^2(\sigma) d\sigma = M \\ |\theta' - \hat{\kappa}| \leq \frac{c_2}{R}. \end{cases} \quad (4) \quad \{\text{eq:auxiliary_0}\}$$

Here

$$\tilde{c}_1 = \frac{4g}{\pi E}, \quad c_2 = \frac{\bar{\sigma}}{E}.$$

The boundary conditions mean that we are fixing an initial inclination of the rod equal to θ_0 and that we are considering just the weight of the rod, without any extra element at the tip, so the intrinsic and the current curvatures coincide. The constraint $\int_s^L \pi \rho_3 R^2(\sigma) d\sigma = M$ is due to the fact that we are fixing the total mass of the main stem. The set of the controls \mathcal{U} will be specified later on in the presentation. We consider the case $\hat{\kappa} \equiv 0$.

We introduce the variables:

$$\begin{aligned} \mu(s) &= \int_s^L R^2(\sigma) d\sigma, \\ \psi &= -R^4(\theta' - \hat{u}_1), \\ u &= R^2, \\ c_1 &= \frac{4g\rho_3}{E}. \end{aligned}$$

To avoid pathological and rather unrealistic situations, we assume to have an upper bound and a lower bound on the variable u , that is $u_M \geq u \geq u_m$. Using these new variables and conditions, we obtain from (4) the optimization problem:

$$\begin{cases} \max_{(u,L) \in \mathcal{U}} L \\ \text{subject to} \\ x'(s) = f_P(x(s), u(s)) & \text{a.e. in } [0, L] \\ (x(0), x(L)) \in C_{P,0} \times C_{P,1} \\ h_{P,1}(x(s), u(s)) \leq 0 & \text{a.e. in } [0, L] \\ h_{P,2}(x(s), u(s)) \leq 0 & \text{a.e. in } [0, L] \end{cases} \quad (P) \quad \{\text{eq:problem0}\}$$

where

- $\theta_0 \in [0, 2\pi]$ and $c_1, c_2, u_0, M \in (0, +\infty)$;
- $x = (\psi, \theta, \mu) \in W^{1,1}([0, L]; \mathbb{R}^3)$;

- $\mathcal{U} = \{(u, L) : L > 0 \text{ and } u : [0, L] \rightarrow \mathbb{R} \text{ Lebesgue measurable}\}$;
- $f_P(x, u) = (c_1 \mu \sin \theta, -\psi/u^2, -u)$;
- $C_{P,0} = \mathbb{R} \times \{\theta_0\} \times \{M\}$;
- $C_{P,1} = \{0\} \times \mathbb{R} \times \{0\}$;
- $h_{P,1}(x, u) = \max\{u_m - u, u - u_M\}$;
- $h_{P,2}(x, u) = |\psi| - c_2 u^{3/2}$.

We will see that the upper bound u_M for u is a fundamental assumption to prove the existence of an optimal solution in the convexified case. In general, the imposition of an upper bound on the set of controls may influence the solution to the optimization problem itself. As we will see, if u_M is large enough, this is not the case.

2.3 Notation for multifunctions

In the following, we denote with

$$F : X \subset \mathbb{R}^n \rightrightarrows \mathbb{R}^m$$

a multifunction from $X \subset \mathbb{R}^n$ to \mathbb{R}^m , that is a function whose domain is X and such that $F(x) \subset \mathbb{R}^m$ for every $x \in X$. The multifunction F is said *Borel measurable* if for any open set $A \subset \mathbb{R}^m$, the set

$$F^{-1}(A) = \{x \in X : F(x) \cap A \neq \emptyset\}$$

is a Borel subset of $X \subset \mathbb{R}^n$. Moreover, we say that the multifunction F is closed, convex or nonempty if for any $x \in X$ the set $F(x) \subset \mathbb{R}^m$ is respectively closed, convex or nonempty. We say that F is uniformly bounded if there exist a constant $\alpha > 0$ such that

$$F(x) \subset \alpha \mathbb{B}^m$$

for any $x \in X$. With \mathbb{B}^m we denote the closed unitary ball centred at the origin of \mathbb{R}^m . The graph of F is the set

$$\{(x, y) : x \in X, y \in F(x)\} \subset \mathbb{R}^n \times \mathbb{R}^m$$

3 Existence of optimal solutions

In this section, we construct a “minimal” modification of problem (P) in order to obtain an optimal control problem for which the existence of an optimal solution is guaranteed. To this aim, we first construct such an enlarged optimal control problem in section 3.1 and then we show that the latter has a feasible solution in section 3.2.

{sec:Rel}

3.1 Relaxation

{sec:Rel1}

To start with, we observe that the dynamics of the optimal control problem (P) can be reformulated in terms of a differential inclusion by defining

$$\dot{x}(s) \in F(x(s))$$

with

$$F(x) = \{(c_1 \mu \sin(\theta), -\psi/u^2, -u) : u \in U(x)\}$$

where

$$U(x) = \left\{ u \in [u_m, u_M], u \geq \left(\frac{|\psi|}{c_2} \right)^{2/3} \right\}.$$

It is well known that a key assumption for the existence of a solution for an optimal control problem is the convexity on the set of admissible velocities F (see e.g. [19]). However, it is easy to see in our case that such a standard existence hypothesis is not verified. A standard procedure to overcome such an issue, known as *relaxation*, is to enlarge the set of admissible trajectories in a way that the existence of a maximum is guaranteed. To this aim, we consider the convexified version of problem (P) :

$$\begin{cases} \max_{L \in [0, +\infty)} L \\ \text{Subject to} \\ x'(s) \in F_d(x(s)) & \text{a.e. } s \text{ in } [0, L] \\ (x(0), x(L)) \in C_{d,0} \times C_{d,1} \end{cases} \quad (P_d) \quad \{\text{eq:problemDI}\}$$

Here we are using the notation:

- $x = (\psi, \theta, \mu) \in W^{1,1}([0, L]; \mathbb{R}^3)$;
- $F_d(x) = \overline{\text{co}} \{F(x)\}$;
- $C_{d,0} = \mathbb{R} \times \{\theta_0\} \times \{M\}$
- $C_{d,1} = \{0\} \times \mathbb{R} \times \{0\}$

We say that $(x, L) \in W^{1,1}([0, L]; \mathbb{R}^3) \times [0, +\infty)$ is a trajectory for (P_d) if it satisfies the differential inclusion, that is $x'(s) \in F_d(x(s))$ for a.e. $s \in [0, L]$. A trajectory for (P_d) is admissible if it satisfies also the constraint $(x(0), x(L)) \in C_{d,0} \times C_{d,1}$. Analogously, we say that $(x, u, L) \in W^{1,1}([0, L]; \mathbb{R}^3) \times \mathcal{U}$ is a trajectory for (P) if $x' = f_P(x, u)$ a.e. in $[0, L]$ and it is admissible if all the constraints are satisfied. By construction, we observe that if (x, u, L) is an admissible trajectory for (P) then (x, L) is an admissible trajectory for (P_d) . Analogue terms are used for problem (P_c) in section 4.1.

{rem:charact}

Proposition 1. *The multifunction F_d has the following characterisation:*

$$F_d(x) = \{c_1 \mu \sin(\theta)\} \times \left\{ \left(-\psi \left(\frac{\lambda_1}{u_1^2} + \frac{\lambda_2}{u_2^2} \right), -(\lambda_1 u_1 + \lambda_2 u_2) \right) : (u_1, u_2, \lambda_1, \lambda_2) \in V(x) \right\},$$

where

$$V(x) = \{(u_1, u_2, \lambda_1, \lambda_2) : u_1, u_2 \in U(x) \text{ and } \lambda_1, \lambda_2 \in [0, 1], \lambda_1 + \lambda_2 = 1\}.$$

Proof. To prove Proposition 1, first we make the following consideration. Fix a point $x = (\psi, \theta, \mu) \in \mathbb{R}^3$ and define

$$u_0 = \max \left(u_m, \left(\frac{|\psi|}{u_m} \right)^{2/3} \right).$$

Then

$$F_d(x) = \{c_1 \mu \sin(\theta)\} \times \overline{c\mathcal{O}} \left\{ \left(\frac{\psi}{u^2}, u \right) : u \in [u_0, u_M] \right\}.$$

Hence, we can focus on the set

$$A := \overline{c\mathcal{O}} \left\{ \left(\frac{\psi}{u^2}, u \right) : u \in [u_0, u_M] \right\}.$$

We want to prove that

$$A = B := \left\{ \left(\lambda_1 u_1 + \lambda_2 u_2, \psi \left(\frac{\lambda_1}{u_1^2} + \frac{\lambda_2}{u_2^2} \right) \right) : (u_1, u_2, \lambda_1, \lambda_2) \in V(x) \right\}.$$

Let us use $g(u)$ to denote the function

$$\begin{aligned} g : [u_0, u_M] &\rightarrow \mathbb{R} \\ g(u) &= \frac{\psi}{u^2} \end{aligned}$$

and with $\ell : [u_0, u_M] \rightarrow \mathbb{R}$ the straight line that joins the point $(u_0, g(u_0))$ to the point $(u_M, g(u_M))$, that is

$$\ell(u) = g(u_0) + \left(\frac{g(u_M) - g(u_0)}{u_M - u_0} \right) (u - u_0).$$

Define

$$C := \text{epi}(g) \cap \text{hyp}(\ell),$$

where

$$\text{epi}(g) = \{(u, \alpha) : u \in [u_0, u_M], g(u) \leq \alpha\}$$

and

$$\text{hyp}(\ell) = \{(u, \beta) : u \in [u_0, u_M], \ell(u) \geq \beta\}.$$

Since g is a convex and continuous function and $\text{hyp}(\ell)$ is a convex set, C is a convex closed set containing $\left\{ \left(\frac{\psi}{u^2}, u \right) : u \in [u_0, u_M] \right\}$. In particular, one has that $A \subseteq C$.

Step 1: $C \subseteq B$.

Consider $(\bar{u}, \bar{v}) \in C$. Then one has that

$$g(\bar{u}) \leq \bar{v} \leq \ell(\bar{u}).$$

Take now the straight line $\ell_0 : [u_0, u_M] \rightarrow \mathbb{R}$ with the same slope of ℓ and such that $\ell_0(\bar{u}) = \bar{v}$, that is

$$\ell_0(u) = \bar{v} + \left(\frac{g(u_M) - g(u_0)}{u_M - u_0} \right) (u - \bar{u}).$$

By construction, one has that

$$\begin{aligned} \ell_0(u_0) &\leq \ell(u_0) = g(u_0), \\ \ell_0(u_M) &\leq \ell(u_M) = g(u_M). \end{aligned}$$

Hence, by using the continuity ℓ_0 , there exist u_1 and u_2 satisfying $u_1 \leq \bar{u} \leq u_2$ and such that

$$\begin{aligned} g(u_1) &= \ell_0(u_1) \\ g(u_2) &= \ell_0(u_2) \end{aligned}$$

which means that the point (\bar{u}, \bar{v}) is a convex combination of the points

$$(u_1, g(u_1)), (u_2, g(u_2)).$$

This shows that $C \subseteq B$.

Step 2: $A = B$.

Since it follows from *Step 1* that $C \subseteq B$, one also has $A \subseteq B$. On the other hand, it follows from the definition of B that also the inclusion $B \subseteq A$ holds. Hence one has that $A = B$. This completes the proof. \square

3.2 Existence of relaxed optimal solutions

{sec:Ref2}

In this section, we will show the existence of an optimal solution for (P_d) . To achieve this result, we begin by proving the existence of at least one admissible trajectory.

