

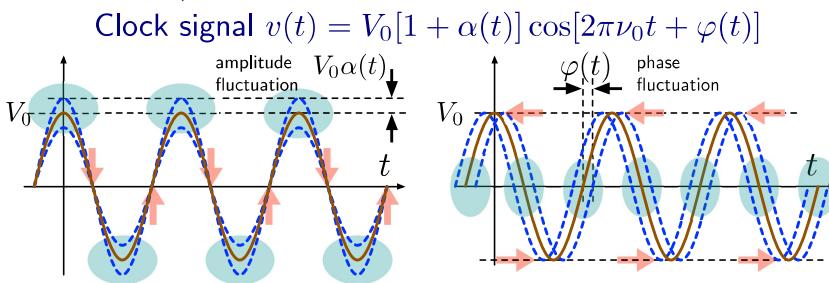
Enrico's Chart of Phase Noise and Two-Sample Variances



Enrico Rubiola - <http://rubiola.org>
 European Frequency and Time Seminar - <http://efts.eu>
 Oscillator Instability Measurement Platform <http://oscillator-imp.com>



Thanks to FIRST-TF <https://first-tf.com>



Boldface notation

total = nominal + fluctuation
 $\varphi(t) = 2\pi\nu_0 t + \varphi(t)$ phase
 $\nu(t) = \nu_0 + (\Delta\nu)(t)$ frequency
 $x(t) = t + x(t)$ time
 $y(t) = 1 + y(t)$ fractional frequency

Phase noise spectrum

Definition

$S_\varphi(f)$ [rad²/Hz] is the one-sided PSD ($f > 0$) of $\varphi(t)$
 $S_\varphi(f) = 2\mathcal{F}\{\mathbb{E}\{\varphi(t)\varphi(t+\tau)\}\}, f > 0$

Evaluation

$$S_\varphi(f) = \frac{2}{T} \langle \Phi_T(f) \Phi_T^*(f) \rangle_m$$

avg on m data, $\Phi_T(f)$ = DFT of $\varphi(t)$ truncated on T

Usage

most often, 'phase noise' refers to $\mathcal{L}(f)$

Only $10\log_{10}[\mathcal{L}(f)]$ is used, given in dBc/Hz

Definition: $\mathcal{L}(f) = \frac{1}{2}S_\varphi(f)$ [the unit c/Hz never used]

Literally, the unit 'c' is a squared angle, $\sqrt{c} = \sqrt{2}$ rad $\approx 81^\circ$

Two-sample (Allan-like) variances

Definition

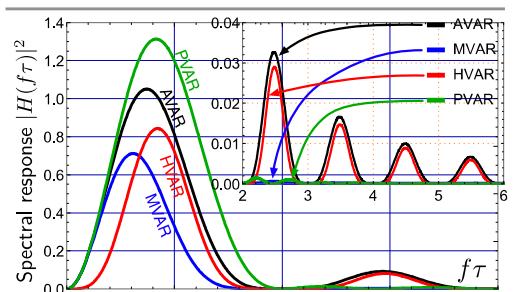
$$\sigma_y^2(\tau) = \mathbb{E}\left\{\frac{1}{2}[\bar{y}_2 - \bar{y}_1]^2\right\} \quad y(t) \rightarrow \bar{y} \text{ averaged over } \tau$$

\bar{y}_2 and \bar{y}_1 are contiguous

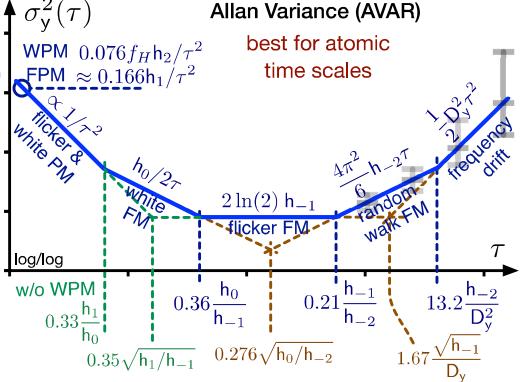
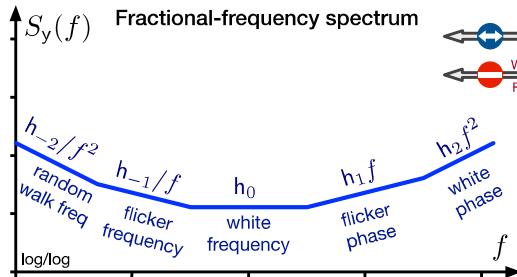
Bare mean \bar{y} \rightarrow Allan variance AVAR
 Weighted averages \rightarrow MVAR, PVAR, etc.

