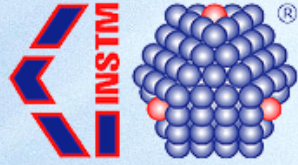




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# A study on the chemical and microstructural optimization of the Ti-48-2-2 alloy processed by Electron Beam Melting

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<sup>4</sup> INSTM, Italy

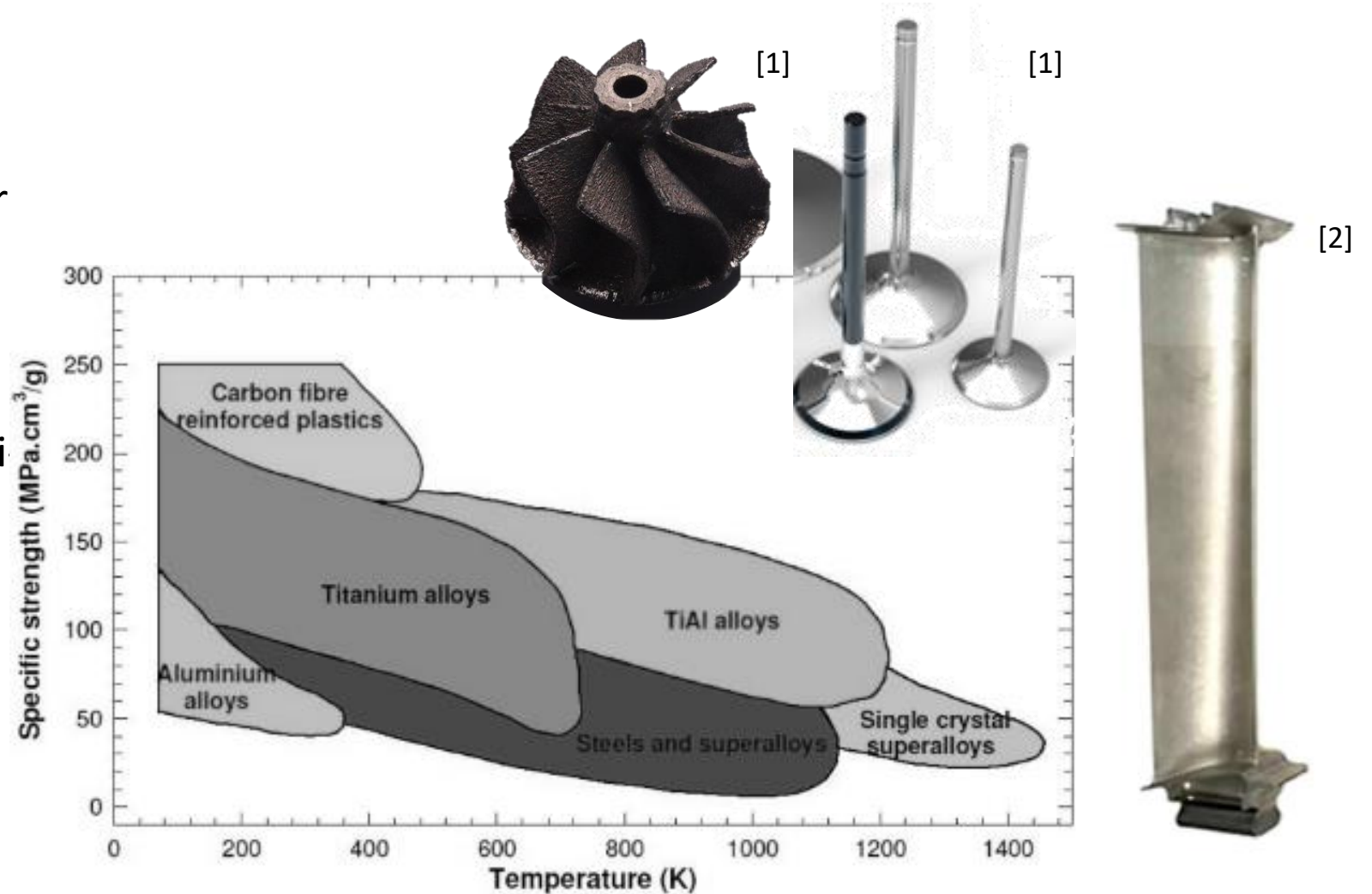


**This project has received funding from the Clean Sky 2 Joint Undertaking under the European Union's Horizon 2020 research and innovation programme under grant agreement No 821274".**

## Context

TiAl alloys are attractive materials for structural aerospace applications at high T in particular low pressure turbine blades:

- Specific strength comparable to Ni base superalloys
- $\gamma$ -TiAl 4 g/cm<sup>3</sup> vs 8 g/cm<sup>3</sup> Ni-base superalloys
- Good oxidation and corrosion resistance up to 750-800 °C

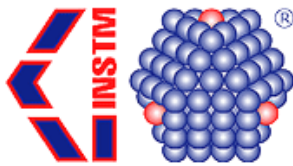


[1] Loria, Intermetallics-2001, "Quo vadis gamma titanium aluminide"

[2] Bewlay, Material at high temperature-2016, "TiAl alloys in commercial aircrafts engines"



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## AIM:

- Develop new **TiAl alloys** for EBM process for the production of the next generation of low pressure turbine (LPT) blades
- ❖ Modifications of the chemical composition with respect to the reference Ti-48Al-2Cr-2-Nb were investigated;
- ❖ Optimization of the EBM process parameters were done coupling experimental trials with the development of simulation tool;
- ❖ Full mechanical characterization of the new alloys and comparison with the reference Ti-48Al-2Cr-2-Nb alloy

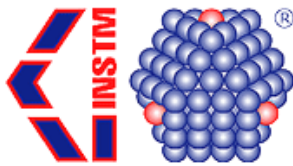


BUDGET 800.000 €



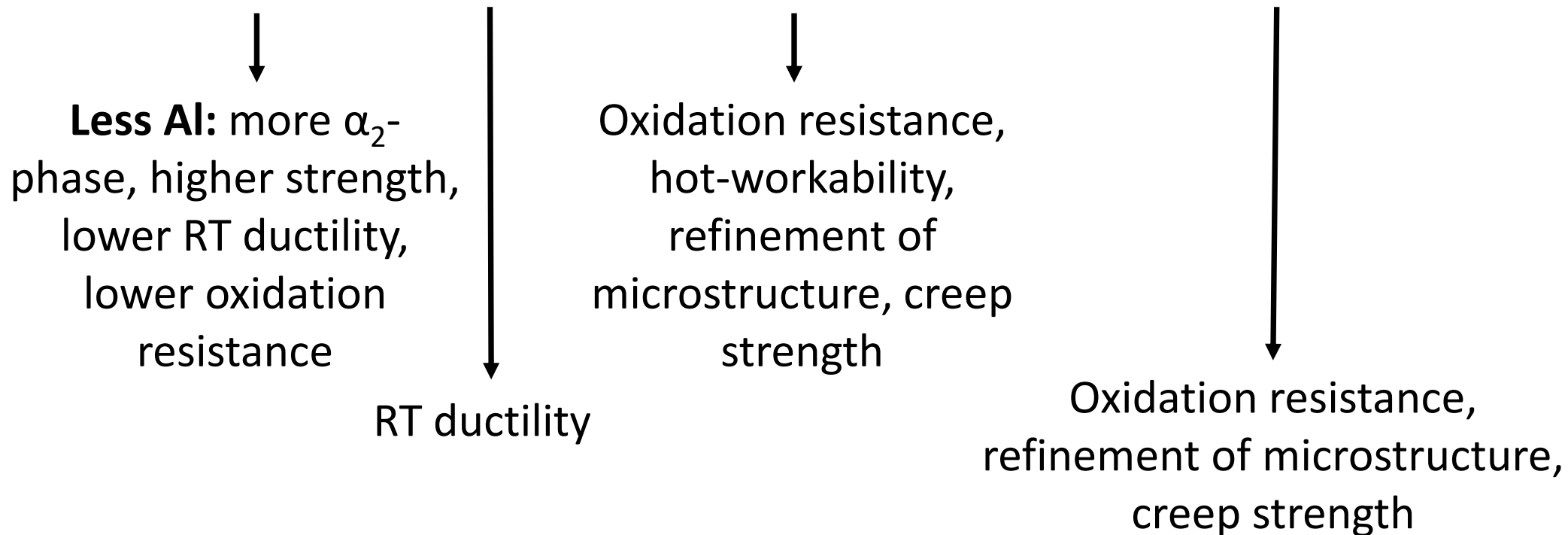


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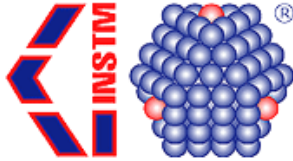
## Designing TiAl alloys for Electron Beam Melting

