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7 Manuscript title:

8 **PERFORMANCE TESTING OF DOSIMETERS USED IN INTERVENTIONAL**  
9 **RADIOLOGY: RESULTS FROM THE VERIDIC PROJECT**

10  
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## 27 Abstract

28 Interventional procedures in radiology and cardiology are associated with high dose to the  
29 patient. Accurate dosimetry is essential and calibration of the equipment is a means to provide  
30 the necessary accuracy of dose assessment.

31 The objective of this work is to investigate the performance of dosimeters used in interventional  
32 procedures in different standard and non-standard X-ray radiation qualities, and to investigate  
33 potential uncertainties related to dose measurements, thus improving accuracy of patient  
34 dosimetry in interventional procedures.

35 Four new reference radiation qualities dedicated to interventional cardiology applications have  
36 been established, allowing calibration of dosimeters used in clinical conditions with appropriate  
37 traceability to primary standards. Testing of solid-state semiconductor detectors and  
38 thermoluminescent dosimeter properties, e.g. influence of photon energy, angle of incidence and  
39 dose rate, was performed in the standard and non-standard radiation qualities.

40 Both dosimeter types showed good performance in the non-standard beams during all  
41 performance tests. Solid-state dosimeters displayed weak dependence on energy, angle of  
42 incidence and dose rate, in the range defined by the manufacturer and requirements of the  
43 international standard. Thermoluminescent dosimeters displayed excellent linearity and angular  
44 dependence. The influence of energy dependence on measurement uncertainty can be reduced if  
45 appropriate radiation quality is selected for calibration.

## 46 Keywords

47 *Diagnostic Radiology, Dosimetry, Interventional Cardiology, Radiation Quality, X-rays*

48

## 49 1. Introduction

50 Diagnostic radiology is a major contributor to the total population dose from artificial sources of  
51 radiation (UNSCEAR, 2011). Dosimetry is an important tool in diagnostic and interventional  
52 radiology to check equipment performance, for optimization of medical practice and risk  
53 assessment. An accurate measurement is ensured by calibration of the instrumentation in  
54 radiation qualities of well-defined properties. The range of clinically used radiation qualities is  
55 wide and depends on the type of X-ray equipment and protocol settings. Radiation quality  
56 influences the response of dosimeters (Hourdakis et al., 2010, Salomon et al., 2020).

57 Radiation qualities are usually specified in terms of the X-ray tube voltage, first and second half  
58 value layer (HVL) (IAEA, 2007). HVL is readily measurable and is related to the mean energy of  
59 the X-radiation, which is usually not known. Standard radiation qualities are defined in IEC  
60 (International Electrotechnic Commission) 61267 standard (IEC, 2005). The clinical beams might  
61 be significantly different from the reference qualities, especially on the side of the high energies  
62 (Järvinen et al., 2015, Salomon et al., 2020). Using the dosimeter outside of the range of radiation  
63 qualities in which it was calibrated introduces significant uncertainty in measurements (Roshau  
64 and Hintenlang, 2003).

65 Dosimeters commonly used in diagnostic and interventional radiology are solid-state dosimeters,  
66 ionisation chambers, thermoluminescent dosimeters (TLD) and gafchromic films  
67 (Hourdakis et al., 2010, IAEA, 2007).

68 Ionisation chambers have been the standard instruments used for diagnostic radiology dosimetry  
69 and quality assurance assessment for many years. Dosimeters based on semiconductor  
70 technology are now becoming widely available, and as the semiconductor detectors are smaller in  
71 size, they are more convenient to use in many situations. Diagnostic dosimeters should be

72 designed in compliance with IEC 61674 (IEC, 1997), which is a standard that pertains to  
73 dosimeters equipped with either ionisation chambers or semiconductor detectors. Traditionally,  
74 the main disadvantage of semiconductor-based devices is their pronounced energy dependence of  
75 response which differs considerably from the relatively constant response of ionisation chambers  
76 in the diagnostic X-ray energy range for measurement of air kerma. Multiple semiconductor  
77 elements are incorporated into the semiconductor detector used for X-ray dosimetry. Dose  
78 compensation is applied automatically and is derived based on radiation quality. The commercial  
79 semiconductor detectors are mounted on lead backing plates, to attenuate radiation incident from  
80 the rear, ensuring that the automatic energy compensation is applied correctly. As a result, these  
81 detectors measure the air kerma incident from the direction of the primary beam and,  
82 consequently, have pronounced angular dependence. The use of lead backing plates in solid-state  
83 dosimeters can also influence the behavior of the X-ray system's automatic exposure control.  
84 Nevertheless, these types of detectors have found many applications in routine clinical  
85 measurements in hospitals. Most of them are capable of determining the air kerma, tube voltage,  
86 half value layer (HVL), and exposure time, as well as the output waveform from a single  
87 irradiation (Martin et al., 2007).

88 According to the requirements of the international standard IEC 61674 (IEC, 1997), the Quality  
89 Control (QC) semiconductor solid-state dosimeters' response variation must be within  $\pm 5\%$  in the  
90 minimum rated range of photon energy,  $\pm 2\%$  for the variation in air kerma rate and  $\pm 3\%$  for  
91 different angles of incidence. When the dosimeters are used in clinical conditions outside of the  
92 rated range of the influence quantities, the response variation might increase. Photon energy  
93 (radiation quality) and air kerma rate are especially important (Hourdakis et al., 2010, IEC,  
94 1997).

95 Thermoluminescent dosimeters exhibit good dosimetric characteristics due to their tissue-  
96 equivalent composition in terms of interactions with photon radiation over a certain energy range.  
97 Thanks to this property they have been used for clinical studies of patient skin dose  
98 measurements in interventional procedures (Bogaert et al. 2009; Dabin et al., 2018). The most  
99 common types of TLDs contain round or square pellets made of LiF:Mg,Ti or LiF:Mg,Cu,P. The  
100 main sources of uncertainty associated with these dosimeters are the energy dependence, angular  
101 dependence, and linearity of the dosimeter response. In addition, thermal treatment and the  
102 reading process can considerably affect the dosimeter properties. Regarding energy dependence  
103 of the dosimeter response, several studies were conducted in the ISO 4037 (ISO, 1996) standard  
104 N-series radiation qualities and reference photon beams of  $^{137}\text{Cs}$  and  $^{60}\text{Co}$  isotopes (Saez-Vergara  
105 et al., 1999; Olko et al., 2002; Davis et al., 2003; Apostolakopoulos et al., 2019; Parisi et al.,  
106 2019), while one study examined the performance of TLDs in the RQR-series (Radiation  
107 Qualities in Radiation beams emerging from the X-ray source assembly) (Carinou et al., 2008).  
108 Two studies were based on irradiations in the quasi monoenergetic beams (Kron et al., 1998;  
109 Duggan et al., 2004), and one in the standard NIST radiation qualities (Nunn et al., 2008). The  
110 results of these different studies show that the relative response curves of LiF:Mg,Ti and  
111 LiF:Mg,Cu,P are fundamentally different. LiF:Mg,Cu,P TLDs usually display a similar shape of  
112 energy response in different studies, with a minimum relative response value in the 80-100 keV  
113 energy range. In case of the LiF:Mg,Ti results were more heterogeneous in different studies, but  
114 TLD energy dependence generally shows a maximum value in the 30-50 keV energy range. The  
115 cause of differences in TLD energy response may be due to the pellet material properties and not  
116 the reading and annealing procedures (Saez-Vergara et al., 1999). In the interventional  
117 procedures energy range from 15 keV up to 120 keV, the energy response deviates up to  $\pm 20\%$   
118 from unity, and up to +40% higher than unity, for LiF:Mg,Cu,P and LiF:Mg,Ti TLDs

119 respectively. In order to properly investigate the behavior of these passive dosimetry systems  
120 irradiations in the non-standard radiation qualities is necessary.

121 High dose values delivered to the patient skin during an interventional procedure may cause  
122 supralinearity of the TLD response, depending on impurity content of the TLD material, thermal  
123 treatment of the dosimeters, reading process, glow peak temperature and the photon energy. This  
124 effect is more pronounced in LiF:Mg,Ti than in LiF:Mg,Cu,P material, which gives this material  
125 a significant advantage for use in interventional procedures (Moscovitch et al., 2007).

126 Radiochromic films (Gafchromic XR type T) are also used for measurements of maximum  
127 delivered skin dose in high dose and high dose rate IC procedures (Farah et al., 2015). The main  
128 consequence of ionising radiation interactions with the radiochromic films is the film color  
129 alteration, whereas the alteration intensity is proportionate to the dose value. The quantitative  
130 post-irradiation analysis and determination of skin dose is strongly dependent on various film  
131 properties and performance under clinical irradiation conditions (Greffier et al., 2017; Didier et  
132 al., 2019). Major factors contributing to the variation in the film response are the energy  
133 dependence and dose rate dependence. A group of authors found a difference of 9% between film  
134 readings in two different clinical beams for the same delivered dose. Clinical beams with medium  
135 (75 kV, 4 mm Al) and high (120 kV, 6 mm Al) beam energy were used. Irradiation conditions in  
136 interventional procedures involve backscattered radiation and high dose rate pulsed fields, in  
137 comparison with laboratory conditions where the fields are continuous and with low dose rate  
138 values. These differences cause the need for characterisation under clinical conditions, similarly  
139 as with thermoluminescent dosimeters. Film-to-film uniformity, film darkening over time and the  
140 impact of scanner used, represent additional influences on the quantification of dose, besides the  
141 before mentioned factors (Farah et al., 2015).

