

Evaluation of Fault Compartmentalization of “XAS” Reservoir, Onshore Niger Delta

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Abstract

The potential that the faults in the XAS reservoir might possibly result in compartmentalization was evaluated. The hypothesis is that unexpected compartmentalization issues due to false negatives and false positives, can infringe on earlier supply arrangement and can thwart production schemes and reserves that are booked from the field, booking of reserves is tight and highly regulated by government authorities. Data were obtained that consists well logs, 3D seismic volume for the XAS field. Petrel version 2014 was used for modelling, the structural model unravel that the reservoir has three faulted compartments. The petrophysical properties of the fault zone which comprised the fault zone permeability, the shale gouge ratio, the fault thickness were observed to fall short of the conditions for constraint of fluid flow across faults in the reservoirs. Thus, the faults are non-sealing but suggested to be barriers or/ baffles.

Keywords: compartmentalization, barriers, baffles, faults, reservoir, seals.

1.0 INTRODUCTION.

Faults play a significant role in the creation of hydrocarbon traps. The risks associated with fault-controlled prospects and production from faulted fields are appreciated by understanding the processes and contributing factors to the sealing of faults.

Reservoir compartmentalization is the segregation of hydrocarbon accumulations into individual fluid or pressure compartments; it has also been defined as the existence of petroleum accumulations in discrete individual compartments in the reservoir (Jolley et al., 2010). The basic seal types that can sustain compartmentalization are static and dynamic seals.

Static seals can prevent fluid flow over geological time frame while dynamic seals can prevent fluid flow during production time scale. Examples of dynamic seals are baffles and barriers (Jolley et al., 2010). Faulted compartmentalization has been one of the attributes that determine the plumbing and orientation of reservoirs (Ainsworth, 2006). The integrity of faulted compartmentalization has been attributed to the clay content of the faults, where Shale-Gouge ratio or Clay smear potential, or shale smear potential had been used as a tool for evaluating and ranking seals and had also been used as a proxy for clay content evaluation (Jolley et al., 2010). The sealing fault potential had been depended on the clay content or shale gouge ratio.

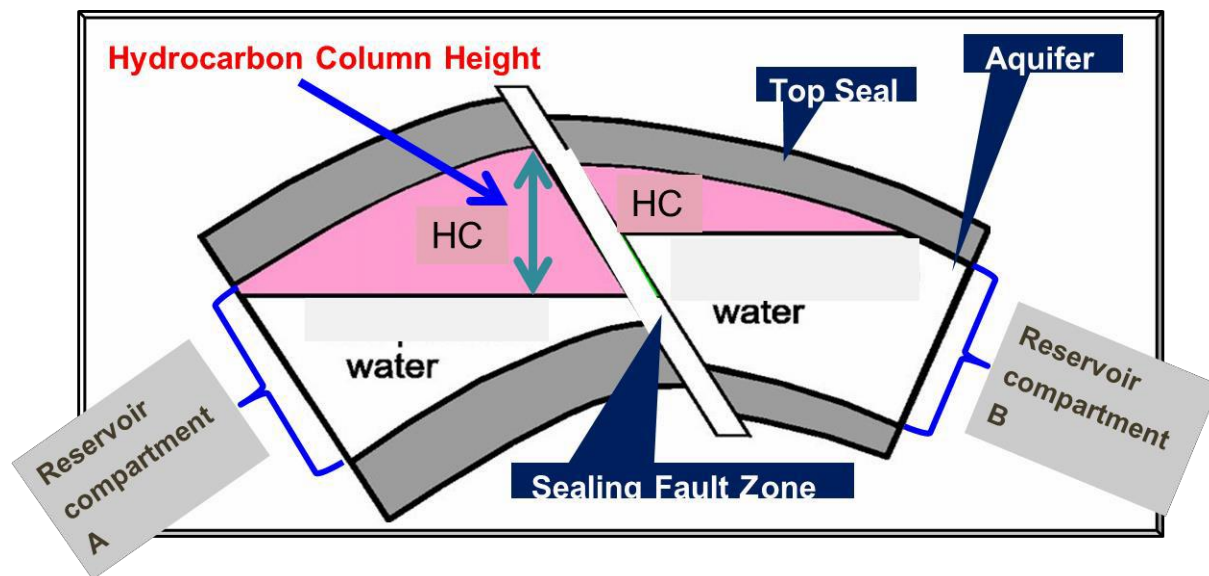


Figure 1: Diagram showing Hydrocarbon Column Height (Modified after Bretan *et al.*, 2003)

Weber *et al.* (1978) experimentally proved clay gouge to be an effective seal to water flow. It has been observed in open cast mines in an unconsolidated Tertiary deltaic sequence that the clay gouge zone gradually thins away from the clay source bed, the thickest clay gouges observed were about 0.5 m (Weber *et al.* 1978).