Ti-(42-48)Al-(0-4)Cr/Mn/V-(0-10)Nb/Ta/W/Mo-(0-2)Si/C/B





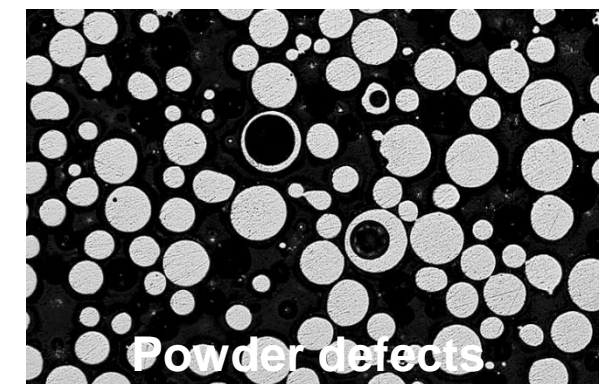
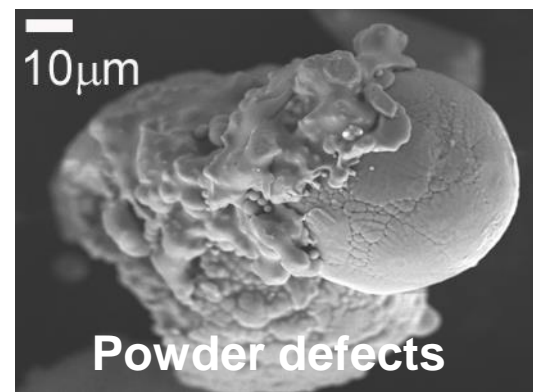
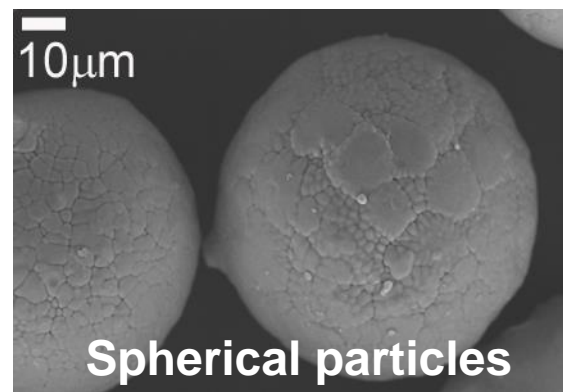
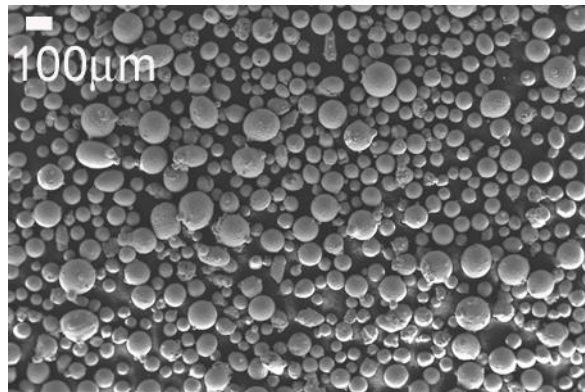
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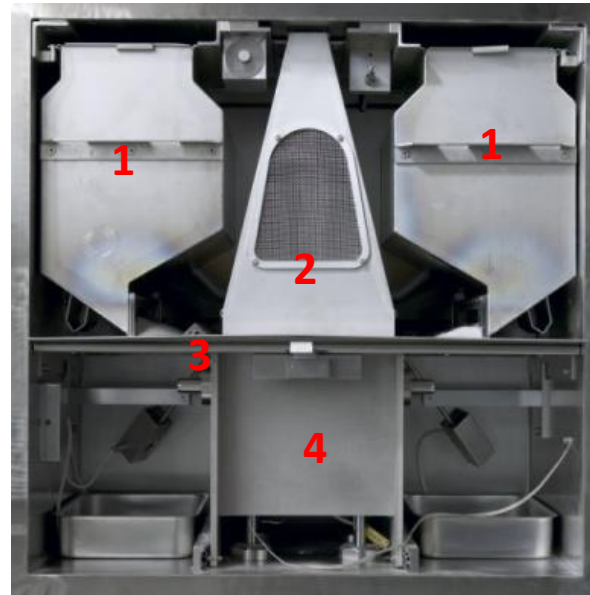
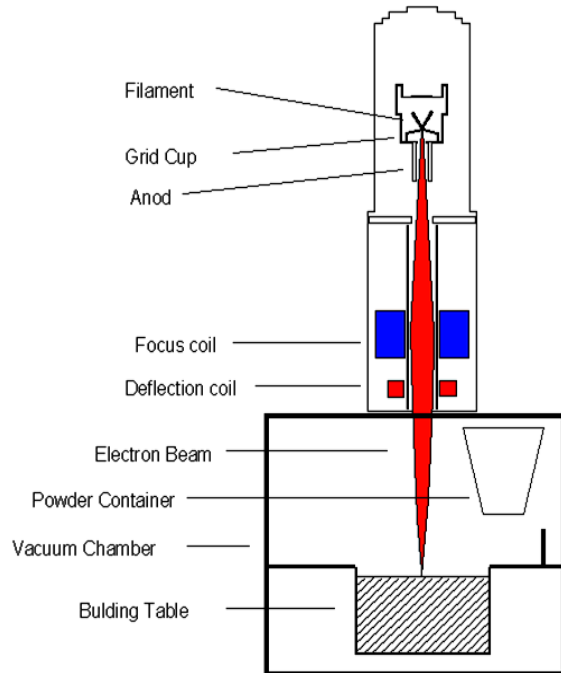
## Powder characteristics are a key parameter

Gas-atomized powder with specifications:

- Chemical composition (to be balanced the loss of evaporating elements)
- Mesh size
- Powder flowability
- Powder apparent density



## The EBM process:



- 1) Powder tanks
- 2) Electron Beam path
- 3) Rake for powder distribution on the building plate
- 4) Building plate which move down layer by layer



### Advantages:

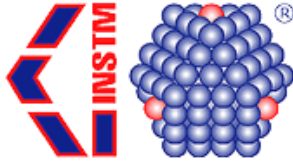
- freedom of design
- dense material with good material properties
- low material waste
- good productivity
- Possibility of preheating powder
- Vacuum melting process (no contaminations)

### Technical features:

- 6 kW electron beam
- High preheating: up to 1000-1100 °C
- Vacuum chamber:  $10^{-3}$  -  $10^{-5}$  mbar
- Approximate chamber dimension: 350x350x350 mm
- E-Beam rate: up to 8000 m/s
- Layer thickness: 70-200 micron
- Approximate build rate: 60 cm<sup>3</sup>/h

