



CLEANKER CONFERENCE  
15<sup>th</sup> of March 2023

# Sorbent properties and lab scale tests for cement applications

Progress at CSIC and USTUTT

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## 1. Sorbent studies at CSIC

❑ Raw meal as CO<sub>2</sub> capture sorbent in Calcium Looping

❑ Calcination kinetics in CO<sub>2</sub>-rich atmosphere

❑ Sulphation phenomena



## 2. Sorbent studies

### Experimental Investigation of Sulfation Phenomena in Calcium Looping Systems Integrated in Cement Plants

Edoardo De Lena,<sup>\*</sup> Mónica Alonso, and J. Carlos Abanades

❑ Cycle experiments

Cite This: *Ind. Eng. Chem. Res.* 2022, 61, 4561–4566

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❑ Entrained flow

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ABSTRACT: The sulfation phenomena of raw meal materials involved in calcium looping (CaL) applications to capture CO<sub>2</sub>



Cite This: *ACS Omega* 2018, 3, 15229–15234

<http://pubs.acs.org>

## 3. Conclusions

### Characterization of a Marl-Type Cement Raw Meal as CO<sub>2</sub> Sorbent for Calcium Looping

Mónica Alonso,<sup>\*</sup> Mathias Hornberger,<sup>†</sup> Reinhold Spörl,<sup>‡</sup> Günter Scheffknecht,<sup>‡</sup> and Carlos Abanades<sup>†</sup>

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ABSTRACT: The use of cement raw meals as sorbent precursors for CO<sub>2</sub> capture can

0.7

air-fired (IFK)

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Cite this: *React. Chem. Eng.*, 2019, 4, 2129

### Calcination kinetics of cement raw meals under various CO<sub>2</sub> concentrations

Jose Ramon Fernandez,<sup>\*</sup> Sandra Turrado and Juan Carlos Abanades



Cite This: *Ind. Eng. Chem. Res.* 2019, 58, 5445–5454

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### Kinetic Study of Belite Formation in Cement Raw Meals Used in the Calcium Looping CO<sub>2</sub> Capture Process

Mónica Alonso,<sup>\*</sup> José Ramón Fernández,<sup>\*</sup> and Juan Carlos Abanades

Spanish Research Council, INCAR-CSIC, Francisco Pintado Fe, n. 26, 33011 Oviedo, Spain

ABSTRACT: Calcium looping technology could be one of the most efficient ways to drastically reduce the carbon footprint of cement manufacture since CaCO<sub>3</sub> is a major component of the raw meal used to produce clinker. However,

Deactivation by belite formation

Quantification (kinetic model)

### Carbonation of Fine CaO Particles in a Drop Tube Reactor

Sandra Turrado, Borja Arias, José Ramón Fernández,<sup>\*</sup> and Juan Carlos Abanades

Spanish Research Council, INCAR-CSIC, Francisco Pintado Fe, n. 26, 33011 Oviedo, Spain

ABSTRACT: The calcium looping technology using entrained flow reactors seems particularly suited for integration in cement plants due to the fine particle diameters and high gas velocities that are characteristic of these plants. However, there is little experimental information available in the literature on the carbonation performance





# Main experimental facilities used at CSIC for CaL gas-solid reactions involving raw meals

- CO<sub>2</sub> carrying capacity
- Belite formation kinetics
- Calcination kinetics
- Carbonation kinetics
- Sulfation kinetics

## Thermogravimetric analysers

TA-Q5000IR



In-house TGA



Reactions with time scales >10 s

Solids/  
Carrier gas

T/CO<sub>2</sub>/O<sub>2</sub>  
Solids sampling

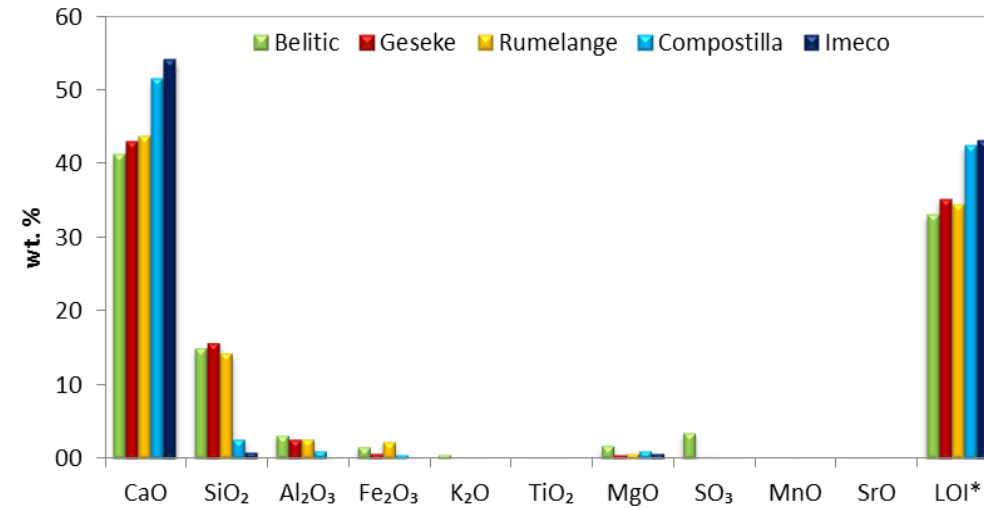


scales <10 s

## 13 Calcium-based raw meals materials

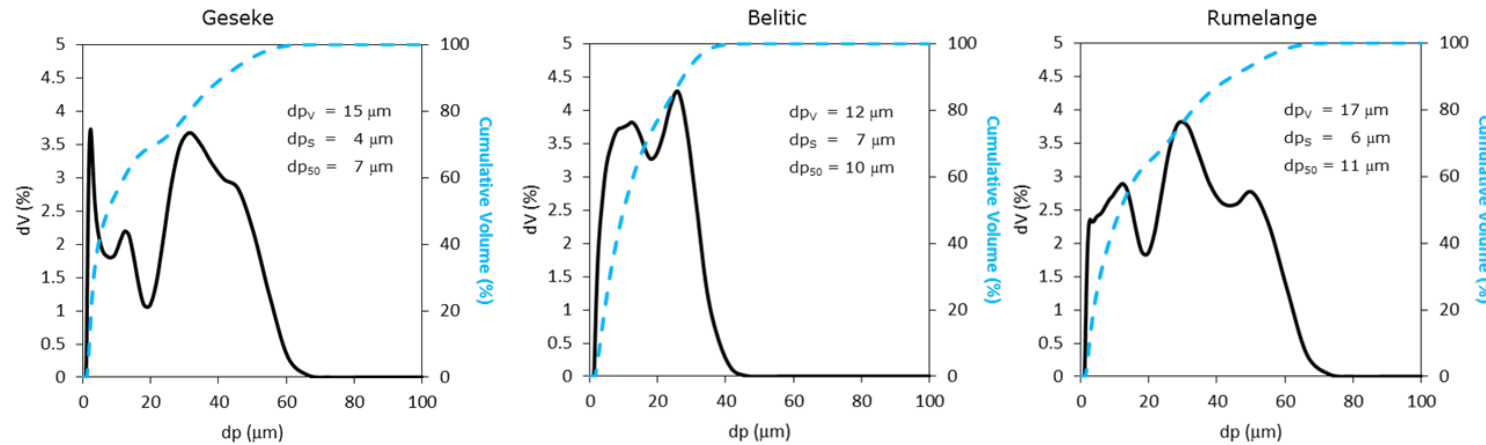
- **Rumelange**: mixture of marl, limestone and slag
- **Belitic**: mixture of marl, limestone and gypsum
- **Geseke**: mixture of marl and a corrective material (4 wt.%)
- **Compostilla**: limestone (<20 µm, 20-36 µm, 36-63 µm)
- **Imeco**: limestone (<20 µm, 20-36 µm, 36-63 µm)
- **Vernasca**: mixture of marl (Marine) and limestone (Calcare)
- **Marine**: marl
- **Calcare**: limestone
- **Bilbao**: marl

## Chemical composition (XRF)



- Similar contents of CaO (41-43 wt.%), SiO<sub>2</sub> (15 wt.%) and Al<sub>2</sub>O<sub>3</sub> (3 wt.%) in the raw meals
- Relevant content of Fe<sub>2</sub>O<sub>3</sub> (2.3 wt.%) in Rumelange (presence of slag)
- High content of SO<sub>3</sub> (3.5 wt.%) in Belitic (presence of gypsum)

## Particle size distribution



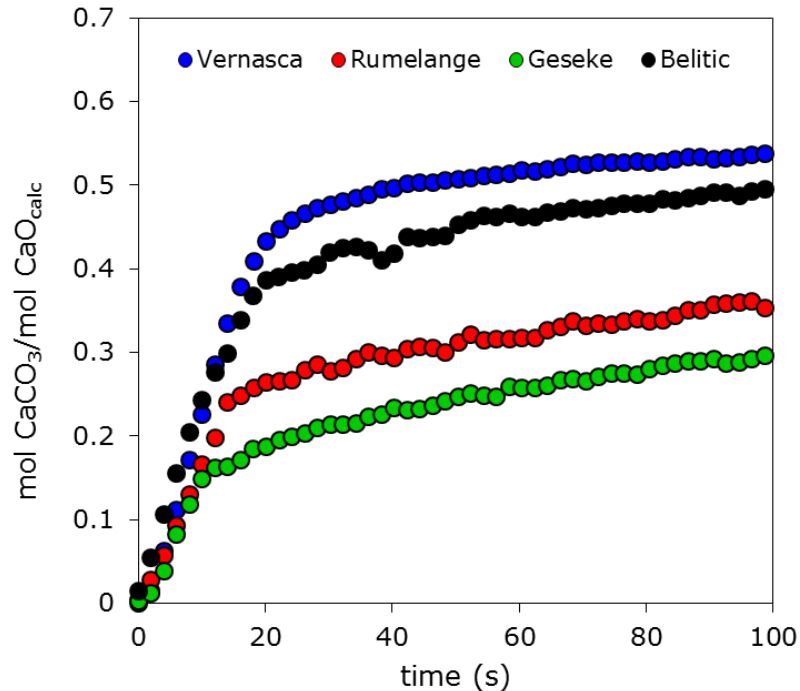
- Clearly separated volumetric fractions
- Similar average diameters (not expected diff. behaviour due to particle size)

## BET surface area

Material	BET area (m <sup>2</sup> /g)
<u>Raw meals/marls</u>	
Vernasca	13.5
Rumelange	6.1
Belitic	10.8
Bilbao	3.6
Geseke	4.3
Marine	13.7
<u>Limestones</u>	
Calcare	1.4
Compostilla <20 μm	4.0
Compostilla 20-36 μm	4.0
Compostilla 36-63 μm	3.1
Imeco <20 μm	0.6
Imeco 20-36 μm	0.6
Imeco 36-63 μm	0.4

- Limestones present in general the lowest BET areas (0.4-4 m<sup>2</sup>/g). BET areas increase as  $d_p$  is reduced (for  $d_p > 20 \mu\text{m}$ )
- Intermediate values (3.6-6.1 m<sup>2</sup>/g) for Bilbao (marl), Geseke (marl) and Rumelange (mixture)
- Largest BET areas (11-13.7 m<sup>2</sup>/g) for Belitic (mixture), Marine (marl) and Vernasca (mixture).