Lindsay *et al.* (1993) described outcrop studies of a Carboniferous fluvio-deltaic sequence shale smear, contrasting the description of Weber *et al.* (1978), unraveled, that the carboniferous rocks were lithified during faulting (burial depth about 2 km). Lindsay *et al.* (1993) then recognized three types of shale smear, namely: abrasion, shear, and injection.

- 1 Shear smears bear a strong resemblance to those described by Weber *et al.* (1978). The smears thicknesses decrease with distance from the source bed and reach a minimum in the central region between the terminations of the hanging-wall and footwall bed.
- 2 Abrasion smears, which are the commonest type in lithified sequences, comprise of a wafer-thin veneer that is abraded by a sandstone wall rock as it slips across shale beds. These smears tend to be thickest when they are made from thicker source layers and when the fault throw is relatively small. In larger throws, the shale veneer tends to be eroded.

- 3 Injection smears are a local response to volume changes during faulting. Injection smear thickness is not easily predictable.

The fault zone commonly contains a sheared mixture of the various wall rocks where a fault offset is greater than the bed thickness. Berg and Avery, (1995) stated that the capillary entry pressure or the permeability of the interface of this type of fault rocks could be two orders of magnitude greater than adjacent reservoir sands. Arch and Maltman, (1990) also stated that the alignment of clays in a shear zone introduces a strong directional permeability contrast. The likelihood of clay/shale smearing are controlled by the following factors:

- 1 Shear-type smears decrease in thickness with distance from the source layer,
- 2 Thick source beds can produce comparatively thicker clay smears,
- 3 Multiple source beds can give rise to a combined continuous smear. These relationships imply a possibility of a quantitative approach to clay smear prediction.
- 4 Abrasion-type smears decrease in thickness with increasing throw.

Watts (1987) stated that fault related seal can be grouped into two, which are the sealing faults and the juxtaposition faults. The mechanisms for sealing faults were stated as Clay smear, Cataclasis, (where grain crushing results in breakage and crushing during fault movement and reduces permeability within the fault zone due to fine grained gouge;) and Diagenetic healing, where preferential cementation along the original fault plane results in increase of capillary entry pressure and low permeability interface.

Bouvier *et al.* (1989) studied the Niger Delta Nun River field. They described a clay smear potential (CSP) as a means of estimating the likelihood of clay smearing in areas of sand-on-sand juxtaposition on faults. The clay smear potential represents the relative amount of clay that has been smeared from individual shale source beds at certain points along a fault plane.

It should be noted that none of the attributes described is entirely a measure of sealing capacity of the fault surface. They should rather be seen as estimates of the relative likelihood of clay smear being developed on the fault surface. However, Onyeagoro *et al.*, (2001) and Yielding *et al.*, (2010) set conditions needed for hydrocarbon fluid flow across faults as:

1. Shale Gouge Ratio (SGR) must be less than 30 %.
2. Fault thickness range must be 2-20 ft.
3. Reservoir permeability (K) ~ 1000 mD.
4. Fault zone permeability (k) greater than 1 mD.

These conditions are being applied in evaluating the integrity of fault seal in this study.

The hypothesis of this study is based on the fact that operators and investors need to be informed and also equipped with the ability to estimate and identify compartmentalized areas and areas likely to become compartmentalized within the reservoir, during production due to high potential for false negatives (compartments assumed absent due to homogeneous fluid properties, when in fact, fluids would have equilibrated even in the presence of compartments), false positives (where fluid differences are interpreted as evidence of compartments, when in fact, there has not been sufficient time for equilibration to occur). Unexpected compartmentalization issues can infringe on earlier arrangement and can thwart production schemes and reserves that are booked

from the field, booking of reserves is tight and highly regulated by government authorities as aspect of future markets.