142 In order to improve the accuracy of dose measurement for patients and medical staff in the  
143 interventional radiology and cardiology procedures, and due to the differences in irradiation  
144 conditions in the calibration laboratories and hospitals, dosimeters should be calibrated in the  
145 radiation qualities whose characteristics are as close as possible to the X-ray beams generated by  
146 the medical systems on-site.

147 VERIDIC project (Validation and Estimation of Radiation Skin Dose in Interventional  
148 Cardiology), focused on the validation of skin dose calculation (SDC) software products in  
149 interventional cardiology, which will optimize radiation protection of patients. One of the  
150 objectives of the VERIDIC project (under Work Package 2) (Dabin et al. 2020) was to develop a  
151 protocol for acceptance and QC tests of SDC software to be used by medical physicists in clinical  
152 practice. The adequate use of such protocol is highly related to the accuracy of dose  
153 measurement of commonly used field dosimeters.

154 Following this, the objective of this work is to investigate the performance of dosimeters used in  
155 interventional procedures in different standard and non-standard radiation qualities, relevant for  
156 clinical practice. Although gafchromic films were tested in the frame of the VERIDIC project for  
157 the sake of completeness, these results were not deemed novel enough to be reported in the  
158 present article. The results are in agreement with more extensive studies performed by Farah et  
159 al. (2015) and Greffier et al. (2017), and are available in an online report (Blideanu et al. 2020).

160 By providing traceability in these radiation qualities and minimizing the differences in calibration  
161 conditions compared to the radiation qualities used in hospitals and by investigating potential  
162 uncertainties related to dose measurements this work intends to improve accuracy of patient  
163 dosimetry in interventional procedures.

164



## 165 2. Materials and Methods

166 To address the issue stated in the objective of this work, four new reference beam qualities  
167 dedicated to interventional cardiology applications have been established, allowing calibration of  
168 dosimeters used in clinical conditions with appropriate traceability to primary standards. Testing  
169 of solid-state semiconductor detector and thermoluminescent dosimeter properties, e.g. influence  
170 of photon energy, angle of incidence and dose rate, was performed in the standard radiation  
171 quality and non-standard radiation qualities which correspond to irradiation conditions  
172 characteristic for fluoroscopically guided interventional procedures in interventional radiology  
173 (IR) and interventional cardiology (IC).

### 174 2.1. X-ray beam qualities

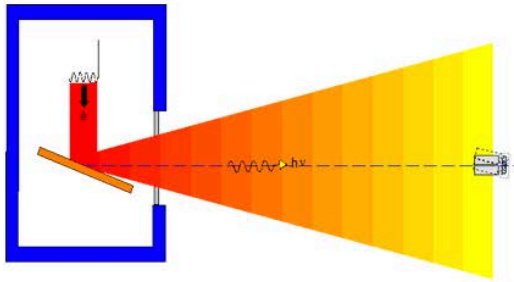
175 In order to investigate performance of the dosimeters under irradiation conditions which differ  
176 from those proposed in the standard RQR series (IEC, 2005), non-standard radiation qualities  
177 corresponding to those used in clinical conditions were established.

178 To investigate typical radiation qualities used in interventional procedures, an inventory of  
179 Radiation Dose Structured Reports (RDSRs) from different interventional procedures was  
180 collected. Six interventional X-ray units (one Canon (Canon Medical Systems, Japan), two GE  
181 (GE Healthcare, USA), one Philips (Philips, Netherlands) and two Siemens (Siemens Helathcare,  
182 Germany)) from hospitals in France, Italy, Ireland and Switzerland were used for the collection  
183 of RDSRs, with a sample of 30 RDSRs per interventional unit. The frequency of use of  
184 combinations of tube voltage and additional filtrations was analyzed, including both fluoroscopy  
185 and cine acquisition regimes. Despite the limited number of procedures and X-ray units, a wide  
186 range of X-ray tube voltages ranging from 57 kV to 125 kV and a range of added filtration in the  
187 primary beam from 0 mm Cu up to 1.0 mm Cu was observed in the collected procedure sample of

188 total 180 RDSRs. The radiation qualities most commonly used included X-ray tube voltages in  
189 the range from 80 kV to 120 kV, and a range of additional filtration of 0, 0.1, 0.3 and 0.9 mm Cu.  
190 Although the X-ray tube voltage and additional filtration values were similar, notable differences  
191 among the interventional units exist (even in the case of the units produced by the same  
192 manufacturer). For instance, the vast majority of all irradiations (between 53% and 98%),  
193 whether using fluoroscopy or cine regime, were performed with additional filtration between 0.1  
194 and 0.3 mm Cu on three systems (Canon, GE and Siemens). On the Philips unit, a similar trend  
195 was observed in cine regime, but fluoroscopy irradiations were performed with a slightly higher  
196 filtration (0.4 mmCu) in about 90% of the cases. On the remaining systems, however, more than  
197 60% of the cine acquisitions were performed without additional filtration. Use of 0.9 mmCu was  
198 only significant (about 10%) in the two GE systems in fluoroscopy regime.

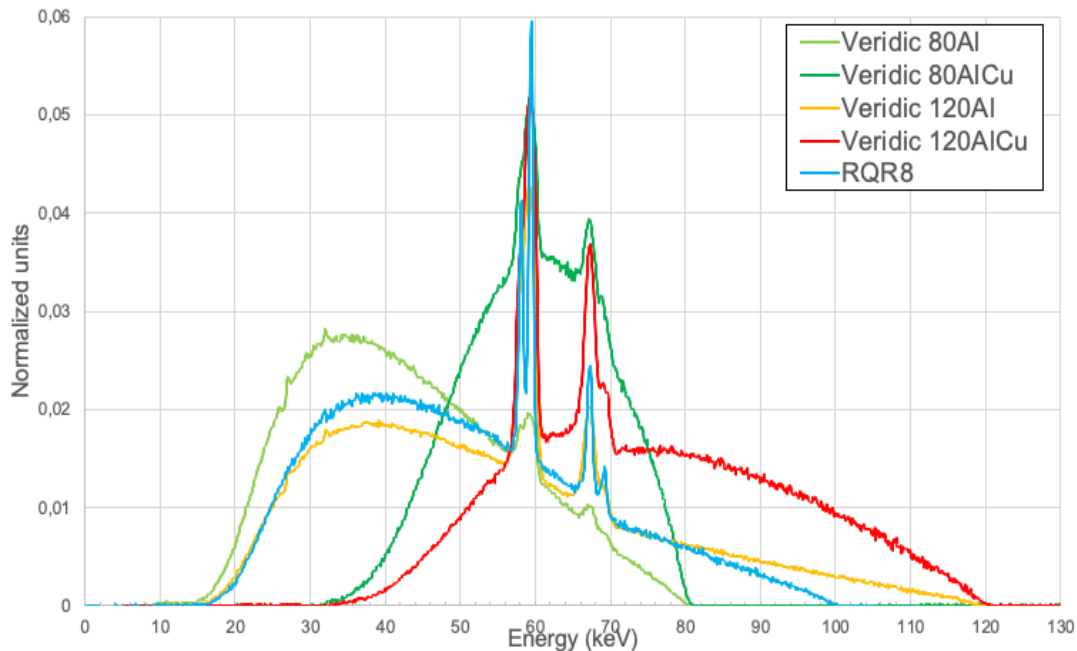
199 The X-ray spectra for selected X-ray tube voltage and filtration combinations were calculated by  
200 using the SpekCalc code, which is a commonly used and extensively validated tool for X-ray  
201 tube applications (Poludniowski et al., 2009). As a balance between accuracy and complexity,  
202 radiation qualities selected for testing of dosimeters included extreme values of the additional Cu  
203 filtration, e.g. 0 and 0.9 mm Cu, for two X-ray tube voltage values (80 kV and 120 kV) and  
204 inherent filtration of 2.5 mm Al.

205 The selected radiation qualities were generated by using a Seifert 320 X-Ray generator (Seifert,  
206 Radevormwald, Germany). For the purpose of validating the non-standard radiation qualities, X-  
207 ray spectra were measured by using a method based on CdTe semiconductor detector which has  
208 been developed by the French Alternative Energies and Atomic Energy Commission (CEA)  
209 (Plagnard, 2014). Measured spectra correspond well with the spectra calculated by SpekCalc. The  
210 measurement set-up used for spectrometry measurements is presented in Fig. 1.