Evaluation

$$\sigma_y^2(\tau) = \frac{1}{2(M-1)} \sum_{k=1}^{M-1} [\bar{y}_{k+1} - \bar{y}_k]^2 \quad M \text{ contiguous samples of } \bar{y}$$



Frequency fluctuation PSD \leftrightarrow Allan Variance



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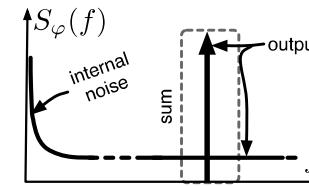
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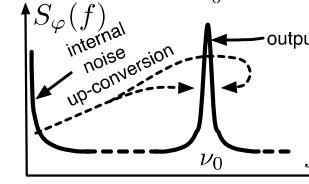
Last update

January 19, 2022

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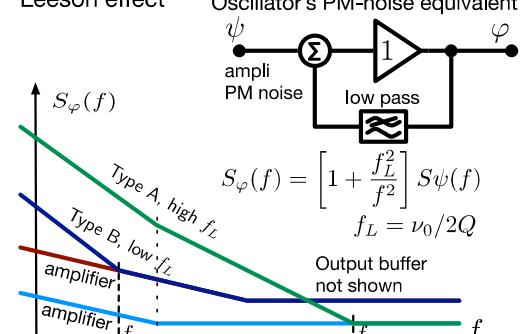


Additive Noise
 RF noise added to the carrier
 Statistically independent AM & PM

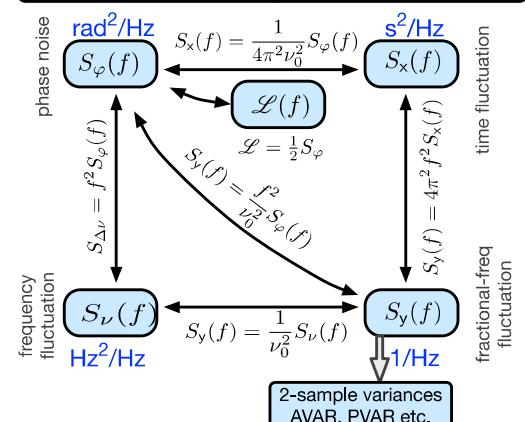
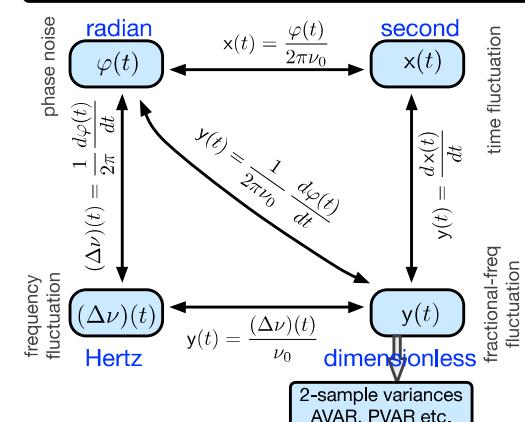


Parametric Noise
 Near-dc noise modulates the carrier
 AM & PM related and narrowband