## CO<sub>2</sub> carrying capacity tests with different raw meals



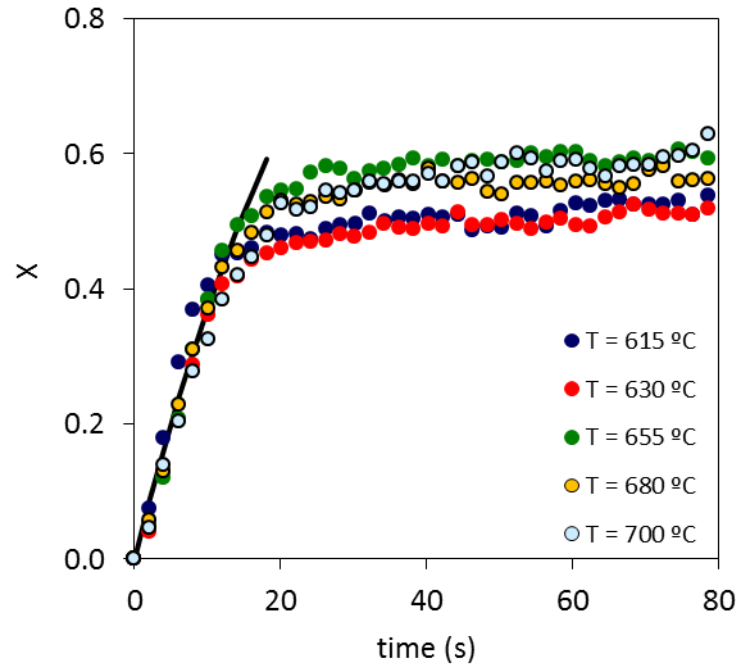
- Materials with higher **Ca-Si aggregation level** show lower **CO<sub>2</sub> carrying capacities** (formation of belite)
- **Geseke** (almost single compound raw meal) shows the lowest CO<sub>2</sub> carrying capacity
- **Belitic** (mixture) exhibits similar behaviour to Vernasca (i.e. similar Ca-Si aggregation level)
- **Rumelange** (mixture) presents lower carbonation conversion than expected. Possible formation of other compound/s that consume active CaO (due to unknown crystalline phase detected by XRD?)

# Reactivity of calcined Vernasca raw meal towards CO<sub>2</sub> (from TG experiments)

- Carbonation expe. and tuning of kinetic model for Vernasca

$$X_{carb} = 1 - (1 - k_{carb}(v_{CO_2} - v_{eq})t)^3$$

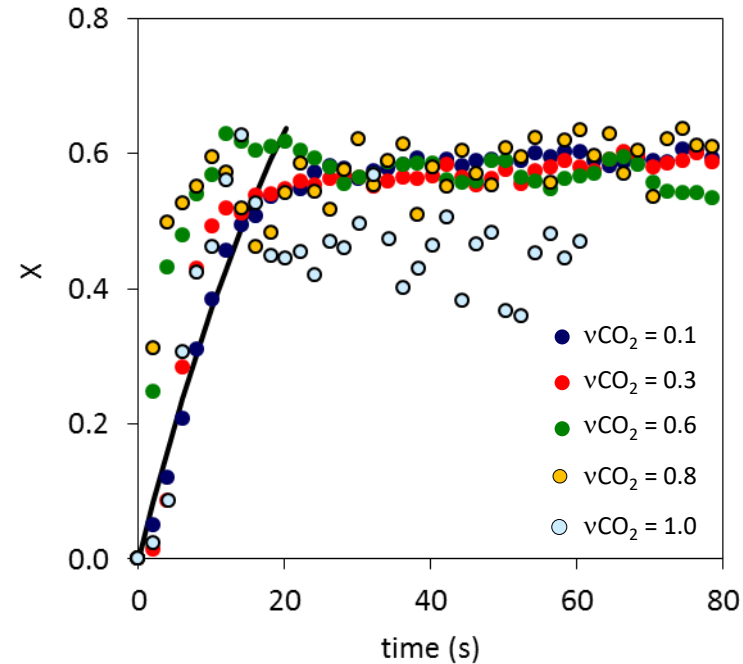
10 vol% CO<sub>2</sub> in air



In the reported range values

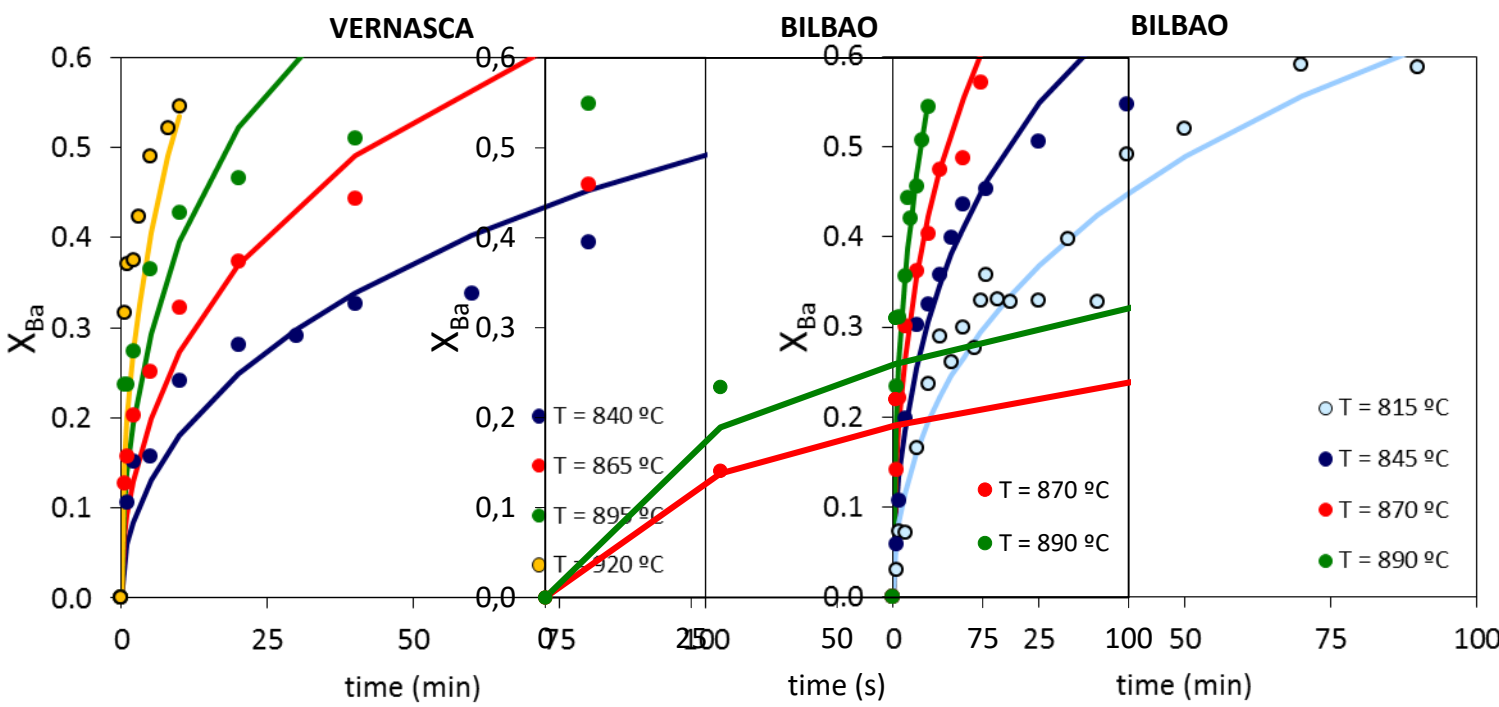
$$k_{0,carb} = 4.61\text{ s}^{-1}; E_a = 26\text{ kJ/mol}$$

$T_{carb} = 655\text{ }^{\circ}\text{C}$



- Similar tendencies than those observed for CaO derived from limestone in the fast stage.
- The CO<sub>2</sub> concentration greatly affects the carbonation rate.

- Extent of belite formation during the calcination of Vernasca



$$X_B = 1 - \left[1 - (k_B t)^{1/2}\right]^3$$

	$k_0 \text{ (s}^{-1}\text{)}$	$E_a \text{ (kJ/mol)}$
Before calcination	6.64	133
After calcination	$4.35 \times 10^{10}$	336

Similar value to Weisweiler et al.