The objectives of the study include, effectively mapping and defining the reservoir structural top (i.e., to identify the reservoir structure and the significant faults running through it); build a fit-for- purpose static model of the reservoir to define its petrophysical attributes and perform fault analysis on relevant intra-reservoir faults to determine the possibility of hydrocarbon fluid flow across these faults.

2.0 LOCATION OF STUDY AREA

‘XAS’ reservoir is one of the numerous reservoirs located in the Central Swamp Depobelt of the wave and tide-dominated Niger Delta basin in the Gulf of Guinea. The field was discovered in 1961. It lies in the seasonally flooded freshwater swamp area, some 110 Km west of Port Harcourt. The target reservoir is an oil and gas bearing reservoir with 5 wells penetration available. All the wells are concentrated at the eastern region of the reservoir.

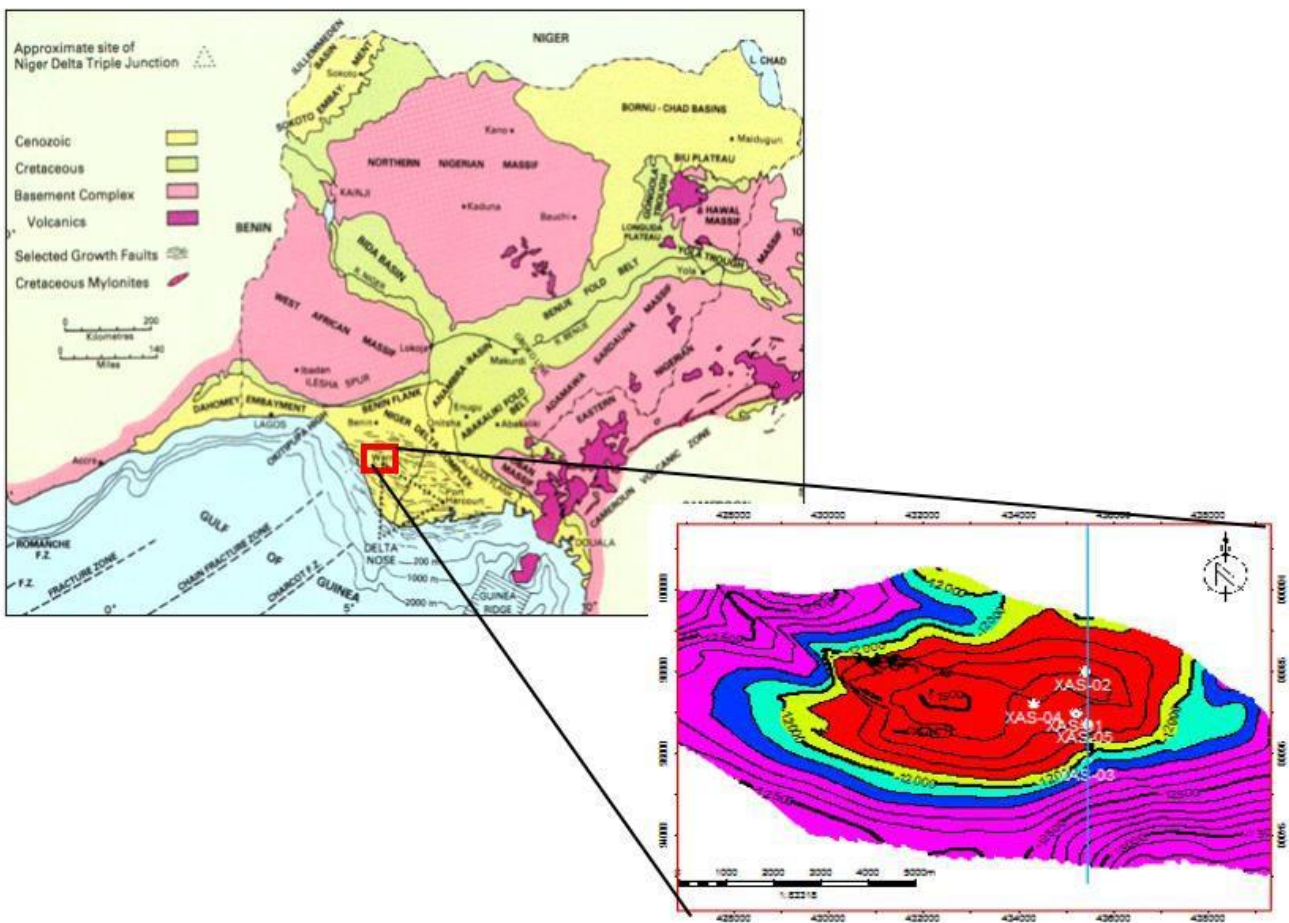


Figure 1a. Nigerian map showing area of study and model seismic cross section

3.0 MATERIALS AND METHODS.

3.1 Available Data.

3D seismic volume (Depth) - Good quality and continuity
 Gas and Oil Water Contacts -11660 ft and -11918 ft
 Well Logs over reservoir section.

Table 1: Summary of wells logs available for the study.

LOG	XAS-01	XAS-02	XAS-03	XAS-04	XAS-05
GR	V	V	V	V	V
Resistivity	V	V	V	V	V
Density	X	X	X	X	V
Neutron	X	X	X	X	V
NTG	V	V	V	V	V
permeability	X	X	X	X	V
Porosity	X	X	X	X	V
V	Available				
X	Not available				

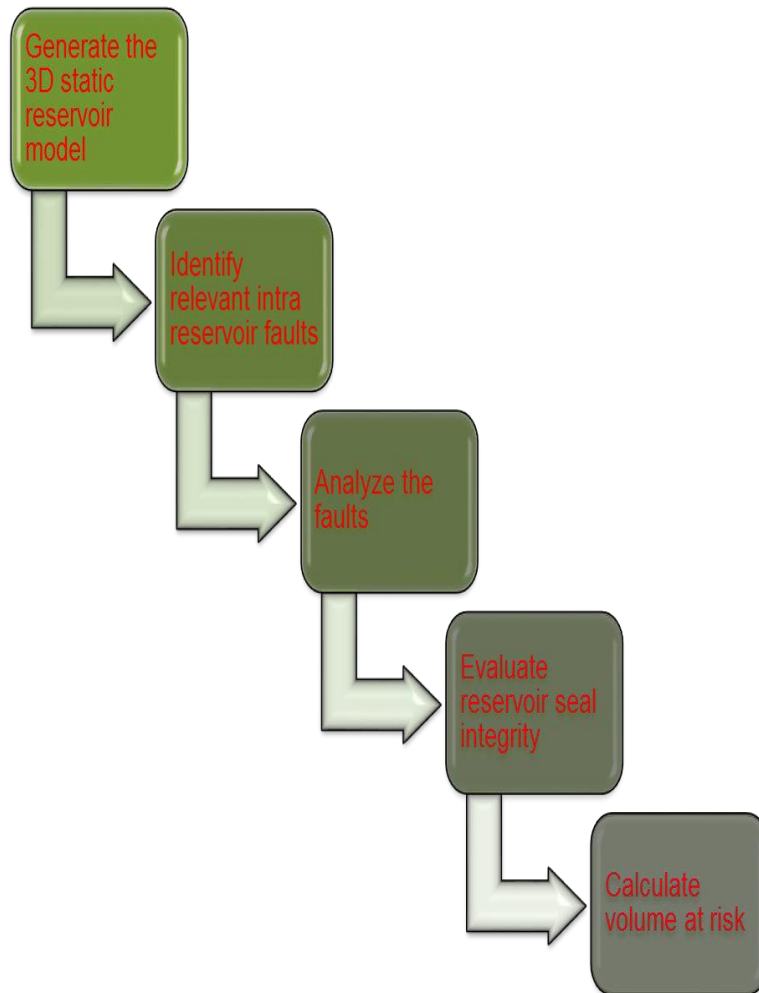


Figure 2: Work flow Chart on data treatment.

4.0 RESULTS AND DISCUSSIONS

4.1 Seismic Interpretations.

30 faults were interpreted. Tops of two reservoirs: XAS Top and T3 reservoir beneath it for stratigraphic control. The structure of the reservoir is anticlinal. Faulting is generally along strike (figures 3a and 3b).