211  
212  
213 *Figure 1. Schematic representation of the spectrometer positioning in the X-ray field (left), and the*  
214 *experimental set-up used for the X-ray spectra measurements, emitted by the CEA X-ray generator (right).*

215 The four newly established radiation qualities were metrologically characterised in terms of air  
216 kerma rate by using the primary standard free-in-air ionisation chamber available at CEA Primary  
217 Standard Dosimetry Laboratory (PSDL). Besides the new non-standard radiation qualities, a  
218 standard radiation quality of similar properties in terms of X-ray spectra, RQR8, has been  
219 selected in order to compare the calibration results between laboratory and hospital irradiation  
220 conditions (IEC, 2005). The measured pulse-height energy spectra of the non-standard radiation  
221 qualities and the standard RQR8 radiation quality are presented in Fig. 2.



222  
 223 *Figure 2. Energy spectra for the IC radiation qualities and the standard RQR8 radiation quality*

224 The established standard and non-standard radiation qualities were further used to test solid-state  
 225 and thermoluminescent dosimeters, in particular to investigate their response as a function of air  
 226 kerma rate, photon energy and angle of incidence.

## 227 2.2. Solid-state quality control dosimeters

228 The commercial semiconductor diagnostic dosimeters that are tested in this paper are: MPD  
 229 (Multi-Purpose Detector) and R100B, both used with the Barracuda electrometer module (RTI  
 230 electronics, Molndal, Sweden), Black Piranha (RTI electronics, Molndal, Sweden), and Unfors  
 231 Xi (RaySafe, Billdal, Sweden). The R100B dosimeter has a single detector element while MPD,  
 232 Piranha and Unfors Xi contain multiple detector elements. These detector elements have thin  
 233 metal layers, providing compensation of the derived detector response for different radiation  
 234 qualities. The MPD and Piranha detectors use some of the detector elements to non-invasively  
 235 determine tube voltage, while the rest of the detector elements are used for measurement of the  
 236 incident air kerma with compensation for detector energy dependence. Technical specifications

237 of these solid-state dosimeters in terms of applicable X-ray tube voltage range, dose and dose rate  
 238 range are displayed in Table 1.

239

240 *Table 1. Technical specifications of the tested QC solid-state dosimeters.*

QC dosimeter	Manufacturer	X-ray tube voltage [kV]		Dose range [Gy]		Dose rate range [mGy·s <sup>-1</sup> ]	
		min	max	min	max	min	max
MPD	RTI Electronics	35	155	1.5×10 <sup>-8</sup>	1×10 <sup>+3</sup>	1.5×10 <sup>-6</sup>	4.5×10 <sup>+2</sup>
R100B	RTI Electronics	Not specified		1×10 <sup>-10</sup>	1.5×10 <sup>+5</sup>	1×10 <sup>-6</sup>	7.6×10 <sup>+1</sup>
Black Piranha	RTI Electronics	50	150	1×10 <sup>-10</sup>	1.5×10 <sup>+3</sup>	1×10 <sup>-6</sup>	3.2×10 <sup>+2</sup>
Xi R/F Classic	RaySafe	35	160	1×10 <sup>-8</sup>	1×10 <sup>+4</sup>	1×10 <sup>-5</sup>	1×10 <sup>+3</sup>

241

### 242 2.3. Thermoluminescent dosimeters

243 The passive dosimetry system that was tested in the reference radiation quality and the IC non-  
 244 standard radiation fields was based on the MCP-N dosimeters. These LiF:Mg,Cu,P dosimeters  
 245 are in form of 4.5 mm diameter circular pellets with 0.9 mm thickness. Sets of three dosimeters  
 246 were prepared for each irradiation used for the performance testing. Prior to every exposure, the  
 247 TLDs were annealed 10 minutes in an oven at 240°C, followed by fast cooling in a freezer down  
 248 to -10°C. In order to monitor the accumulated dose during transportation and storage, two sets of  
 249 four TLDs were used. Following the exposure to a certain radiation field, the dosimeters were  
 250 heated at 120°C in an oven for a period of 30 minutes. The TLDs were read on a Harshaw 5500  
 251 system with a constant temperature increment rate of 10°C/s, in range from room temperature up  
 252 to 240°C. The TLD signal output was corrected for the individual sensitivity of each dosimeter,  
 253 which was determined by using a reference <sup>137</sup>Cs radionuclide source.

## 254 2.4. Irradiation set up at the SSDL

255 The performance testing of solid-state QC dosimeters used in diagnostic and interventional  
256 radiology was performed in the Secondary Standard Dosimetry Laboratory (SSDL) of Vinca  
257 Institute of Nuclear Sciences (IAEA, 2018). A vented ionisation chamber Magna (Standard  
258 Imaging Inc, Middleton, WI, USA) was used as a reference standard, whereas a dedicated  
259 metrological continuous radiation mode X-ray unit X80-225 kV-E (Hopewell Designs,  
260 Alpharetta, GA, USA) was used to generate standard and non-standard beam qualities.

261 Traceability to primary standard, for standard and non-standard radiation qualities was ensured  
262 by calibration of the reference standard in French PSDL in CEA. The reference air kerma rate  
263 values were measured by using a reference standard ionisation chamber Exradin A600 whose  
264 calibration coefficients are displayed in Table 2, for standard (RQR8) and non-standard radiation  
265 qualities.

266 Irradiation set up for all dosimeters was arranged in accordance with the International Atomic  
267 Energy Agency (IAEA) Code of Practice TRS 457 (IAEA, 2007), applying a substitution  
268 method, while using a monitor chamber in order to account for X-ray beam output variations. The  
269 reference air kerma rate measurements were corrected for the influence of ambient conditions,  
270 whereas the stability of the X-ray generator was monitored using a monitor chamber type  
271 PTW 34014 (PTW, Freiburg, Germany). Air-kerma rate was measured at the focus to detector  
272 distance of 100 cm.

273 The dosimeter performance tests for both standard and non-standard radiation qualities include  
274 energy dependence, angular dependence and the linearity test. The X-ray tube current was held  
275 constant at 10 mA for the energy dependence and angular dependence tests, while any variations  
276 in the X-ray generator output were accounted for and corrected with the PTW 34014 chamber

277 measurements. In the case of linearity test, variation of air kerma rate was achieved by changing  
278 the X-ray tube current values in the range from 3 mA up to 25 mA.

279 The selected standard radiation quality routinely used for dosimeter calibration in the field of  
280 diagnostic radiology in laboratory conditions is the RQR8 (IAEA, 2007). The properties of  
281 standard radiation quality and non-standard radiation qualities (Section 2.1) used in this research  
282 are presented in Table 2. The inherent filtration for 80 kV and 120 kV non-standard radiation  
283 qualities was 2.5 mm Al, and 0.9 mm Cu was added to the inherent filtration to establish  
284 radiation qualities denoted as Veridic3 80AlCu and Veridic4 120AlCu, respectively, as presented  
285 in Table 2. Veridic1 80Al and Veridic2 120Al radiation qualities were established without any  
286 added copper filtration. The half-value layer of Veridic1 80Al beam (2.55 mm Al) is slightly less  
287 than the minimum permissible first HVL at 80 kV(2.9 mm Al) as per the current European  
288 guidelines (EC, 2012); however, this is deemed to be fairly representative of the low beam  
289 qualities used in practice.

290 During the angular dependence test in RQR8 and Veridic3 80AlCu beams, the range of angle of  
291 incidence was set from  $0^\circ$  to  $\pm 90^\circ$ , with an increment of  $15^\circ$ . The dosimeters were positioned free  
292 in air, while the dosimeter holders used for positioning contain low  $Z$  materials (such as  
293 polymethyl methacrylate, PMMA) in order to reduce the contribution of scattered radiation to the  
294 primary beam measurements. The angle of incidence was defined between the primary beam axis  
295 and the front surface of the dosimeter, where the  $0^\circ$  angle of incidence is achieved by positioning  
296 the dosimeter front surface perpendicular to the primary beam axis direction. In order to vary the  
297 angle of incidence values the dosimeters with appropriate holders were positioned on a custom-  
298 made rotary table. On the X-ray tube focus-detector distance of 100 cm, the dosimeters were  
299 positioned within the 99% isodose area, which corresponds to the 8 cm beam diameter uniform  
300 X-ray field cross-section surface. Heel effect is negligible in the case of X-ray generators used in

301 the calibration laboratories, as evidenced by the investigated field uniformity (Makarić et al.,  
302 2019).