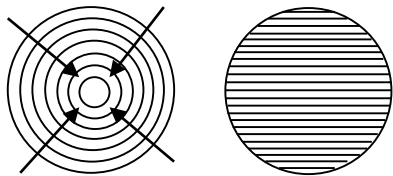
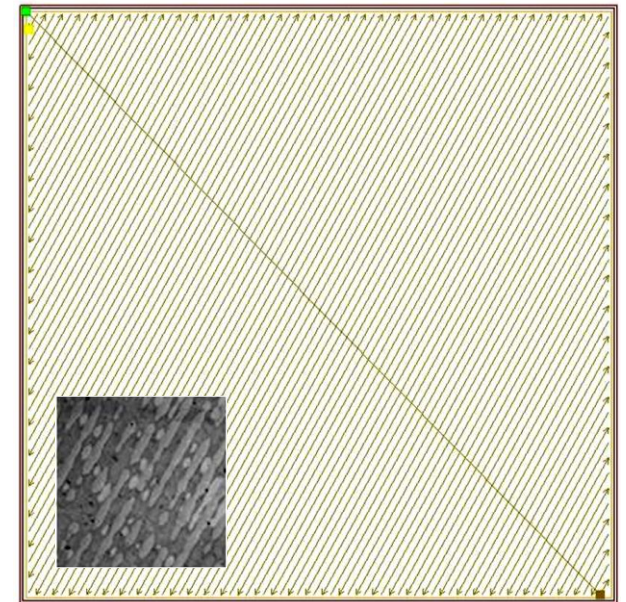
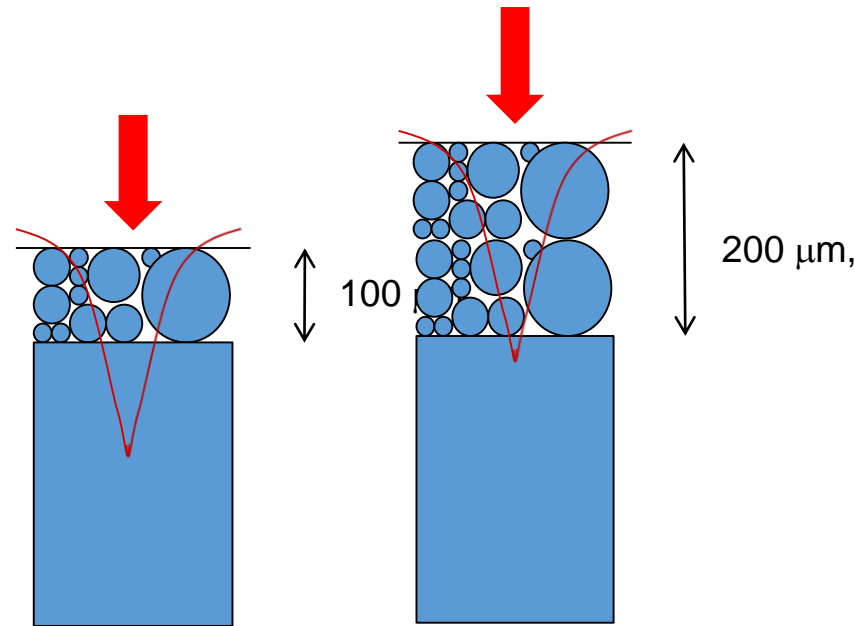


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There are a lot of EBM parameters that have to be optimized in order to produce defects free materials:

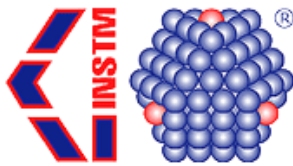
- Process power
- Powder layer thickness
- Scanning velocity
- Line offset
- Scanning strategy
- Preheating temperature



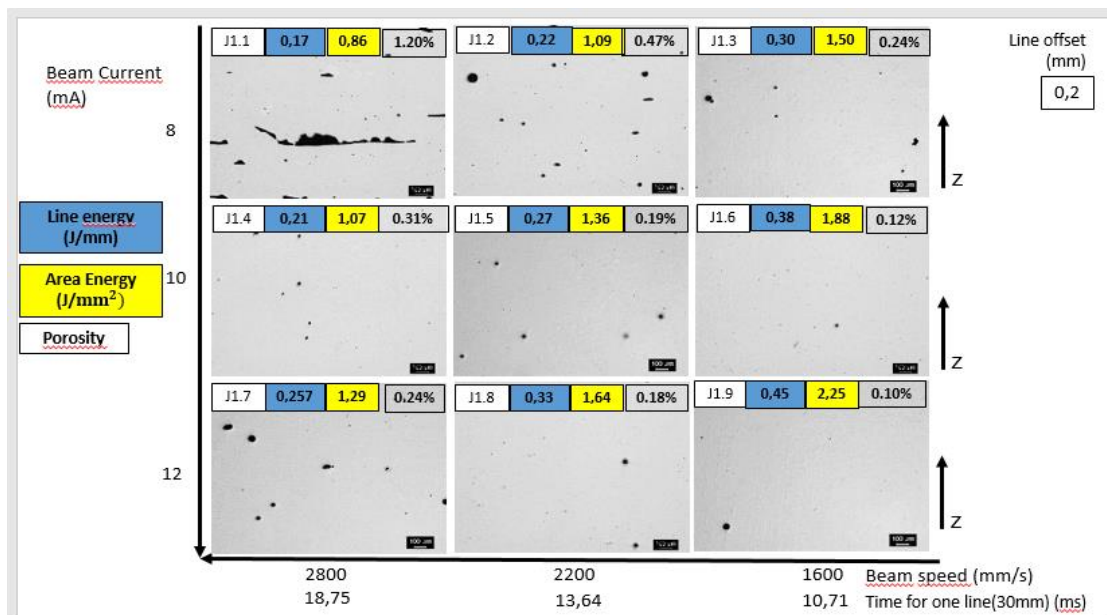
They affect: process productivity, residual defects, obtained microstructure



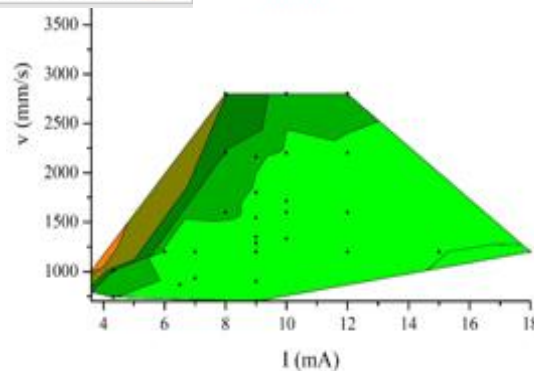
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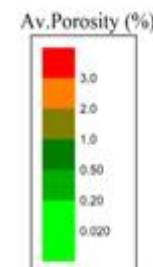
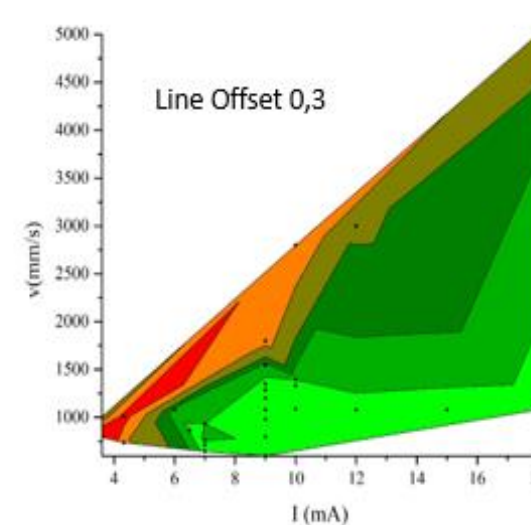
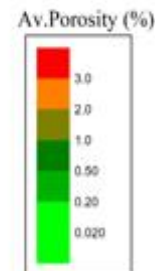
# Optimization of the process parameter for the reduction of the residual defects