{prop:admissible}

Proposition 2. *Fix the constants*

$$c_1, c_2, u_m, M \in (0, +\infty) \text{ and } \theta_0 \in [0, 2\pi]$$

and choose

$$u_M \geq \max \left\{ u_m, c_1 M^2, M^{1/3}, \left(\frac{c_1}{c_2} M^2 \right)^{2/5} \right\}. \quad (HP_{max}) \quad \{\text{eq:umax}\}$$

Then there exists an admissible trajectory (x, u, L) for (P) .

Consequently, also problem (P_d) has at least one admissible trajectory.

Proof. To prove the statement, we make use of a fixed point argument. Let us fix the constant control $u = M/L$; for $L \leq M/u_m$ we have $u \geq u_m$, which implies that the lower bound given by $h_{P,1}$ is satisfied. Now, let us consider $\mu(t) =$

$(L-t)M/L$. It is easy to observe that the trajectory $((\psi, \theta + \theta_0, \mu), M/L, L)$ is admissible for problem (P) if and only if (ψ, θ, μ) solves the system

$$\begin{cases} \psi' = c_1 \frac{M(L-t)}{L} \sin(\theta + \theta_0) \\ \theta' = -\psi \frac{L^2}{M^2} \\ \psi(L) = 0 \\ \theta(0) = 0 \\ |\psi| \leq c_2 u^{3/2} \end{cases} \quad (5) \quad \{\text{eq:auxiliary_1}\}$$

for all $t \in [0, L]$. We define $X = \{\psi, \theta \in C([0, L]) : \psi(L) = \theta(0) = 0\}$. Then $(X, \|\cdot\|_\infty)$ ¹ is a Banach space. Consider the function $F : X \rightarrow X$

$$\begin{aligned} F(\psi, \theta)(s) &= \left(-\int_s^L c_1 \frac{M(L-t)}{L} \sin(\theta(t) + \theta_0) dt, -\int_0^s \psi(t) \frac{L^2}{M^2} dt \right) \\ &= (F_1(\psi, \theta), F_2(\psi, \theta)) \end{aligned}$$

To prove the existence of a solution to system (5) we just need to prove that for L small enough, F is a contraction and the inequality for $|\psi|$ is satisfied. Let be $(\psi, \theta), (\bar{\psi}, \bar{\theta}) \in X$.

$$\begin{aligned} \|F_1(\psi, \theta) - F_1(\bar{\psi}, \bar{\theta})\|_\infty &\leq c_1 LM \|\theta - \bar{\theta}\|_\infty \\ \|F_2(\psi, \theta) - F_2(\bar{\psi}, \bar{\theta})\|_\infty &\leq \frac{L^3}{M^2} \|\psi - \bar{\psi}\|_\infty \end{aligned}$$

This means that for $L < \min\left\{\frac{1}{c_1 M}, M^{2/3}\right\}$, F is a contraction. Moreover, we notice that $\|\psi'\|_\infty \leq c_1 M$. The bound on the derivative and the terminal condition let us notice that $\|\psi\|_\infty \leq c_1 LM$. Then, the inequality on ψ is always satisfied if

$$c_1 LM \leq c_2 (M/L)^{3/2}$$

which gives the upper bound $L \leq \left(\frac{c_2}{c_1} \sqrt{M}\right)^{2/5}$.

Collecting all the upper bounds for L , we can define

$$\bar{L} = \min\left(\frac{M}{u_m}, \frac{1}{c_1 M}, M^{2/3}, \left(\frac{c_2}{c_1} \sqrt{M}\right)^{2/5}\right)$$

and we can take $u = M/\bar{L}$. So, if condition (HP_{max}) is satisfied, then $u \leq u_M$. That is, the trajectory $((\psi, \theta + \theta_0, \mu), u, \bar{L})$ is admissible for (P) and consequently $((\psi, \theta + \theta_0, \mu), \bar{L})$ is an admissible solution for (P_d) . \square

To prove the existence of a minimising trajectory we need a bound on the initial condition of the optimal trajectory. This property descends from the limited mass M at our disposal and the boundedness of the dynamic.

¹Here, we use $\|\cdot\|_\infty$ to denote the standard supremum norm in $C([0, L])$.

{prop:boundedness}

Proposition 3. *The set of admissible trajectories for (P_d) does not change if we replace $C_{d,0}$ defined in (P_d) with*

$$\tilde{C}_{d,0} = \left[-\frac{c_1 M^2}{u_m}, \frac{c_1 M^2}{u_m} \right] \times \{\theta_0\} \times \{M\}$$

Moreover, for any admissible trajectory $(x, L) \in W^{1,1}([0, L]; \mathbb{R}^3) \times [0, +\infty)$ we have

$$\begin{aligned} L &\in \left(0, \frac{M}{u_m} \right], & |\psi(s)| &\leq \frac{c_1 M^2}{u_m}, \\ |\theta(s) - \theta_0| &\leq c_1 \left(\frac{M}{u_m} \right)^3, & 0 \leq \mu(s) &\leq M, \end{aligned}$$

for every $s \in [0, L]$.

Proof. Let $x = (\psi, \theta, \mu)$ be an admissible trajectory for (P_d) . Since $\mu(0) = M > 0 = \mu(L)$, we must have $L > 0$. Moreover, one has that

$$M = - \int_0^L \mu'(\sigma) d\sigma \geq u_m L,$$

which implies the bound

$$L \leq \frac{M}{u_m}.$$

The bound on μ follows immediately from the dynamics. Indeed, by definition of F_d , one has $\mu' \leq 0$. Hence

$$0 \leq - \int_s^L \mu'(\sigma) d\sigma = \mu(s) = M + \int_0^s \mu'(\sigma) d\sigma \leq M$$

For what concerns the variable ψ , we have

$$|\psi(s)| = \left| \int_s^L c_1 \mu(\sigma) \sin(\theta(\sigma)) d\sigma \right| \leq c_1 M L \leq c_1 \frac{M^2}{u_m},$$

which gives the bound for ψ in $[0, L]$.

Finally, by taking into account the equation for θ' , we observe that

$$|\theta(s) - \theta_0| \leq \int_0^s \theta'(\sigma) d\sigma \leq \frac{c_1 M^2}{u_m} \frac{1}{u_m^2} \frac{M}{u_m} = c_1 \frac{M^3}{u_m^4}.$$

Hence, all the bounds of the thesis are verified. \square

To prove the existence of a maximizer we employ a compactness theorem stated in Proposition 2.5.3 in [19], and the bound on the admissible lengths L stated in Proposition 3.

{thm:existence}

Theorem 1. *Assume (HP_{max}) holds. Then, problem (P_d) admits a maximizer.*

Proof. Define the closed and bounded set $X \subset \mathbb{R}^3$,

$$X = \left[-\frac{c_1 M^2}{u_m}, \frac{c_1 M^2}{u_m} \right] \times \left[-|\theta_0| - \frac{c_1 M^3}{u_m^3}, |\theta_0| + \frac{c_1 M^3}{u_m^3} \right] \times [0, M]$$

In view of proposition 3, for any admissible trajectory $(x, L) \in W^{1,1}([0, L]; \mathbb{R}^3) \times [0, +\infty)$, one has that $(\psi, \theta, \mu)(t) \in X$ for all $t \in [0, L]$.

Step 1: $F_d : \mathbb{R}^3 \rightrightarrows \mathbb{R}^3$ is a closed, convex, nonempty, Borel measurable multifunction.

F_d is closed, convex and nonempty by definition. Concerning the Borel measurability, define

$$f_{u_1, u_2, \lambda}(x) := \left(c_1 \mu \sin(\theta), -\psi \left(\frac{\lambda}{u_1^2} + \frac{1-\lambda}{u_2^2} \right), -(\lambda u_1 + (1-\lambda)u_2) \right).$$

Take any open set $A \subset \mathbb{R}^3$. By taking into account Proposition 1 and the continuity of $f_{u_1, u_2, \lambda}(x)$ with respect u_1, u_2, λ and x , we have

$$\begin{aligned} F_d^{-1}(A) &= \{x \in \mathbb{R}^3 : F_d(x) \cap A \neq \emptyset\} \\ &= \bigcup_{u_1 \leq u_2 \in \mathbb{Q} \cap [u_m, u_M]} \bigcup_{\lambda \in \mathbb{Q} \cap [0, 1]} \left[f_{u_1, u_2, \lambda}^{-1}(A) \cap \left((-\infty, c_2 u_1^{3/2}] \times \mathbb{R}^2 \right) \right] \end{aligned}$$

Hence, $F_d^{-1}(A)$ is a countable union of Borel sets, that is a Borel set itself.

Step 2: F_d has a closed graph.

Let $(x_n)_n$ and $(v_n)_v$ two sequences in \mathbb{R}^3 such that for each n ,

$$v_n \in F_d(x_n)$$

and $x_n \rightarrow x$, $v_n \rightarrow v$ for some $x, v \in \mathbb{R}^3$. We want to prove that $v \in F_d(x)$.

It follows from Proposition 1 that, for each n , there exist $u_{1,n}, u_{2,n}, \lambda_n$ such that

$$f_{u_{1,n}, u_{2,n}, \lambda_n}(x_n) = v_n.$$

Since $u_{1,n}, u_{2,n} \in [u_m, u_M]$ and $\lambda_n \in [0, 1]$ for each n , then there exist $u_1, u_2 \in [u_m, u_M]$ and $\lambda \in [0, 1]$ such that $u_{1,n} \rightarrow u_1$, $u_{2,n} \rightarrow u_2$ and $\lambda_n \rightarrow \lambda$ at least along a subsequence. Thus, by continuity, we have

$$\begin{aligned} f_{u_1, u_2, \lambda}(x) &= v, \\ u_1, u_2 &\geq \left(\frac{|\psi|}{c_2} \right)^{2/3}, \end{aligned}$$

that is exactly $v \in F_d(x)$.

Step 3: $F_d(x) \subset \alpha \mathbb{B}^3$ for any $x \in X$.

It follows from the definition of X and the boundedness of the control set that, for any $x \in X$, we have

$$F_d(x) \subset \max \left\{ c_1 \frac{M^2}{u_m}, c_1 \frac{M^3}{u_m^3}, \frac{M u_M}{u_m} \right\} \mathbb{B}^3$$

where we recall that $\mathbb{B}^3 \subset \mathbb{R}^3$ is the closed unitary ball centred at the origin.

Step 4: Passing to the limit from a maximising sequence.

Consider a maximising sequence of admissible trajectories $(x_n, L_n)_n$ for problem (P_d) . In view of Proposition 2, such a sequence exists. It follows from Proposition 3 that the end-time sequence $(L_n)_n$ is bounded. So, along a subsequence (we do not relabel), there exists $L > 0$ such that $L_n \rightarrow L$. Furthermore, it is not restrictive to assume that $L_n \leq L$ for all n sufficiently large along a subsequence (the case $L_n \geq L$ can be treated by using similar arguments). Hence, we can extend x_n to the whole $[0, L]$ by defining

$$y_n(s) = \begin{cases} x_n(s) & s \in [0, L_n] \\ x_n(L_n) & s \in [L_n, L] \end{cases},$$

so that $y_n \in W^{1,1}([0, L]; \mathbb{R}^3)$ with $y'_n = x'_n$ in $[0, L_n]$ and $y'_n \equiv 0$ in $[L_n, L]$. It follows from Proposition 3 that $y_n \in X$ for every n . Since F_d restricted to X is bounded, $y'_n \in F(y_n)$ a.e. in $[0, L_n]$ and $y'_n \equiv 0$ in $[L_n, L]$ for every n , the sequence $(y'_n)_n$ is uniformly essentially bounded. Moreover, by invoking again Proposition 3, one has that $(y_n(0))_n$ is a bounded sequence.