4.2 Structural Model.

29 faults out of 30 interpreted faults were relevant faults for the model, with 12 faults defined to likely impede or act as baffles to fluid flow. Faults F3 and a connecting F8 (figure 3a) segmenting the reservoir into a Northern and Southern accumulations (A, and B), respectively as portrayed in figure 3b. While faults 48, 26, 23, 5, and 28 could further separate the northern accumulation into A1 and A2, (figure 3a).

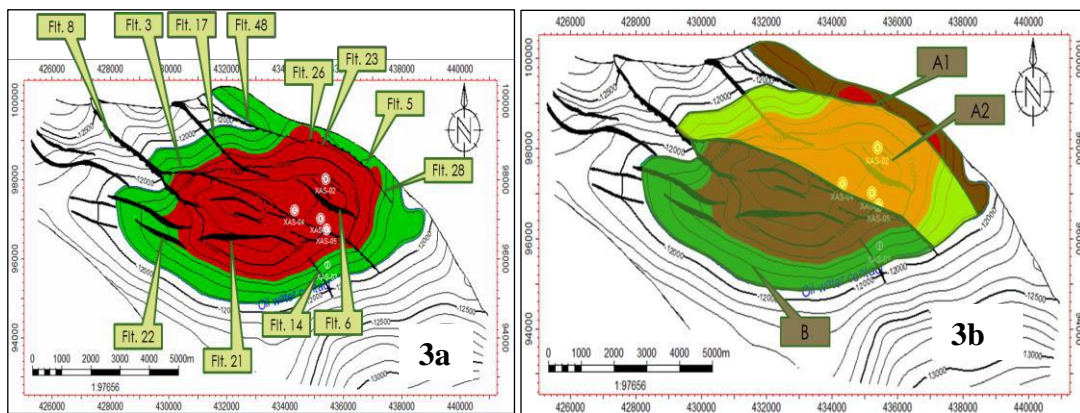


Figure. 3 (a and b): Modelled reservoir faults and the hydrocarbon accumulations and segmentation of the XAS reservoir.

4.3 Reservoir Well Correlations.

The XAS reservoir correlations was achieved using the suites of logs available from all the wells penetrating the reservoir. Correlation panels across the reservoir of the field which is based on GR log signatures was generated, showing detailed reservoir subdivisions as in figures 4 and 4a. Reservoir wide dip section correlation of XAS top and base and T3 top (for stratigraphic control) figure 4a shows that sand quality degrades as portrayed in figure 4 left to right (North to South). This is due to deposition of finer materials basin wards of the reservoir.

4.4 Flow Units and Facies Interpretation.

Five interpreted distinguishable genetic units were identified (channel, lower shoreface, upper shoreface, heterolith and shale) as in figure 4a, with dominant facies units consist of good quality upper shoreface and channel sandstone reservoir units.

