

# Performance investigations of a cycle- & mechanically-integrated parallel hybrid-electric turboshaft

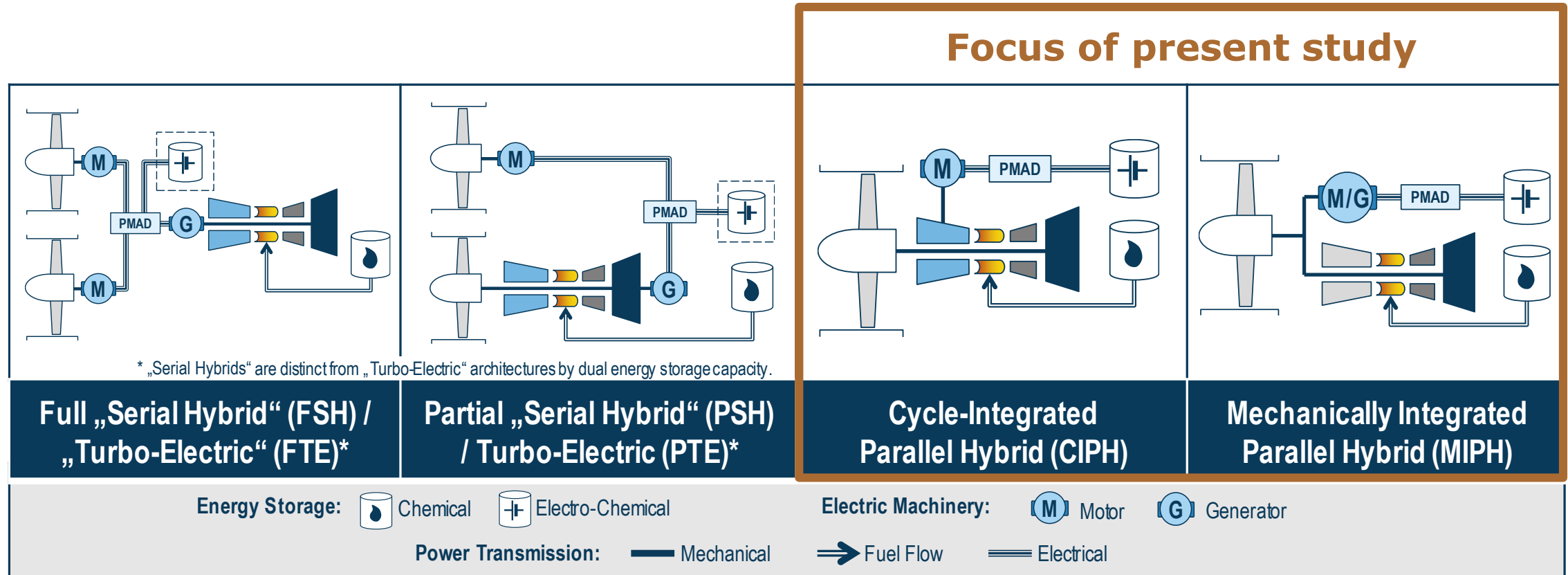
P. Maas, A. Seitz, D. Wirth, P. Geiger, M. Hornung

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# Basic Approaches to Hybrid Electric Propulsion



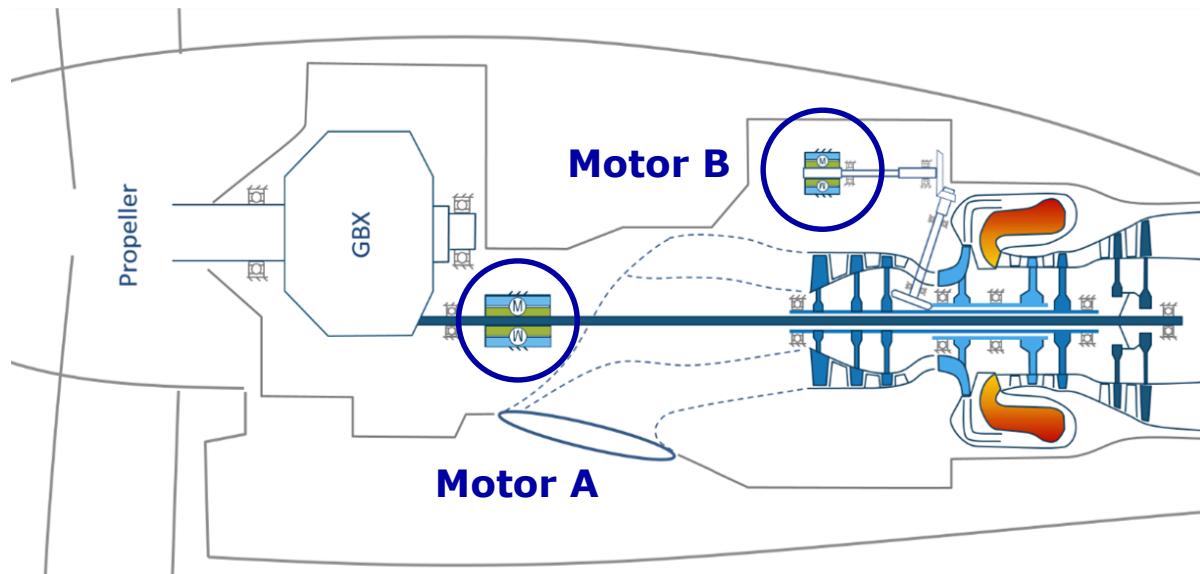
**Degree of power hybridization:**

$$H_P = \frac{P_{sup,el}}{P_{sup,tot}} = \frac{P_{Bat,prop}}{P_{Bat,prop} + P_{Fuel}}$$

Source: Seitz et al. (2018) Proc. IMechE Part G, Vol. 232(14) pp. 2688–27122018.