Line Offset 0,2

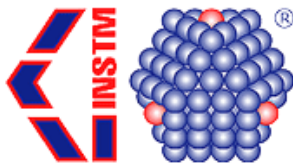


Porosity chart

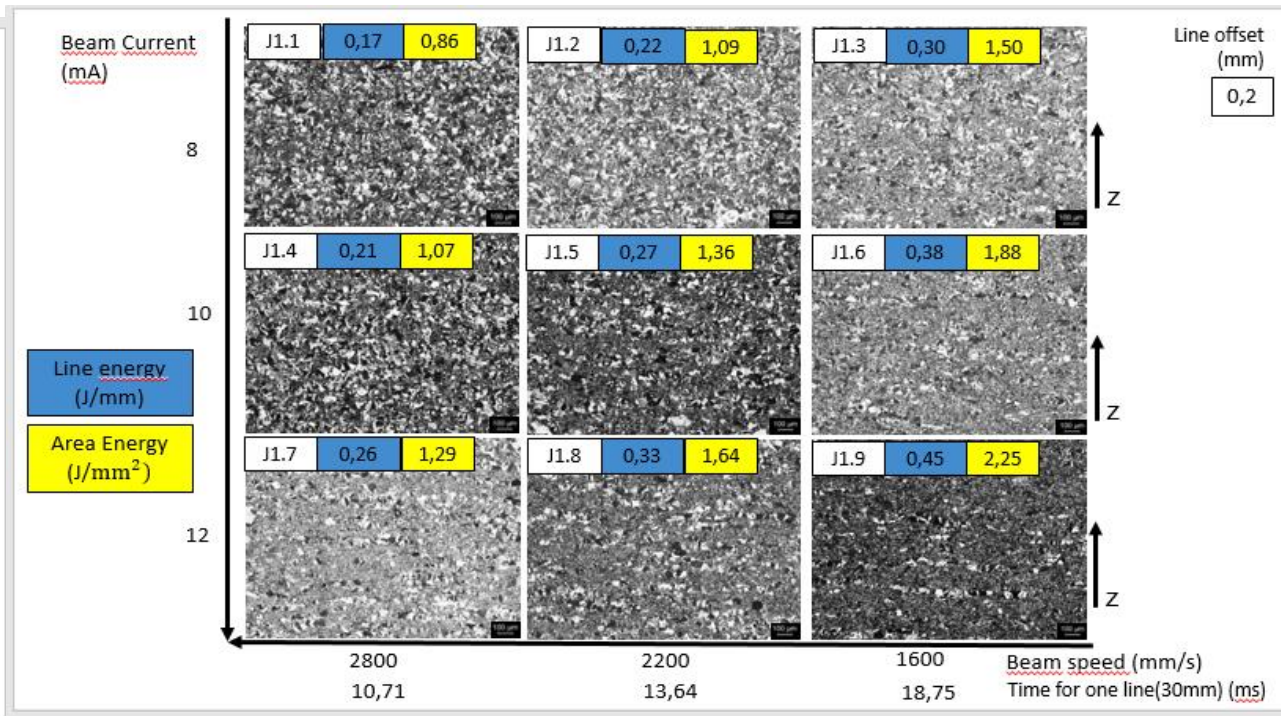
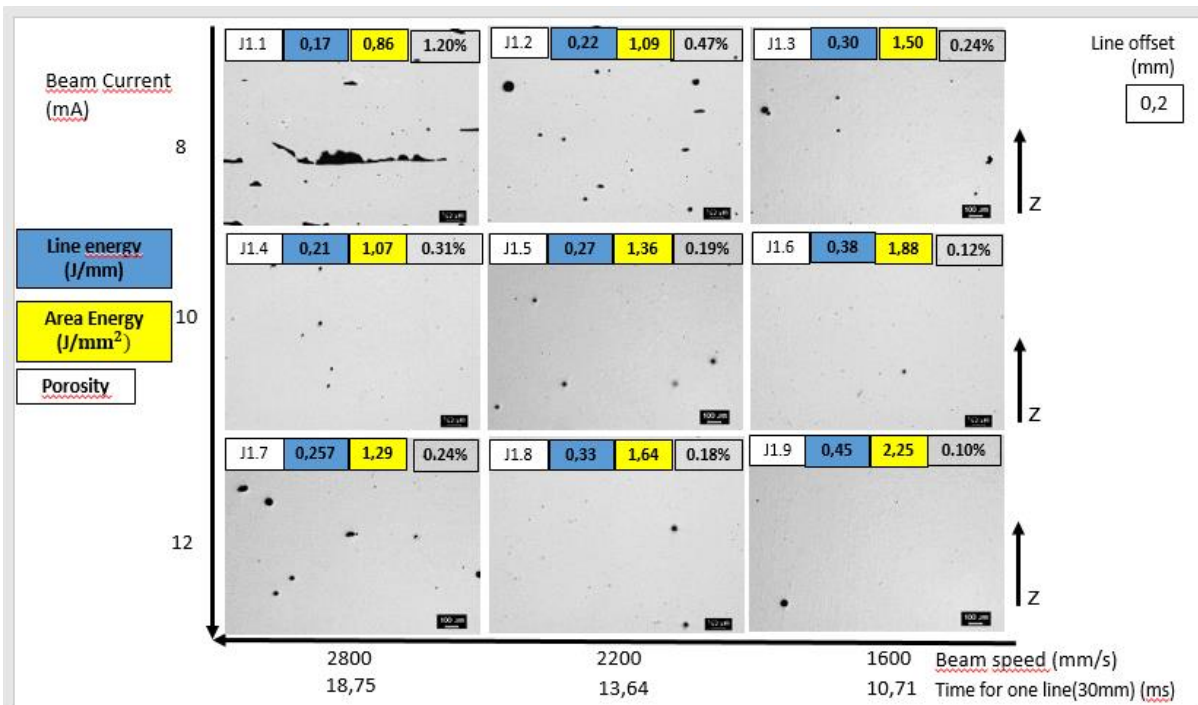




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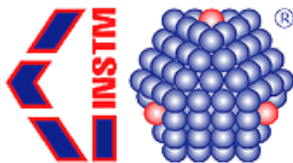


# Optimization of the process parameter for the improvement of the microstructure homogeneity

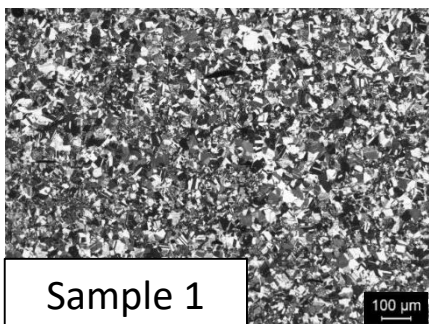
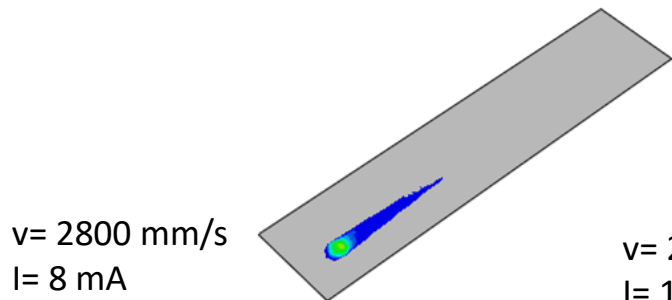
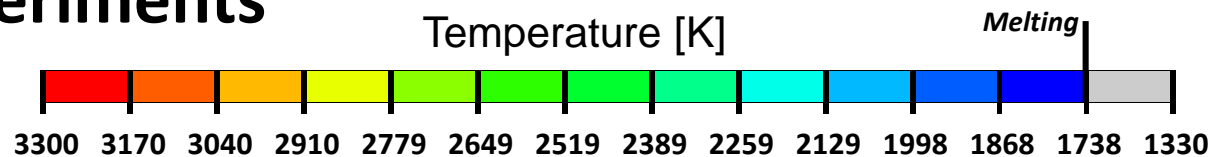