303 *Table 2. Properties of radiation qualities used for performance testing of solid-state and*  
304 *thermoluminescent dosimeters. Calibration coefficients of the Exradin A600 ionisation chamber used for*  
305 *reference air kerma values in the QC dosimeter tests are provided in the rightmost column.*

Radiation quality	X-ray tube voltage [kV]	Half-value layer [mm Al]	Additional filtration [mm Cu]	Calibration coefficient of reference standard [mGy nC <sup>-1</sup> ]
RQR8	100	3.97	/	17.82
Veridic1 80Al	80	2.55	0	17.90
Veridic3 80AlCu	80	8.63	0.9	17.66
Veridic2 120Al	120	3.73	0	17.76
Veridic4 120AlCu	120	11.33	0.9	17.39

306

## 307 2.5. Solid-state quality control dosimeters performance tests

### 308 2.5.1. Energy dependence test

309 Energy dependence of the dosimeter response is an important characteristic that needs to be  
310 accounted for when performing measurements in various radiation fields that may greatly differ  
311 from the reference radiation quality, under which the instrument has been calibrated. In this work  
312 the influence of photon energy was tested for four solid-state detectors described in Section 2.2.  
313 The energy dependence test results are expressed in terms of relative response of the dosimeter,  
314 normalized to the response in RQR8 radiation quality. The relative response is determined by  
315 using the following equation (IAEA, 2007):

$$316 \quad r = \frac{R}{R_0} = \frac{M / (Q \cdot N_K \cdot k_D \cdot k_M)}{R_0} \quad (1)$$

317 where  $R$  and  $R_0$  are the absolute response values for the non-standard radiation qualities and the  
318 standard (reference) radiation quality, respectively. The absolute dosimeter response is defined as



319 the quotient of the value  $M$  indicated by the solid-state detector, and the reference value of air  
320 kerma rate defined by the term  $Q \cdot N_K \cdot k_D \cdot k_M$ , which includes collected charge in the active  
321 volume of the ionisation chamber, the ionisation chamber calibration coefficient, the air density  
322 correction factor and the monitor chamber correction factor for the X-ray generator output,  
323 respectively. The IEC standard 61674 (IEC, 1997) requires a variation in the dosimeter response  
324 within  $\pm 5\%$  in the 50 kV - 150 kV X-ray tube voltage range, in standard radiation qualities.

### 325 *2.5.2. Angular dependence test*

326 Pronounced angular dependence of the solid-state dosimeters' response mainly exists due to their  
327 design, e.g. placement of lead backing plates to attenuate the radiation that is incident from the  
328 rear of the detector, even though these detectors are potentially sensitive to incident radiation  
329 from all directions (Roshau and Hintenlang, 2003). The influence of angle of incidence on the  
330 indication of the solid-state detectors was tested in the standard RQR8 radiation quality, and the  
331 non-standard Veridic3 80AlCu beam. The relative angular dosimeter response was determined by  
332 normalizing the measured absolute response to the response acquired for the  $0^\circ$  angle of  
333 incidence, for each beam quality independently. IEC 61674 (IEC, 1997) standard imposes a  $\pm 3\%$   
334 upper limit of dosimeter response variation, but this limit is applicable in the angle of incidence  
335 range of  $\pm 5^\circ$  from the reference orientation. This study covered much wider range of angles, so  
336 this limit is not applicable.

### 337 *2.5.3. Dose rate dependence test*

338 The linearity test was performed for the standard RQR8 and non-standard Veridic3 80AlCu  
339 radiation qualities in the X-ray tube current range from 3 mA up to 25 mA. Those values  
340 correspond to the tube current range available on the X-ray system for the selected irradiation  
341 settings. The linearity test results were expressed as the normalized dosimeter response to the

342 reference air kerma rate value chosen for the tube current of 9 mA, for each of the radiation  
343 qualities separately. According to the IEC 61674 (IEC, 1997) the deviation criteria is  $\pm 2\%$  from  
344 the calibration condition, over the whole air kerma rate range.

## 345 2.6. Thermoluminescent dosimeters performance tests

346 TLDs containing LiF:Mg,Cu,P pellet material were irradiated in the standard RQR8 radiation  
347 quality and non-standard radiation qualities. Previous to irradiation, the TLDs were annealed for  
348 ten minutes at 240°C, followed by fast cooling at -10°C. Two sets of four TLDs were used to  
349 monitor the accumulated dose during storage and transportation. Following exposure, the  
350 dosimeters were heated at 120°C for 30 minutes. Harshaw 5500 system was used for dosimeter  
351 readout, and the acquired data was corrected for individual sensitivity of the dosimeters, which  
352 was determined by using a reference  $^{137}\text{Cs}$  source. Energy dependence, angular dependence and  
353 dose rate dependence of the dosimeter response were examined.

### 354 2.6.1. Dose rate dependence test

355 The influence of dose rate on TLD response was studied in the reference RQR8 radiation quality  
356 at CEA PSDL using X-ray tube current ranging from 0.9 mA to 24.1 mA, corresponding to air  
357 kerma rates between 5 mGy min<sup>-1</sup> and 140 mGy min<sup>-1</sup>. Those values correspond to the tube  
358 current range available on the X-ray system for the selected irradiation settings. For each of the  
359 irradiation conditions response was averaged for a sample of three dosimeters. The response was  
360 normalized to the value measured at 5 mGy min<sup>-1</sup> dose rate.

### 361 2.6.2. Angular dependence test

362 Angle of incidence influence quantity was investigated in the RQR8 radiation quality and the  
363 non-standard Veridic3 80AlCu and Veridic2 120Al radiation qualities. Angle values ranged from  
364 0° up to 90°, with a 15° increment, similarly to the angular dependence test of the solid-state

365 dosimeters. The symmetry of angular response was tested in the CEA radiation fields for RQR8  
366 and Veridic3 80AlCu qualities, while the response for Veridic2 120Al radiation quality was  
367 tested in the Vinca SSDL radiation field. The response was normalized to the value measured at  
368 0° angle of incidence, when the TLD pellet surface is perpendicular to the incident beam.

### 369 *2.6.3. Energy dependence test*

370 The influence of radiation quality was tested by irradiating the TLD batches in the standard  
371 radiation quality RQR8 and the four non-standard qualities. The energy response was normalized  
372 to the value acquired for the reference <sup>137</sup>Cs radiation field. Variation of the dosimeter response  
373 depending on the radiation quality used for the passive dosimetry system calibration was tested  
374 by calibrating the system in all five radiation qualities respectively (standard and non-standard).

## 375 *2.7. Uncertainty assessment*

376 Measurement uncertainty was evaluated for each measurement of variation of QC solid-state  
377 detector response with investigated parameters (energy, angle of incidence and dose rate). In all  
378 cases, the expanded combined uncertainty ( $k = 2$ ) was larger than 1/5 of the limit of variation and  
379 smaller than 1/2. According to IEC 61674, the limits of variation are expanded by adding the  
380 measurement uncertainty (IEC, 1997). Relative response for reference conditions was 1 by  
381 definition, and this value has no measurement uncertainty assigned. Expanded combined  
382 measurement uncertainty in case of energy dependence was between 2.2% and 2.4%, and most  
383 important contributions were calibration factors of reference chamber (for two radiation  
384 qualities), reference chamber stability and difference between radiation quality established in  
385 CEA PSDL and SSDL of Vinca Institute of Nuclear Sciences. In case of angular dependence and  
386 linearity tests, measurement uncertainty was 1.0%. Major contributions were repeatability of  
387 measurements by QC dosimeter, change in air density, i.e. temperature and pressure during the

388 test, QC dosimeter positioning, and in case of linearity test – electrometer non-linearity (two  
389 electrometers were used for the test). Angle of incidence was measured with absolute  
390 measurement uncertainty of 2°.

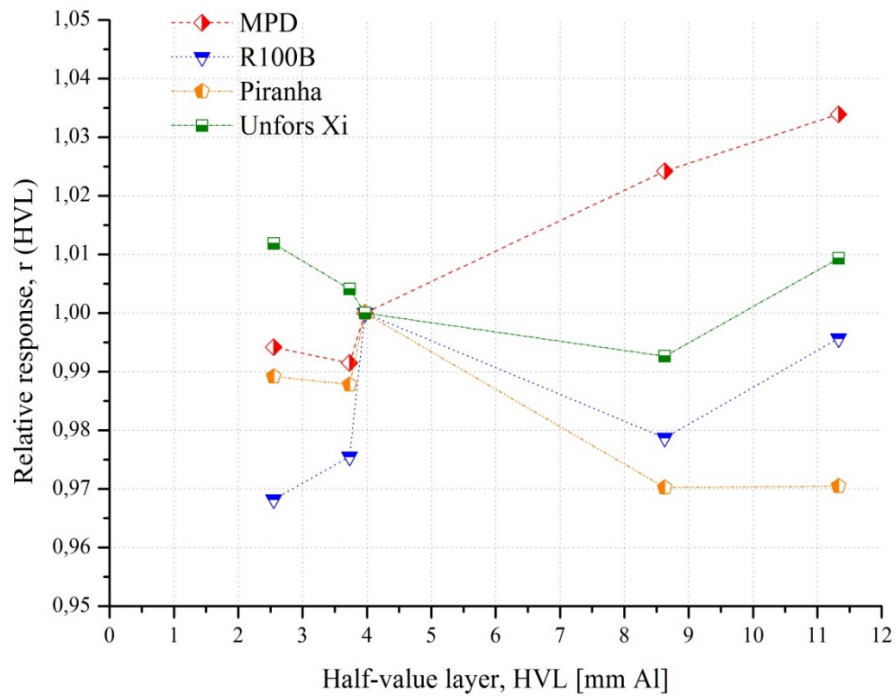
391 Regarding dose estimation with TLDs a standard deviation of the energy response of 5% can be  
392 estimated taking into account maximum and minimum responses for different system  
393 calibrations. The contribution of angular dependence to the measurement uncertainty is a  
394 standard uncertainty of 4% ( $k = 1$ ). An expanded uncertainty (with  $k = 2$ ; 95% interval of  
395 confidence) of 16% can be estimated for skin dose measurements in interventional procedures  
396 with LiF:Mg,Cu,P TLDs, considering the contribution of energy response ( $k = 1$ , 5%), angular  
397 response ( $k = 1$ , 4%), and the uncertainties associated with the dosimetry system (fading 3%,  
398 individual dosimeter sensitivity 2%, repeatability 1%, calibration coefficients 1.4%, and  
399 calibration doses 2.2%). Additionally, in cases where the position of maximum skin dose is  
400 unknown, a correction factor up to 40% with additional uncertainty with standard deviation of  
401 12% should be used to account for the probability that no dosimeter is in the region of the  
402 maximum skin dose (Dabin et al., 2015).