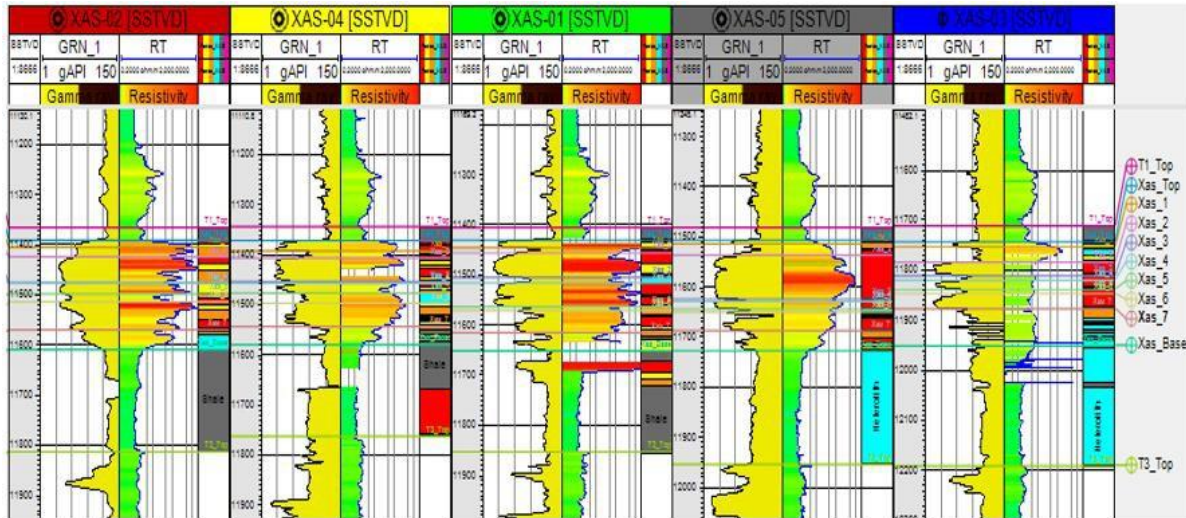


Figure. 4: Correlation panel showing reservoir section showing interpreted facies and flow units.

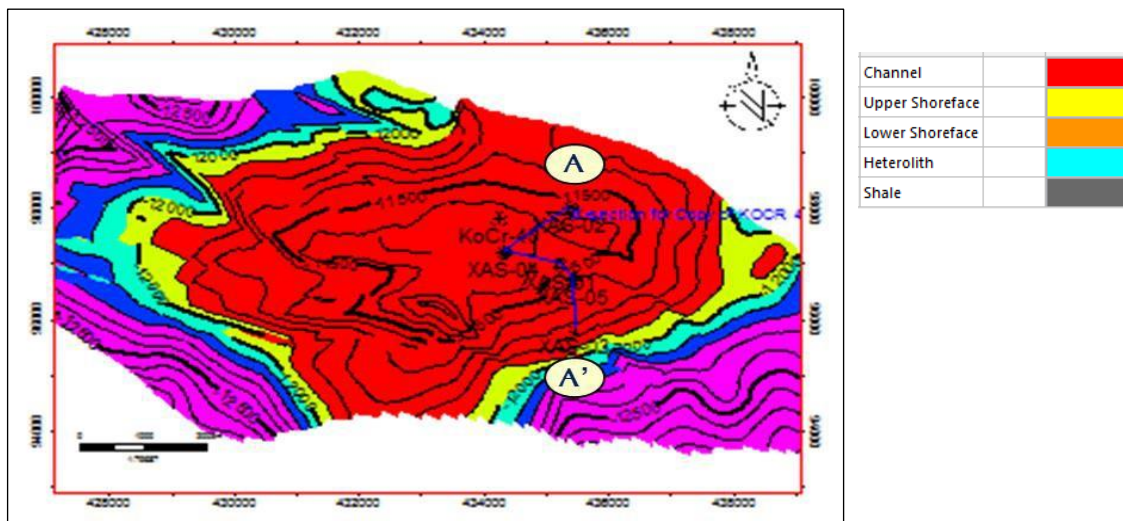


Figure 4a. 2D Reservoir section showing interpreted facies and flow units.

4.5 3D Facies and Petrophysical modelling

The variogram settings for the facies modelling are based on Niger Delta facies description. Channel and Shoreface facies are dominant. Shoreface facies are extensive East–West, while the channels cut through the Shoreface in the North–South direction. Petrophysical models were biased to the facies model.

The conditions considered by Onyeagoro *et al.*, (2001) and Yielding *et al.*, (2010) is being used to assess the potential for hydrocarbon fluid flow across faults.

These considerations are:

1. Shale Gouge Ratio (SGR), must be < 30 %.
2. Fault thickness range must be 2-20 ft.
3. Reservoir permeability (K) ~ 1000 mD
4. Fault zone permeability (k) > 1 mD

Juxtaposition analysis shows that Central faults have large juxtapositions while boundary faults have no juxtaposition, and the juxtaposition of interest are those above the oil water contact - 11918 ft (figure 5).

