# Benchmark: Axisymmetric liquid droplets on viscoelastic substrates

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## **Abstract**

We report on the data from a numerical benchmark of a stationary axisymmetric droplet on viscoelastic Neo-Hookean substrates obtained using FEniCS [\[3\]](#page-4-0). Numerical results using our Lagrangian phase-field approach [\[4\]](#page-4-1) are compared with results by Van Brummelen et al.  $[6]$  and by Aland & Mokbel  $[2]$ .

### **1 Problem description**



Figure 1: Sketch of axisymmetric droplet on viscoelastic substrate

We derived in [\[4\]](#page-4-1) that the corresponding model of Neo-Hookean viscoelastic droplet relaxation can be written as a gradient flow, which we formulate in terms of a weak formulation, where we seek  $q$ :  $[0, T] \rightarrow \mathscr{Q}$  such that

$$
s(\partial_t q, v) = -\langle \mathcal{D}\mathcal{L}(q), v \rangle, \tag{1}
$$

for all  $v$  from suitable spaces  $\mathscr{Q}$ . The state variable  $q$  contains displacements  $u$  and possible multiplier  $\lambda$ . The Lagrangian  $\mathscr L$  defined in [\(2\)](#page-1-0) is the sum of a free energy and possible incompressibility constraints using the deformation gradient  $F = \mathbb{I} + \nabla u$ . The bilinear form s is the Stokesian dissipation defined in [\(3\)](#page-1-1). The liquid, solid and gas phase are encoded using *phase indicator* fields  $\varphi_i : \Omega \to \mathbb{R}$  with  $0 \leq \varphi_i \leq 1$ and  $\sum_{i=1}^{3} \varphi_i(x) = 1$  for every  $x \in \Omega$ .

For this specific benchmark problem the phase indicators  $\varphi_i$  do not evolve in time, which for the continuous displacement field u corresponds to a no-slip boundary condition (continuous displacements and velocities) at the interface. The phase indicators are chosen so that the solid reference  $\varphi_1$  has a flat interface at  $z = h$  with the liquid and with the gas phase. The entire computational domain itself is

$$
\Omega = \{ (r, z) \in \mathbb{R}^2 : 0 < z, r < L \}.
$$

Note that parts of the energy are written in terms of  $-1 \leq \psi_i = 2\varphi_i - 1 \leq 1$ . We use the spaces  $u \in$  $U = H_0^1(\Omega)$  and  $\lambda \in \Lambda = L^2(\Omega)$  for displacement and multiplier, where the displacements vanish at  $z =$ 0 and  $z = H$  and the horizontal component of the

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<span id="page-1-2"></span>Figure 2: Locally refined undeformed mesh (white lines) of phase fields (color shading) at the interfaces showing substrate (blue), fluid (green) and gas (red).

displacements vanishes at  $r = 0$  and  $r = L$ . The For the viscous dissipation we use a (Lagrangian) Lagrangian is has elastic, surface and compressibility Kelvin-Voigt Stokesian dissipation contributions, where

$$
\mathcal{L}(q) = \int_{\Omega} (E_{\text{elast}} + E_{\text{phase}} + E_{\text{comp}}) \, \mathrm{d}V \qquad (2)
$$
  
\n
$$
E_{\text{elast}} = \frac{G(\varphi_i)}{2} \operatorname{tr}(F^T F - \mathbb{I})
$$
  
\n
$$
E_{\text{surf}} = \sum_{i=1}^3 \frac{3\sigma_i}{2\sqrt{2}} \left[ \frac{\varepsilon}{2} |F^{-T} \nabla \psi_i|^2 + \frac{1}{4\varepsilon} (\psi_i^2 - 1)^2 \right] J
$$
  
\n
$$
E_{\text{comp}} = \begin{cases} \lambda(J-1) & \text{incompressible} \\ \kappa(J-1)^2 & \text{compressible} \end{cases}
$$

with volume element  $dV = 2\pi r dr dz$  and  $J = det F$ . Note that for incompressible materials the second term in  $E_{\text{surf}}$  vanishes upon differentiation w.r.t u. For compressible solids the elastic energy  $E_{\text{elast}}$  contains a term  $-\log(J)$ , which we neglect since we are interested in the limit  $\kappa \to \infty$ . In the compressible case  $q = u \in U = \mathcal{Q}$  with large penalization constant  $\kappa \in \mathbb{R}$  and in the incompressible case  $q = (u, \lambda) \in U \times \Lambda = \mathscr{Q}$  with Lagrange multiplier  $\lambda$ . The axisymmetric deformation gradient and scalar gradient that appear above are

$$
\nabla u = \begin{pmatrix} \partial_r u_r & 0 & \partial_z u_r \\ 0 & \frac{1}{r} u_r & 0 \\ \partial_r u_z & 0 & \partial_z u_z \end{pmatrix}, \quad \nabla \psi = \begin{pmatrix} \partial_r \psi \\ 0 \\ \partial_z \psi \end{pmatrix}.
$$

The elastic modulus is defined as the linear combination  $G(\varphi_i)(x) = \sum_{i=1}^3 G_i \varphi_i(x)$  with constant  $G_i \ge 0$ . Fig. [2](#page-1-2) to resolve the interface thickness  $\varepsilon = 1/800$ .