403

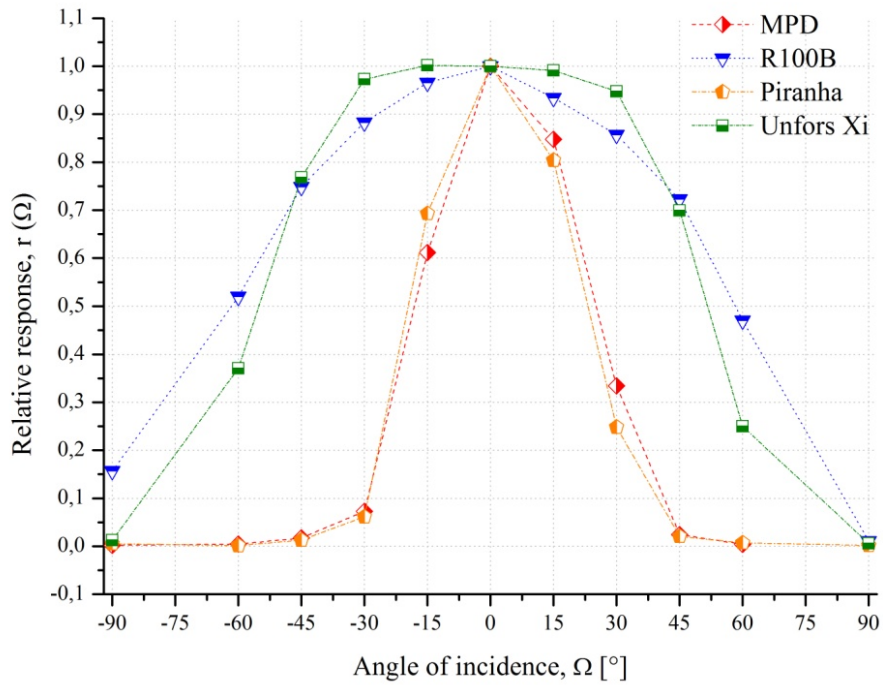
## 404 3. Results

### 405 3.1. Solid-state quality control dosimeters

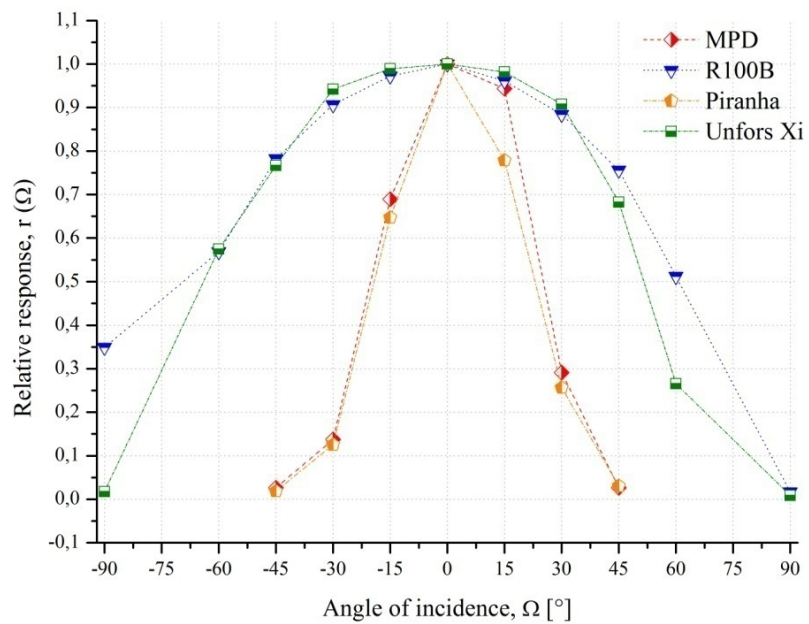
406 Solid-state dosimeter behavior in the non-standard X-ray beams was evaluated in terms of  
407 relative response normalized to the absolute response for the standard RQR8 radiation quality.  
408 Results are presented in Fig. 3. Relative response was within 5% for all tested radiation qualities  
409 which is in line with the requirements of the standard (IEC, 1997). In the whole HVL range (from  
410 2.55 mm Al for Veridic1 80Al up to 11.33 mm Al for Veridic4 120AlCu), Unfors Xi dosimeter  
411 showed excellent performance with the relative response deviation of approximately up to  $\pm 1\%$   
412 from the reference value. Other detectors also demonstrated compliance with the requirements of  
413 IEC 61674 standard for all radiation qualities (IEC, 1997). The angular dependence of solid-state  
414 detector response was measured for standard RQR8 radiation quality (Fig. 4a) and non-standard  
415 highly filtered Veridic3 80AlCu radiation quality (Fig. 4b). Solid-state detectors R100B and  
416 Unfors Xi showed relatively small angular dependence. When the measurement uncertainty is  
417 taken into account, response for  $\pm 15^\circ$  is within the limits of variation defined in IEC 61674 for  
418 both detectors in both radiation qualities. However, more robust multiple element detectors, MPD  
419 and Piranha, have a rapidly decreasing angular response with the increase of angle and all the  
420 results are outside of limits of variation in both radiation qualities. Dose rate dependence of the  
421 solid-state dosimeters was tested in the X-ray tube current range from 3 mA to 25 mA, by  
422 normalizing the response to the dose rate value at 9 mA. Results are presented in Fig. 5a and 5b  
423 for standard RQR8 radiation quality and non-standard highly filtered Veridic3 80AlCu radiation  
424 quality, respectively. All relative responses were between 0.99 and 1.01 for both standard RQR8  
425 and non-standard Veridic3 80AlCu beam qualities. Considering the measurement uncertainty of  
426 1%, these values are not significantly different from unity.



427  
 428 *Figure 3. Relative response of four solid-state detectors measured for one standard (reference) radiation*  
 429 *quality (RQR8) under laboratory conditions, and four non-standard radiation qualities which correspond*  
 430 *to clinical conditions (Veridic1 80Al, Veridic2 120Al, Veridic3 80AlCu and Veridic4 120AlCu).*