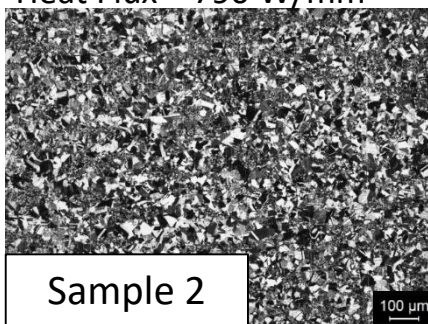
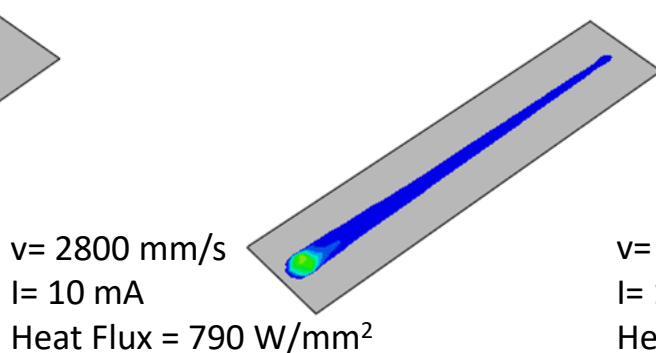
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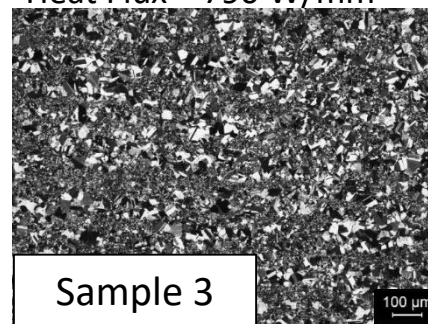
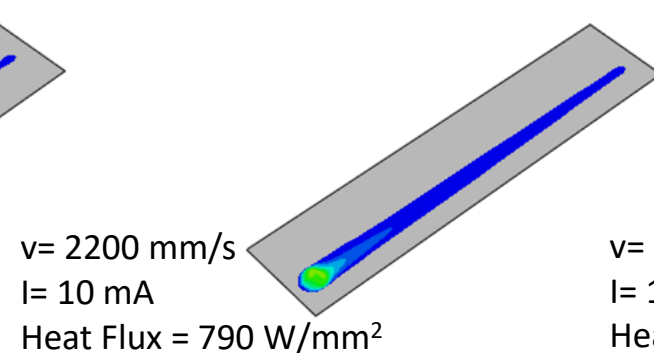
# Simulation and Experiments



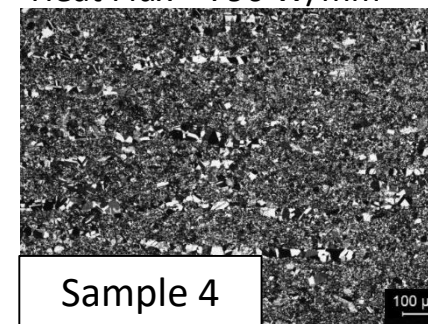
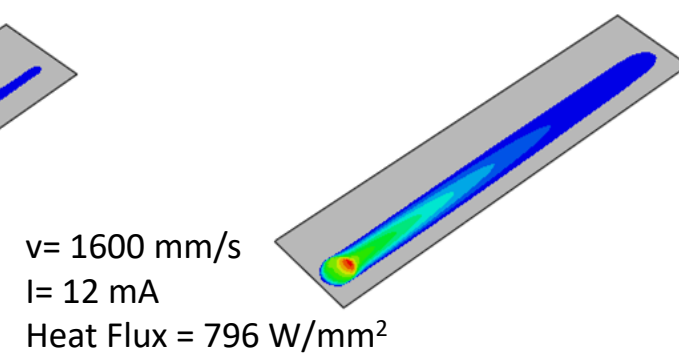
Line Energy =  $0.171 \text{ J/mm}$   
 Area Energy =  $0.86 \text{ J/mm}^2$



Line Energy =  $0.214 \text{ J/mm}$   
 Area Energy =  $1.07 \text{ J/mm}^2$

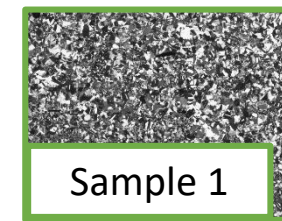
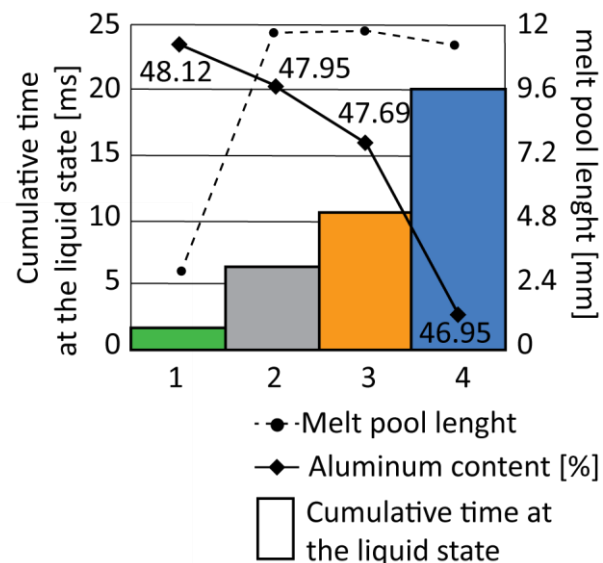
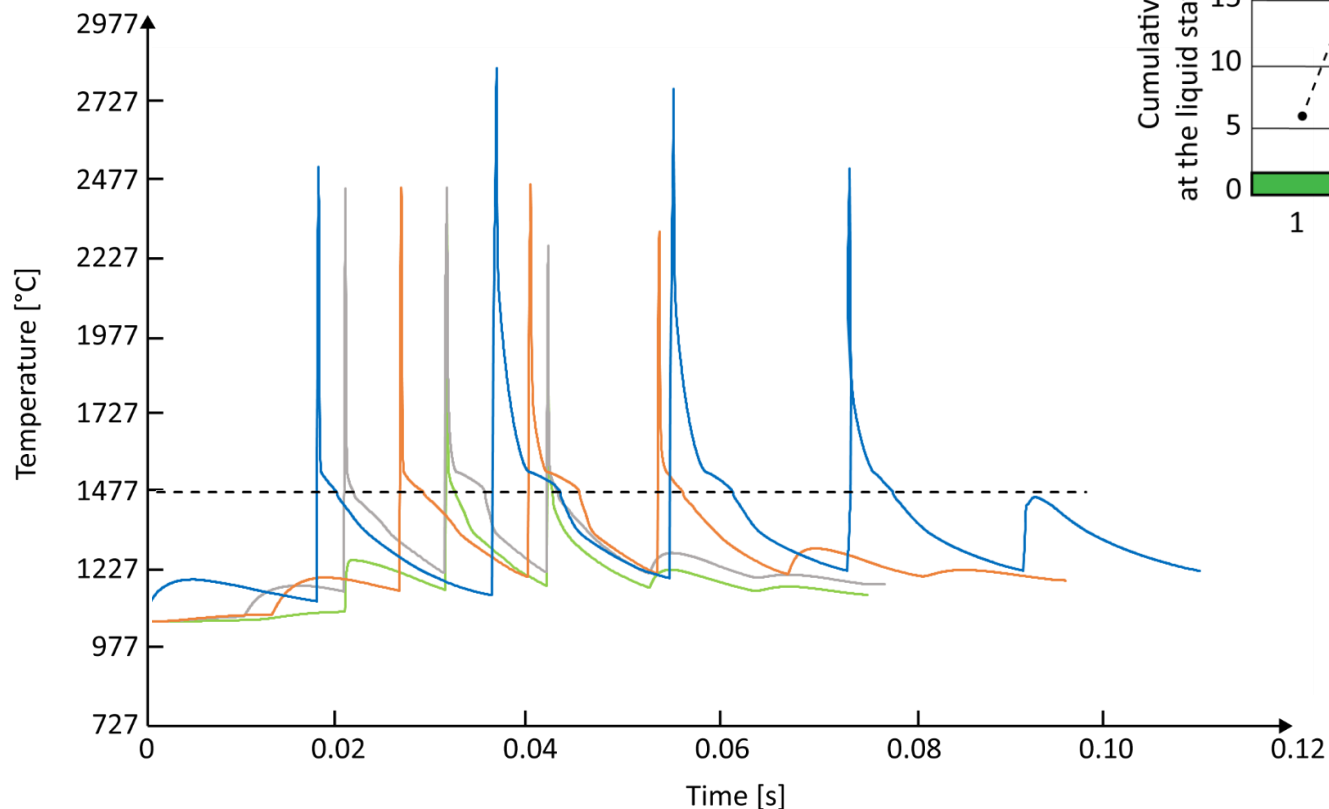