Let us define $A_n = [0, L_n]$ and observe that $\mathcal{L}(A_n) = L_n \rightarrow L$ as $n \rightarrow +\infty$. It follows from Proposition 2.5.3 of [19] that there exists a function $x \in W^{1,1}([0, L]; \mathbb{R}^3)$ such that $x' \in F(x)$ a.e. in $[0, L]$ and $(x(0), x(L)) \in C_{0,d} \times C_{1,d}$, that is (x, L) is an admissible trajectory for (P_d) . Since L is the maximal value for problem (P_d) , then (x, L) is a maximizer for (P_d) . This concludes the proof. \square

4 Necessary Conditions

4.1 Reformulation

{sec:NecCond}

{sec:reformulation}

Proposition 1 characterizes the velocity set F_d . Using such a characterization, we recast Problem (P_d) into the following system:

$$\begin{cases} \max_{(u,L) \in \mathcal{V}} L \\ \text{Subject to} \\ x'(s) = f_c(x(s), u(s)) & \text{a.e. } s \in [0, L], \\ (x(0), x(L)) \in C_{d,0} \times C_{d,1} \\ h_c(x(s), u(s)) \leq 0 & \text{a.e. } s \in [0, L] \end{cases} \quad (P_c) \quad \{\text{eq:problemC0}\}$$

with

- $x = (\psi, \theta, \mu) \in W^{1,1}([0, L]; \mathbb{R}^3)$;
- $u = (u_1, u_2, \lambda)$;
- $\mathcal{V} = \{(u, L) : u : [0, L] \rightarrow \mathbb{R} \times \mathbb{R} \times [0, 1] \text{ Lebesgue measurable, } L \in [0, +\infty)\}$;

- $f_c(x) = \left(c_1 \mu \sin(\theta), -\psi \left(\frac{\lambda_1}{u_1^2} + \frac{\lambda_2}{u_2^2} \right), -(\lambda_1 u_1 + \lambda_2 u_2) \right)$
with $\lambda_1 = \lambda$ and $\lambda_2 = 1 - \lambda$;
- $h_c(x, u) = \max \left\{ |\psi| - c_2 u_i^{3/2}, u_m - u_i, u_i - u_M, -\lambda, \lambda - 1 \right\}$,
where the use of the subscript i means that the maximum is taken over both $i = 1, 2$.

In view of Proposition 9 (see Appendix), problem (P_c) is equivalent to problem (P_d) .

Proposition 4. *Let (x, u, L) and admissible trajectory for problem (P_c) such that $\theta(0) = \pi/2$. Then if one of the following two conditions holds true*

{prop:signs}

$$c_1 < \frac{\pi}{2} \left(\frac{u_m}{M} \right)^3 \quad \text{or} \quad c_2 < \frac{\pi \sqrt{u_m}}{2L}, \quad (HP_{2c}) \quad \{\text{eq:c2max}\}$$

we have:

- θ is increasing and $\theta(s) \in [\pi/2, \pi)$ for all $s \in [0, L]$;
- ψ is increasing and $\psi(s) < 0$ for all s in $[0, L)$.

Proof. Assume $u_1 \leq u_2$. From the velocity constraint f_p we observe that

$$\theta' = -\psi \left(\frac{\lambda_1}{u_1^2} + \frac{\lambda_2}{u_2^2} \right). \quad (6) \quad \{\text{prop}_7\text{-eq1}\}$$

Furthermore, from the state constraint, we have that

$$|\psi| \leq c_2 u_1^{3/2}. \quad (7) \quad \{\text{prop}_7\text{-eq2}\}$$

Consequently it follows from (6), (7) and from Proposition 3 that

$$|\theta'| \leq c_2 u_1^{3/2} \left(\frac{\lambda_1}{u_1^2} + \frac{\lambda_2}{u_2^2} \right) \leq \frac{c_2}{\sqrt{u_1}}.$$

So, if $c_2 < \frac{\pi \sqrt{u_m}}{2L}$, for every $s \in [0, 1]$

$$\left| \theta(s) - \frac{\pi}{2} \right| \leq \frac{c_2 L}{\sqrt{u_1}} \leq c_2 \frac{L}{\sqrt{u_m}} \leq \frac{\pi}{2}$$

and we get that $\theta \in (0, \pi)$. On the other hand, if $c_1 < \frac{\pi}{2} \left(\frac{u_m}{M} \right)^3$, by proposition 3 we obtain the same conclusion.

The bound $\theta \in (0, \pi)$ determines the signs of ψ' and ψ :

$$\begin{aligned} \psi'(s) &= c_1 \mu(s) \sin(\theta(s)) \geq 0, \\ \psi(s) &= - \int_s^L c_1 \mu(\sigma) \sin(\theta(\sigma)) d\sigma \leq 0. \end{aligned}$$

Using the above relations, we refine the bound on θ and get the monotonicity property:

$$\begin{aligned}\theta'(s) &= -\psi(s) \left(\frac{\lambda_1(s)}{u_1^2(s)} + \frac{\lambda_2(s)}{u_2^2(s)} \right) \geq 0, \\ \theta(s) - \frac{\pi}{2} &= \int_0^s (-\psi)(\sigma) \left(\frac{\lambda_1(\sigma)}{u_1^2(\sigma)} + \frac{\lambda_2(\sigma)}{u_2^2(\sigma)} \right) d\sigma \geq 0.\end{aligned}$$

which means that θ is increasing and $\theta \in (\pi/2, \pi)$, concluding the proof. \square

Remark 1. In proposition 4 the condition for the constant c_2 depends on the length L of the admissible trajectory. However, using the upper bound on L given in proposition 3, it is possible to obtain

$$c_2 < \frac{\pi u_m^{3/2}}{2M}$$

so that if c_2 satisfies this condition, then (HP_{2c}) holds for any admissible trajectory.

4.2 Notations for basic non-smooth analysis

The mixed constraint h_c leads to a formulation of the Pontryagin's maximum principle that involves just absolutely continuous adjoint trajectories. This version of the Pontryagin's maximum principle can be found in theorem 2.1 in [20]. Before discussing the necessary conditions for the optimization problem (P_c) , we fix some essential notations of non-smooth analysis.

Given a non-empty closed set $S \subset \mathbb{R}^n$, we define the *proximal normal cone* to S at a point $x \in S$ as

$$N_S^P(x) = \{\xi \in \mathbb{R}^n : \exists M > 0 \text{ such that } \forall x' \in S, \langle \xi, x' - x \rangle \leq M|x' - x|^2\}.$$

Any element of the proximal normal cone is called *proximal normal vector*. We define the *limiting normal cone* (also known as *Mordukhovich's normal cone*) as

$$N_S^L(x) = \{\xi : \xi = \lim_i \xi_i \text{ for any } \xi_i \in N_S^P(x_i) \text{ such that } x_i \in S, x_i \rightarrow x\}$$

and we also define the *generalised normal cone* (also known as *Clarke's normal cone*) as

$$N_S^C(x) = \overline{\text{co}}N_S^L(x).$$

It is clear from the definitions that

$$N_S^P(s) \subset N_S^L(x) \subset N_S^C(x).$$

In an analogous way, we define proximal, limiting and generalised subgradients for a lower semicontinuous function $f : \mathbb{R}^n \rightarrow \mathbb{R}$:

$$\begin{aligned}\partial^P f(x) &= \{\xi : (\xi, -1) \in N_{\text{epi}(f)}^P(x)\}, \\ \partial^L f(x) &= \{\xi : \xi = \lim_i \xi_i \text{ for any } \xi_i \in \partial^P f(x_i) \text{ s.t. } x_i \rightarrow x, f(x_i) \rightarrow f(x)\}, \\ \partial^C f(x) &= \text{co}\{\partial^L f(x)\}\end{aligned}$$

and

$$\partial^P f(x) \subset \partial^L f(x) \subset \partial^C f(x).$$

There is a well-known relation between the level sets of a function and its subgradient, which is stated in the following theorem (see Theorem 11.38 in [21]).

{thm:setgradient}

Theorem 2. *Let f be a locally Lipschitz function and define*

$$S = \{x : f(x) \leq 0\}.$$

Fix $x \in S$ such that $f(x) = 0$. If $0 \notin \partial^L f$, then

$$N_S^L(x) \subset \{\lambda \xi : \lambda \geq 0, \xi \in \partial^L f\}.$$

The proof of this statement can be found in theorem 11.38 in [21]. Another useful theorem is the so-called *max rule* (see for instance theorem 5.5.2 in [19])

{thm:maxrule}

Theorem 3. *Let $f_i : \mathbb{R}^n \rightarrow \mathbb{R}$, $i = 1, \dots, m$ a collection of m locally Lipschitz continuous functions. Define $f : \mathbb{R}^n \rightarrow \mathbb{R}$ as*

$$f(x) = \max_i f_i(x)$$

and

$$\Lambda = \{(\lambda_1, \dots, \lambda_m) \in \mathbb{R}^m : \lambda_i \geq 0 \text{ for every } i = 1, \dots, m \text{ and } \lambda_1 + \dots + \lambda_m = 1\}.$$

Then

$$\partial^L f(x) \subset \left\{ \partial^L \left[\sum_{i=1}^m \lambda_i f_i \right] (x) : (\lambda_1, \dots, \lambda_m) \in \Lambda, \text{ and } f_i(x) < f(x) \implies \lambda_i = 0 \right\}.$$

4.3 A Pontryagin's maximum principle

4.3.1 The bounded slope condition

To derive the necessary conditions for (P_d) , it is important to verify the Lipschitz continuity and the boundedness of F_d (see for instance section 2.3 in [22]). These properties are implied by the *bounded slope condition*, which requires a relation between the partial derivatives of F_d . A single-valued function is easier to manage than a multifunction, so we look at this condition for problem (P_c) . A single-valued formulation of the bounded slope condition can be found in condition $\mathbf{BS}_{*}^{\epsilon, \mathbf{R}}$ of [20], which we summarise here.

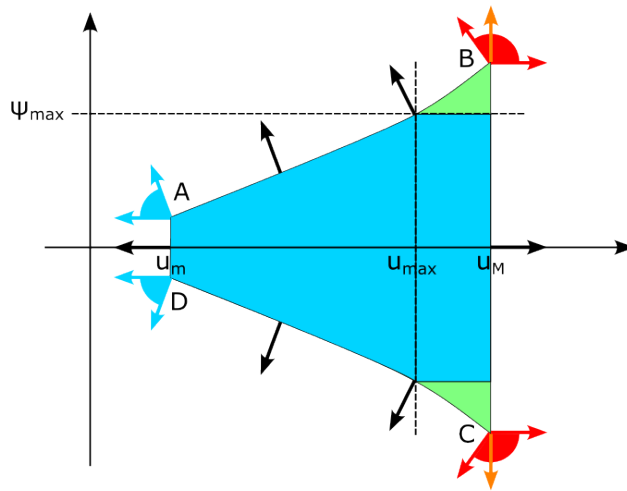


Figure 1: Constraint set given by the conditions $u \in [u_m, u_M]$ and $|\psi| \leq c_2|u|^{3/2}$. The black arrows represent the normal vectors to the edges of the sets; in the corners A, B, C, D , since we have a discontinuity, those normal vectors become normal cones. The value u_{max} is the one given by condition (HP^1_{max}) , while ψ_{max} is the corresponding maximum value of ψ , that is $\psi_{max} = (c_1 M^2)/u_m$. The bounded slope condition in this situation can be translated in this geometrical concept: there must not be arrows vertically oriented near the optimal trajectory. As shown by the orange arrows in the figure, corners B and C are clearly a threat to this condition. However, since for any admissible trajectory we have $|\psi| \leq \psi_{max}$, the optimal trajectory (and more in general, any admissible trajectory) will never reach the green area of the figure.