- Calcination temperature greatly affects the reaction.
- In Vernasca raw meal (low level of Ca/Si aggregation) the model overestimates belite formation at long times
- Belite formation in Bilbao raw meal (marl) is accurately described

**I&EC research**  
Initiated & Engineering Chemistry Research

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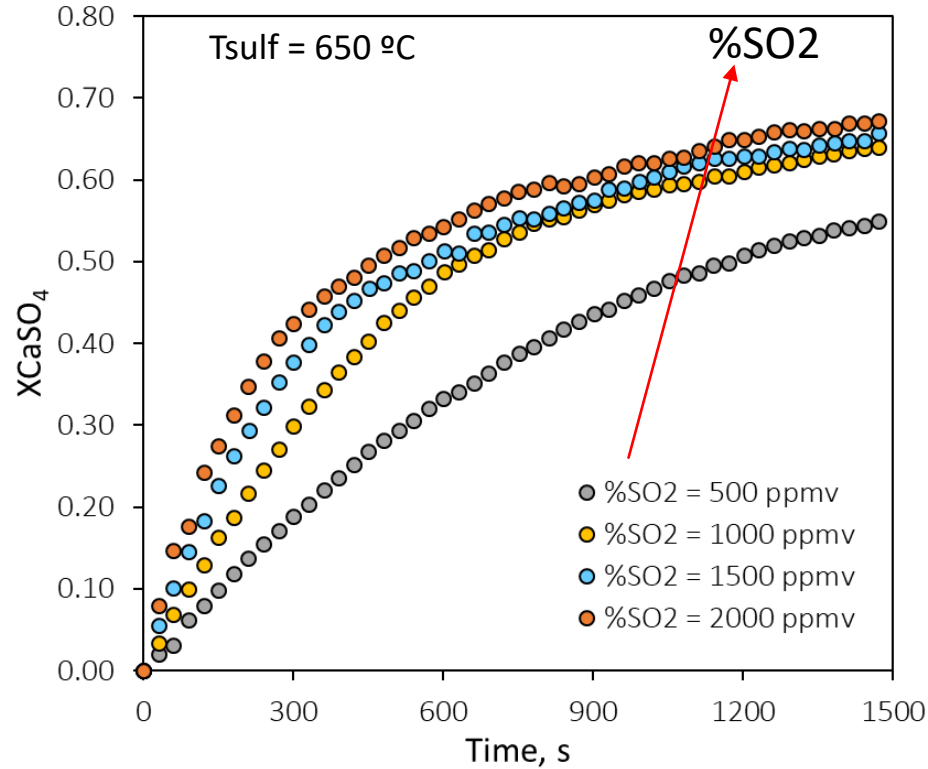
Cite This: Ind. Eng. Chem. Res. 2019, 58, 5445–5454  
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**Kinetic Study of Belite Formation in Cement Raw Meals Used in the Calcium Looping CO<sub>2</sub> Capture Process**  
Mónica Alonso, José Ramón Fernández, and Juan Carlos Abanades  
Spanish Research Council, INCAR-CSIC, Francisco Pintado Fe, n. 26, 33011 Oviedo, Spain

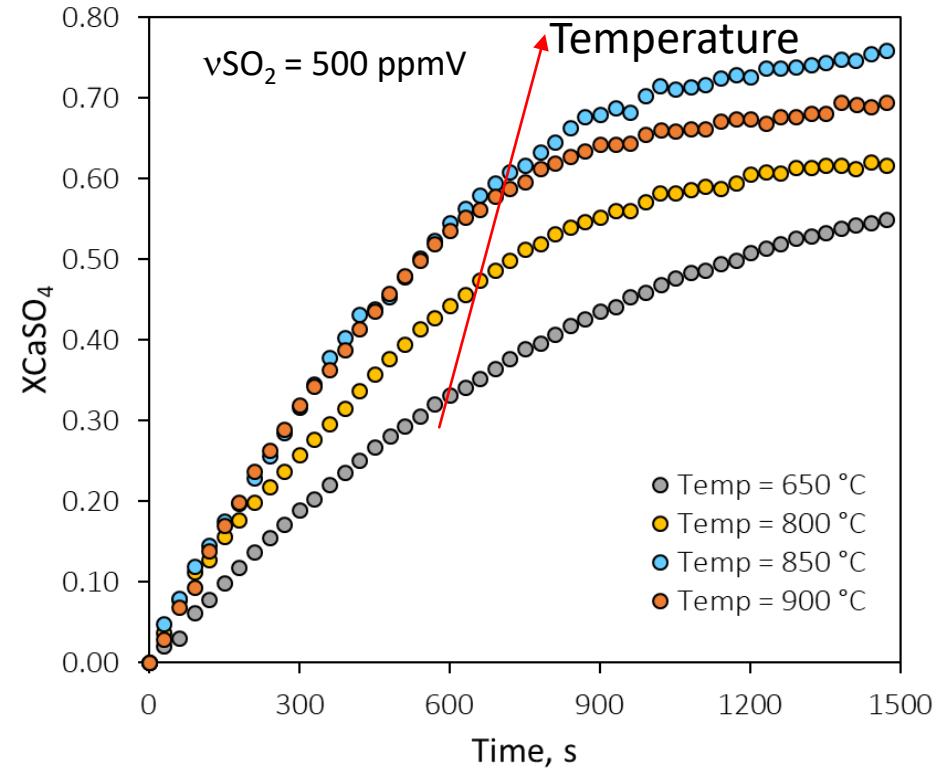
**ABSTRACT:** Calcium looping technology could be one of the most efficient ways to drastically reduce the carbon footprint of cement manufacture since CaCO<sub>3</sub> is a major component of the raw meal used to produce clinker. However, the deactivation of the process by belite formation is a major concern. This work presents a kinetic study of the deactivation of the process by belite formation. The results show that the deactivation is more pronounced at higher temperatures and higher Ca/Si ratios. A kinetic model was developed to describe the deactivation process, and the activation energy was determined to be 336 kJ/mol.



- Effect of sulfation temperature and  $\text{SO}_2$  concentration on Vernasca (non belite)

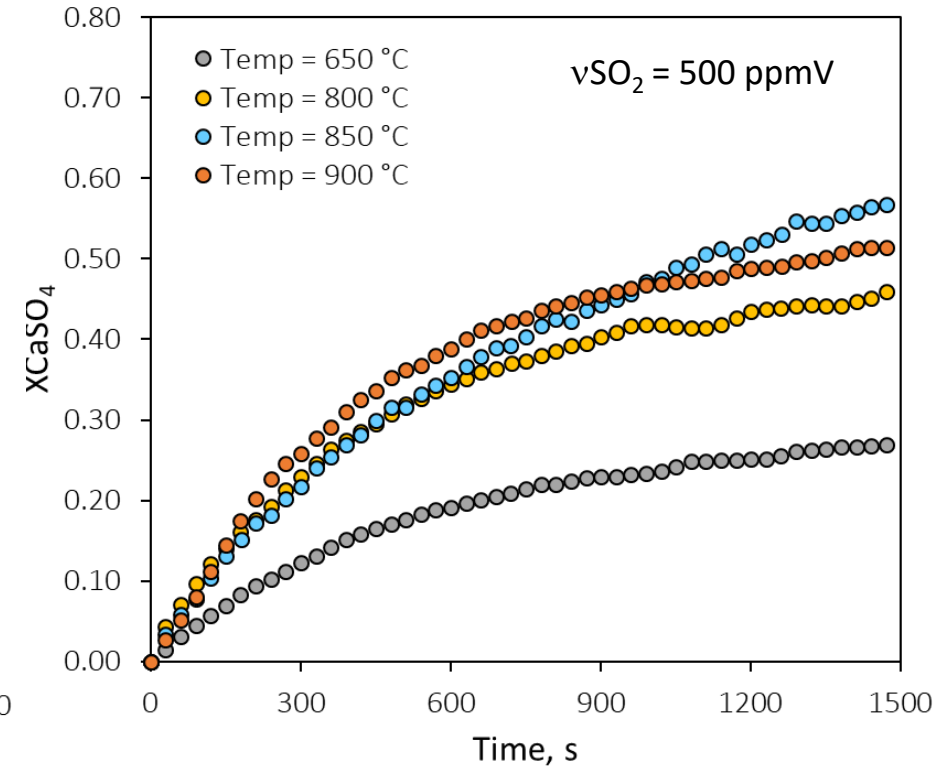
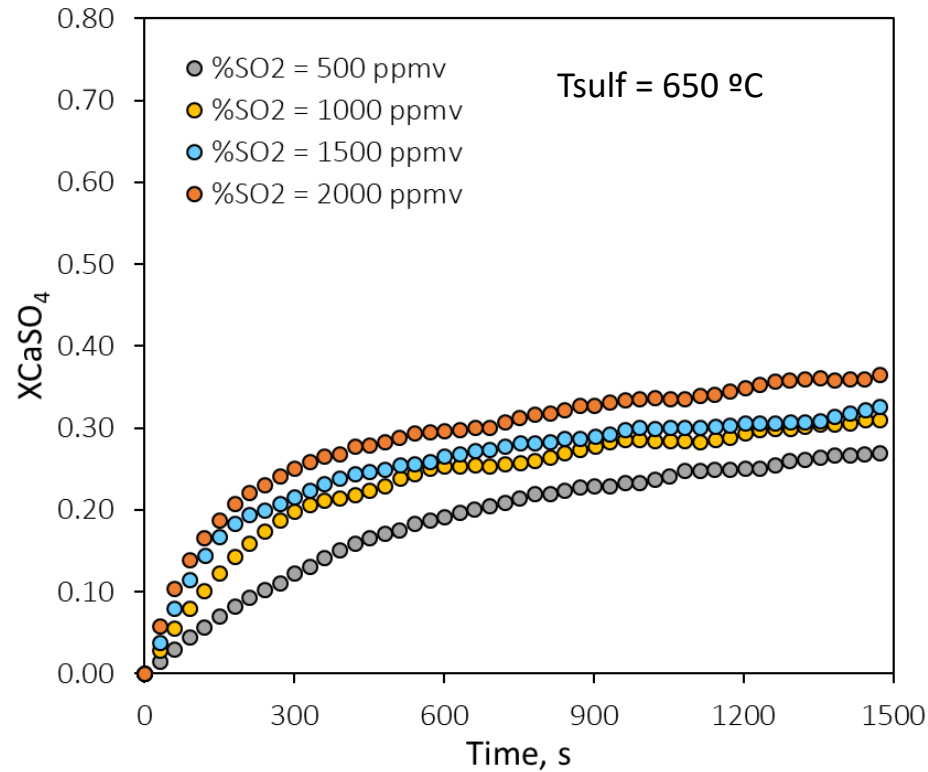


There is an increase in sulfation as the sulphur content in the flue gas increases