4.6 Fault Thickness

Fault thickness range for juxtaposed areas from the model ranges from 2.5 ft. to about 4 ft, and it corroborates with Onyeagoro *et al.*, (2001) and Yielding *et al.*, (2010) and such will permit hydrocarbon fluid flow across the faults (figure 6)

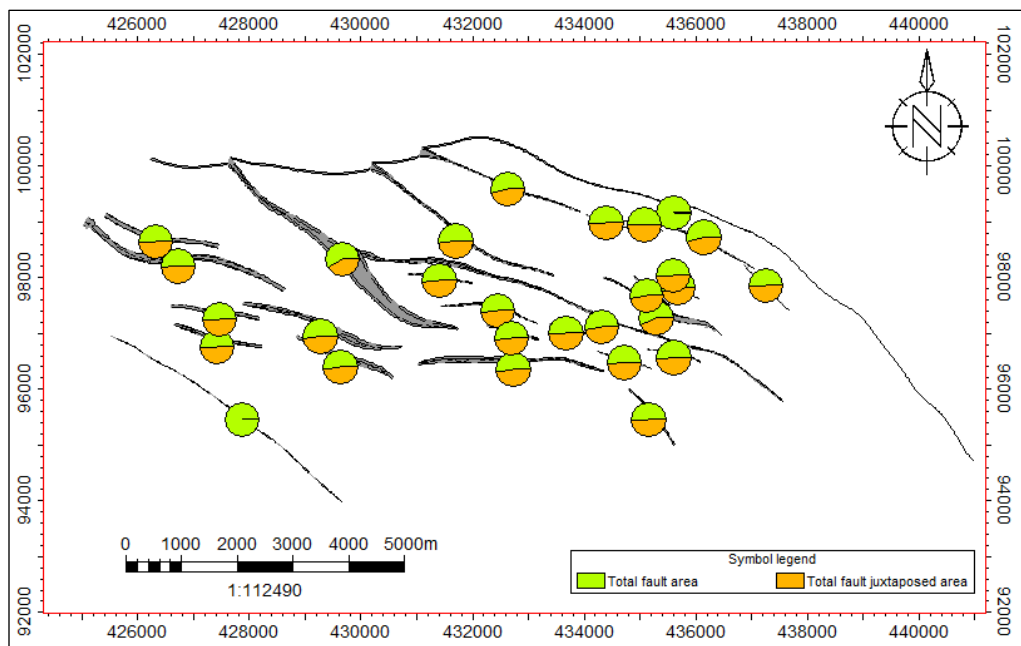


Figure. 5: Ratio of fault juxtaposition of the faults.

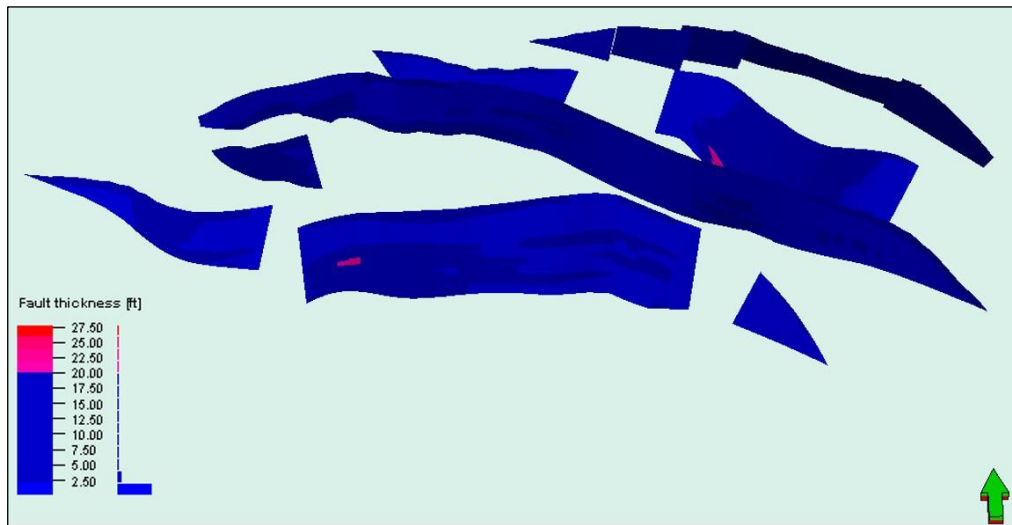


Figure.6: Fault thickness analysis results showing the fault thickness for various faults.

4.7 Shale Gouge Ratio

Shale gouge ratio for juxtaposed areas of faults that will allow hydrocarbon fluid flow across the faults ranges of 10% to 25 %. Parts of the area with SGR above 30 % is circled in black (figure 7). These areas can constraint hydrocarbon fluid flow and may serve as barriers or seals.