{fig:bounded_slope}

Assume we are considering an optimisation problem whose admissible trajectories (x, u) (where u is the control) satisfy the constraint $(t, x(t), u(t)) \in S$, where S is a closed set. Let (x^*, u^*, L^*) be an optimal process and $R(t) > 0$ an arbitrary positive measurable function. Define a tube around the optimal process (x^*, u^*, L^*) in S

$$S_*^{\varepsilon, R}(t) = \{(t, x, u) \in S : |x - x^*(t)| \leq \varepsilon, |u - u^*(t)| \leq R(t)\}$$

for a.e. $t \in [0, L^*]$. The bounded slope condition requires the existence of a measurable real-valued function k_S such that

$$(x, u) \in S_*^{\varepsilon, R}(t), (\alpha, \beta) \in N_{S(t)}^P(x, u) \implies |\alpha| \leq k_S(t)|\beta|$$

In our case, $S = [0, L^*] \times \{(x, u) : h_c(x, u) \leq 0\}$ and in the following proposition, we verify the bounded slope condition for a fixed R . An intuitive idea of why in our case this condition holds is given in figure 1.

{prop:bounded_slope}

Proposition 5. *Let*

$$E = \{(x, u) : h_c(x, u) \leq 0\}$$

If

$$u_M > \left(\frac{c_1 M^2}{c_2 u_m} \right)^{2/3} \quad (HP_{max}^1) \quad \{\text{eq:umax1}\}$$

then there exist $\varepsilon_c, K_c \in [0, +\infty)$ such that for any admissible trajectory (x, u, L) for problem (P_c) and for any $s \in [0, L]$

$$|x - x(s)| \leq \varepsilon_c, |u - u(s)| \leq \varepsilon_c, (\alpha, \beta) \in N_E^P(x, u) \implies |\alpha| \leq K_c |\beta|$$

Notice that we prove a stronger condition than the bounded slope condition, since we show such a property in the neighbourhood of any admissible process (x, u, L) and not just for the optimal process (x^*, u^*, L^*) .

Proof. Consider the functions

$$\begin{cases} a_i(x, u) = |\psi| - c_2 u_i^{3/2} & i = 1, 2 \\ b_i(x, u) = u_m - u_i & i = 1, 2 \\ c_i(x, u) = u_i - u_M & i = 1, 2 \\ d(x, u) = -\lambda \\ e(x, u) = \lambda - 1 \end{cases}$$

Each of the above functions is smooth in E and by definition

$$h_c = \max(a_1, a_2, b_1, b_2, c_1, c_2, d, e)$$

In the notations of theorem 3

$$\begin{aligned} G(x, u) = \{ & (\lambda_{a,1} \nabla a_1 + \dots + \lambda_e \nabla e)(x, u) : (\lambda_{a,1}, \dots, \lambda_e) \in \Lambda, \\ & \text{and if } a_i \text{ or } \dots \text{ or } e < 0 \text{ then } \lambda_{a,i}, \text{ or } \dots \text{ or } \lambda_e = 0 \text{ respectively} \} \end{aligned} \quad (8) \quad \{\text{eq:G_def}\}$$

and by its application, we have

$$\partial^L h_c(x, u) \subset G(x, u)$$

We can compute explicitly the gradients of the functions:

$$\begin{aligned} \nabla a_1 &= [\text{sgn}(\psi) & 0 & 0 & -c_2 \frac{3}{2} \sqrt{u_1} & 0 & 0] \\ \nabla a_2 &= [\text{sgn}(\psi) & 0 & 0 & 0 & -c_2 \frac{3}{2} \sqrt{u_2} & 0] \\ \nabla b_1 &= [0 & 0 & 0 & -1 & 0 & 0] \\ \nabla b_2 &= [0 & 0 & 0 & 0 & -1 & 0] \\ \nabla c_1 &= [0 & 0 & 0 & 1 & 0 & 0] \\ \nabla c_2 &= [0 & 0 & 0 & 0 & 1 & 0] \\ \nabla d &= [0 & 0 & 0 & 0 & 0 & -1] \\ \nabla e &= [0 & 0 & 0 & 0 & 0 & 1] \end{aligned}$$

We want to see that for any $g = (g_1, \dots, g_6) \in G(x, u)$, we have $(g_4, g_5, g_6) \neq (0, 0, 0)$. The case $(g_4, g_5, g_6) = (0, 0, 0)$ can happen only in the following situations:

1. $\tilde{\lambda} \nabla b_i + \tilde{\lambda} \nabla c_i = 0$ for some $\tilde{\lambda} > 0$;
2. $\tilde{\lambda} \nabla d + \tilde{\lambda} \nabla e = 0$ for some $\tilde{\lambda} > 0$;
3. $\lambda_{a,i} \nabla a_i + \lambda_{c,i} \nabla c_i = 0$ for some $\lambda_{a,i}, \lambda_{c,i} > 0$.

Cases 1 and 2 cannot happen. Indeed, assume for instance that case 1 holds true. Since $\tilde{\lambda} > 0$, this is possible only if $b_i(x, u) = c_i(x, u) = 0$, consequently $u_i = u_m = u_M$ and this is not possible. Similar reasoning can be applied to case 2.

Now, we want to show that for (x, u) sufficiently close to $(x(s), u(s))$ for any $s \in [0, L]$, case 3 never occurs. Indeed, to have $\lambda_{a,i}, \lambda_{c,i} > 0$, we need

$$\begin{cases} u_i = u_M \\ \left(\frac{|\psi|}{c_2}\right)^{2/3} = u_i \end{cases} \quad (9) \quad \{\text{eq:auxiliary_2}\}$$

By proposition 3, we know that

$$|\psi(s)| \leq \frac{c_1 M^2}{u_m}$$

So, if u_M satisfies hypothesis (HP_{max}^1) , then $(x(s), u(s))$ cannot satisfy the conditions in (9), because

$$\left(\frac{|\psi(s)|}{c_2}\right)^{2/3} \leq \left(\frac{|c_1 M^2|}{c_2 u_m}\right)^{2/3} < u_M.$$

So, if we take a constant $\varepsilon_c > 0$ such that

$$\left(\frac{|c_1 M^2 + \varepsilon_c|}{c_2 u_m}\right)^{2/3} < u_M - \varepsilon_c$$

then, for any $s \in [0, L]$ and for any $(x, u) \in E$ such that

$$|x - x(s)| \leq \varepsilon_c, |u - u(s)| \leq \varepsilon_c \quad (10) \quad \{\text{eq:auxiliary_3}\}$$

we have

$$\left(\frac{|\psi|}{c_2}\right)^{2/3} \leq \left(\frac{|c_1 M^2 + \varepsilon_c|}{c_2 u_m}\right)^{2/3} < u_M - \varepsilon_c.$$

Consequently, system (9) cannot be satisfied.

Thus, for any $(\alpha, \beta) \in G(x, u)$ with (x, u) satisfying condition (10), where α considers the partial derivatives with respect to the x and β the partial derivatives with respect the control u , we have

$$\begin{aligned} |\alpha| &\leq 1 \\ |\beta| &\geq \min\left(c_2 \frac{3}{2} \sqrt{u_i}, 1\right) \geq \min\left(c_2 \frac{3}{2} \sqrt{u_m}, 1\right) \end{aligned}$$

So, by choosing

$$K_c = \max\left(\frac{2}{3c_2 \sqrt{u_m}}, 1\right)$$

we always have $|\alpha| \leq K_c |\beta|$. We also observe that in this situation, we always have $|(\alpha, \beta)| \neq 0$. For this reason, we can apply theorem 2 and consequently

$$N_E^P(x, u) \subset N_E^L(x, u) \subset \{\tilde{\lambda}(\alpha, \beta) : \tilde{\lambda} \geq 0, (\alpha, \beta) \in G(x, u)\}$$

which concludes the proof. □

\{\text{rem:normal_cone}\}

Remark 2. *The set $G(x, u)$ defined in (8) is convex and closed. This means that also the set*

$$\{\tilde{\lambda}\xi : \tilde{\lambda} \geq 0, \xi \in G(x, u)\}$$

is convex and closed. Consequently, we also have the inclusion

$$N_E^C(x, u) \subset \{\tilde{\lambda}\xi : \tilde{\lambda} \geq 0, \xi \in G(x, u)\},$$

where $E = \{(x, u) : h_c(x, u) \leq 0\}$.

For any fixed $\xi \in N_E^C(x, u)$, we use ξ_ψ to denote the component of ξ corresponding to ψ . The notations ξ_{u_i} and ξ_λ have a similar meaning. Furthermore, in view of the proof of Proposition 5, we can observe that

$$\text{sgn}(\xi_\psi) = \text{sgn}(\psi).$$

4.3.2 The adjoint system

Given $\bar{L} \geq L > 0$ and a measurable function $x : [0, L] \rightarrow \mathbb{R}^n$, we define

$$x_{\bar{L}}(s) = \begin{cases} x(s) & s \in [0, L] \\ x(L) & s \in [L, \bar{L}] \end{cases}.$$

We say that an admissible trajectory (x^*, u^*, L^*) is an ε -local maximum for (P_c) if for any other admissible trajectory (x, u, L) such that

$$|L^* - L|, |x_{\bar{L}}(s) - x_L^*(s)|, |u_{\bar{L}}(s) - u_L^*(s)| \leq \varepsilon$$

for a.e. $s \in [0, \bar{L} = \max\{L^*, L\}]$, the inequality $L^* > L$ holds.