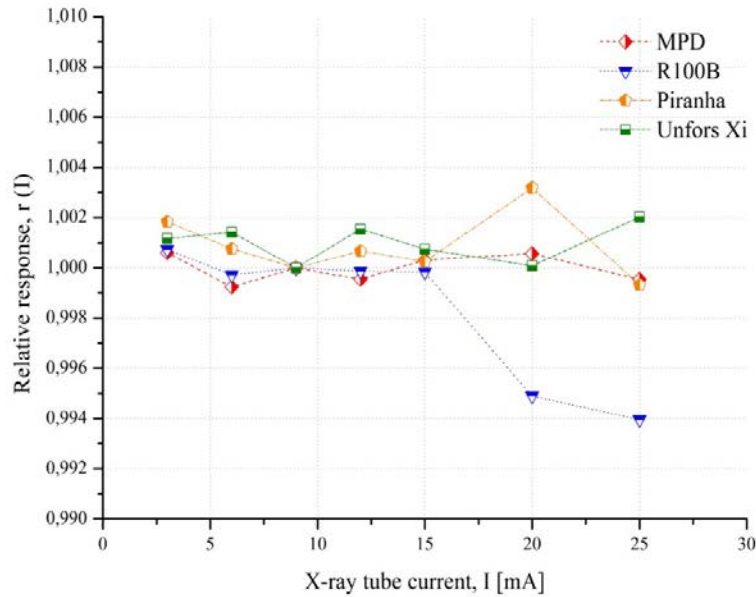


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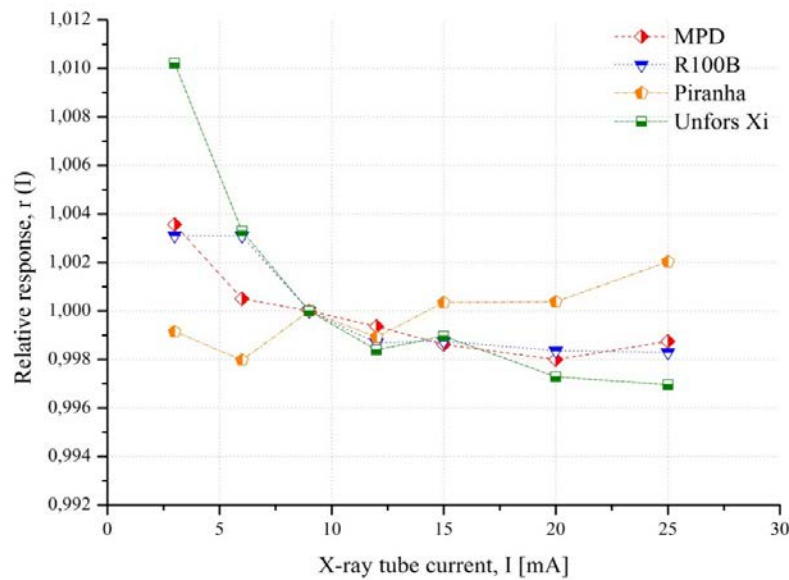


432

433 Figure 4. The angular dependence test results of four solid-state detectors for: a) the reference standard  
 434 RQR8 radiation quality; b) the non-standard Veridic3 80AlCu radiation quality - in the angle range from  
 435  $0^\circ$  to  $\pm 90^\circ$ . The relative angular response was normalized to absolute response value for  $0^\circ$ .



436



437 Figure 5. The linearity test results for four solid-state detectors in the air-kerma rate range determined by  
 438 the X-ray tube current range from 3 mA to 25 mA, for: a) the reference standard RQR8 radiation quality;  
 439 the X-ray tube current range from 3 mA to 25 mA, for: b) the non-standard Veridic3 80AlCu radiation quality.

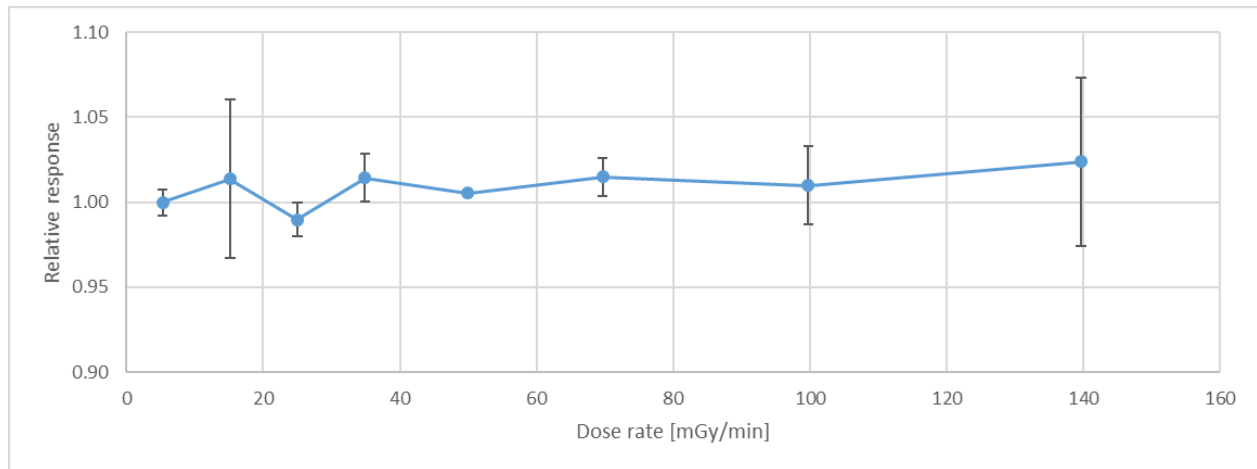


440 b) the non-standard Veridic3 80AlCu radiation quality. The relative response was normalized to the  
441 absolute response value at 9 mA X-ray tube current.

### 442 3.2. Thermoluminescent dosimeters

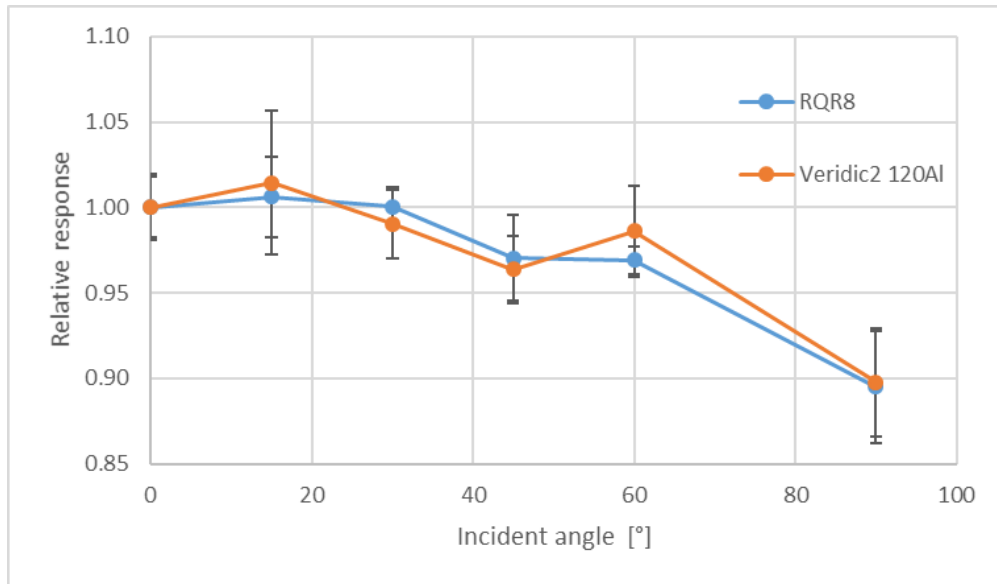
443 TLD performance testing results are presented in Figs. 6-10. Dose rate dependence is shown in  
444 Fig. 6, where response was normalized to  $5 \text{ mGy min}^{-1}$ . Comparison of angular dependence in  
445 RQR8 and Veridic2 120Al radiation qualities normalized to  $0^\circ$  is presented in Fig. 7, while the  
446 comparison of angular dependence in RQR8 and Veridic3 80AlCu radiation qualities, including  
447 response symmetry evaluation is given in Fig. 8. The energy response of TLDs for all five  
448 radiation qualities (one standard, four non-standard) is normalized to  $^{137}\text{Cs}$  and compared with  
449 other energy dependence studies of the LiF:Mg,Cu,P material in Fig. 9. Fig. 10 shows the  
450 influence of system calibration radiation quality on the relative energy response.

451

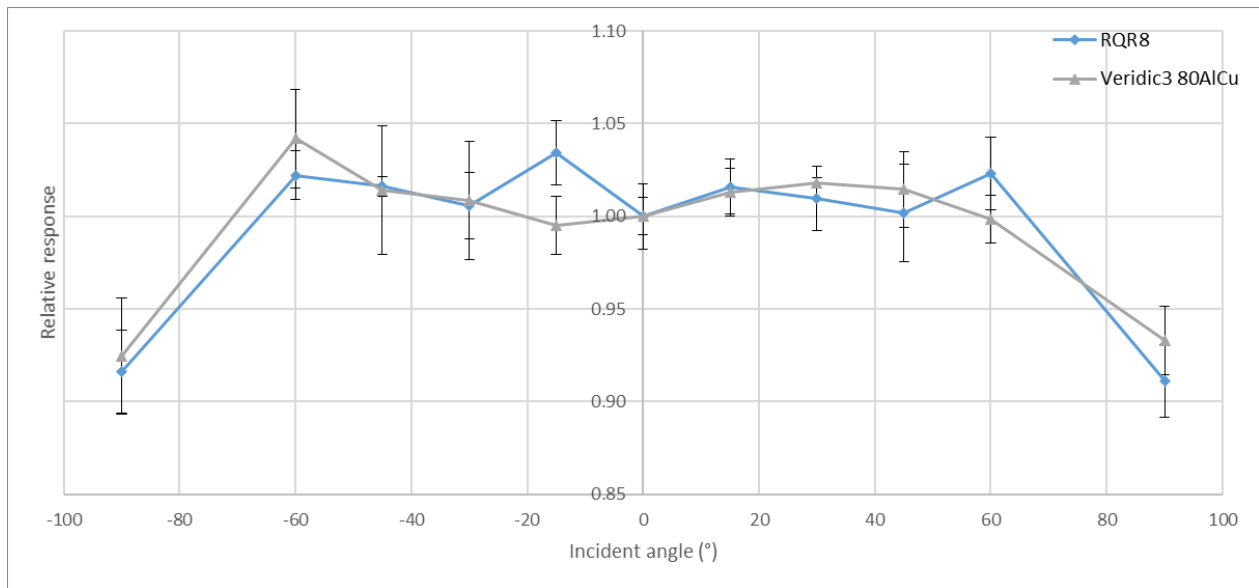


452  
453 *Figure 6. Dose rate dependence of the LiF:Mg,Cu,P response for the RQR8 radiation quality, normalized*  
454 *to the value measured at  $5 \text{ mGy min}^{-1}$ . Each data point represents average response of three dosimeters,*  
455 *and the error bars represent standard deviation of the average response.*