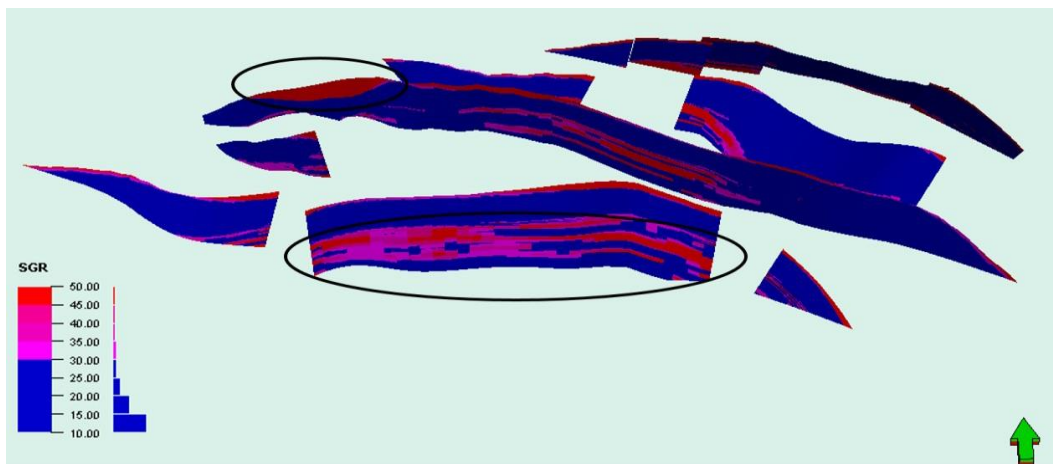


Figure 7: Faults SGR analysis results of the relevant faults.

4.8 Permeability

Fault permeability for juxtaposed areas from the model, show that greater portion of the faults will permit hydrocarbon fluid flow across the faults, since they have fault zone permeability greater than 1mD as in figure 8

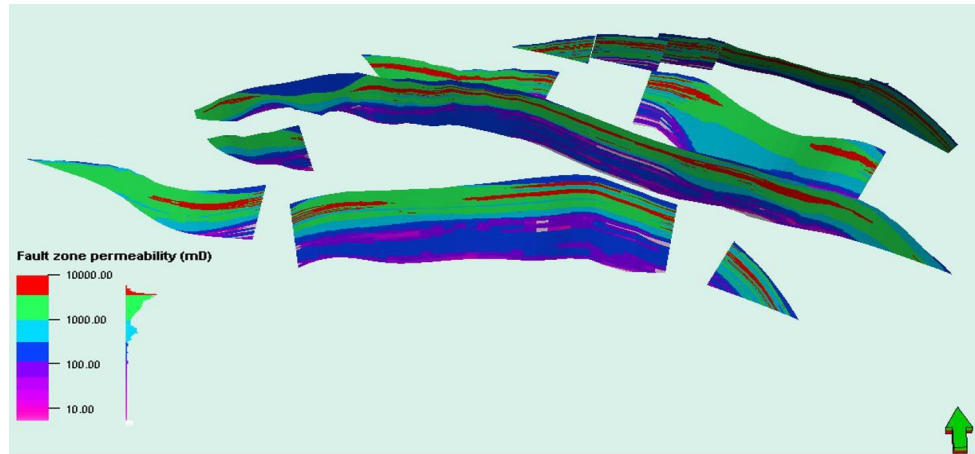


Figure 8: Fault permeability analysis results.

5.0 CONCLUSIONS

The 3D model shows the facies distribution across the XAS reservoir interval.

The model showed 3 (three) major compartments A1, A2 and B. the A1 compartment is the only accumulation without a well.

The fault juxtaposition analysis showed the area of the faults of interest that are juxtaposed above the OWC.

The SGR, fault thickness, and fault zone permeability for the juxtaposed areas bear greater values than the threshold considerations used for delineating faults zone that will constraint fluid flow, thus the faults may not compartmentalize the reservoir into pressure compartments, they may serve as or barriers or baffles to fluid flow across the faults.

The knowledge obtained from this study can be used to optimized well placement and will serve as considerations for efficient production.

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