Theorem 4. *Assume (HP_{max}^1) is satisfied and let ε_c be the constant of proposition 5. Let (x^*, u^*, L^*) be an ε_c -local maximum for (P_c) and define the set of the constraints*

$$E = \{(x, u) : h_c(x, u) \leq 0\}.$$

Then, there exists an arc $p = (p_\psi, p_\theta, p_\mu) \in W^{1,1}([0, L^]; \mathbb{R}^3)$ and a number $\lambda_0 \in \{0, 1\}$ satisfying the non-triviality condition*

$$(\lambda_0, p(s)) \neq 0, \forall s \in [0, L^*]$$

such that

$$\begin{cases} p'_\psi = p_\theta \left(\frac{\lambda_1^*}{(u_1^*)^2} + \frac{\lambda_2^*}{(u_2^*)^2} \right) + \xi_\psi \\ p'_\theta = p_\psi (-c_1 \mu^* \cos \theta^*) \\ p'_\mu = -p_\psi c_1 \sin \theta^* \\ p_\psi(0) = 0 \\ p_\theta(L^*) = 0 \end{cases} \quad (11) \quad \{\text{eq:adj0}\}$$

and

$$\begin{cases} p_\psi c_1 \mu^* \sin \theta^* - p_\theta \psi^* \left(\frac{\lambda_1^*}{(u_1^*)^2} + \frac{\lambda_2^*}{(u_2^*)^2} \right) - p_\mu (\lambda_1^* u_1^* + \lambda_2^* u_2^*) = -\lambda_0 \\ 2p_\theta \psi^* \frac{\lambda_i^*}{(u_i^*)^3} - p_\mu \lambda_i^* - \xi_{u_i} = 0 \\ -p_\theta \psi^* \left(\frac{1}{(u_1^*)^2} - \frac{1}{(u_2^*)^2} \right) - p_\mu (u_1^* - u_2^*) - \xi_\lambda = 0 \end{cases} \quad i = 1, 2 \quad (12) \quad \{\text{eq:adj1}\}$$

almost everywhere in $[0, L^*]$, where $\xi : [0, L^*] \rightarrow \mathbb{R}^7$ is a measurable function such that $\xi(s) \in N_E^C(x^*(s), u^*(s))$ for a.e. $s \in [0, L^*]$. Let

$$H(x, u, p) = p_\psi c_1 \mu \sin \theta - p_\theta \psi \left(\frac{\lambda_1}{u_1^2} + \frac{\lambda_2}{u_2^2} \right) - p_\mu (\lambda_1 u_1 + \lambda_2 u_2)$$

be the unmaximized Hamiltonian. Then, the Weierstrass condition holds. So, for almost every $s \in [0, L^*]$ and for every $u \in \mathbb{R}^3$ such that $(x^*(s), u) \in E$ and $|u - u^*(s)| \leq \varepsilon_c$, we have

$$H(x^*(s), u, p(s)) \leq H(x^*(s), u^*(s), p(s)) \quad (13) \quad \{\text{eq:adj2}\}$$

Notice that the non-triviality condition holds for every $s \in [0, L^*]$.

Proof. We reformulate the free end-time problem (P_c) into a fixed end-time maximization by a transformation of the independent variable. So, we consider

the following system

$$\begin{cases}
\min_{(u_1, u_2, \lambda, \tau)} -\tau_a(L^*) \\
\text{Subject to} \\
\psi' = c_1 \mu \sin(\theta) \tau & \text{a.e. in } [0, L^*] \\
\theta' = -\psi \tau \left(\frac{\lambda_1}{u_1^2} + \frac{\lambda_2}{u_2^2} \right) & \text{a.e. in } [0, L^*] \\
\mu' = -\tau (\lambda_1 u_1 + \lambda_2 u_2) & \text{a.e. in } [0, L^*] \\
\tau_a' = \tau & \text{a.e. in } [0, L^*] \\
|\psi| - c_2 u_i^{3/2} \leq 0 & i = 1, 2; \text{ a.e. in } [0, L^*] \\
u_i \in [u_m, u_M] & i = 1, 2; \text{ a.e. in } [0, L^*] \\
\lambda_1 = 1 - \lambda_2 \in [0, 1] \\
\tau \in \left[-\frac{\varepsilon_c}{L^*} + 1, \frac{\varepsilon_c}{L^*} + 1 \right] \\
\psi(L^*) = 0 \\
\theta(0) = \theta_0 \\
\mu(0) = M, \mu(L^*) = 0 \\
\tau_a(0) = 0
\end{cases} \quad (14) \quad \{\text{eq:auxiliary_7}\}$$

where τ is now a further control function. It is clear that if (x^*, u^*, L^*) is a ε_c -local maximum for (P_c) , then $(x^*, (u^*, \tau^* \equiv 1))$ is a ε_c -local minimum of (14). The conclusion follows from an application of the Pontryagin's maximum principle (see Theorem 2.1 of [20]). Indeed, in view of Proposition 5, we know that the bounded slope condition $\mathbf{BS}_*^{\varepsilon, R}$ holds true for (14). It remains to verify the Lipschitz continuity of the function

$$f_L(x, u, \tau) = \left(c_1 \mu \sin(\theta) \tau, -\psi \tau \left(\frac{\lambda_1}{u_1^2} + \frac{\lambda_2}{u_2^2} \right), -\tau (\lambda_1 u_1 + \lambda_2 u_2), \tau \right)$$

for (\tilde{x}, \tilde{u}) in the set

$$T_c(s) = \{(x, u) : |x - x^*(s)|, |u - u^*(s)| \leq \varepsilon_c\}.$$

for a.e. $s \in [0, L^*]$. Thanks to Proposition 3, we know that $|\psi^*|$ and μ^* are bounded. This means that $T_c(s)$ is a compact set. Moreover, $(x, 0) \notin T_c(s)$ for any s . Consequently, f_L is smooth in $T_c(s)$ and the Lipschitz continuity follows from the compactness of $T_c(s)$. \square

5 Properties of the adjoint arc

$\{\text{sec:prop_adj_arc}\}$

In this section, we analyse the behaviour of the adjoint arc p in Theorem 4, in order to gain more information on the optimal control. From now on, we assume that the initial inclination of the elastic rod is

$$\theta_0 = \frac{\pi}{2}.$$

Remark 3. *In the notations of Theorem 3 and Theorem 4, for any $s \in [0, L^*]$ such that $h_c(x^*(s), u^*(s)) = 0$, given $\xi(s) \in N_E^C(x^*(s), u^*(s))$, we have* {rem:norm_sign}

$$\xi = \tilde{\lambda} \begin{bmatrix} -(\lambda_{a,1} + \lambda_{a,2}) \\ 0 \\ 0 \\ 0 \\ -\lambda_{a,1}c_2\frac{3}{2}\sqrt{u_1} - \lambda_{b,1} + \lambda_{c,1} \\ -\lambda_{a,2}\frac{3}{2}\sqrt{u_2} - \lambda_{b,2} + \lambda_{c,2} \\ \lambda_d - \lambda_e \end{bmatrix}$$

with $\tilde{\lambda} \geq 0$ and $(\lambda_{a,1}, \dots, \lambda_e) \in \Lambda$. Recalling Remark 2, it follows from Proposition 4 that

$$\xi_\psi \leq 0.$$

Moreover, recalling the proof of Proposition 5, if (HP_{max}^1) holds and $u_i = u_M$, then $\xi_{u_i} \geq 0$.

Proposition 6. *Let (x^*, u^*, L^*) be an optimal trajectory for problem (P_c) . Let p be an adjoint arc which satisfies system (11) and assume that hypothesis (HP_{max}^1) and (HP_{2c}) hold. Then there exists $\bar{s} \in [0, L^*]$ such that if $\bar{s} < L^*$, then* {prop:adj_sign}

$$\begin{cases} p_\theta(s) > 0 & s \in [0, \bar{s}) \\ p_\psi(s) = p_\theta(s) = 0 & s \in [\bar{s}, L^*] \end{cases}.$$

Otherwise, if $\bar{s} = L^*$, only the condition on p_θ holds, that is, $p_\theta(s) > 0$ for $s \in [0, L^*)$.

Proof. Let us define the functions

$$a = \left(\frac{\lambda_1^*}{(u_1^*)^2} + \frac{\lambda_2^*}{(u_2^*)^2} \right),$$

$$b = -c_1\mu^* \cos \theta^*$$

Since (x^*, u^*) is fixed, a and b can be regarded as the time-dependent functions appearing in (11). Furthermore, in view of hypothesis (HP_{2c}) , it follows from Proposition 4 that $a, b > 0$ in $[0, L^*)$. Then the adjoint system (11) can be written as

$$\begin{cases} p'_\psi = p_\theta a + \xi_\psi \\ p'_\theta = p_\psi b \\ p_\psi(0) = 0 \\ p_\theta(L^*) = 0 \end{cases} \quad (15) \quad \{\text{eq:auxiliary_14}\}$$

where $\xi(s) \in N_E^C(x^*(s), u^*(s))$.

As a first step in the proof of Proposition 6, we will prove the following claim.

Claim: *there does not exist $s_0 \in [0, L^*)$ such that*

$$p_\psi(s_0) \leq 0, p_\theta(s_0) < 0. \quad (16) \quad \{\text{eq_claim}\}$$

Let us define

$$s_1 = \min\{s \in [s_0, L^*] : p_\theta(s) \geq 0\}$$

It follows from the assumption (16) that $s_1 > s_0$. If $s_1 \leq L^*$, then $p_\theta(s) < 0$ for $s \in [s_0, s_1)$ and $p_\theta(s_1) = 0$. Hence, it follows from Proposition 4, the condition (16) and Remark 3 that

$$p_\psi(s_1) = p_\psi(s_0) + \int_{s_0}^{s_1} p_\theta(\sigma)a(\sigma)d\sigma + \int_{s_0}^{s_1} \xi_\psi(\sigma)d\sigma < 0$$

and, by continuity of $p_\psi(\cdot)$, there exists $\delta > 0$ such that

$$p_\psi(s) < 0 \quad \text{for all } s \in (s_1 - \delta, s_1 + \delta). \quad (17) \quad \{\text{eq_claim_2}\}$$

However, by appealing again to Proposition 4, condition (16) and (17), one has that

$$p_\theta(s_1) = p_\theta(s_1 - \delta) + \int_{s_1 - \delta}^{s_1} p_\psi(\sigma)b(\sigma)d\sigma < 0,$$

which contradicts the relation $p_\theta(s_1) = 0$. Hence the condition $s_1 \leq L^*$ is not satisfied, implying that $s_1 = +\infty$. But even this situation cannot occur since in particular it implies $p_\theta(L^*) < 0$, contradicting the boundary condition $p_\theta(L^*) = 0$. Hence, the condition (16) cannot occur and this proves the claim.

The main implication of the claim is to rule out the possibility to have the initial condition $p_\theta(0) < 0$. Indeed, this follows immediately from an application of the claim statement combined with the results of Proposition 4. The following situations remain then to be studied:

Case 1: $p_\theta(0) = 0$.

In this case, we will show that one can only have $p_\psi \equiv p_\theta \equiv 0$. Indeed, by the Duhamel's formula, the solution to system (15) with the initial datum $p_\theta(0) = 0$ can be written as

$$\begin{bmatrix} p_\psi \\ q_\theta \end{bmatrix} = \int_0^t \exp \left\{ (t-s) \begin{bmatrix} 0 & a(s) \\ b(s) & 0 \end{bmatrix} \right\} \begin{bmatrix} \xi_\psi(s) \\ 0 \end{bmatrix} ds$$

By using the definition of matrix exponential, one has

$$\exp \left\{ (t-s) \begin{bmatrix} 0 & a(s) \\ b(s) & 0 \end{bmatrix} \right\} = \sum_{n=0}^{\infty} \frac{(t-s)^n}{n!} \begin{bmatrix} 0 & a(s) \\ b(s) & 0 \end{bmatrix}^n = \begin{bmatrix} v_1(t,s) & v_2(t,s) \\ v_3(t,s) & v_4(t,s) \end{bmatrix}.$$

Since $a(s), b(s) \geq 0$ for a.e. $s \in [0, L^*]$, the functions $v_i(t, s) \geq 0$, for all $t \in [0, L^*]$, a.e. $s \in [0, t]$ and for all $i = 1, \dots, 4$. Consequently, it follows from Remark 3 that

$$\begin{aligned} p_\psi &= \int_0^t v_1(t,s)\xi_\psi(s)ds \leq 0 \\ p_\theta &= \int_0^t v_3(t,s)\xi_\psi(s)ds \leq 0 \end{aligned}$$

By the dynamics (15) and the claim, the only possibility is to have $p_\psi \equiv p_\theta \equiv 0$.