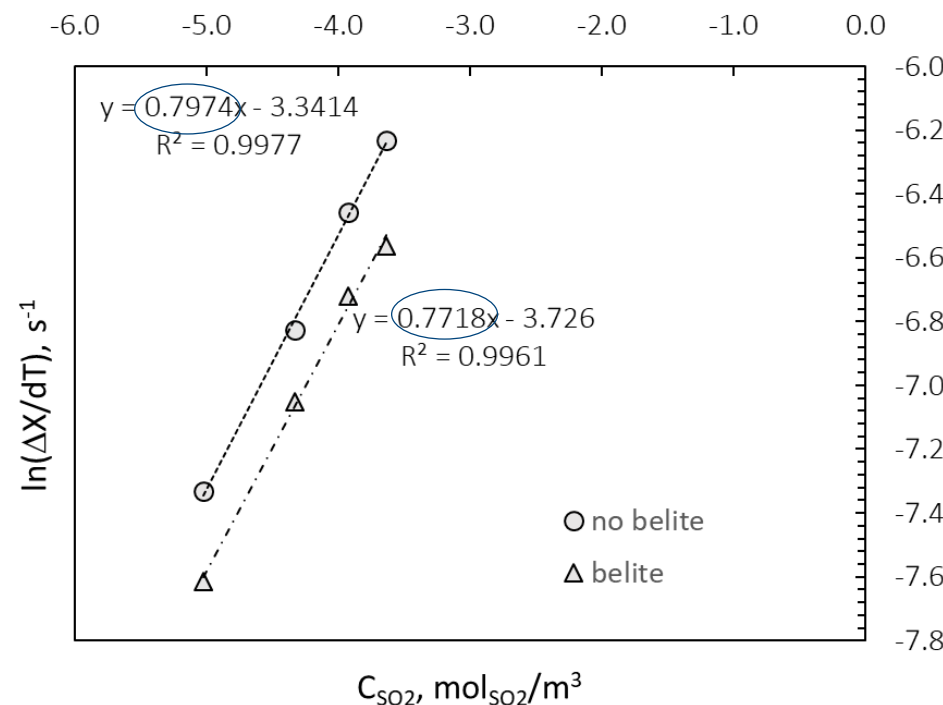
There is also an increase in sulfation as the temperature increases. But the maximum was achieved at 850 °C

- Effect of sulfation temperature and  $\text{SO}_2$  concentration on Vernasca (maximum belite)

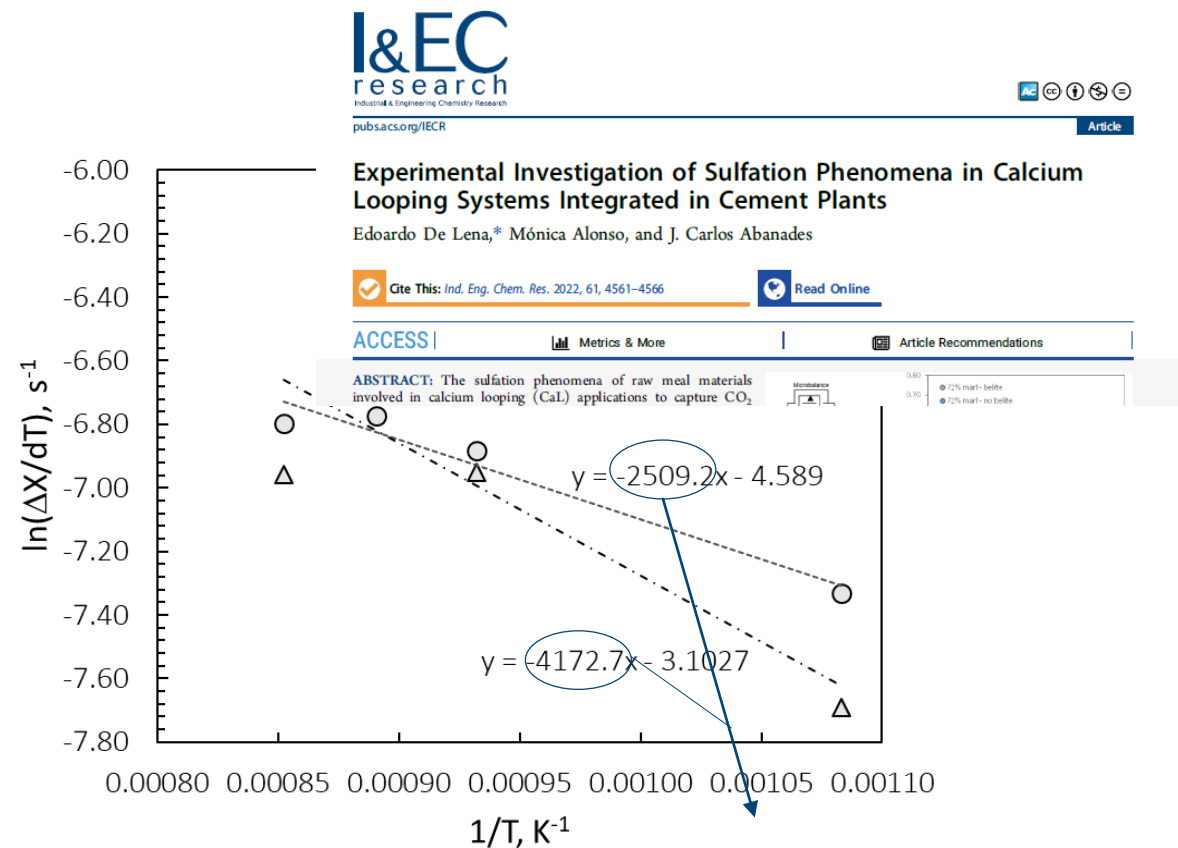


*The shape of the obtained curves are the same but with a lower conversion, due to the presence of the belite*

- Kinetic regime parameters

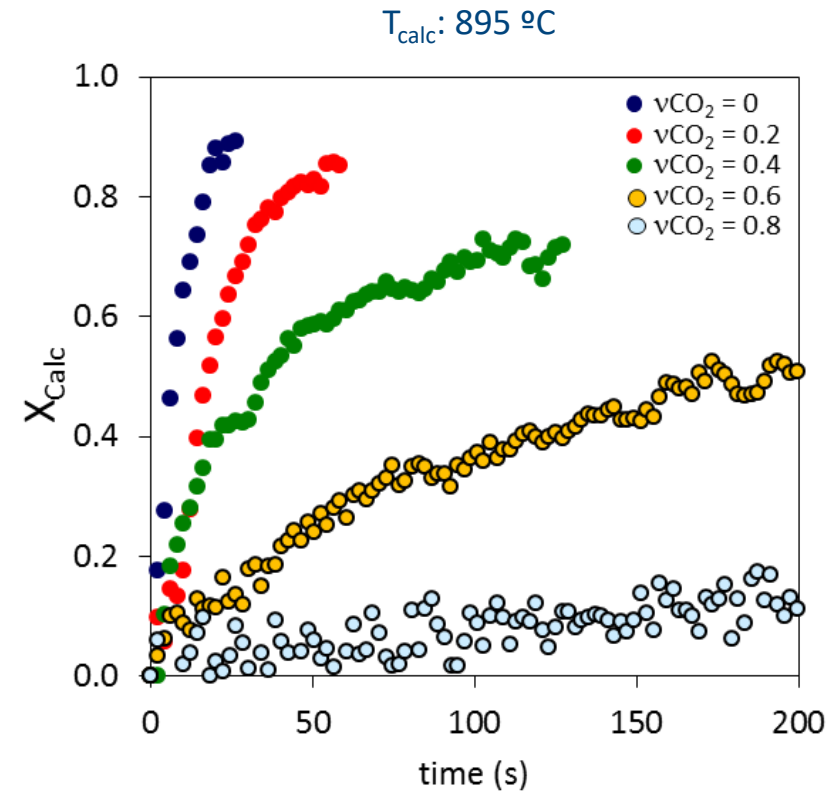


Apparent reaction order of 0.8  
(very similar to a reaction order  
for a limestone between 0.6 – 1)



Activation energy for the kinetic regime  
between 20.9 kJ/mol and 34.7 kJ/mol  
(very similar to E<sub>act</sub> for a limestone  
between 20-41 kJ/mol)

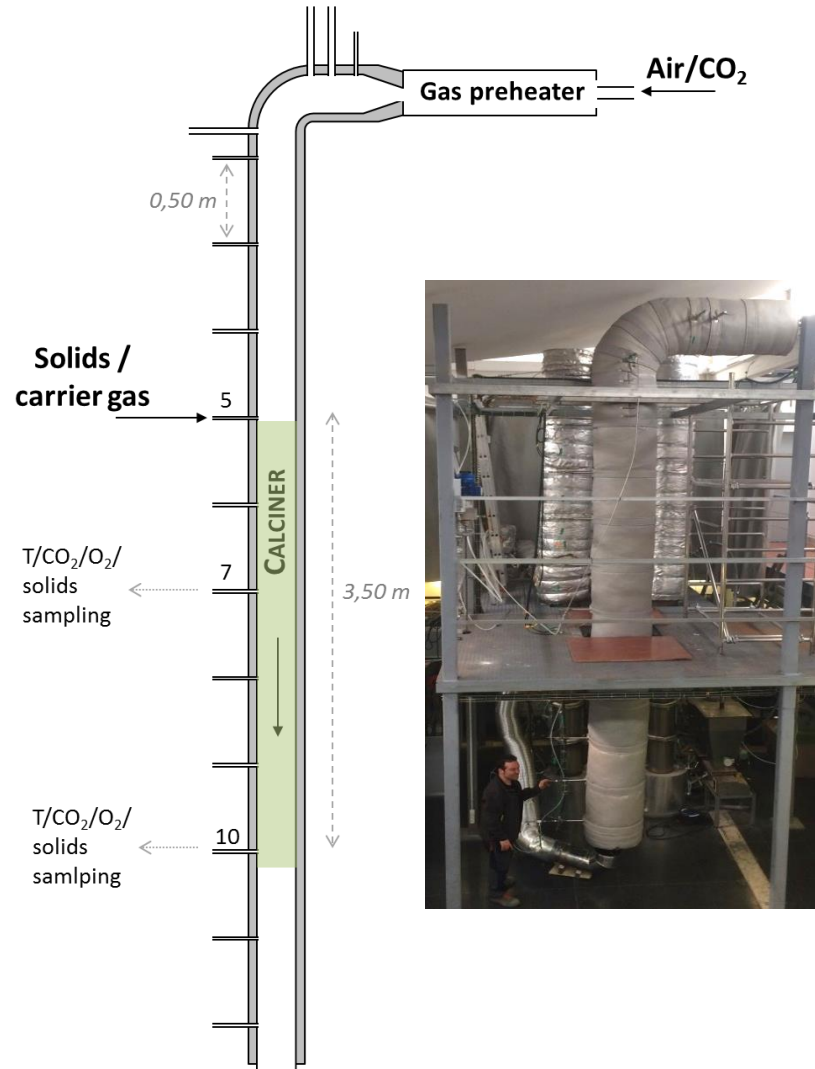
- Calcination experiments with Vernasca



- Much longer calcination times than those found in suspension reactors.
- Heat transfer resistance has been identified as the main limitation to measure reliable kinetics of very fast reactions.