Line Energy =  $0.27 \text{ J/mm}$   
 Area Energy =  $1.36 \text{ J/mm}^2$



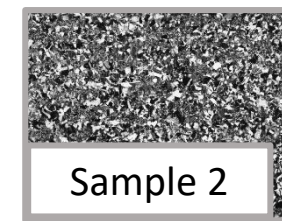
Line Energy =  $0.450 \text{ J/mm}$   
 Area Energy =  $2.25 \text{ J/mm}^2$

# Simulation and Experiments



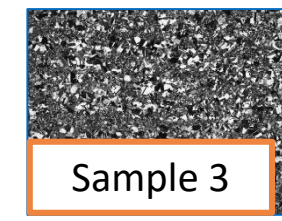
Sample 1

$v = 2800 \text{ mm/s}$   
 $I = 8 \text{ mA}$   
 Heat Flux =  $828 \text{ W/mm}^2$



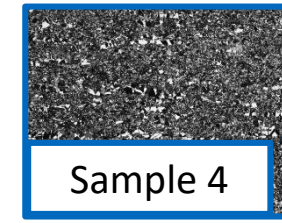
Sample 2

$v = 2800 \text{ mm/s}$   
 $I = 10 \text{ mA}$   
 Heat Flux =  $790 \text{ W/mm}^2$



Sample 3

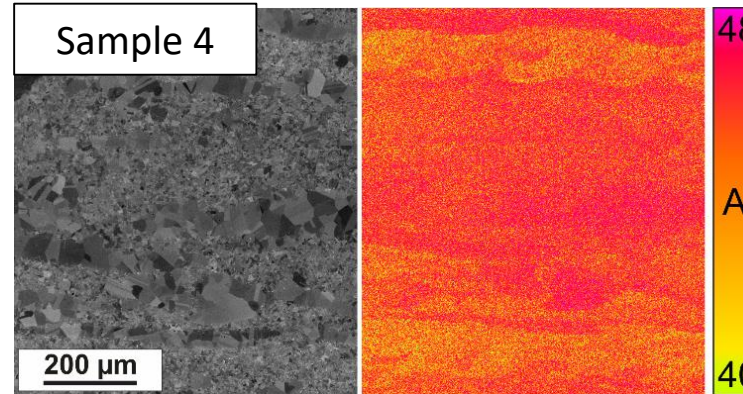
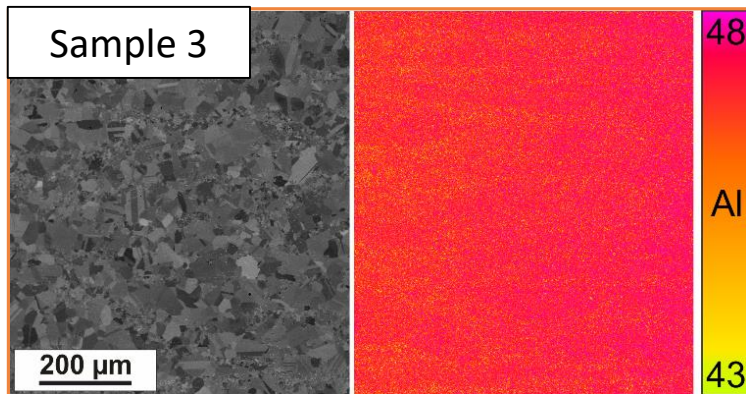
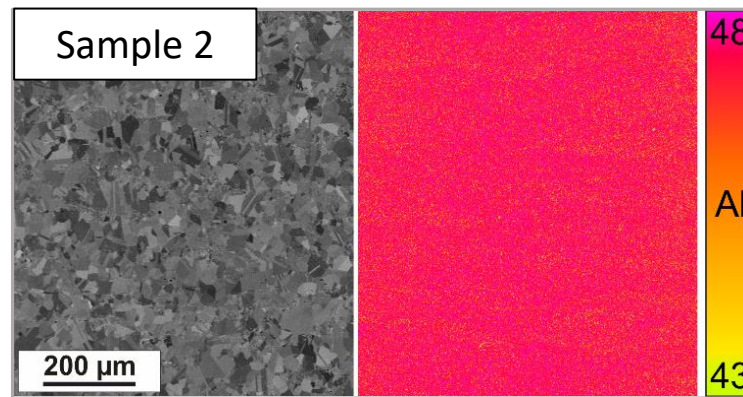
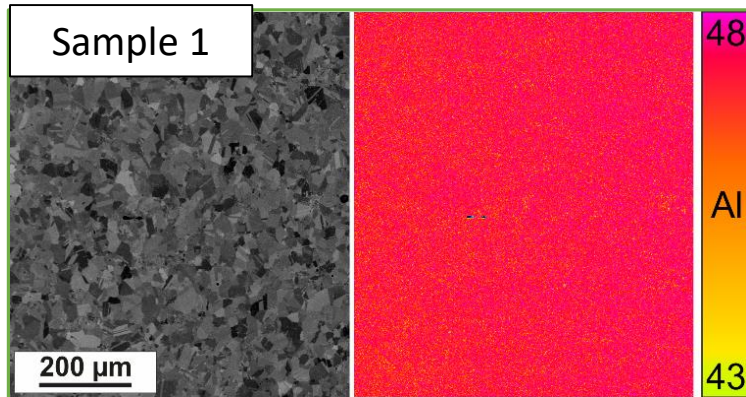
$v = 2200 \text{ mm/s}$   
 $I = 10 \text{ mA}$   
 Heat Flux =  $790 \text{ W/mm}^2$



Sample 4

$v = 1600 \text{ mm/s}$   
 $I = 12 \text{ mA}$   
 Heat Flux =  $796 \text{ W/mm}^2$

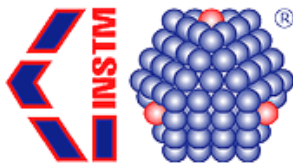
## Chemical homogeneity by electron probe micro analysis



- Chemical homogeneity and overall chemistry are a function of processing parameters due to evaporation.
- Inhomogeneous Al distributions might lead to banded microstructures after heat treatment.



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# Effects of the heat treatment on the microstructure

Sample 2

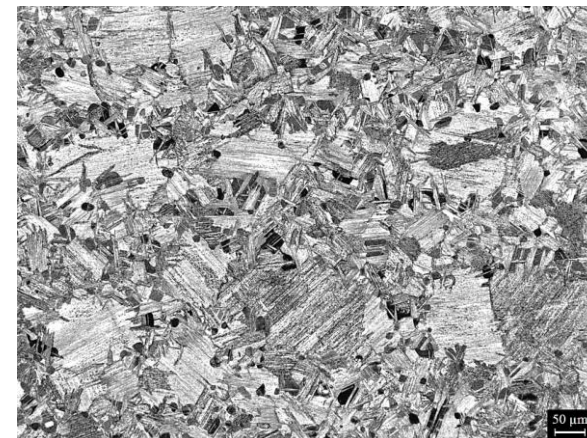
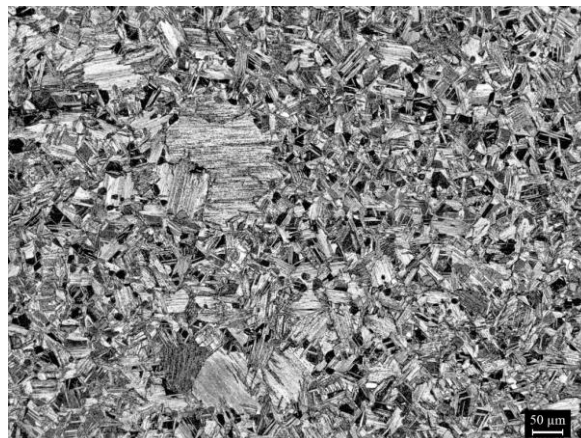
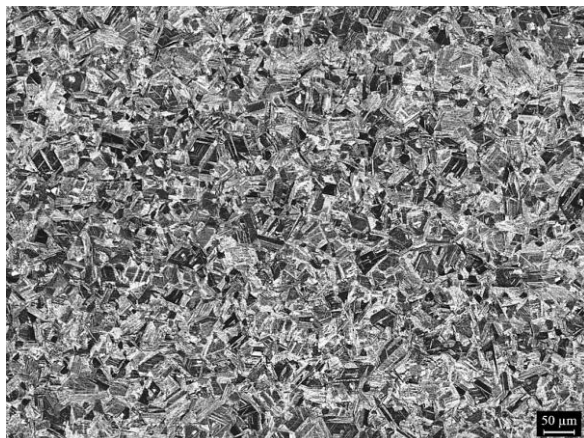
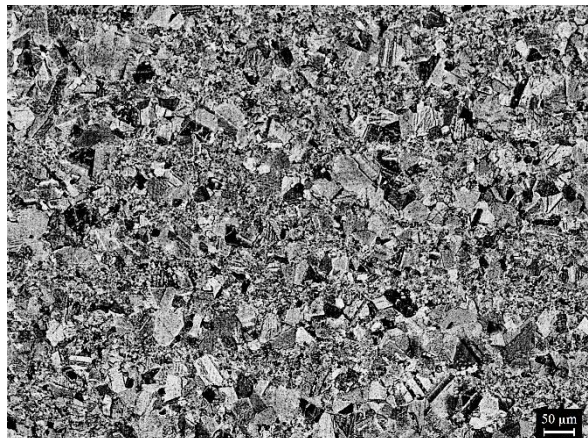
$v=2800\text{mm/s}$