Case 2: $p_\theta(0) > 0$.

Let us set

$$\bar{s} = \min\{s \in [0, L^*] : p_\theta(s) \leq 0\}.$$

Then one has that $\bar{s} > 0$ and $p_\theta(\bar{s}) = 0$. If $\bar{s} = L^*$, then $p_\theta(s) > 0$ for all $s \in [0, L^*)$ and we have nothing to prove. If $\bar{s} < L^*$, by arguing again as in the proof of the claim, one can show that it is not possible to have $p_\psi(\bar{s}) > 0$, because this would imply $p_\theta(\bar{s}) > 0$, contradicting the definition of \bar{s} . Furthermore, one cannot obtain $p_\psi(\bar{s}) < 0$. Indeed, if $p_\psi(\bar{s}) < 0$, then by continuity of the adjoint arc $p_\psi(\cdot)$, there exists $\delta > 0$ such that $p_\psi(s) < 0$ for any $s \in [\bar{s} - \delta, \bar{s} + \delta]$. It then follows that

$$p_\theta(\bar{s} + \delta) = \int_{\bar{s}}^{\bar{s} + \delta} p_\psi(\sigma) b(\sigma) d\sigma < 0$$

However, the latter inequality contradicts the statement of the claim, providing a contradiction. Hence, the only possibility is that $p_\psi(\bar{s}) = 0$ and by applying the arguments of Case 1 in the interval $[\bar{s}, L^*]$, one has that $p_\psi \equiv p_\theta \equiv 0$ in $[\bar{s}, L^*]$ and that $p_\theta(s) > 0$ for all $s \in [0, \bar{s})$. This completes the proof. \square

Proposition 7. *Let (x^*, u^*, L^*) be an optimal trajectory for problem (P_c) . Let $p = (p_\psi, p_\theta, p_\mu)$ be an adjoint arc which satisfies system (11) and assume that hypotheses (HP_{max}^1) and (HP_{2c}) hold true. Then*

$$p_\mu(s) \geq 0 \quad \text{for all } s \in [0, L^*].$$

Proof. We will structure the proof of the proposition in three main steps.

Step 1: One has that $p_\mu(0) \geq 0$.

Assume by contradiction that $p_\mu(0) < 0$. By continuity of $p_\mu(\cdot)$, there exist constants $\varepsilon, \delta > 0$ such that

$$\begin{aligned} p_\psi(s) c_1 \mu(s) \sin(\theta(s)) &> -\varepsilon \\ \left(p_\mu(s) (\lambda_1(s) u_1(s) + \lambda_2(s) u_2(s)) \leq \right) & \quad p_\mu(s) u_m < -\varepsilon \end{aligned}$$

for a.e. $s \in [0, \delta]$. Hence, by using the first equation in (12), one has that

$$p_\psi c_1 \mu \sin \theta - p_\mu (\lambda_1 u_1 + \lambda_2 u_2) > 0, \quad \text{a.e. in } [0, \delta].$$

On the other hand, it follows from Proposition 6 that $p_\theta \geq 0$ and from Proposition 4 that $\psi^* \leq 0$ for all $s \in [0, L^*)$. So, by using again the first equation of system (12), one obtains the relation

$$p_\psi c_1 \mu \sin \theta - p_\mu (\lambda_1 u_1 + \lambda_2 u_2) \leq 0 \quad \text{a.e. } s \in [0, L^*]$$

and obtains a contradiction. Consequently, this shows that $p_\mu(0) \geq 0$.

Step 2: Let us set

$$A = \{s \in [0, L^*] : p_\mu(s) \leq 0\}.$$

{prop:pmu_sign}

Then $p_\psi \leq 0$ for a.e. $s \in A$.

Indeed, let us recall again that Proposition 6 asserts that $p_\theta \geq 0$ for all $s \in [0, L^*)$, while Proposition 4 asserts that $\psi^* \leq 0$ for all $s \in [0, L^*)$. It then follows from the first equation of system (12) that

$$p_\psi c_1 \mu \sin \theta - p_\mu (\lambda_1 u_1 + \lambda_2 u_2) \leq 0, \quad \text{a.e. } s \in A$$

that is

$$p_\psi \leq p_\mu \frac{\lambda_1 u_1 + \lambda_2 u_2}{c_1 \mu \sin \theta} \leq 0, \quad \text{a.e. } s \in A.$$

This shows the assertion of *Step 2*.

Step 3: $p_\mu(s) \geq 0$ for all $s \in [0, L^*]$.

Assume that there exists $s_0 \in [0, L^*]$ such that $p_\mu(s_0) < 0$ and define

$$s_1 = \sup\{s < s_0 : p_\mu(s) \geq 0\}.$$

Since $p_\mu(0) \geq 0$, $s_1 \in [0, s_0]$ and $p_\mu(s_1) = 0$. In view of *Step 2*, one has that $p_\psi(s) \leq 0$ for a.e. $s \in [s_1, s_0]$. Using the third equation in system (11), we obtain the inequality

$$p_\mu(s_0) = - \int_{s_0}^{s_1} p_\psi c_1 \sin \theta \geq 0$$

and reach a contradiction. This completes the proof of Proposition 7. \square

The non-negativity of p_θ and p_μ are important in the determination of the optimal control. In the following, we use \mathcal{L} to denote the Lebesgue measure in \mathbb{R} .

Theorem 5. *Let (x^*, u^*, L^*) be an optimal trajectory for problem (P_c) . Assume that hypothesis (HP_{2c}) , (HP_{max}^1) hold true. Then, for a.e. $s \in [0, L^*]$, one has*

$$u_1^*(s) = u_2^*(s) = \max \left\{ u_m, \left(\frac{|\psi^*(s)|}{c_2} \right)^{2/3} \right\}. \quad (18) \quad \{\text{thm:u_opt}\} \quad \{\text{eq:u_opt}\}$$

Proof. It follows from the control constraints of the optimal control problem that

$$u_m \leq u_i^* \leq u_M \quad \text{and} \quad u_i^* \geq \left(\frac{|\psi^*|}{c_2} \right)^{2/3} \quad \text{for } i = 1, 2.$$

As a first step, we prove that

$$\lambda_i^*(s) > 0 \implies u_i^*(s) \in \left\{ \max \left\{ u_m, \left(\frac{|\psi^*(s)|}{c_2} \right)^{2/3} \right\}, u_M \right\}, \quad (19) \quad \{\text{cond}_1\}$$

that is, u_i^* cannot be an internal point of the admissible range of control values. Assume that this is not true for $i = 1$. So, there exists a set $D \subset [0, L^*]$ such that $\mathcal{L}(D) > 0$ and

$$\lambda_1^*(s) > 0, \quad u_1^*(s) \notin \left\{ \max \left\{ u_m, \left(\frac{|\psi^*|}{c_2} \right)^{2/3} \right\}, u_M \right\}$$

for every $s \in D$. Let p be an adjoint arc given by theorem 4. From system (12) we have

$$\frac{\partial}{\partial u_1} H(x^*, u^*, p) = -p_\mu \lambda_1^* - 2p_\theta(-\psi^*) \frac{\lambda_1^*}{(u_1^*)^3} = 0 \quad (20) \quad \{\text{eq:auxiliary_4}\}$$

in a.e. D . So, $u_1^*(s)$ is a.e. a critical point for the Hamiltonian. Let $\bar{s} \in [0, L^*]$ be the time which appears in the statement of Proposition 6. It then follows from Proposition 4 and Proposition 6 that

$$\frac{\partial^2}{\partial u_1^2} H(x^*(s), u, p(s)) = 6p_\theta(s)(-\psi(s)) \frac{\lambda_1(s)}{(u_1(s))^4} \begin{cases} > 0 & \text{a.e. in } [0, \bar{s}) \\ = 0 & \text{a.e. in } [\bar{s}, 1] \end{cases} \quad (21) \quad \{\text{eq:auxiliary_5}\}$$

If $\mathcal{L}(D \cap [0, \bar{s}]) > 0$, then conditions (20)-(21) imply that $u_1^*(s)$ is a minimum for H in a set of positive measure, contradicting condition (13). Therefore, we can assume $D \subset (\bar{s}, L^*]$. In view of condition (20), we observe that $p_\mu = 0$ in D . Hence this implies $p_\psi \equiv p_\theta \equiv p_\mu \equiv 0$ in D . By using the first equation of system (12), one obtains the relation $\lambda_0 = 0$. However, this implies that the non-triviality condition is violated a.e. in D , reaching a contradiction. Hence it follows that the relation (19) has to be satisfied.

We can now prove the thesis. Assume by contradiction that there exists a set E such that $\mathcal{L}(E) > 0$ and $\lambda_1(s) > 0$, $u_1(s) = u_M$ for a.e. $s \in E$. It follows from the second equation of system (12) and from the inequality $\xi_{u_1}(s) \geq 0$ a.e. $s \in [0, L^*]$ (see Remark 3) that

$$2(-p_\theta)(-\psi^*) \frac{\lambda_1^*}{(u_1^*)^3} - p_\mu \lambda_1^* \geq 0$$

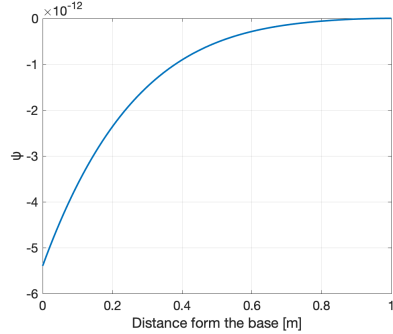
a.e. in E . On the other hand, it follows from Proposition 6 and Proposition 7 that the previous inequality holds true only if $p_\mu \equiv p_\theta \equiv 0$ a.e. in E . Then, by using again Proposition 6, this implies that also $p_\psi \equiv 0$ in $[\text{ess inf}(E), L^*]$. Hence, by appealing again to the first equation of system (12), there exists a set with positive Lebesgue measure such that one obtains the relation $\lambda_0 = 0$. This contradicts the non-triviality condition appearing in the necessary conditions. The case regarding u_2 is analogous. This completes the proof. \square

$\{\text{rem:non-relaxed_control}\}$

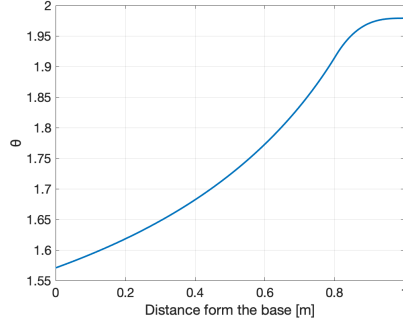
Remark 4. *Problem (P_c) is a relaxation of the original Problem (P) . Nevertheless, Theorem 5 states that the optimal control is not relaxed, in the sense that $u_1^* = u_2^*$ a.e. in $[0, L^*]$. Consequently, Theorem 5 shows the equivalence between problems (P_c) and (P) , since in both cases the optimal control (18) leads to the same optimal length L^* .*

$\{\text{rem:nomrality}\}$

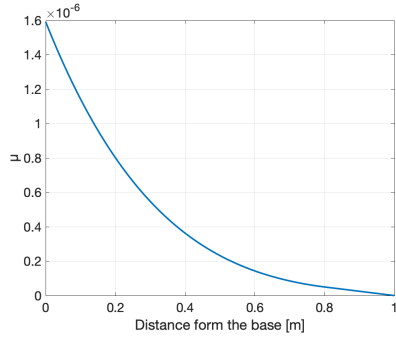
Remark 5. *All the logical passages used until now are valid independently of the normality of the problem. By the first equation of system (12), if the adjoint arc p is null, then also the multiplier λ_0 is null. This excludes the possibility to have a trivial p and a non-trivial λ_0 . However, the vice-versa, and consequently the normality of the problem itself, is not immediate. A multiplier $\lambda_0 \neq 0$ can keep track of any rescaling operation that involves the adjoint arc p . As we will see in the next section, this leads to a procedure for the numerical computation of the adjoint trajectories.*



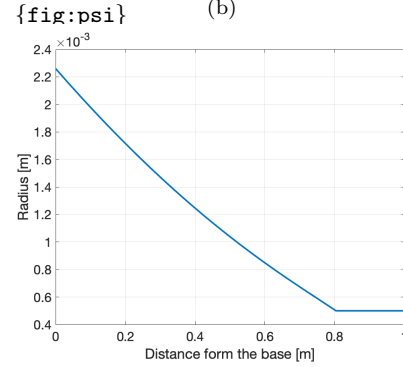
(a)



(b)



(c)



(d)

Figure 2: Numerical integration of system (22) (Figures 2a-2b-2c) and optimal radius (Figure 2d). As stated in proposition 4, both ψ and θ are increasing. The former is always negative, while the latter is always in the interval $[\pi/2, \pi)$. As displayed in Figure 2d, the radius always decreases. Around 0.8 m from the base the radius becomes constant. This is because, at that point, the optimal u^* reaches the minimal value u_m . Since $|\psi|$ is decreasing, from that point on, u^* is constantly u_m .