## ✦ Mechanically- & Cycle-Integrated Parallel Hybrid configuration

- ✦ 3-spool architecture with cycle-integrated system driving the high pressure (HP) spool
- ✦ Axial compressor driven by intermediate pressure (IP) spool, radial compressor driven by HP spool
- ✦ Use of towershaft for integration of cycle-integrated electrical machine
- ✦ Mechanically-integrated system driving the power turbine (PT) shaft

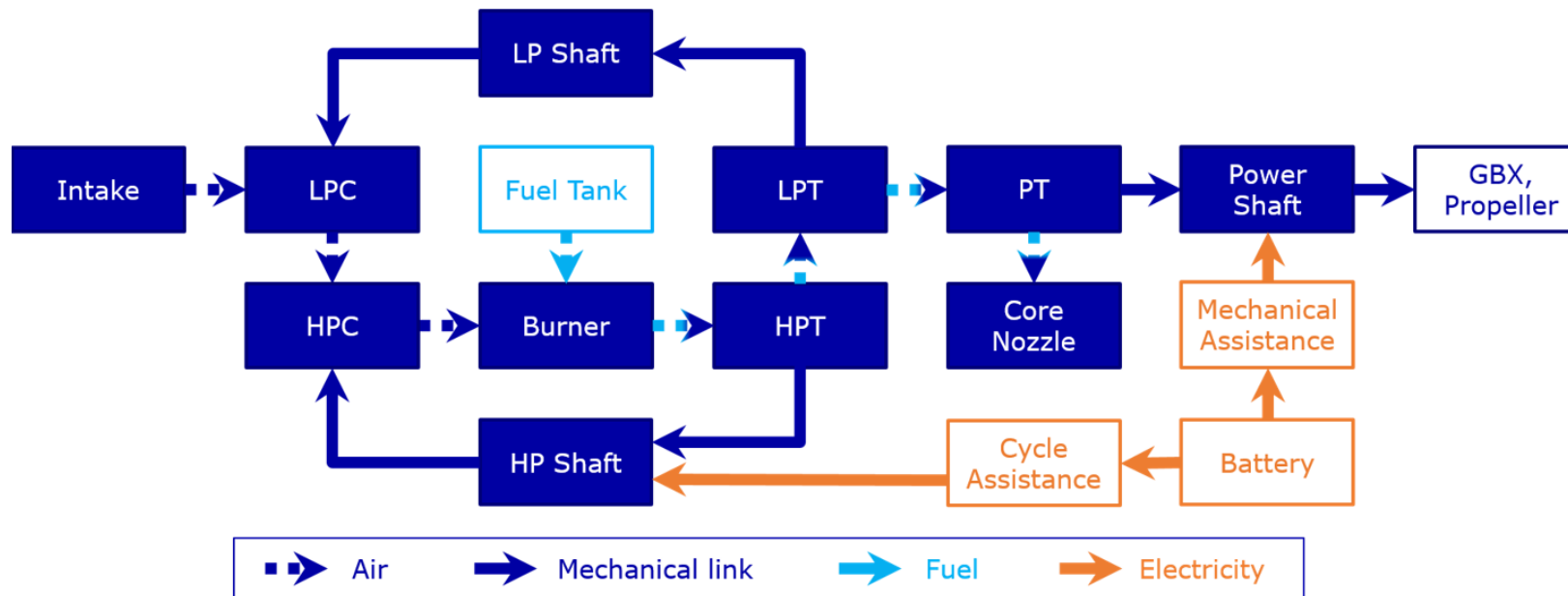


### Power split:

$$S_P = \frac{P_{MotorA}}{P_{MotorA} + P_{MotorB}}$$

Motor A: Mechanically-integrated assistance  
Motor B: Cycle-integrated assistance (turboshaft)