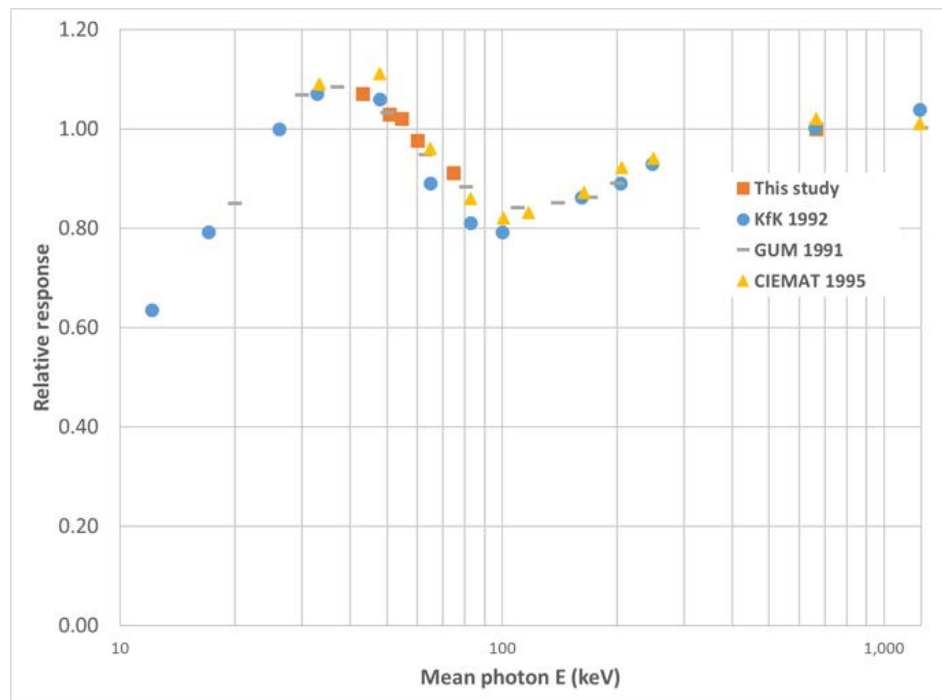
456 The relative angular response has values within  $\pm 4\%$  for angles of incidence between  $0^\circ$  and  $60^\circ$ ,  
457 while the deviation is between  $-10\%$  and  $+4\%$  over the whole angle range.



458  
 459 *Figure 7. Angular dependence of LiF:Mg,Cu,P response normalized to the value at 0°. Combined energy*  
 460 *and angular dependence was tested for RQR8 and Veridic2 120Al radiation qualities. Each data point*  
 461 *represents average response of three dosimeters, and the error bars represent standard deviation of the*  
 462 *average response.*

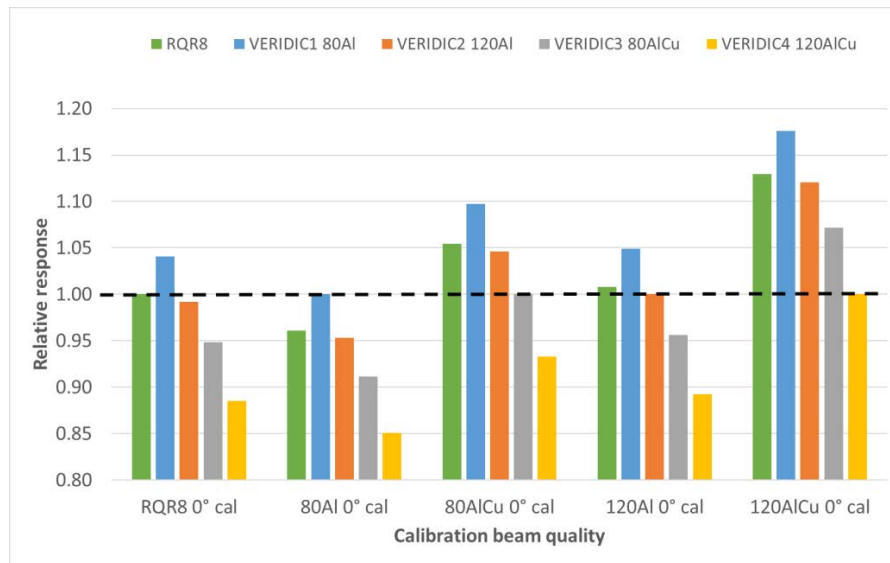


463  
 464 *Figure 8. Angular dependence of LiF:Mg,Cu,P response normalized to the value at 0°. Combined energy*  
 465 *and angular dependence was tested for RQR8 and Veridic3 80AlCu radiation qualities, including*  
 466 *symmetry of the angular response. Each data point represents average response of three dosimeters, and*  
 467 *the error bars represent standard deviation of the average response.*



469  
 470 *Figure 9. Energy dependence of the LiF:Mg,Cu,P response comparison from various studies (Olko et al.,*  
 471 *2002).*

472 To evaluate the impact of the TLD system calibration to the TLD energy response, the calibration  
 473 of the TLDs was performed in each of the tested radiation qualities. As presented in Fig. 12,  
 474 relative response of TLDs was calculated as a ratio of the TLD response in any radiation quality  
 475 and TLD response in the radiation quality used for calibration.



476  
 477 *Figure 10. Energy dependence of the LiF:Mg,Cu,P response for the system calibrated for RQR8, Veridic1*  
 478 *80Al, Veridic3 80AlCu, Veridic2 120Al and Veridic4 120AlCu, respectively.*

#### 479 4. Discussion

480 Although it is generally believed that semiconductors have pronounced energy dependence  
 481 (Roshau and Hintenlang, 2003), results of tests in this study demonstrated good performance in  
 482 terms of energy dependence, i.e. relative response was within 5% for all tested radiation qualities  
 483 which is in line with the requirements of the standard (IEC, 1997). In the whole HVL range  
 484 Unfors Xi dosimeter showed excellent performance with the relative response deviation of  
 485 approximately up to  $\pm 1\%$  from the reference value. All the other detectors also conform to the  
 486 requirements of IEC 61674 standard for all radiation qualities, even though the range of HVLs  
 487 was wider than the minimum rated range. Seven out of 12 relative response values for these  
 488 detectors were not significantly different from unity.

489 Tests performed to evaluate the influence of angle of incidence showed that some dosimeters  
 490 behaved well even for angles of incidence up to  $\pm 30^\circ$ . Solid-state dosimeters are very sensitive to  
 491 the influence of angle of incidence, but R100B and Unfors Xi show relatively small angular

492 dependence. When the measurement uncertainty is taken into account, response for  $\pm 15^\circ$  is  
493 within the limits of variation defined in IEC 61674 for both detectors in both radiation qualities.  
494 On the other hand, more robust multiple element detectors, MPD and Piranha, have a rapidly  
495 decreasing angular response with the increase of angle and all the results are outside of limits of  
496 variation in both radiation qualities. It should be noted that all the tested angles were outside of  
497 the minimum rated range. All dosimeters show similar variation in response with increasing  
498 angle of incidence in both standard and non-standard radiation quality.

499 Performance testing of X-ray equipment often requires the assessment of doses and dose rates for  
500 X-ray beams with many different radiation qualities and in non-ideal conditions. Solid state  
501 dosimeters provide a viable alternative to ionization chambers and are configured to give  
502 measurements of air kerma independent of radiation quality. The solid state detectors are  
503 mounted on lead backing plates, affecting the variation in sensitivity with angle. Nevertheless, it  
504 is important to note that other factors, such as direction of incident radiation, extra focal radiation  
505 and scattered radiation could increase the overall uncertainty of the measurement and potentially  
506 push the dosimeters outside of the acceptable range, which can be expected with the effect of  
507 scattered radiation (IAEA, 2007; Martin et al., 2007, Hourdakakis et al., 2010).

508 The effects of dose rate in the tested continuous fields produced by the X-ray generator in  
509 laboratory conditions were not significant, considering the IEC standard requirements of  $\pm 2\%$   
510 (IEC, 1997). All relative responses were between 0.99 and 1.01 for both standard RQR8 and non-  
511 standard Veridic3 80AlCu beam qualities. Considering the measurement uncertainty of 1%, these  
512 values are not significantly different from unity. However, it should be noted that tube current  
513 ranging only up to about 25 mA (continuous) were used, due to technical limitation of the X-ray  
514 generator, while values up to about 1000 mA (pulsed) can be encountered in practice (for  
515 instance, Farah et al., 2015).