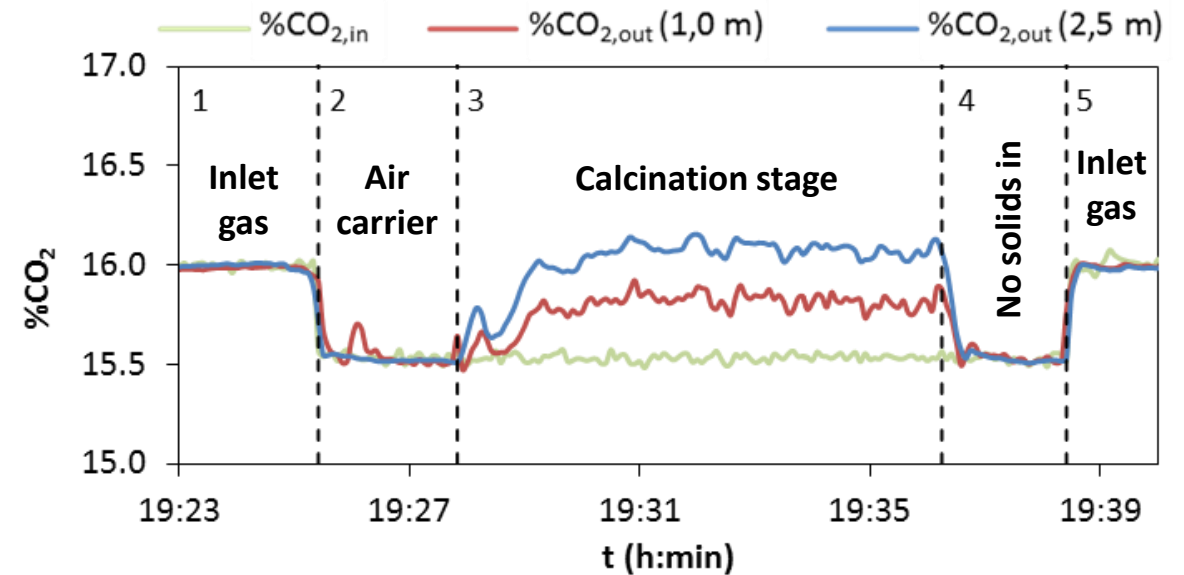
## Experimental methodology



## Main operating conditions tested in the drop tube

Calciner temperature (°C)	$T_{calc}$	790-1000
Calciner inlet velocity (m/s)	$u_{calc}$	1.1 - 2.2
Inlet CO <sub>2</sub> to the calciner	vol. %	0 - 90
Solids flowrate (kg/h)	$\dot{m}_s$	0.2 - 1.0

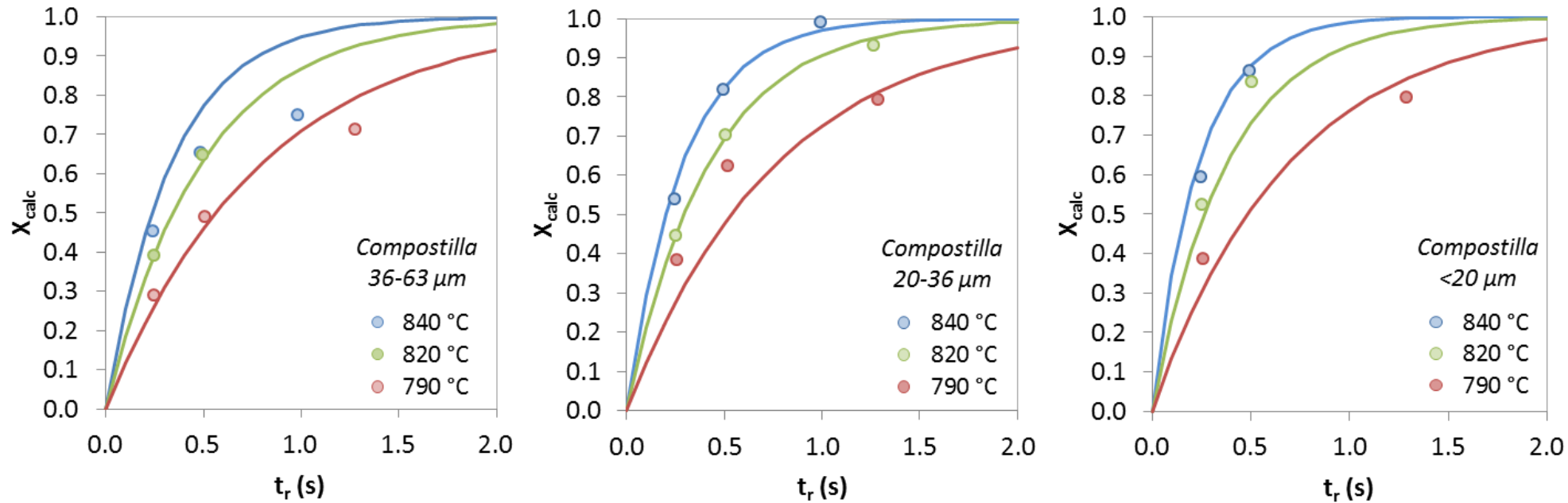
Pulverized coal was mixed (up to 10% wt) with raw meals for tests at  $T > 900^\circ\text{C}$



Experimental conditions (reference test): material Compostilla 36-63  $\mu\text{m}$ ,  $T = 860^\circ\text{C}$ ,  $u_{gas} = 2 \text{ m/s}$ ,  $\text{solids}_{in} = 0.65 \text{ kg/h}$ ,  $\%CO_{2in} = 15.5$

## 2. Experimental results: kinetic studies of calcination

### Effect of particle size and surface area on calcination kinetics



- Higher surface BET areas accelerate the calcination of  $CaCO_3$
- Calcination in air (0 vol.%  $CO_2$ ),  $T = 820$  °C and  $t_r = 0.5$  s:

### RESULTS CONSISTENT WITH BORGWARD'S MODEL (1985)

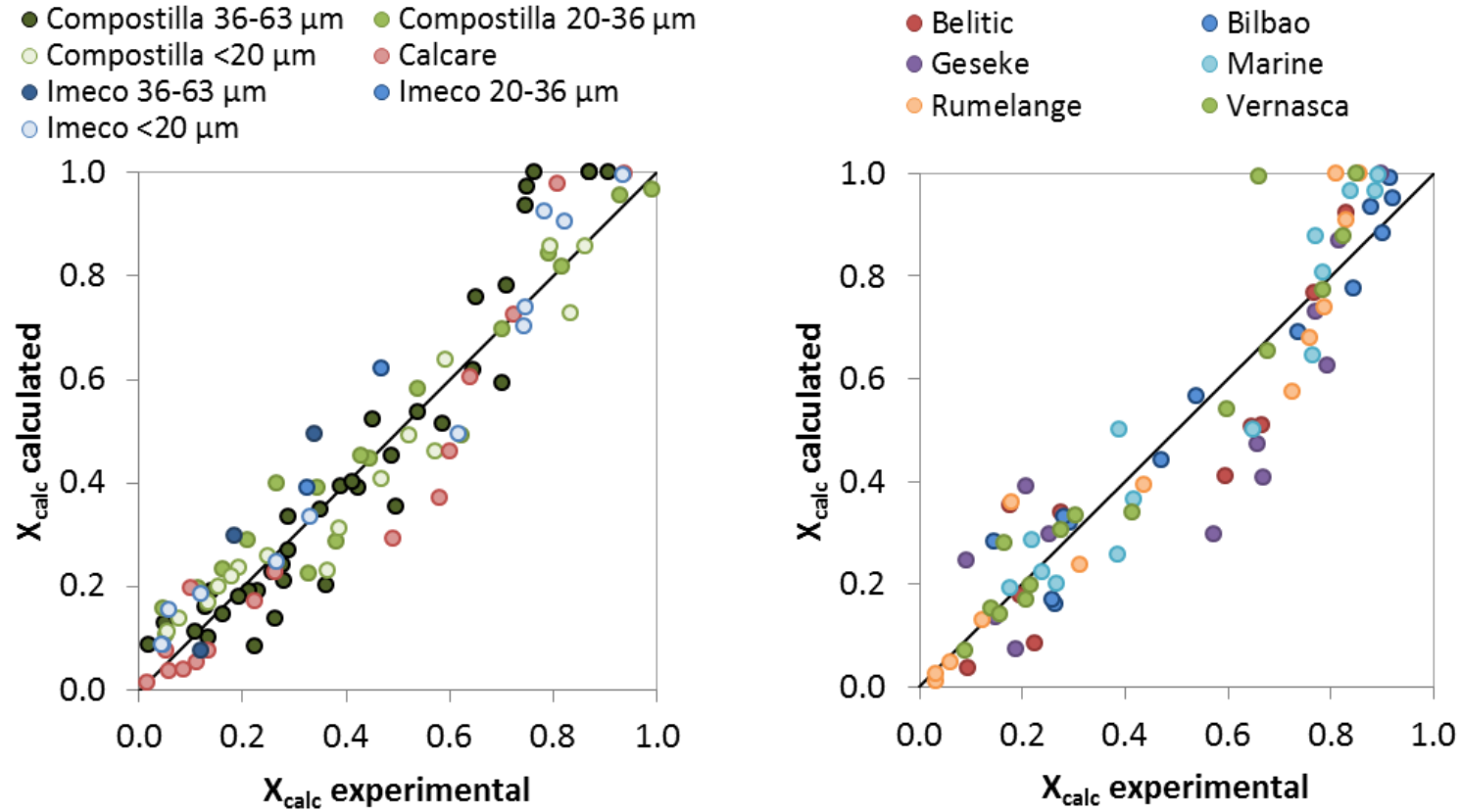
(calcination in atmospheres free of  $CO_2$ )