## ✈ Model Layout



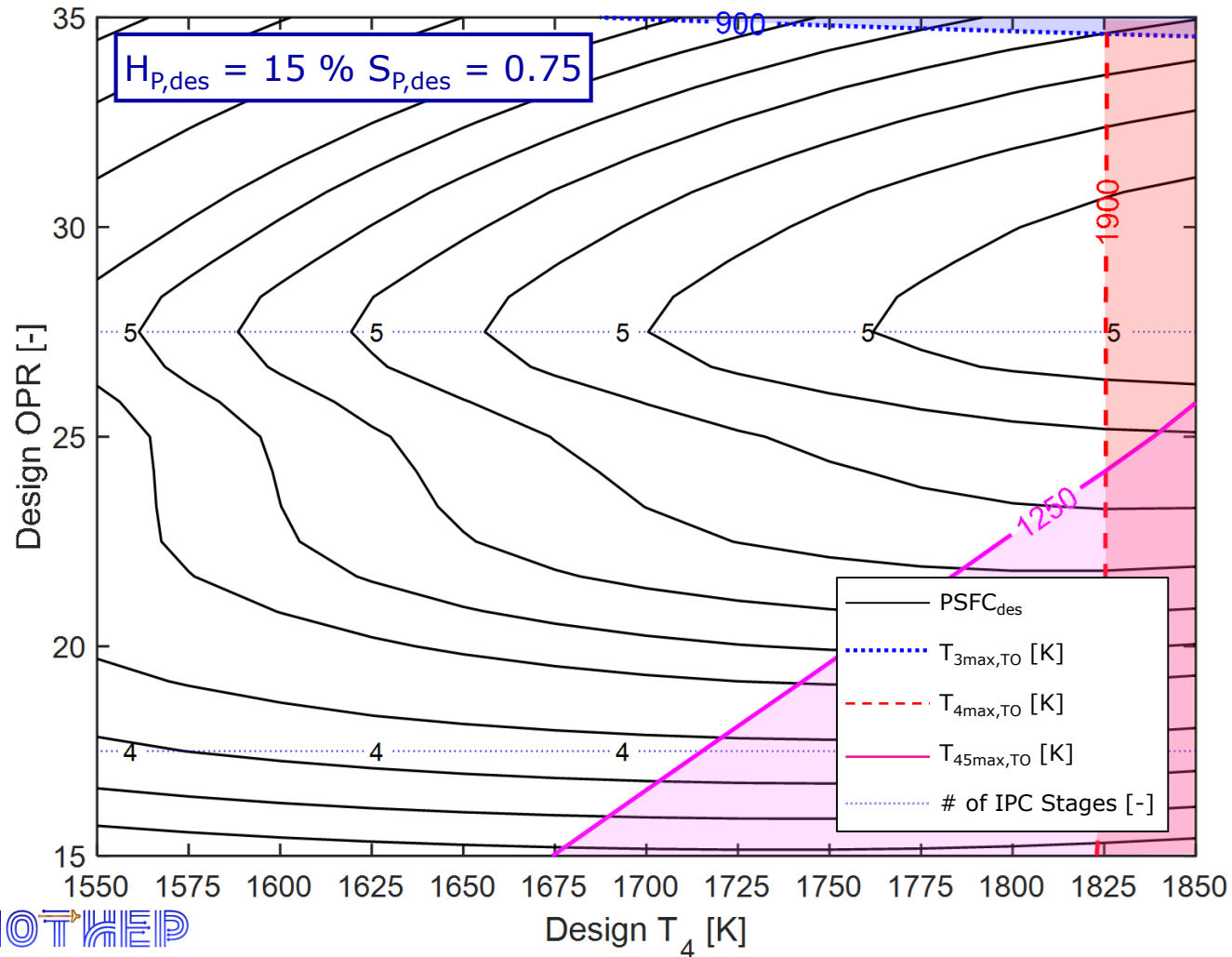
Note: only dark blue components are modelled as part of the present study

## ✈ Model Settings

- ✈ Use of BHL in-house framework «Aircraft Propulsion System Simulation» (APSS)
- ✈ Flow path sizing at TOC conditions (M0.4, FL150, ISA+10)
- ✈ Baseline turbo component efficiencies based on expert knowledge
- ✈ Typical geometric settings (hub-to-tip ratios, turbo component axial Mach numbers, circumferential speeds)
- ✈ BHL in-house flow path sizing laws & cooling air model