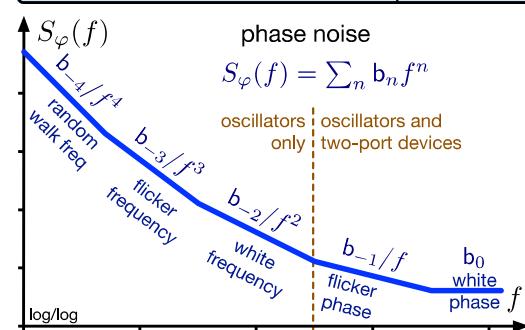
Leeson effect



Frequency Domain

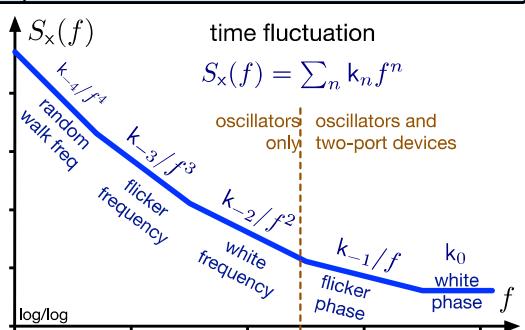


Spectra and Polynomial Law



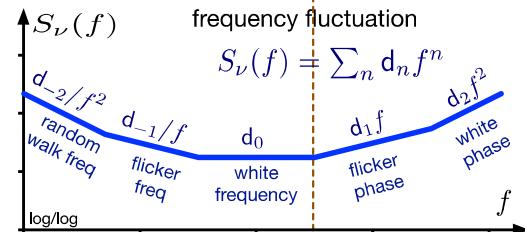
$$S_\varphi(f) = \sum_n b_n f^n$$

oscillators only
two-port devices

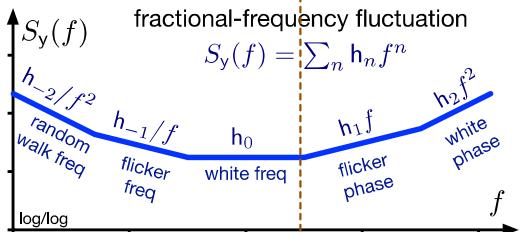


$$S_x(f) = \sum_n k_n f^n$$

oscillators only
two-port devices



$$S_\nu(f) = \sum_n d_n f^n$$



$$S_y(f) = \sum_n h_n f^n$$

Enrico's Chart of Phase Noise and Two-Sample Variances

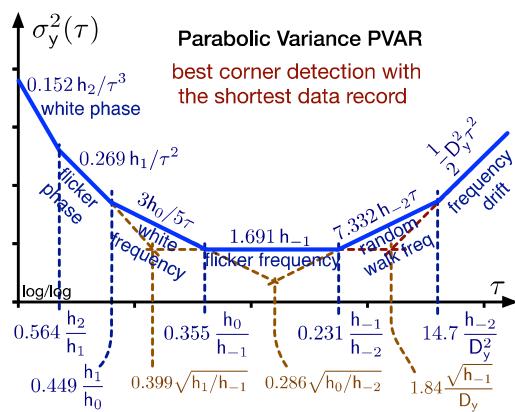


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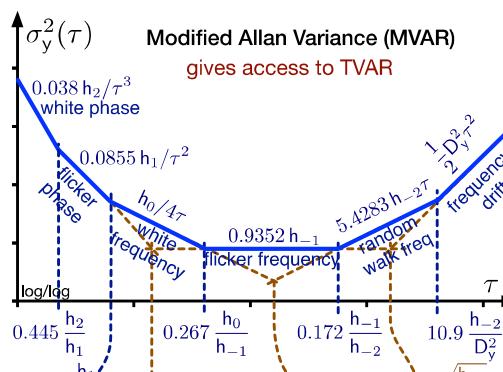


Frequency Counter		Wavelet Variance	
$\bar{y}(\tau) = \int_{\mathbb{R}} y(t) w(t; \tau) dt$		$\sigma_y^2(\tau) = \mathbb{E}\left\{\frac{1}{2}\left[\bar{y}_2 - \bar{y}_1\right]^2\right\} = \mathbb{E}\left\{\int_{\mathbb{R}} [y(t) w(t; \tau)]^2 dt\right\}$	
type of frequency counter	II		AVAR w_A
	Δ		MVAR w_M
	Ω		PVAR w_P
	(Δ)		HVAR w_H
<small>Note: this representation is only for theoretical purposes There are no commercial Δ counters</small>		<small>Note: the wavelet representation hides the second difference in the evaluation of the variance</small>	

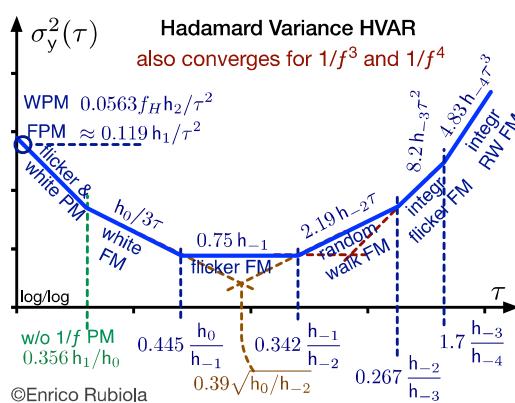
Other Two-Sample Variances



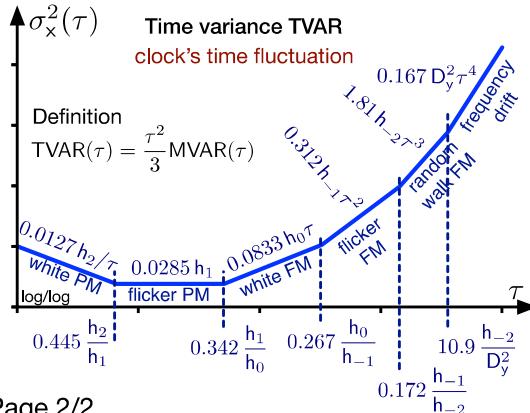
Parabolic Variance PVAR
best corner detection with the shortest data record