Remark 6. *In the proofs of Proposition 7 and Theorem 5, we have used the condition that along the optimal trajectory, the Hamiltonian H is constantly equal to $-\lambda_0$. This equality holds true because the dynamic used for problem (P) is autonomous, that is, f , $h_{P,1}$, $h_{P,2}$ and \mathcal{U} does not depend explicitly from $s \in [0, L]$. This “time” independency follows from our modelling assumptions. For instance, we considered the volume density ρ_3 and Young’s modulus E constant all along the shoot. The inclusion of a time-dependent dynamic would require further analysis of the sign of H .*

6 Simulations

If conditions (HP_{max}^1) and (HP_{2c}) hold true, then Theorem 5 determines the optimal control in feedback form. As discussed in Remark 4, this result pre-

Parameter	Value	Unit of Measure
g	9.81	$m \cdot s^{-2}$
L^*	1	m
M	$(5 \cdot 10^{-3})/(\pi\rho_3)$	m^3
ρ_3	10^3	$Kg \cdot m^{-3}$
E	$3 \cdot 10^9$	$N \cdot m^{-2}$
u_m	$(0.5 \cdot 10^{-3})^2$	m^2

Table 1: Parameters used for the numerical integration of system (22). The values are an approximation of the estimates done in [13]. In particular, the fresh mass of a searcher shoot of length L^* without leaves is approximately 10 g . Assuming that half of this mass is due to the leaves, we estimate a stem fresh mass of 5 g . This explains our choice for the value of M . The volume density ρ_3 is set as the density of the water and the minimum diameter is assumed to be 1 mm .

{tab:parameters}

scribes $u_1^* = u_2^*$ a.e., so we can consider $\lambda_1^* \equiv 1$ and problem (P_c) becomes equivalent to (P) . Therefore, the optimal trajectory solves the boundary value problem

$$\begin{cases} \psi' = c_1 \mu \sin(\theta) \\ \theta' = -\frac{\psi}{(u^*)^2} \\ \mu' = -u^* \\ \psi(L^*) = 0 \\ \theta(0) = \frac{\pi}{2} \\ \mu(0) = M, \mu(L^*) = 0 \\ \hline u^* = \max\left(u_m, \left(\frac{|\psi|}{c_2}\right)^{2/3}\right) \\ c_1 = \frac{4g\rho_3}{E}, c_2 = \frac{\bar{\sigma}}{E} \end{cases} \quad (22) \quad \{\text{eq:problem_num}\}$$

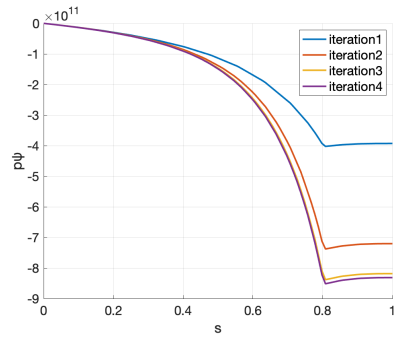
In our parameter pool (see table 1), we don't have the value of the parameter $\bar{\sigma}$. On the other hand, we know the value of the maximal length L^* . So, to integrate system (22), we have to determine those values of $\psi(0)$ and c_2 such that $\psi(L^*) = \mu(L^*) = 0$. To achieve these endpoint conditions, we wrote a **Matlab** script which employs the function **bvp5c** to solve a boundary value problem. The parameters displayed in Table 1 lead to a constant c_1 which satisfies condition (HP_{2c}) . Indeed

$$c_1 = \frac{4g\rho_3}{E} = 13.08 \cdot 10^{-6} < 6 \cdot 10^{-3} \sim \frac{\pi}{2} \left(\frac{u_m}{M}\right)^3$$

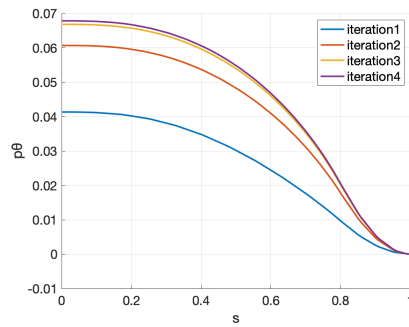
Since we don't need to set any value of u_M , conditions (HP_{max}) and (HP_{max}^1) are immediately satisfied.

6.1 Simulation of the adjoint system

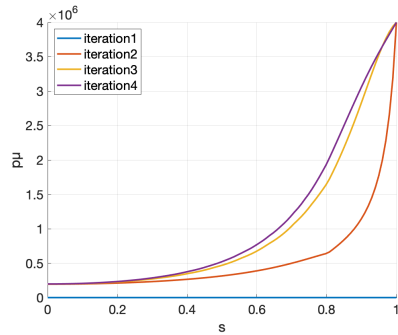
The normal cone in the dynamic of the adjoint arc makes the simulation of the adjoint system a non-trivial procedure. However, the second equation of system



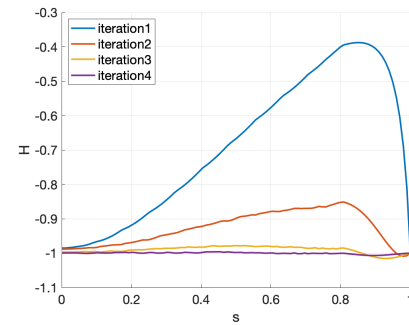
(a)



(b)



(c)



(d)

Figure 3: The adjoint arc (Figures 3a-3b-3c) and the Hamiltonian (Figure 3d). Each graph displays four iterations of the process expressed by equations (25). The iterations show that each component of the adjoint arc and the Hamiltonian are converging at least pointwise. We notice that p_θ and p_μ are always non-negative. So, the adjoint arc is following the results of propositions 6 and 7, and the iterations of the Hamiltonian are converging to a function constantly equal to -1 .

{fig:ptheta}

{fig:ppsi}

{fig:pmu}

{fig:ham}

{fig:adjoint_hamiltonian}

(12) and remark 3 suggest the following heuristic iterative process to generate the component ξ_ψ of the normal vector.

Define $s_0 \in [0, L^*]$ the value in which

$$u^*(s_0) = \left(\frac{|\psi|(s_0)}{c_2} \right)^{2/3} = u_m.$$

Assume that equation (11) has been rescaled with a piecewise constant function γ_0 in $[0, L^*]$, so that

$$\xi_{\psi,0}(s) = \frac{\xi_\psi(s)}{\gamma_0(s)} = \begin{cases} -1 & s \in [0, s_0] \\ 0 & s \in [s_0, L^*] \end{cases}.$$

The value of s_0 can be estimated by integrating system (22), and for $t > s_0$ the trajectory x is not activating the constraint on $|\psi|$, that is, $|\psi| < u_m^{3/2} c_2$. Consequently, $\xi_{\psi,0} \equiv \xi_\psi \equiv 0$ in $[s_0, L^*]$. Denote with $p_{\psi,0}, p_{\theta,0}$ the solutions to the boundary value problem

$$\begin{cases} p'_\psi = \frac{p_\theta}{u^*} - \xi_{\psi,0} \\ p'_\theta = p_\psi(-c_1 \mu \cos \theta) \\ p_\psi(0) = 0 \\ p_\theta(L^*) = 0 \end{cases}. \quad (23) \quad \{\text{eq:auxiliary_9}\}$$

Here, $p_{\psi,0}$ and $p_{\theta,0}$ are the first two components of the adjoint arc p solution to the adjoint system (11) rescaled by γ_0 . That is, if p is a solution of the adjoint system (11), then $(p_\psi/\gamma_0, p_\theta/\gamma_0)$ is a solution of (23) and vice-versa. p_μ is not considered by system (23) because it doesn't affect the behaviour of the other components of the adjoint arc and because we don't have any information on its boundary values. However, we can retrieve the values of $p_{\mu,0} = p_\mu/\gamma_0$ in $[0, s_0]$ by considering the second equation of system (12). So, we have

$$p_{\mu,0} = 2p_{\theta,0}\psi \frac{1}{(u^*)^3} - \xi_{u,0}$$

with $\xi_{u,0} = \xi_u/\gamma_0$.

In the interval $[0, s_0]$ we know that without the rescaling by γ_0 we have (see remark 3)

$$\begin{aligned} \xi_\psi &= -\tilde{\lambda} \\ \xi_u &= -\tilde{\lambda} c_2 \frac{3}{2} \sqrt{u^*} \end{aligned}$$

since $\xi_\psi/\gamma_0 = \xi_{\psi,0}$, we deduce that in $[0, s_0]$

$$\xi_{u,0} = \xi_{\psi,0} \cdot c_2 \frac{3}{2} \sqrt{u^*}$$

This allow us to estimate $p_{\mu,0}$ in $[0, s_0]$.

We now make a further assumption: the problem is normal, that is in the first equation of system (12) we have $\lambda_0 = 1$. Hence, we can estimate γ_0 in $[0, s_0]$, since we have

$$p_{\psi,0}c_1\mu \sin \theta - p_{\theta,0} \frac{1}{(u^*)^2} - p_{\mu,0}u^* = -\frac{1}{\gamma_0} \quad (24) \quad \{\text{eq:auxiliary_10}\}$$

Of course, this reasoning works only if we assume that the rescaling function γ_0 is at most a piecewise constant function. However, we can reiterate this procedure considering

$$\begin{aligned} \xi_{\psi,i} &= -\gamma_{i-1}\xi_{\psi,i-1} \\ \xi_{u,i} &= \xi_{\psi,i}c_2 \frac{3}{2}\sqrt{u^*} \\ p_{\mu,i} &= 2p_{\theta,i}\psi \frac{1}{(u^*)^3} - \xi_{u,i} \end{aligned} \quad (25) \quad \{\text{eq:iterations}\}$$

and taking $p_{\xi,i}, p_{\theta,i}$ as the solutions to system (23) with $\xi_{\psi,i}$ instead of $\xi_{\psi,0}$, for $i = 1, 2, \dots$.