<span id="page-1-1"></span>
$$
s(w, v) = \int_{\Omega} \mu \nabla w : \nabla v \, dV, \tag{3}
$$

<span id="page-1-0"></span>which is sufficient, since we are only interested in energy minimizers. We denote  $A : B = \sum_{ij} A_{ij} B_{ij}$ the Frobenius inner product between matrices  $A, B \in$  $\mathbb{R}^{d \times d}$ . In principle, one would have to use a Eulerian Kelvin-Voigt rheology with the viscosity  $\mu = \mu(\varphi_i)$ and  $\nabla w : \nabla v \to \text{sym}(\nabla w F^{-1}) : \text{sym}(\nabla v F^{-1})J$  with  $\text{sym } A = \frac{1}{2}(A + A^T)$  to be more realistic but should end up with the same energy minimizers (assuming uniqueness).

In the following we shortly elaborate on the used finite element space and time discretization. For this we are going to present result from an incompressible and a compressible model, where for the incompressible model we discretize the problem using  $P_1/P_1$  elements for displacement and multiplier und for the compressible model we discretize the problem using  $P_2$  elements to avoid locking phenomena common for nearly incompressible problems. After discretization in space we solve the fully implicit problem

$$
s(q^{n}-q^{n-1}/\tau, v) = -\langle \mathcal{D}\mathcal{L}(q^{n}), v \rangle,
$$

which guarantees descent of the free energy, see [\[4\]](#page-4-1). At the interfaces set by the indicator functions  $\varphi_i$ we perform local refinement of the mesh as shown in



<span id="page-2-0"></span>Figure 3: Stationary axisymmetric droplet (blue) on viscoelastic Neo-Hookean substrate (gray), where darker shading indicates larger energy density  $E_{\text{elast}}$ . Grid visualizes displacement of uniform planar substrate.



<span id="page-2-1"></span>Figure 4: Stationary droplet for the axisymmetric domain  $\Omega = [0, 10] \times [0, 10]$  showing (top left) phase fields combined into  $\varphi = \sum_{i=1}^{3} i\varphi_i(x)$  and (botton left) elastic energy density  $E_{\text{elast}}$  in the solid substrate (blue=low, red=high) and (right column) corresponding quantities near the contact line. In lines in the lower left image highlight the displacement, while all other lines (black or white) show the mesh.



<span id="page-3-0"></span>Figure 5: Benchmark comparison of experiments by Style et al. [\[5\]](#page-4-4) in comparison with simulations by van Brummelen et al. [\[6\]](#page-4-2) and Aland & Mokbel [\[1\]](#page-4-5) compared to our simulations for incompressible materials with  $P_1/P_1$  elements and compressible materials with  $P_2$  elements and  $\kappa = 10^4 G_1$ .

#### **2 Results**

Following [\[6,](#page-4-2) [2\]](#page-4-3) we choose the model parameters in Table [1](#page-4-6) for the benchmark. Note the the surface tensions  $\sigma_i$  are related to the standard interfacial tensions via  $\sigma_{\rm sl} = \sigma_1 + \sigma_2$  (solid-liquid),  $\sigma_{\rm sa} = \sigma_1 + \sigma_3$ (solid-air),  $\sigma_{\text{la}} = \sigma_2 + \sigma_3$  (liquid-air) where

$$
\sigma_{\rm sl} = 36 \cdot 10^{-3} \,\rm Jm^{-2},
$$
  
\n
$$
\sigma_{\rm sa} = 31 \cdot 10^{-3} \,\rm Jm^{-2},
$$
  
\n
$$
\sigma_{\rm la} = 46 \cdot 10^{-3} \,\rm Jm^{-2}.
$$

The corresponding stationary solutions with  $P_1/P_1$ FE are shown in Fig. [3](#page-2-0) and Fig. [4.](#page-2-1) A direct comparison of the solid/liquid and solid/gas interface shape with the ones in  $[6, 2, 5]$  $[6, 2, 5]$  $[6, 2, 5]$  $[6, 2, 5]$  are shown in Fig. [5.](#page-3-0) For this benchmark comparison we provide the data summarized in Tab. [2.](#page-5-0) We provide a dataset for stationary solutions of the incompressible model with  $P_1/P_1$  elements and for the compressible models with  $P_2$  elements. Except for the csv files, each dataset comes with the computational mesh. The pvd/vtu/xdmf files were created in Python/FEniCS and imported and postprocessed with ParaView and FEniCS itself. The comparison of interface shapes stored in csv files were performed with MATLAB.

The overall agreement between the simulation appears good, taking into account the different numerical methods used, i.e.,

- phase fields vs sharp interfaces between the solid and the other two phases,
- Eulerian vs Lagrangian description of elasticity,
- the involved scaling limits  $\varepsilon \to 0$  and vanishing Cahn-Hilliard mobility.

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name $G_1$ $G_{2,3}$		$\sigma_1$	$\sigma_2$	$\sigma_3$ $L$ $R$		
				unit Pa Pa $J/m^2$ $J/m^2$ $J/m^2$ h h h		
				value $10^3$ 0 $10.5 \cdot 10^{-3}$ $25.5 \cdot 10^{-3}$ $20.5 \cdot 10^{-3}$ 10 $176.7/50$ $1/800$		

<span id="page-4-6"></span>Table 1: Benchmark parameters with lengths  $L, R, \epsilon$  rescaled by substrate thickness  $h = 5 \cdot 10^{-5}$  m

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<span id="page-5-0"></span>Table 2: Description of data/files for the benchmark. The files stationary\_P1P1.h5 and stationary\_P2.h5 are readable in FEniCS using the postprocessing\_P1P1.py and postprocessing\_P2.py scripts. The pvd/vtu/xdmf files are readable with the ParaView visualization tool. The csv data tables are readable using the MATLAB script benchmark.m.