516 The presented results are in good agreement with similar studies (Martin et al., 2007, Hourdakias  
517 et al., 2010) that confirmed that different irradiation conditions, acquisition modes (radiographic  
518 or fluoroscopic), air kerma rate values, as well as the dosimeter's operational mode (integrating  
519 or dose rate) did not affect the response of dosimeters significantly.

520 The energy dependence of the LiF:Mg,Cu,P is the dominant source of measurement uncertainty  
521 of skin dose measurements. Therefore, it is important to choose an appropriate highly filtered  
522 radiation quality, characteristic for interventional procedures, in order to calibrate the system.  
523 From the present work, an incorrect radiation quality can cause an under- or over-estimation of  
524 the dose by 15%. However, without specific knowledge of the radiation qualities used in  
525 interventional procedures assuming a uniform distribution covering the radiation quality energies  
526 used in this work, would result in 5% standard deviation of the energy response. The influence of  
527 the backscattered radiation in interventional procedures is not taken into account when estimating  
528 the before-mentioned standard deviation. However, the uncertainty component caused by  
529 backscattered radiation is limited, owing to a limited decrease in mean energy by 6-17%  
530 compared to the incident beam (Aoki and Koyama, 2002) and no more than 80% increase in the  
531 primary beam dose at the entrance surface (usually 30 to 40%) for various field sizes and photon  
532 energies encountered in interventional procedures (Benmakhlouf et al., 2013).

533 Besides the energy dependence, angular dependence of LiF:Mg,Cu,P response is a major  
534 contributor to the measurement uncertainty, with under-response up to 10% for perpendicular  
535 exposure of dosimeters. Owing to the various angulations of the X-ray source during  
536 interventional procedures, passive dosimeters can be irradiated from multiple directions, resulting  
537 in a uniform distribution of angle of incidence, and an expanded uncertainty of 4%.

538 In order to limit the uncertainty associated with the energy response of thermoluminescent  
539 dosimeters, calibration of the passive dosimetry system should be performed in a beam quality

540 which results in the smallest extent of relative response. According to the data presented in Fig.  
541 10, the use of Veridic1 80Al and Veridic4 120AlCu radiation qualities for system calibration  
542 would lead to systematic underestimation or overestimation of the dose, respectively. On the  
543 other hand, relative responses for calibration radiation qualities RQR8, Veridic2 120Al and  
544 Veridic3 80AlCu are spread around unity, i.e. these qualities appear to be more adequate for  
545 passive dosimetry system calibration.

546 The dose rate dependence of LiF:Mg,Cu,P variation is between -1% and +2% over the whole  
547 dose rate range, based on the average TLD response (calculated for a sample of three dosimeters  
548 for each dose rate value). Considering the inherent measurement uncertainty of the TLDs, these  
549 results are not significantly different from unity. Again, it should not be overlooked that tube  
550 current ranging only up to about 25 mA (continuous) were used, while values up to about  
551 1000 mA (pulsed) can be encountered in practice.

552 This study is first to our knowledge, that investigated the performance of diagnostic dosimeters in  
553 radiation qualities typical for interventional procedures, following essential principle of  
554 metrological traceability. The results of this study revealed that modern solid-state dosimeters  
555 and TLDs have good performance in a range of irradiation conditions, including non-standard  
556 conditions typical for clinical environment.

## 557 5. Conclusion

558 The results of testing of two types of dosimeters commonly used in clinical practice in diagnostic  
559 and interventional radiology are presented in this work. The tests included investigation of the  
560 energy dependence, angular dependence and linearity of the dosimeter response. Solid-state  
561 dosimeters containing single or multiple detector elements showed excellent energy dependence  
562 and linearity. Relative response normalized to the standard RQR8 radiation quality was within

563  $\pm 4\%$  for all dosimeters. Deviations from linearity were not significant for any of the tested solid  
564 state dosimeters. Angular dependence tests have shown that the tested single element detector  
565 meets the standard requirements even outside of the minimum rated range, up to  $30^\circ$ . However,  
566 multiple element detectors have rapidly decreasing response with increasing angle of incidence  
567 and can be used only in perpendicular geometry. TLDs have shown satisfactory linearity in the  
568 range of  $\pm 3\%$  from the reference dose rate value, and the relative angular response within  $\pm 4\%$   
569 over a wide range of angles of incidence up to  $60^\circ$ . Energy dependence of the TLD response was  
570 in good agreement with previous studies (Olko et al, 2002).

571 In order to minimize the measurement uncertainty, traceable dosimeter calibration and testing  
572 should be performed in the radiation beam qualities which correspond to the radiation beams  
573 used in fluoroscopically guided interventional procedures in clinical conditions, in addition to the  
574 standard radiation beam qualities used for regular calibration of the QC equipment (IEC, 2005).  
575 Selecting appropriate radiation quality for passive dosimetry system calibration performed in this  
576 work will contribute to the decrease of the measurement uncertainty.  
577 By comparing the energy response of QC dosimeters in standard RQR8 and non-standard  
578 radiation fields it can be concluded that for some dosimeter types the deviation introduced by  
579 non-standard qualities can influence the dosimeter indication up to  $\pm 4\%$ , in the range of beam  
580 qualities that can be generated during a single interventional procedure, due to its dynamic nature  
581 and rapid change of X-ray tube voltage and filtration. This effect is more pronounced for certain  
582 types of dosimeters. In addition, due to the generally lower air kerma rates with non-standard  
583 beam qualities, accuracy of dose measurement can also be affected by the dose rate dependence  
584 of certain types of dosimeters. Therefore, examination of dosimeter response and performance in  
585 non-standard beams is recommended. Furthermore, the user should be aware of the properties of



586 the dosimeters used, in order to use the instrument correctly and control the measurement  
587 uncertainty.

588

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## 595 Disclaimer

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## 750 Figure captions

751 *Figure 1. Schematic representation of the spectrometer positioning in the X-ray field (left), and the*  
752 *experimental set-up used for the X-ray spectra measurements, emitted by the CEA X-ray generator (right).*

753 *Figure 2. Energy spectra for the IC radiation qualities and the standard RQR8 radiation quality*

754 *Figure 3. Relative response of four solid-state detectors measured for one standard (reference) radiation*  
755 *quality (RQR8) under laboratory conditions, and four non-standard radiation qualities which correspond*  
756 *to clinical conditions (Veridic1 80Al, Veridic2 120Al, Veridic3 80AlCu and Veridic4 120AlCu).*

757 *Figure 4. The angular dependence test results of four solid-state detectors for: a) the reference standard*  
758 *RQR8 radiation quality; b) the non-standard Veridic3 80AlCu radiation quality - in the angle range from*  
759 *0° to ±90°. The relative angular response was normalized to absolute response value for 0°.*

760 *Figure 5. The linearity test results for four solid-state detectors in the air-kerma rate range determined by*  
761 *the X-ray tube current range from 3 mA to 25 mA, for: a) the reference standard RQR8 radiation quality;*  
762 *b) the non-standard Veridic3 80AlCu radiation quality. The relative response was normalized to the*  
763 *absolute response value at 9 mA X-ray tube current.*

764 *Figure 6. Dose rate dependence of the LiF:Mg,Cu,P response for the RQR8 radiation quality, normalized*  
765 *to the value measured at 5 mGy min<sup>-1</sup>. Each data point represents average response of three dosimeters,*  
766 *and the error bars represent standard deviation of the average response.*

767 *Figure 7. Angular dependence of LiF:Mg,Cu,P response normalized to the value at 0°. Combined energy*  
768 *and angular dependence was tested for RQR8 and Veridic2 120Al radiation qualities. Each data point*  
769 *represents average response of three dosimeters, and the error bars represent standard deviation of the*  
770 *average response.*

771 *Figure 8. Angular dependence of LiF:Mg,Cu,P response normalized to the value at 0°. Combined energy*  
772 *and angular dependence was tested for RQR8 and Veridic3 80AlCu radiation qualities, including*



773 *symmetry of the angular response. Each data point represents average response of three dosimeters, and*  
774 *the error bars represent standard deviation of the average response.*

775 *Figure 9. Energy dependence of the LiF:Mg,Cu,P response comparison from various studies (Olko et al.,*  
776 *2002).*

777 *Figure 10. Energy dependence of the LiF:Mg,Cu,P response for the system calibrated for RQR8, Veridic1*  
778 *80Al, Veridic3 80AlCu, Veridic2 120Al and Veridic4 120AlCu, respectively.*

779

780 **Tables**

781 *Table 1. Technical specifications of the tested QC solid-state dosimeters.*

782 *Table 2. Properties of radiation qualities used for performance testing of solid-state and*  
783 *thermoluminescent dosimeters. Calibration coefficients of the Exradin A600 ionisation chamber used for*  
784 *reference air kerma values in the QC dosimeter tests are provided in the rightmost column.*

785