7 Results

The numerical solution of system (22) is displayed in the graphs of Figure 2. The optimal trajectory respects the conditions of Proposition 6 and 7, as we expect since condition (HP_{2c}) is satisfied. In particular, ψ is negative and increasing, which means that $|\psi|$ is decreasing. By Theorem 5, the optimal control is directly proportional to $|\psi|$, consequently the optimal radius $\sqrt{u^*}$ is decreasing until it reaches the value u_m .

Regarding the simulation of the adjoint system, as displayed in Figure 3, the sequence of the adjoint arcs $(p_{\xi,i}, p_{\theta,i}, p_{\mu,i})$ is converging to some function $(p_{\xi}, p_{\theta}, p_{\mu})$ and the Hamiltonian is converging to the constant value -1 . Again, the simulated trajectories respect the conditions of propositions 6 and 7. So, we observe a positive p_{θ} in $[0, L^*)$ and a non negative p_{μ} .

8 Discussion

The control u determines the rate of mass decrease μ' and without the constraint

$$u \geq \left(\frac{|\psi|}{c_2} \right)^{2/3}, \quad (26) \quad \{\text{eq:auxiliary_12}\}$$

it can assume any value in the interval $[u_m, u_M]$. Since we require $\mu(0) = M$ and $\mu(L) = 0$, the lower is u , the slower μ decreases, the larger L is. In this situation, the optimal strategy would be to take the lowest value u allowed, that is u_m . This reasoning motivates the intuition of relation (18) for the optimal control since in (P) the constraint (26) gives a lower bound for u .

From the relations

$$\begin{aligned} u &= R^2; \\ \psi &= -R^4\theta', \end{aligned}$$

where we recall that R is the radius of the cross-section, we can formulate equation (18) as follows:

$$R = \frac{c_2}{|\theta'|}. \quad (27) \quad \{\text{eq:auxiliary_13}\}$$

Equation (27) gives a relation between the curvature $|\theta'|$ and the radius of the cross-section R . Rephrasing, if we assume that searcher shoots grow optimising their length, then their cross-section is regulated with a feedback control system. Indeed, at each point of the shoot, the cross-section, together with other physical parameters, influences the curvature of the shoot. Then, as expressed by equation (27), the resulting curvature provides feedback on the cross-section, closing the loop.

The feedback control mechanism is common in biological systems and in particular in plants [23]. Consider for instance the gravitropic mechanism. In general, plants are able to perceive their local inclination and their local curvature through some specialised cells [1, 24]. This information is compared with a target inclination and a target curvature [25], inducing a flux of hormones to regulate growth and posture [4, 5]. The plant then attains a new shape, which has different local inclinations and curvatures, and the cycle is repeated.

Further improvements in the modelling can be achieved by considering for instance (i) variable volume density and Young's modulus (ii) the mass of the leaves. In addition, c_2 is a dimensionless constant. From equation (27), we observe that it is equal to the product between the radius R of the cross-section and the curvature $|\theta'|$. A comparison with experimental data on radius and curvature would improve the accuracy of the model.

9 Conclusion

Control theory has an extremely wide range of applications, from the design of mechanical devices to physics, economics and biology. Starting from a physical model of a searcher shoot based on the Euler-Bernoulli theory of elastic rods, we used the optimal control theory to study the behaviour of the radius for the maximisation of the length. The system (P) resulted to be a boundary value problem with non-linear dynamics and constraints on the state variable. Our approach to this problem consisted of the use of relaxation to convexify the dynamic and the application of the Pontryagin Maximum Principle for mixed state-constrained systems. The resulting optimal control expressed in Theorem 5 proves the equivalence between the original problem (P) and the relaxed one (P_c). Moreover, it gives a relation between the radius and the inverse of the curvature through the dimensionless constant c_2 .

A Admissible trajectories

In this section, we prove that any admissible trajectory of problem (P_d) is an admissible trajectory of problem (P_c) . To achieve this aim, we need the following statements whose proof can be found in [19].

{apx:AdmTrj}

Proposition 8. *Take a Borel measurable multifunction $V : \mathbb{R}^m \rightrightarrows \mathbb{R}^n$ and a Lebesgue measurable function $x : [0, L] \rightarrow \mathbb{R}^m$. Then the multifunction $F \circ x : [0, L] \rightrightarrows \mathbb{R}^n$ is Lebesgue measurable.*

{prop:2.3.2_vint}

Theorem 6. *Consider a closed nonempty multifunction $G : [0, L] \rightrightarrows \mathbb{R}^n$. Then G is Lebesgue measurable if and only if its graph $Gr(G)$ is a measurable subset of $[0, L] \times \mathbb{R}^n$.*

{thm:2.3.7_vint}

We can now prove the following relation between (P_c) and (P_d) .

Proposition 9. *(x, L) is an admissible trajectory for problem (P_d) if and only if there exists a measurable (u, L) in \mathcal{V} such that (x, u, L) is admissible for problem (P_c) . Moreover, (x^*, L^*) is an optimal trajectory for problem (P_d) if and only if there exists a measurable u^* such that $(u^*, L^*) \in \mathcal{V}$ and (x^*, u^*, L^*) is an optimal trajectory for problem (P_c) .*

{prop:equiv_DI_CO}

Proof. We just need to prove that for any $x \in W^{1,1}([0, L] : \mathbb{R}^3)$ such that (x, L) is a trajectory of (P_d) there exist some measurable functions u_1, u_2, λ such that $(x, (u_1, u_2, \lambda), L)$ is an admissible trajectory for (P_c) . Consider the multifunction $V : \mathbb{R}^3 \rightrightarrows \mathbb{R}^3$

$$V((\psi, \theta, \mu)) = \{(u_1, u_2, \lambda) : |\psi| \leq c_1 \min(u_1, u_2)^{3/2}; \\ u_1, u_2 \in [u_m, u_M]; \lambda \in [0, 1]\}$$

that essentially is the one defined in remark 1. Proceeding as in the proof of theorem 1, we observe that V is a Borel measurable multifunction. By proposition 8, the multifunction

$$G : [0, L] \rightrightarrows \mathbb{R}^3 \\ G(s) = V(x(s))$$

is a Lebesgue-measurable multifunction. By definition of V , G is always a closed multifunction. We can then apply theorem 6 to observe that the graph $Gr(G)$ is a measurable subset of $[0, 1] \times \mathbb{R}^3$. We can then apply theorem the Generalized Filippov Selection Theorem (see for instance theorem 2.3.13 of [19]) to obtain that the multifunction $U' : [0, 1] \rightrightarrows \mathbb{R}^3$ defined by

$$U'(s) = \{u \in G(s) : f_c(x(s), u) = x'(s)\}$$

has a measurable graph. Finally, by the Aumann's measurable selection theorem (see theorem 2.3.12 in [19]) we find a measurable selection of U' and this concludes the proof. \square

References

- [1] Hugo Chauvet et al. “Revealing the hierarchy of processes and time-scales that control the tropic response of shoots to gravi-stimulations”. In: *Journal of Experimental Botany* 70.6 (2019), pp. 1955–1967.
- [2] Renaud Bastien et al. “Unifying model of shoot gravitropism reveals proprioception as a central feature of posture control in plants”. In: *Proceedings of the National Academy of Sciences* 110.2 (2013), pp. 755–760.
- [3] Bruno Moulia et al. “Posture control in land plants: growth, position sensing, proprioception, balance, and elasticity”. In: *Journal of Experimental Botany* 70.14 (2019), pp. 3467–3494.
- [4] Yasmine Meroz, Renaud Bastien, and L Mahadevan. “Spatio-temporal integration in plant tropisms”. In: *Journal of the Royal Society Interface* 16.154 (2019), p. 20190038.
- [5] Derek E Moulton, Hadrien Oliveri, and Alain Goriely. “Multiscale integration of environmental stimuli in plant tropism produces complex behaviors”. In: *Proceedings of the National Academy of Sciences* 117.51 (2020), pp. 32226–32237.
- [6] Nick Rowe, Sandrine Isnard, and Thomas Speck. “Diversity of mechanical architectures in climbing plants: an evolutionary perspective”. In: *Journal of Plant Growth Regulation* 23.2 (2004), pp. 108–128.
- [7] Nick P Rowe and Thomas Speck. “Biomechanical characteristics of the ontogeny and growth habit of the tropical liana *Condylocarpon guianense* (Apocynaceae)”. In: *International Journal of Plant Sciences* 157.4 (1996), pp. 406–417.
- [8] Nick P Rowe and Thomas Speck. “Stem biomechanics, strength of attachment, and developmental plasticity of vines and lianas”. In: *Ecology of lianas* (2015), pp. 323–341.
- [9] Isabella Fiorello et al. “Taking inspiration from climbing plants: methodologies and benchmarks—a review”. In: *Bioinspiration & biomimetics* 15.3 (2020), p. 031001.
- [10] Barbara Mazzolai et al. “Emerging technologies inspired by plants”. In: *Bioinspired Approaches for Human-Centric Technologies*. Springer, 2014, pp. 111–132.
- [11] Barbara Mazzolai. “Plant-inspired growing robots”. In: *Soft Robotics: Trends, Applications and Challenges*. Springer, 2017, pp. 57–63.
- [12] Fabian Meder, Saravana Prashanth Murali Babu, and Barbara Mazzolai. “A plant tendril-like soft robot that grasps and anchors by exploiting its material arrangement”. In: *IEEE Robotics and Automation Letters* 7.2 (2022), pp. 5191–5197.
- [13] Tom Hattermann et al. “Mind the Gap: Reach and Mechanical Diversity of Searcher Shoots in Climbing Plants”. In: *Frontiers in Forests and Global Change* 5 (2022).

- [14] Joseph B Keller. “The shape of the strongest column”. In: *Archive for Rational Mechanics and Analysis* 5 (1960), pp. 275–285.
- [15] Yossi Farjoun and John Neu. “The tallest column—a dynamical system approach using a symmetry solution”. In: *Studies in Applied Mathematics* 115.3 (2005), pp. 319–337.
- [16] Z Wei, S Mandre, and L Mahadevan. “The branch with the furthest reach”. In: *Europhysics Letters* 97.1 (2012), p. 14005.
- [17] Alain Goriely. *The mathematics and mechanics of biological growth*. Vol. 45. Springer, 2017.
- [18] Barry J Goodno and James M Gere. *Mechanics of materials*. Cengage learning, 2020.
- [19] Richard B Vinter and RB Vinter. *Optimal control*. Springer, 2010.
- [20] Francis Clarke and M do R De Pinho. “Optimal control problems with mixed constraints”. In: *SIAM Journal on Control and Optimization* 48.7 (2010), pp. 4500–4524.
- [21] Francis Clarke. *Functional analysis, calculus of variations and optimal control*. Vol. 264. Springer, 2013.
- [22] Francis Clarke. *Necessary conditions in dynamic optimization*. American Mathematical Soc., 2005.
- [23] Yasmine Meroz. “Plant tropisms as a window on plant computational processes”. In: *New Phytologist* 229.4 (2021), pp. 1911–1916.
- [24] Bruno Moullia, Stéphane Douady, and Olivier Hamant. “Fluctuations shape plants through proprioception”. In: *Science* 372.6540 (2021), eabc6868.
- [25] Yasmine Meroz and Wendy K Silk. “By hook or by crook: how and why do compound leaves stay curved during development?” In: *Journal of Experimental Botany* 71.20 (2020), pp. 6189–6192.