Compostilla 36-63 $\mu m$ ( $S_{BET} = 3.1 \text{ m}^2/\text{g}$ )	$\longrightarrow$	$X_{cal} = 0.60$
Compostilla 20-36 $\mu m$ ( $S_{BET} = 4.0 \text{ m}^2/\text{g}$ )	$\longrightarrow$	$X_{cal} = 0.70$
Compostilla $<20 \mu m$ ( $S_{BET} = 4.0 \text{ m}^2/\text{g}$ )	$\longrightarrow$	$X_{cal} = 0.70$



## 2. Kinetic studies of calcination

### Experimental vs. model



- The model predicts reasonably well the extent of the solids conversion for all the materials tested in this study ( $r^2 \approx 0.90$ )



## 2. Kinetic studies of calcination

### Kinetic model

Borgwardt (1985):  $X_{calc} = 1 - e^{-k_1 S_g t_r}$

Valverde et al. (2015):  $\beta(T, P_{CO_2}) = k_1 \left( 1 - \frac{v_{CO_2}}{v_{CO_2,eq}} \right) \frac{1}{1 + K_1 \frac{v_{CO_2}}{v_{CO_2,eq}}}$

$$X_{calc} = 1 - e^{-a_1 e^{(-E_1/RT)} \left( 1 - \frac{v_{CO_2}}{v_{CO_2,eq}} \right) \frac{1}{1 + A_1 e^{(-\Delta_1 H^0/RT)} \frac{v_{CO_2}}{v_{CO_2,eq}}} S_g t_r}$$

194.5 kJ/mol (Borgwardt, 1985)

150 kJ/mol (Valverde et al., 2015)

Material	$a_1$ (mol/m <sup>2</sup> s)	$A_1$ (-)
Compostilla	$11.7 \cdot 10^6$	$153 \cdot 10^6$
Imeco	$45.8 \cdot 10^6$	$152 \cdot 10^6$
Calcare	$11.9 \cdot 10^6$	$219 \cdot 10^6$
Vernasca	$2.9 \cdot 10^6$	$137 \cdot 10^6$
Marine	$3.0 \cdot 10^6$	$43 \cdot 10^6$
Geseke	$5.8 \cdot 10^6$	$66 \cdot 10^6$
Rumelange	$4.9 \cdot 10^6$	$239 \cdot 10^6$
Belitic	$1.6 \cdot 10^6$	$28 \cdot 10^6$
Bilbao	$9.6 \cdot 10^6$	$27 \cdot 10^6$

### Reaction Chemistry & Engineering

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Cite this: DOI: 10.1039/c9re00361d

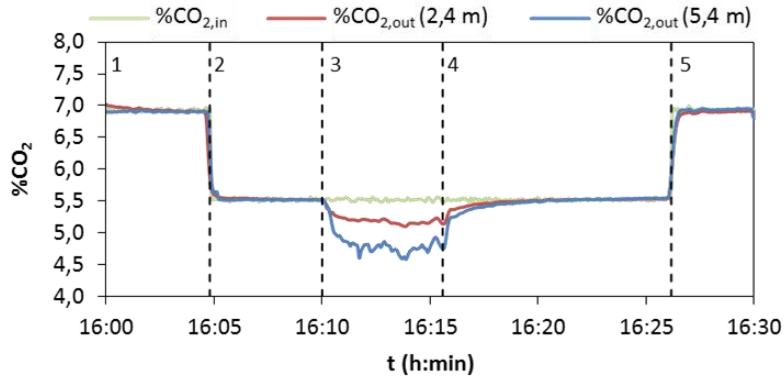
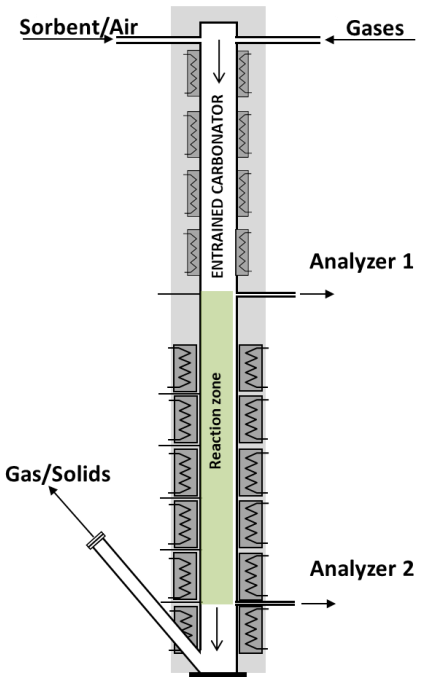
Calcination kinetics of cement raw meals under various CO<sub>2</sub> concentrations





## 2. Kinetic studies of carbonation

### Experimental methodology



### Main operating conditions tested in the drop tube

Carbonator temperature (°C)	$T_{carb}$	590 - 720
Inlet velocity (m/s)	$u_{carb}$	0,5 - 2,0
Inlet CO <sub>2</sub> to carbonator	$v_{CO_2}$	0,05 - 0,30
Inlet H <sub>2</sub> O to carbonator	$v_{H_2O}$	0 - 0,25
$X_{ave}$	$X_{ave}$	0,17 - 0,67
Solid flow rate(kg/h)	$\dot{m}_s$	0,3 - 8,0
$dp_{50}$ (μm)	$d_{p50}$	48 - 53

### Carbonation of Fine CaO Particles in a Drop Tube Reactor

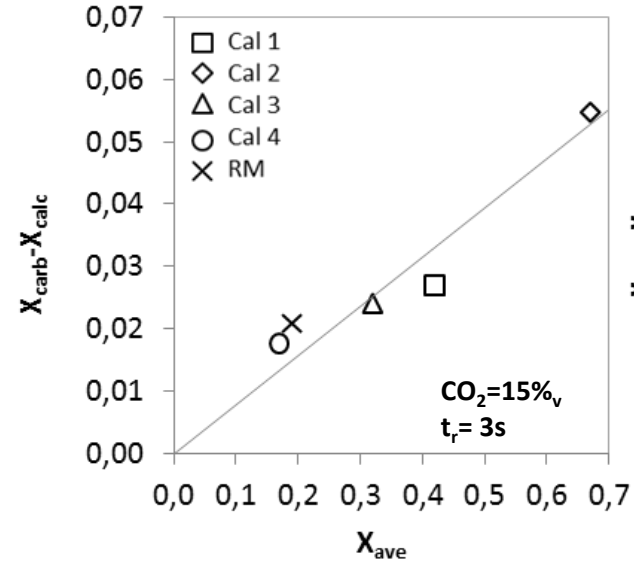
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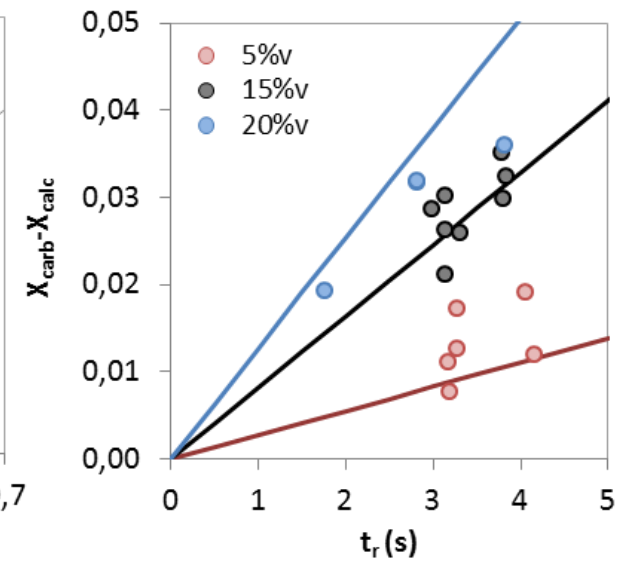
**ABSTRACT:** The calcium looping technology using entrained flow reactors seems particularly suited for integration in cement plants due to the fine particle diameters and high gas velocities that are characteristic of these plants. However, there is little experimental



### Effect of $X_{ave}$ on carbonation conversion



### Effect of CO<sub>2</sub> concentration on carbonation conversion



### Basic carbonation kinetic model

$$\left(\frac{dX}{dt}\right)_{\text{Reactor}} = k_s \phi X_{ave} (\overline{v_{CO_2}} - v_{CO_2 \text{ eq}})$$

$0.16 \text{ s}^{-1}$  (in agreement with values reported in the literature)

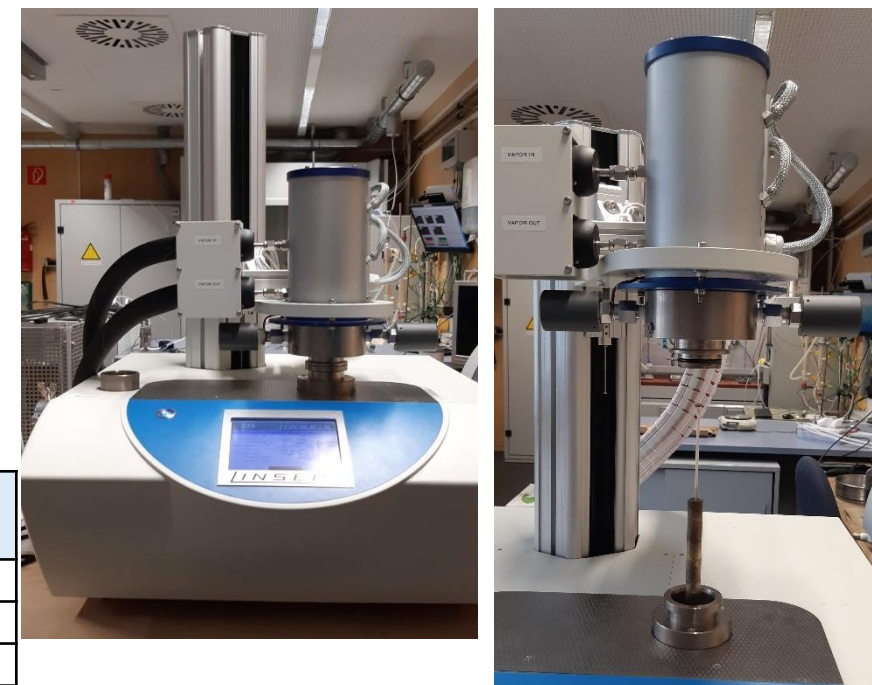
# 1. Sorbent studies at USTUTT: Cycle experiments