$I=10\text{ mA}$

Heat Flux=  $790\text{ W/mm}^2$

Increased set point temperature during heat treatment

As-built

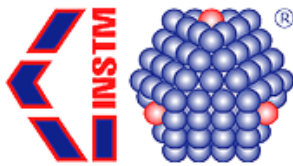




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## Effects of the heat treatment on the microstructure

As-built

After HT

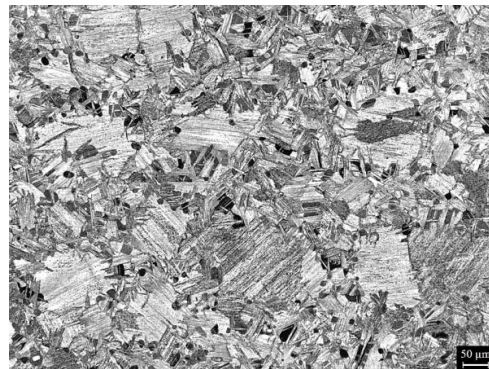
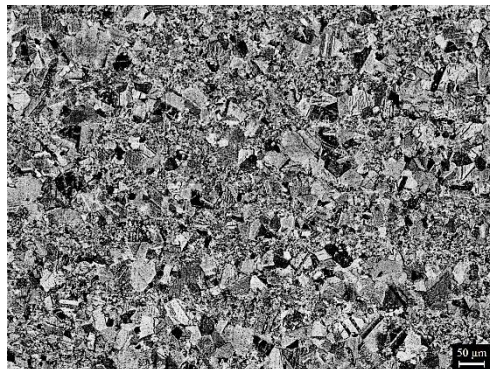
### Sample 2

$v=2800\text{mm/s}$

$I=10\text{ mA}$

Heat Flux=  $790\text{ W/mm}^2$

**33,7 wt% Al**



### Sample 4

$v=1600\text{mm/s}$

$I=12\text{ mA}$

Heat Flux=  $796\text{ W/mm}^2$

**32,6 wt% Al**

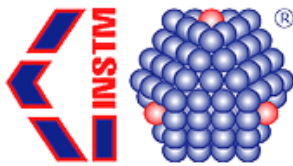




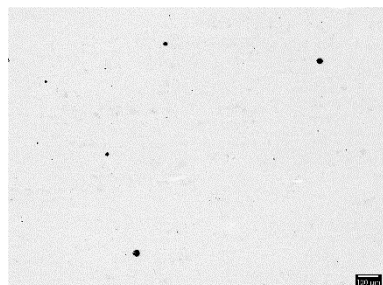
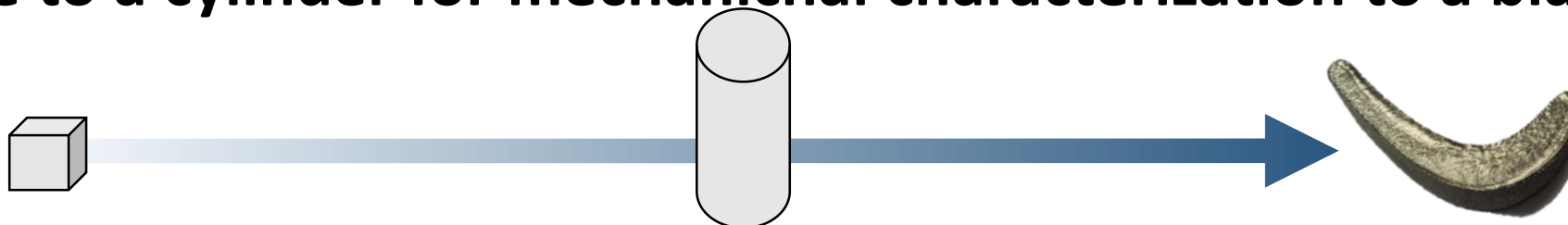
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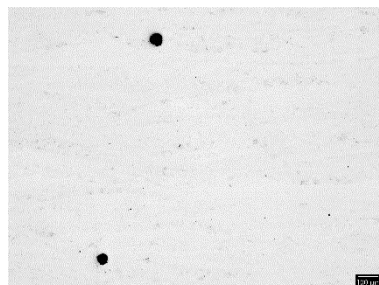
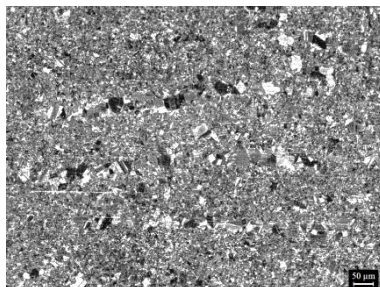
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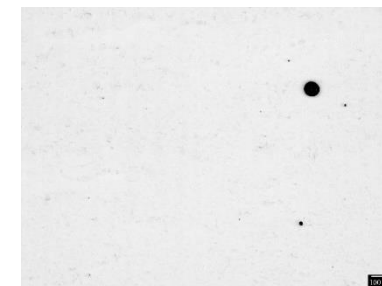
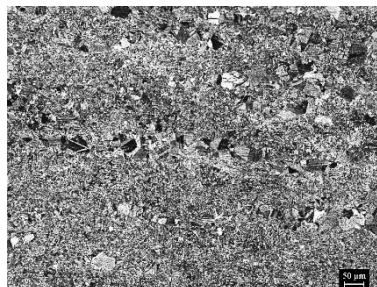
## From a cube to a cylinder for mechanical characterization to a blade



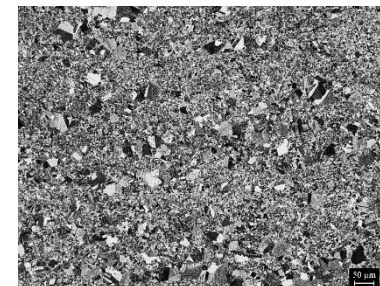
Av.P: 0,12% Dmax: 100  $\mu$ m



Av.P: 0,14% Dmax:120  $\mu$ m

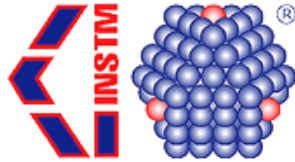


Av.P: 0,12% Dmax:120  $\mu$ m





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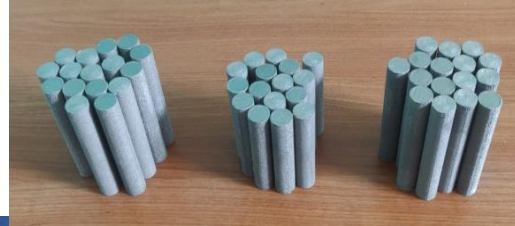
**Per each alloy:**

- ❖ Production of cylinders for tensile, creep and HCF;
- ❖ Production of representative portion of dem blades