# Propulsion System Sizing Study

All electric motors operative (AMO),  $HP_{TO} = HP_{des}$

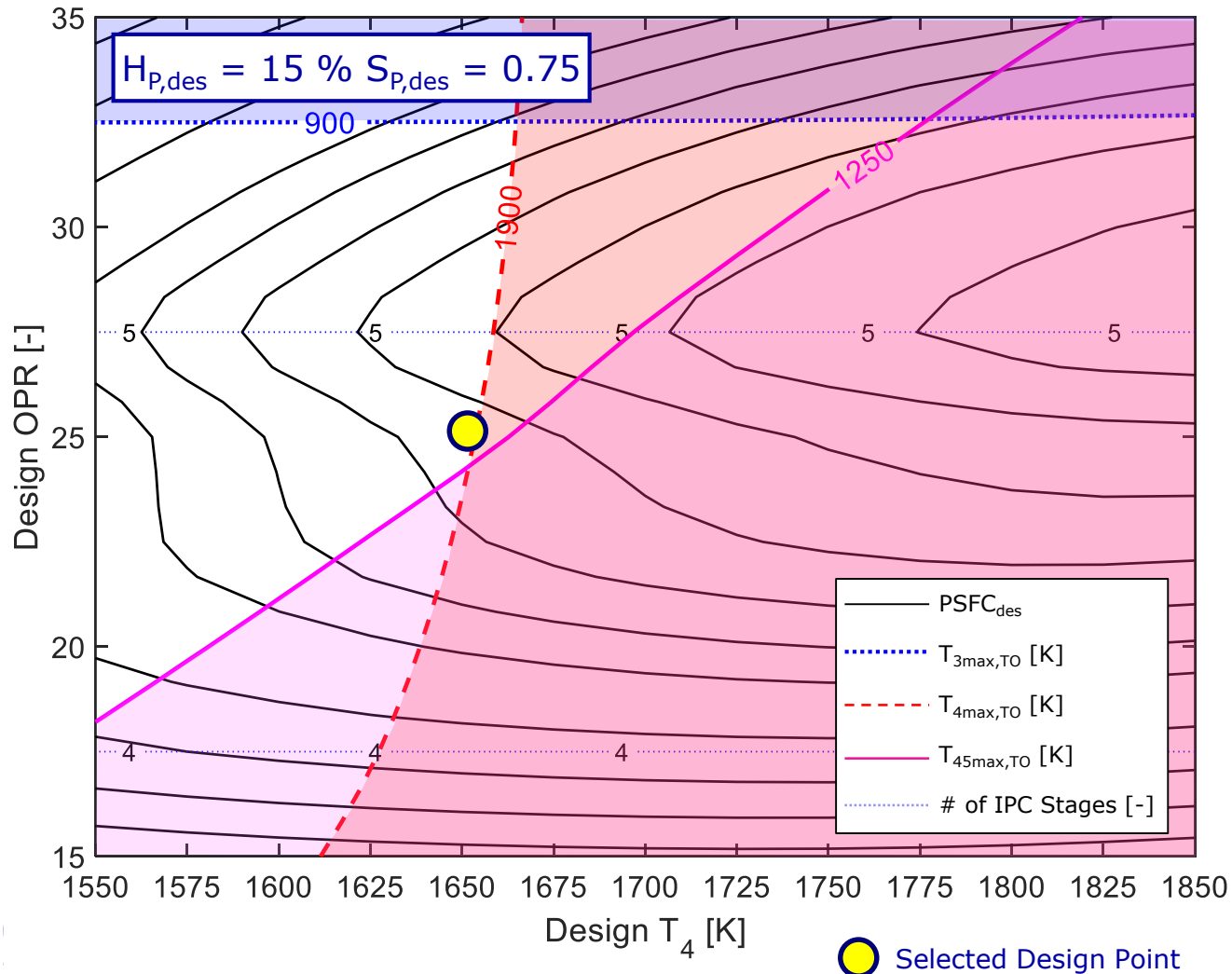


## ✦ Study Settings

- ✦ Multi-point sizing study
- ✦ Variation of design cycle parameters ( $OPR_{des}$  &  $T4_{des}$ )
- ✦ Flow path sizing at TOC conditions (M0.4, FL150, ISA+10)
- ✦ Take-Off rotation conditions (M0.17, SL, ISA)

# Propulsion System Sizing Study

All electric motors inoperative (AMI),  $HP_{TO} = 0$



## Study Settings

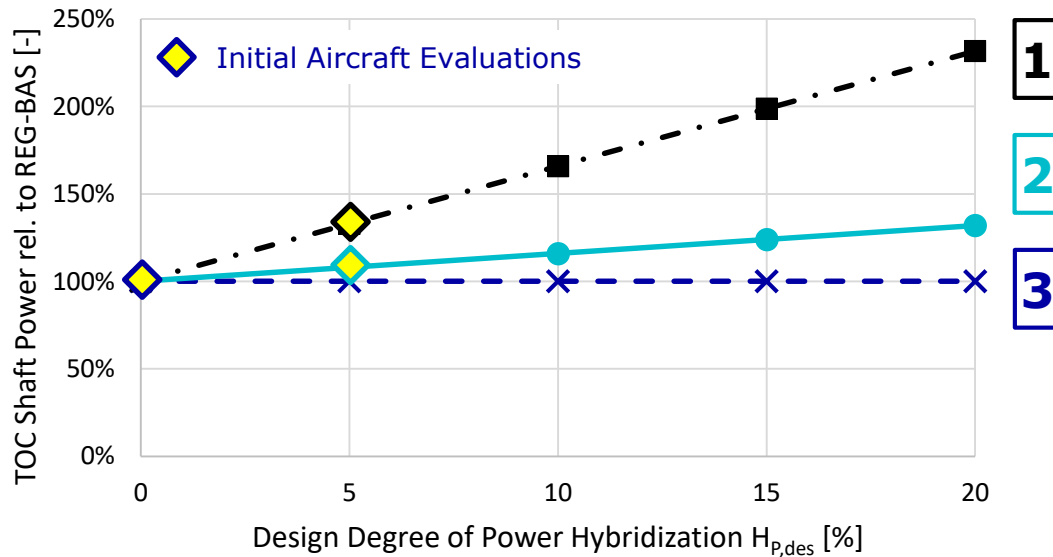
- Multi-point sizing study
- Variation of design cycle parameters ( $OPR_{des}$  &  $T_{4des}$ )
- Flow path sizing at TOC conditions (M0.4, FL150, ISA+10)
- Take-Off rotation conditions (M0.17, SL, ISA)