## Properties of cycle experiments:

- TGA conditions set in order to represent entrained flow conditions as good as possible
  - Fast heat up and cool down ramps
  - Short dwell time at calcining conditions
- Oxy-fuel and air calcination
- Sample weight of approx. 12 mg
- Investigated raw meals:
  - Vernasca raw meal
  - Bilbao
  - Geseke
  - Rumelange
  - Vernasca Calcare

	Vernasca	Bilbao	Geseke	Rumelange	Vernasca Calcare
$\gamma_{CaO}$	0,4127	0,4007	0,4345	0,4576	0,5035
$\gamma_{SiO_2}$	0,1673	0,1439	0,1455	0,1367	0,0298
$\gamma_{Fe_2O_3}$	0,0233	0,0195	0,0089	0,0253	0,0047
$\gamma_{Al_2O_3}$	0,0356	0,0628	0,0227	0,0272	0,0091
$\gamma_{MgO}$	0,0121	0,0138	0,0044	0,0018	0,0176
$\gamma_{CO_2}$	0,3307	0,3349	0,3704	0,3371	0,4315
$\gamma_{others}$	0,0184	0,0245	0,0135	0,0142	0,0039

## Experimental setup

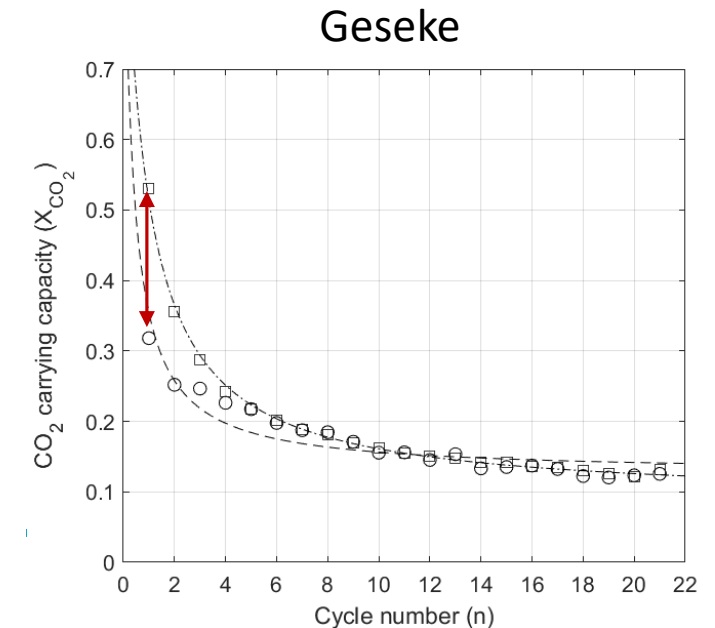
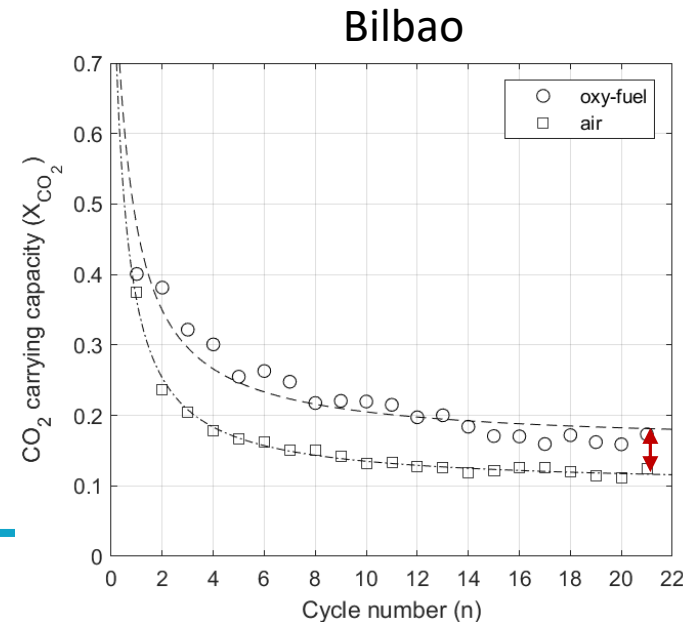
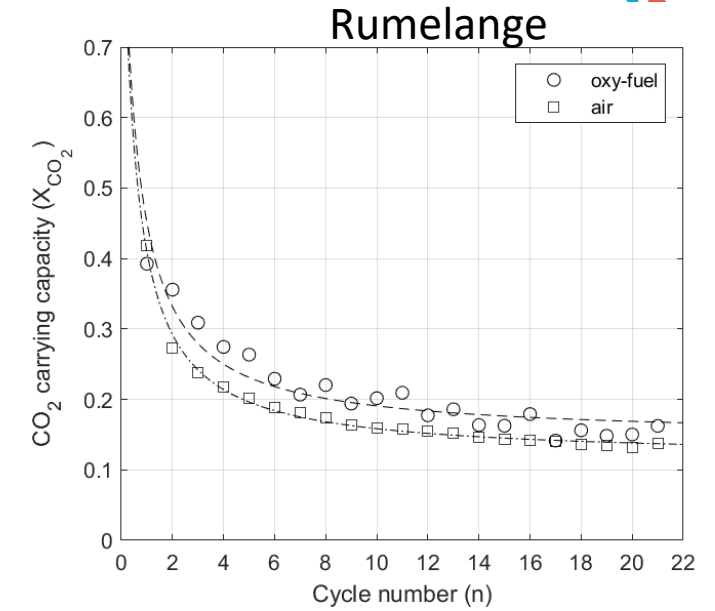
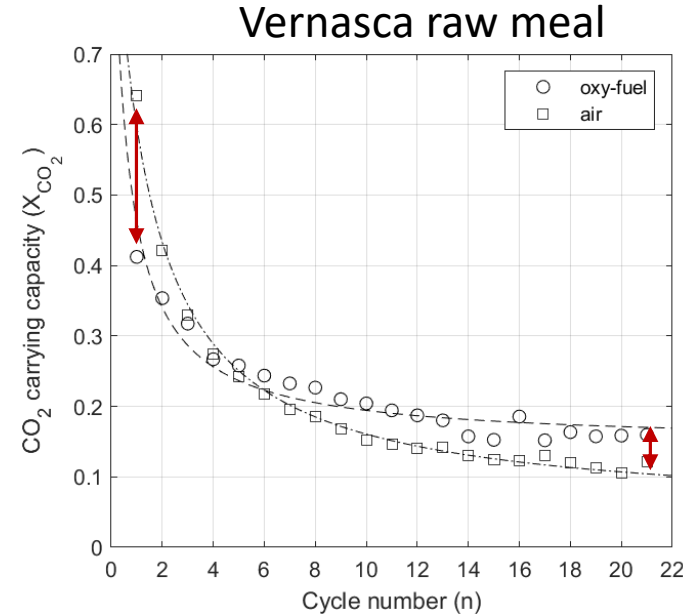


Linseis STA PT 1100

# 1. Sorbent studies at USTUTT: Cycle experiments

## Results:

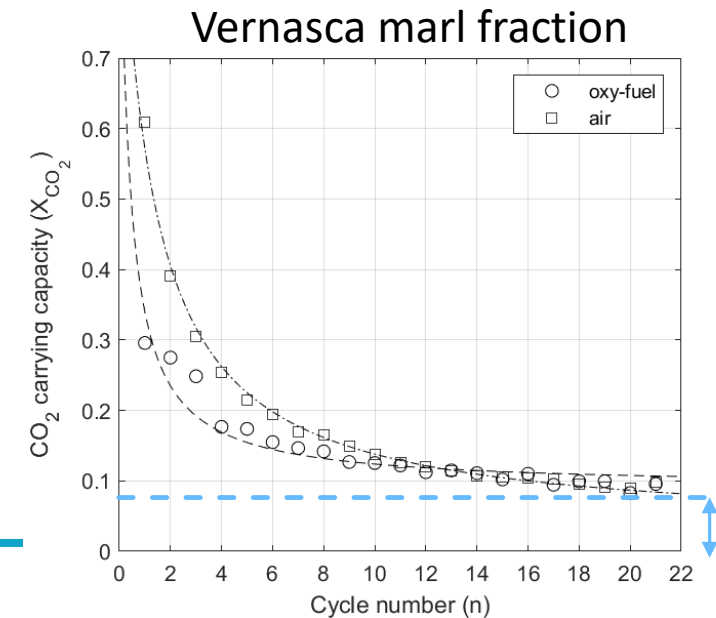
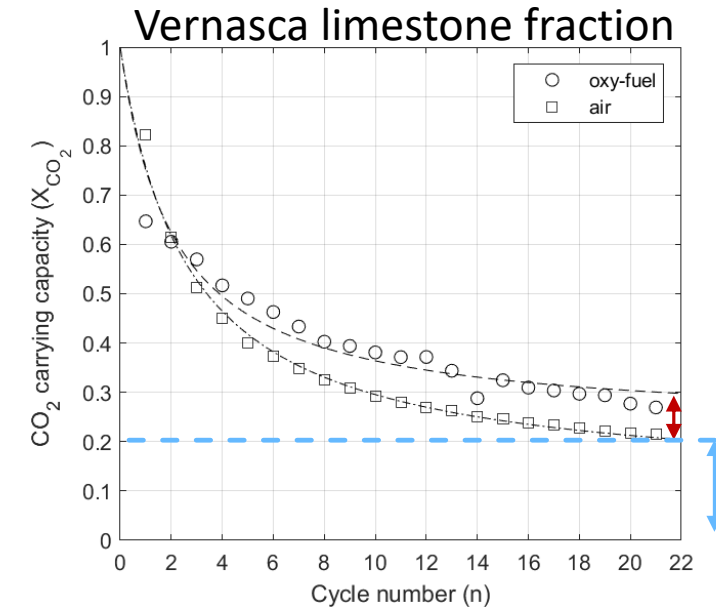
- Initial deactivation & residual activity  
→ appear to be dependent from the reaction atmosphere
- Cycles with oxy-fuel calcination show higher residual activity
- Different properties between the raw meals have big impact on results