Modified Allan Variance (MVAR)
gives access to TVAR



Hadamard Variance HVAR
also converges for $1/f^3$ and $1/f^4$



Time variance TVAR
clock's time fluctuation

Spectra to Variances Conversion

noise type	$S_y(f)$	AVAR $\sigma_y^2(\tau)$	MVAR $M_{\sigma_y^2}(\tau)$	HVAR $H_{\sigma_y^2}(\tau)$	PVAR $P_{\sigma_y^2}(\tau)$	TVAR $T_{\sigma_x^2}(\tau)$
white PM	$h_2 f^2$	$\frac{3f_H}{4\pi^2} \frac{h_2}{\tau^2}$	$\frac{3}{8\pi^2} \frac{h_2}{\tau^3}$	$\frac{5f_H}{9\pi^2} \frac{h_2}{\tau^2}$	$\frac{3}{2\pi^2} \frac{h_2}{\tau^3}$	$\frac{1}{8\pi^2} \frac{h_2}{\tau}$
flicker PM	$h_1 f$	$\frac{3\gamma - \ln 2 + 3 \ln(2\pi f_H \tau)}{4\pi^2} \frac{h_1}{\tau^2}$ $[3\gamma - \ln 2 + 3 \ln(2\pi f_H \tau)]/4\pi^2 = 0.166$	$\frac{(24 \ln 2 - 9 \ln 3) h_1}{8\pi^2} \frac{h_1}{\tau^2}$	$\simeq \frac{5[\gamma + \ln(\sqrt[4]{48\pi f_H \tau})] h_1}{9\pi^2} \frac{h_1}{\tau^2}$ $5[\gamma + \ln(\sqrt[4]{48\pi})]/9\pi^2 = 0.1187$	$\frac{3 [\ln(16) - 1] h_1}{2\pi^2} \frac{h_1}{\tau^2}$	$\frac{(8 \ln 2 - 3 \ln 3)}{8\pi^2} \frac{h_1}{\tau}$
white FM	h_0	$\frac{1}{4} \frac{h_0}{\tau}$	$\frac{1}{3} \frac{h_0}{\tau}$	$\frac{1}{3} \frac{h_0}{\tau}$	$\frac{3}{5} \frac{h_0}{\tau}$	$\frac{1}{12} \frac{h_0 \tau}{h_1}$
flicker FM	$h_{-1} f^{-1}$	$2 \ln(2) h_{-1}$ $1.386 h_{-1}$	$\frac{8 \ln 2 - 32 \ln 2}{8} h_{-1}$ $0.935 h_{-1}$	$\frac{8 \ln 2 - 3 \ln 3}{3} h_{-1}$ $0.750 h_{-1}$	$\frac{2 [7 - \ln(16)]}{5} h_{-1}$ $1.691 h_{-1}$	$\frac{27 \ln 3 - 32 \ln 2}{24} h_{-1} \tau^2$ $0.312 h_{-1} \tau^2$
random walk FM	$h_{-2} f^{-2}$	$\frac{2\pi^2}{3} h_{-2} \tau$ $6.58 h_{-2} \tau$	$\frac{11\pi^2}{20} h_{-2} \tau$ $5.43 h_{-2} \tau$	$\frac{2\pi^2}{9} h_{-2} \tau$ $2.19 h_{-2} \tau$	$\frac{28\pi^2}{35} h_{-2} \tau$ $7.33 h_{-2} \tau$	$\frac{11\pi^2}{60} h_{-2} \tau^3$ $1.81 h_{-2} \tau^3$
integrated flicker FM	$h_{-3} f^{-3}$	not converging	not converging	$\pi^2 [27 \ln(3) - 32 \ln(2)] h_{-3} \tau^2$ $8.205 h_{-3} \tau^2$	not converging	not converging
integrated RW FM	$h_{-4} f^{-4}$	not converging	not converging	$\frac{44\pi^2}{90} h_{-4} \tau^3$ $4.825 h_{-4} \tau^3$	not converging	not converging
linear drift D_y		$\frac{1}{2} D_y^2 \tau^2$	0	$\frac{1}{2} D_y^2 \tau^2$	$\frac{1}{6} D_y^2 \tau^4$	$\frac{\tau^2}{3} \frac{2 \sin^6(\pi f \tau)}{(\pi f \tau)^4}$
spectral response $ H(\theta) ^2$, $\theta = f \tau$		$\frac{2 \sin^4(\theta)}{\theta^2}$	$\frac{16 \sin^6(\theta)}{9\theta^2}$	$\frac{9 [2 \sin^2(\theta) - \theta \sin(2\theta)]^2}{2\theta^6}$	$\frac{\tau^2}{3} \frac{2 \sin^6(\pi f \tau)}{(\pi f \tau)^4}$	$\frac{\tau^2}{3} \frac{M_{\sigma_y^2}(\tau)}{M_{\sigma_y^2}(\tau)}$

$$\text{The cutoff frequency } f_H \text{ is explicit in AVAR. In MVAR, PVAR and TVAR, } f_H \text{ is implicit in sampling frequency } 1/\tau_0.$$

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