Propulsion system sizing depends on considered failure mode

Most critical cycle limitation during dual failure of electric motors



## 3 Engine Sizing Scenarios



- 1. Linear Extrapolation of initial REG-CON**  
incl. hybridization of holding & diversion
- 2. Linear Extrapolation of initial REG-CON**  
no hybridization of holding & diversion
- 3. Constant Shaft Power Demand**  
based on initial REG-BAS aircraft



**Analysis of Power-Specific Fuel Consumption PSFC vs. Design Hybridization**



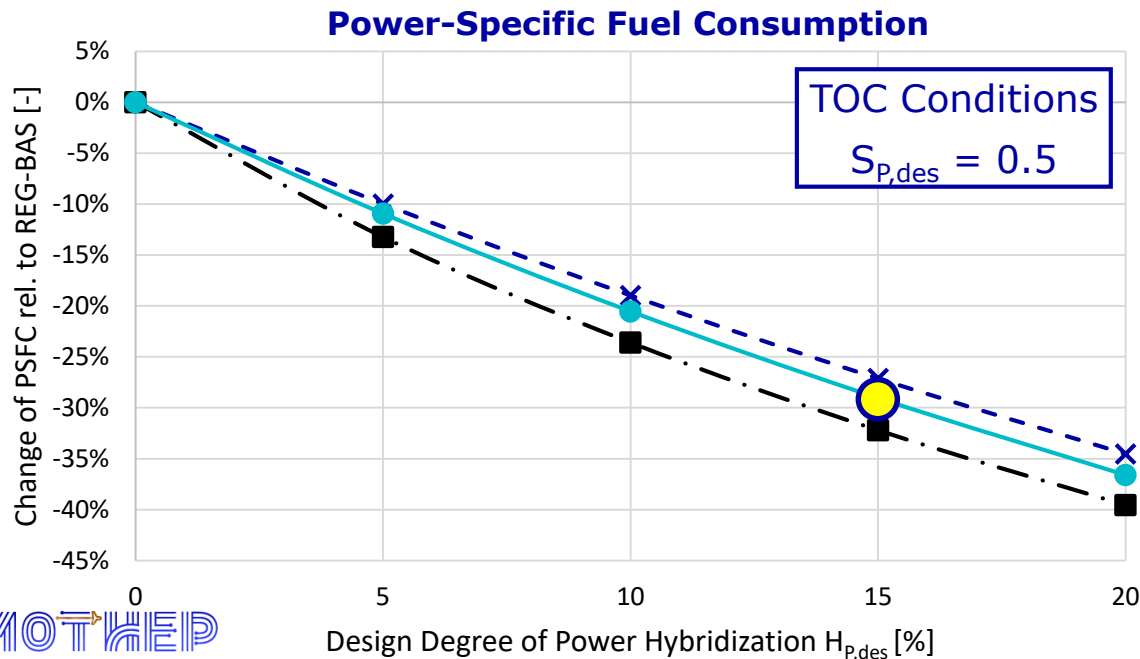
**Analysis of Fuel Flow vs. Design Hybridization**