# 1. Sorbent studies at USTUTT: Cycle experiments

## Results:

- additionally, the two main components of the Vernasca raw meal were investigated separately
  - Marl fraction of the raw meal:
    - Residual activity not dependent from the reaction conditions
    - Much lower residual activity compared to limestone fraction
- Predominantly responsible for the deactivation of the Vernasca raw meal



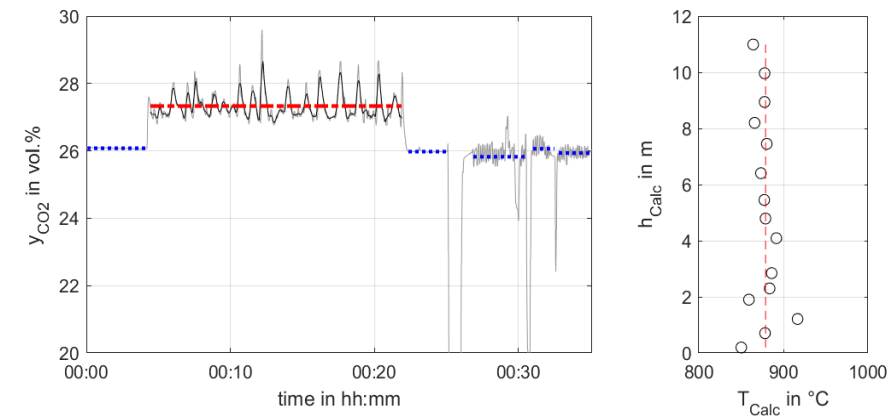


## 2. Sorbent studies at USTUTT: Calcination experiments in entrained flow reactor

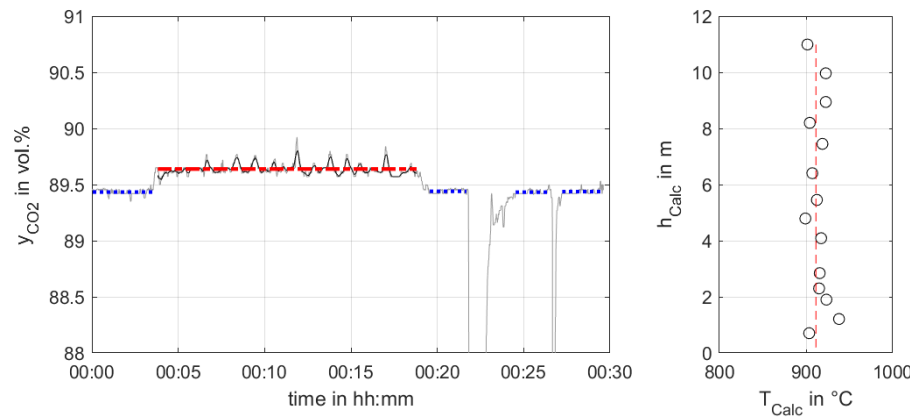
### Properties of calcination experiments:

- Test rig:
  - Electrically heated, 120 kW<sub>el</sub>
  - 12.4 m height, 68 mm diameter
- Three different setups:
  - Air calcination at 860°C and CO<sub>2</sub> concentration of 0.26 m<sup>3</sup>/m<sup>3</sup>
  - Oxy-fuel calcination at 900°C and CO<sub>2</sub> concentration of ~0.90 m<sup>3</sup>/m<sup>3</sup>
  - Oxy-fuel calcination at 920°C and CO<sub>2</sub> concentration of ~0.90 m<sup>3</sup>/m<sup>3</sup>

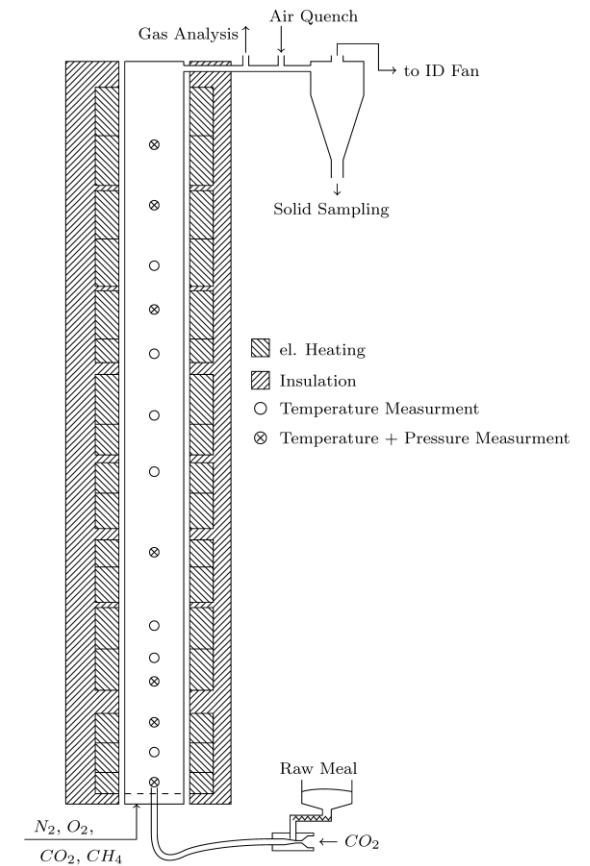
Air calcination



Oxy-fuel calcination



### Experimental setup



USTUTT's entrained flow reactor

## 2. Sorbent studies at USTUTT: Calcination experiments in entrained flow reactor

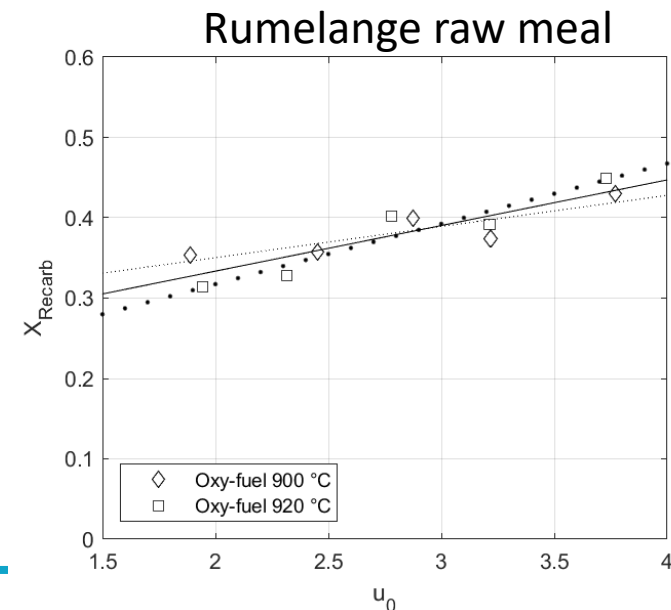
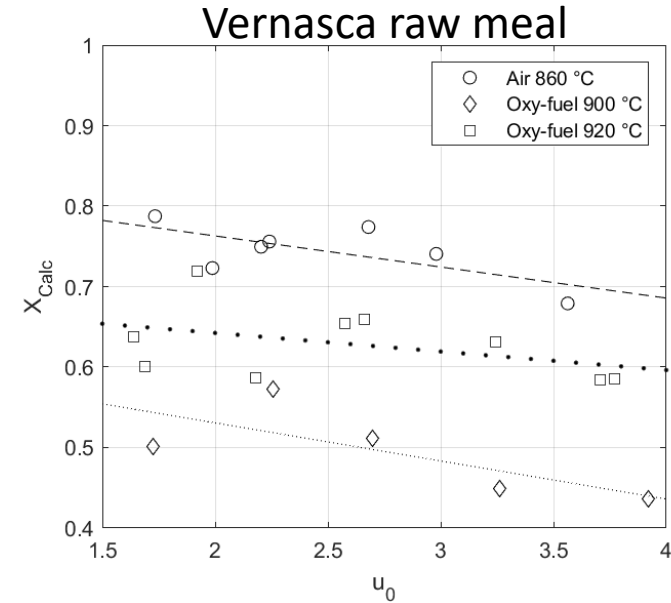
### Results:

#### Calcination Degree

- Common trends over different raw meals:
  - Calcination kinetics improve with higher temperature
  - Calcination rate increases with reaction time

#### Recarbonation Degree

- Common trends over different raw meals:
  - Higher ability to absorb CO<sub>2</sub> with increasing velocity (i.e. shorter residence time)
  - Samples from oxy-fuel calcination: no significant influence of the calcination temperature on the recarbonation observable



- The **performance of raw meals** in all gas-solid reaction CaL-Systems **strongly depend on their chemical and physical composition** and level of aggregation of Ca/Si atoms
- **Carbonation:**
  - Active fraction of CaO, kinetics of carbonation, sulfation rates and belite formation rates can be determined by TG analysis
  - Carbonation rate is shown to be proportional to the CO<sub>2</sub> carrying capacity of the sorbent, regardless the origin of the calcined material under the experimental conditions tested
  - Marl fraction of the raw meal predominantly responsible for the deactivation of the Vernasca raw meal
- **Calcination:**
  - Calcination in oxy-fuel conditions requires drop tube / entrained flow apparatus
  - Within short gas-solid contact times, reasonable calcination rates possible
  - Dependency of calcination rate and surface area of the carbonate, activation energy and the standard enthalpy of CaCO<sub>3</sub> decomposition noticeable

**This project has received funding from the European Union's Horizon 2020 research and innovation programme under Grant Agreement n. 764816**

**This work is supported by the China Government (National Natural Science Foundation of China) under contract No.91434124 and No.51376105**



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