# Design Hybridization Study (2/2)

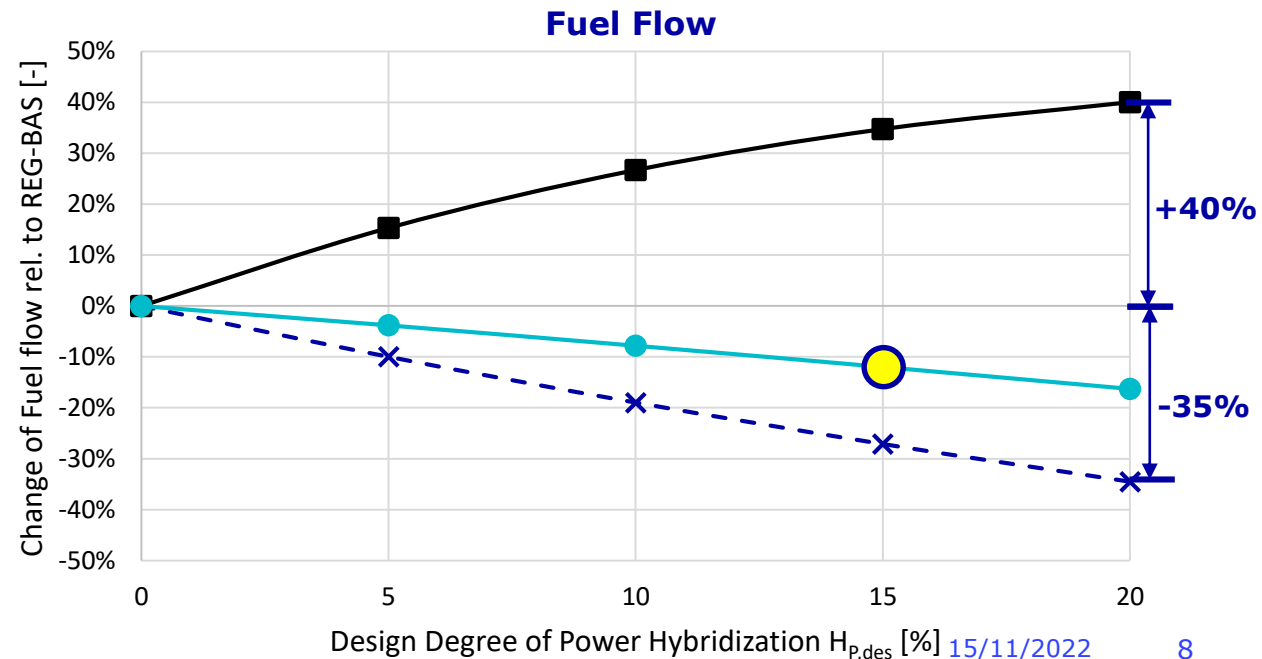


**Good match with overall aircraft level results**

● Habermann et al., *Study of a regional turboprop aircraft with hybrid-electric turboshaft assistance*, EASN Conference 2022



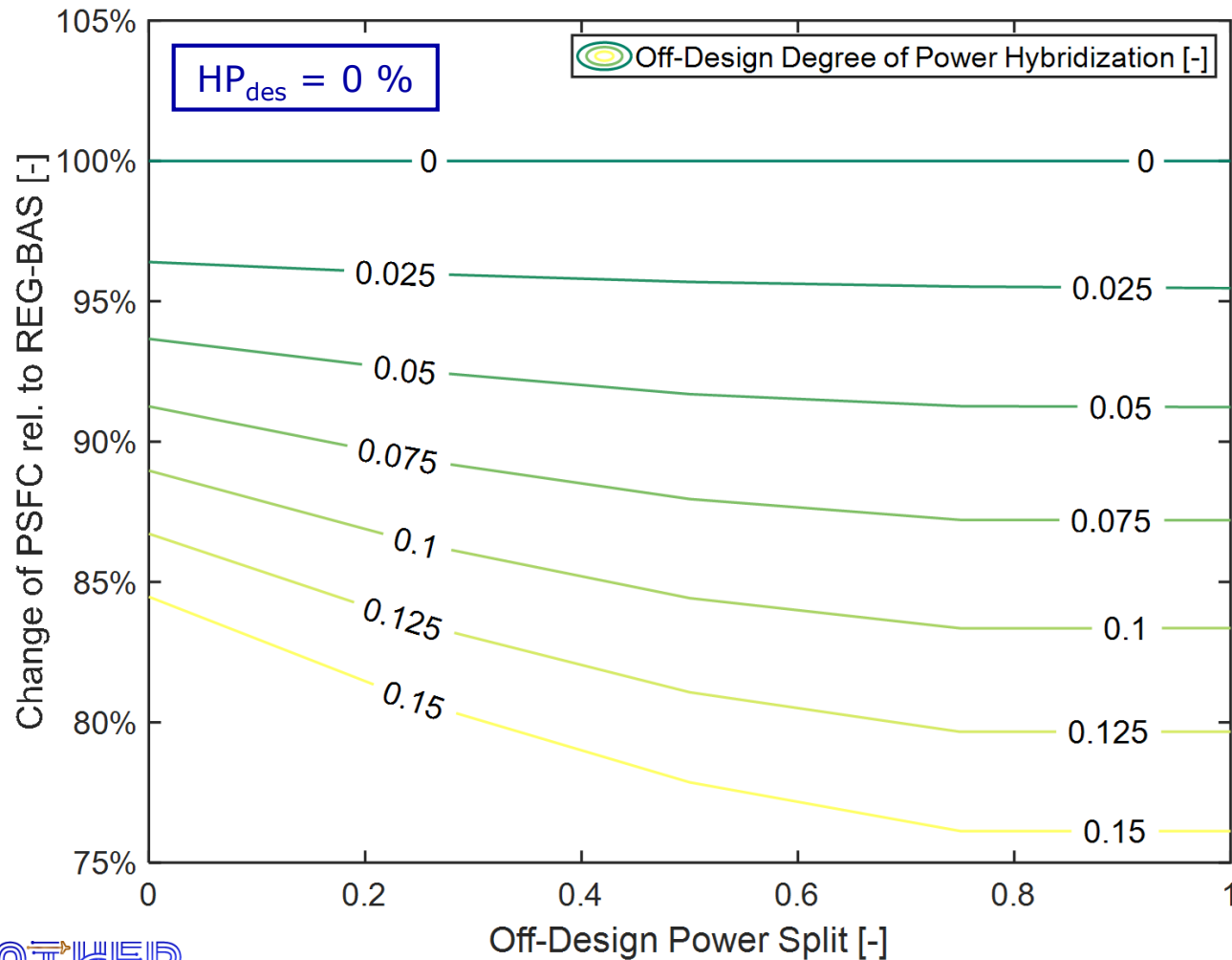
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- 3. Constant Shaft Power Demand**  
based on initial REG-BAS aircraft





# Off-Design Hybridization Study (1/2)

## Variation of Electrical Power Split



### Study Settings

- 0 % < H<sub>P,od</sub> < 15 %
- 0 < S<sub>P,od</sub> < 1
- TOC conditions (M0.4, FL150, ISA+10)
- P<sub>sh,od</sub> = P<sub>sh,des</sub>

For REG-BAS (H<sub>P,od</sub> = 0),  
electrical power split has  
no impact on PSFC

For H<sub>P,od</sub> > 0, usage of  
P<sub>MotorA</sub> (MIPH system) is  
more beneficial

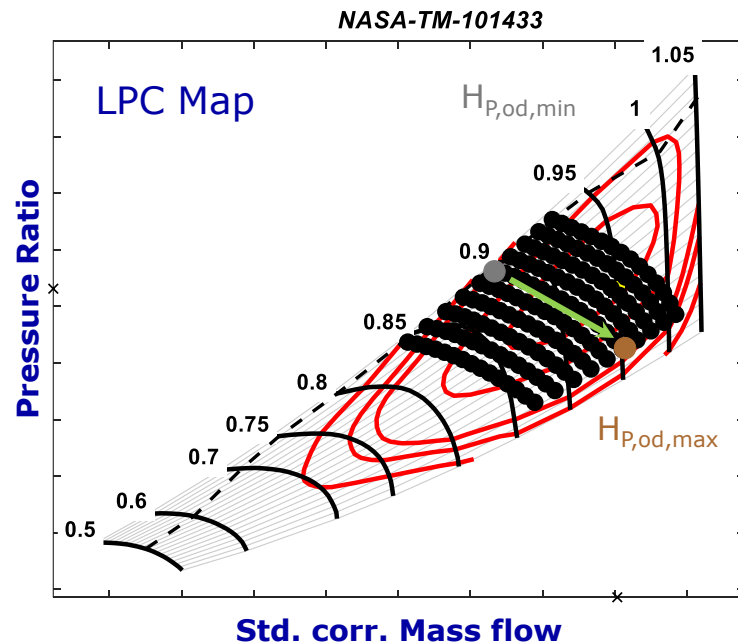
Power split:

$$S_P = \frac{P_{MotorA}}{P_{MotorA} + P_{MotorB}}$$

# Off-Design Hybridization Study (2/2)

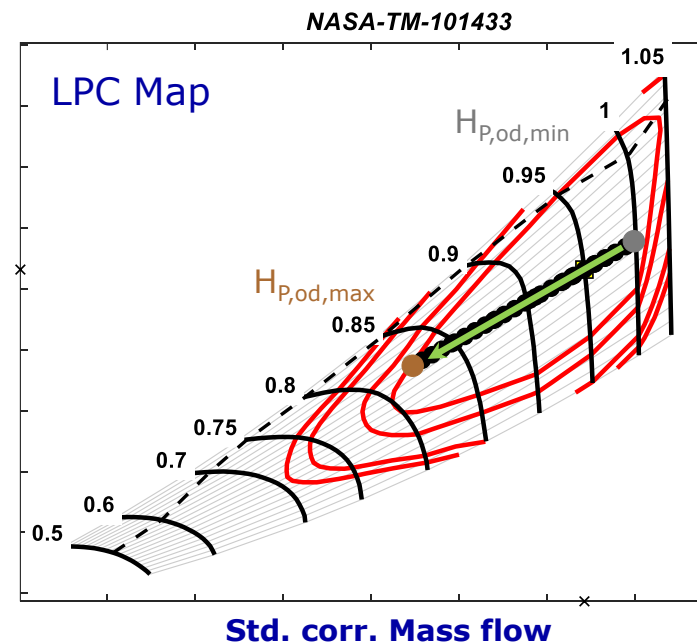
## ⊕ Cycle-Integrated Electrification

- ⊕  $S_{P,od} = 0.0$
- ⊕ LPC most critical turbo component



## ⊕ Mechanically-Integrated Electrification

- ⊕  $S_{P,od} = 1.0$
- ⊕ LPC most critical turbo component



## ⊕ Study Settings

- ⊕  $H_{P,des} = 10 \%$
- ⊕ TOC conditions (M0.4, FL150, ISA+10)
- ⊕  $P_{sh,od} = 50 - 100 \%$   $P_{sh,des}$

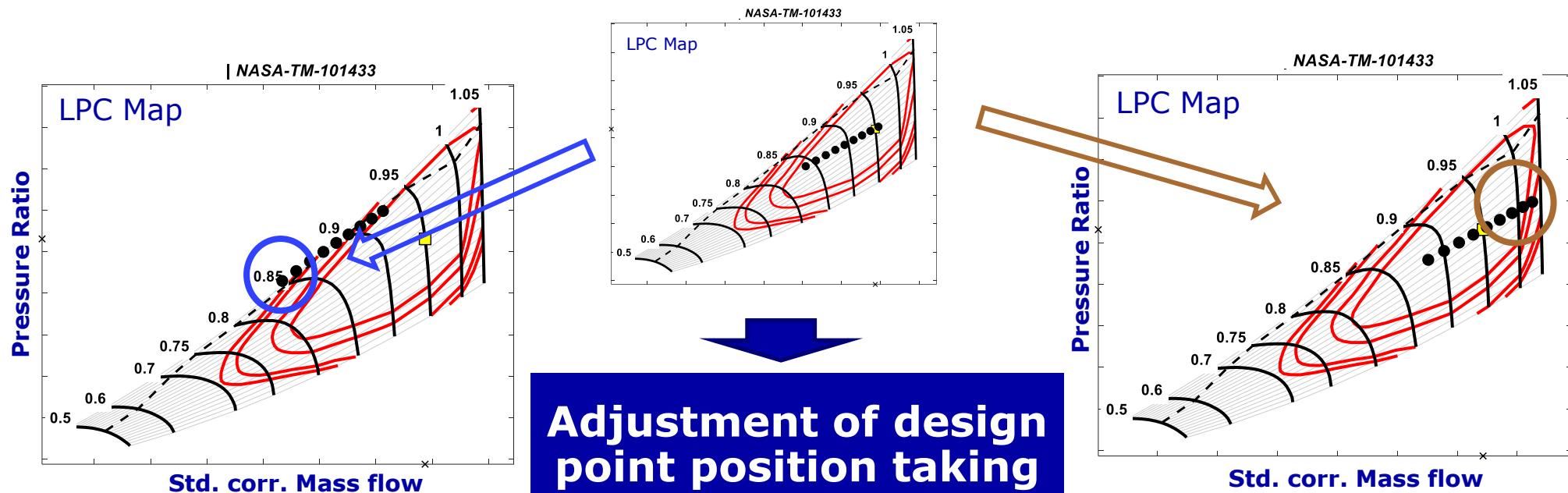
HP electrification  
limited by LPC  
choke/surge line

LP electrification  
limited by LPC spool  
speeds

# Impact of Electric System Failure

- ✦ **Loss of electric assistance to HP shaft leads to critical LPC surge margin values at low part-power points**

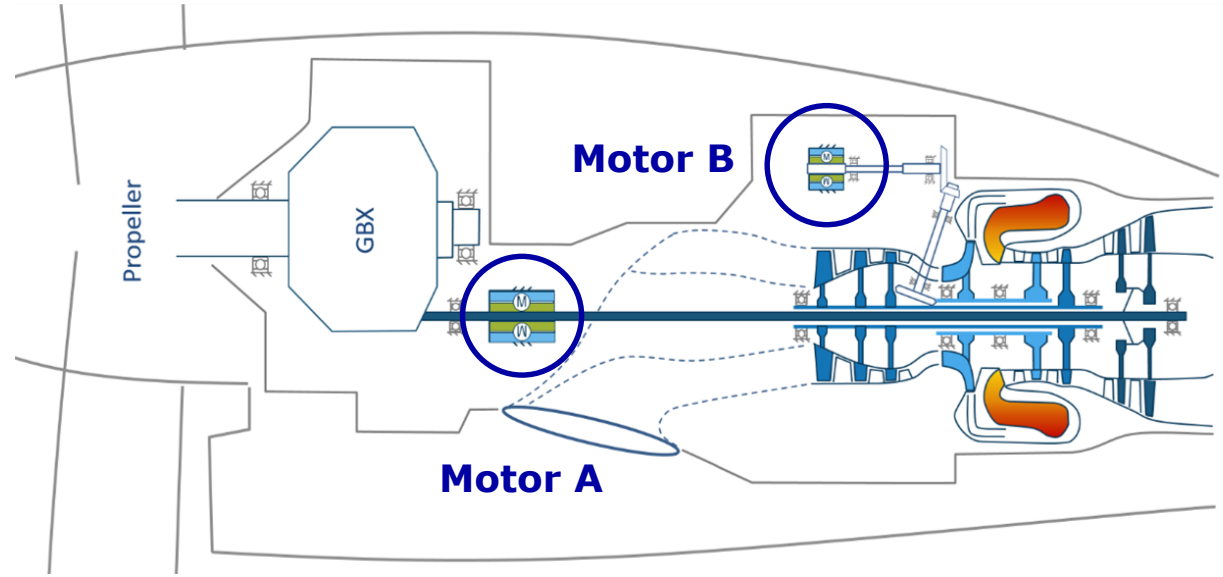
- ✦ **Loss of electric assistance to power shaft leads to critical LPC speed values (overspeeding) at high power points**



**Adjustment of design point position taking into account penalty in efficiency, size and weight**

# Conclusions

- ✦ **Parallel hybrid-electric propulsion can significantly improve efficiency on propulsion system level**
- ✦ **However, electric system failure needs to be considered during propulsion system sizing**
- ✦ **For high power degrees of hybridization, electric assistance to the power shaft (Motor A) is more relevant**



**Contact:**

**[Philipp.Maas@Bauhaus-Luftfahrt.net](mailto:Philipp.Maas@Bauhaus-Luftfahrt.net)**



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