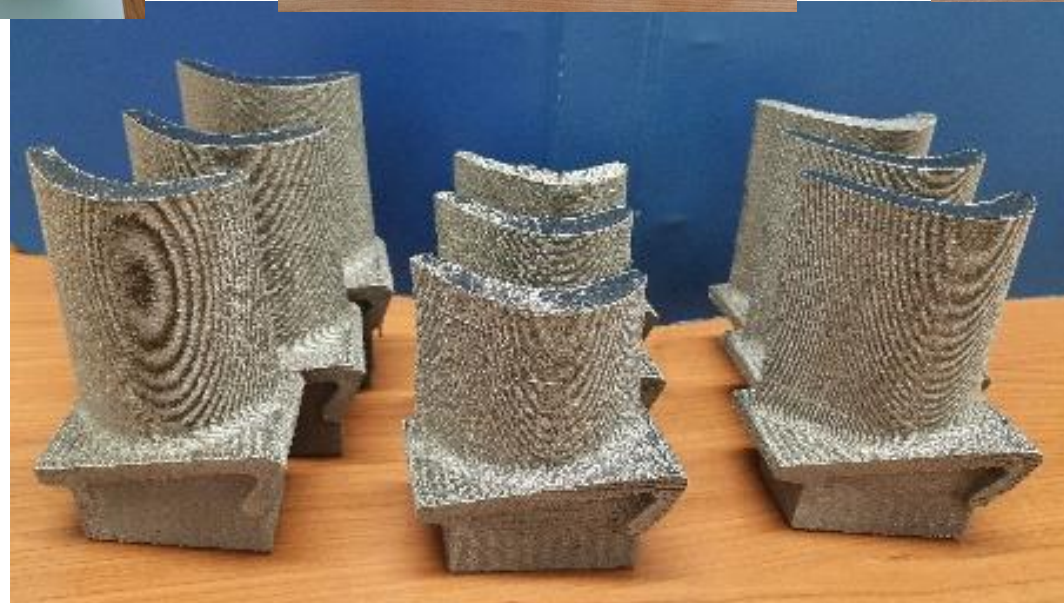
**Alloy 1: ref material**



**Alloy 2**



**Alloy 3**

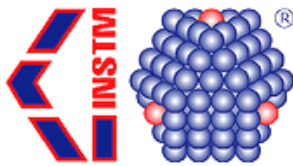




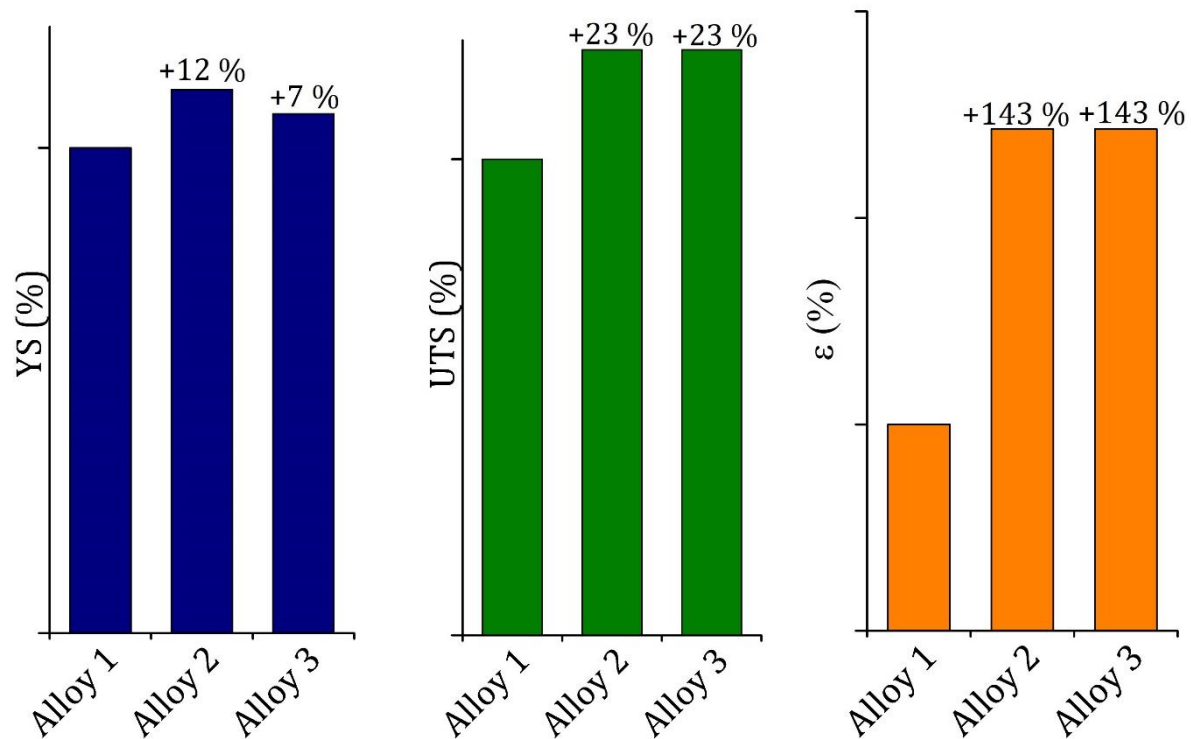
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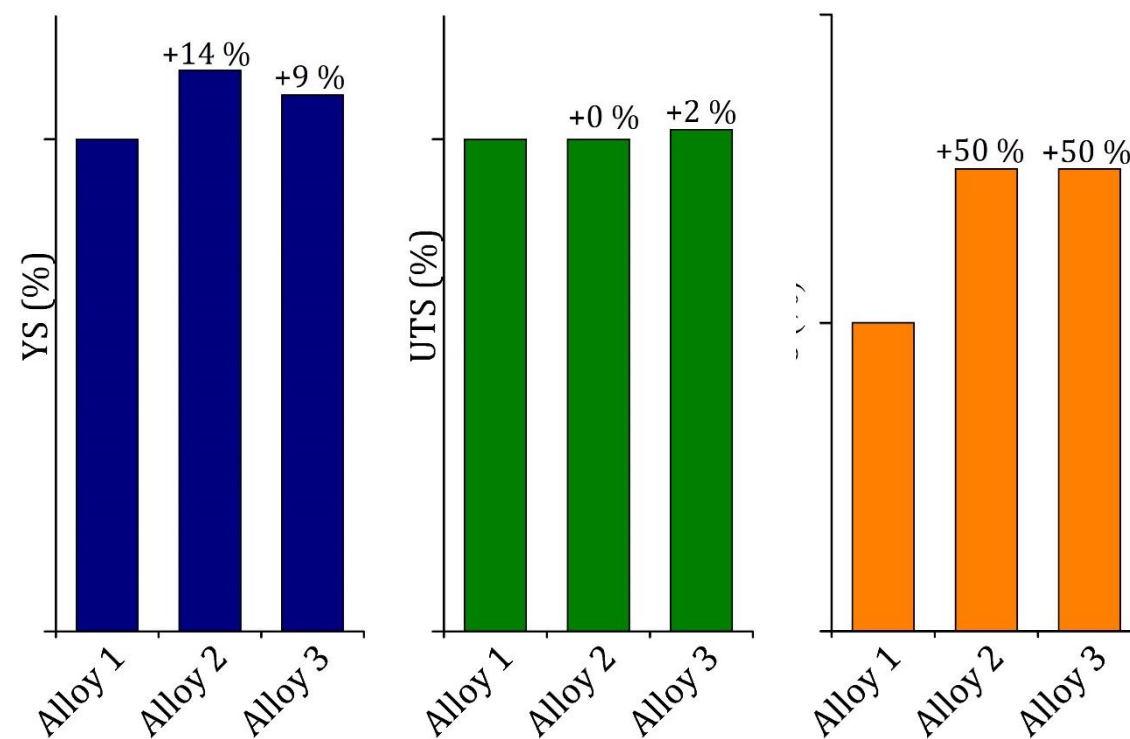
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## Tensile at room temperature

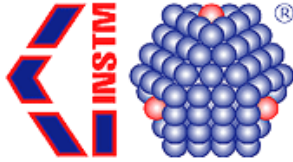


## Tensile at 760°C



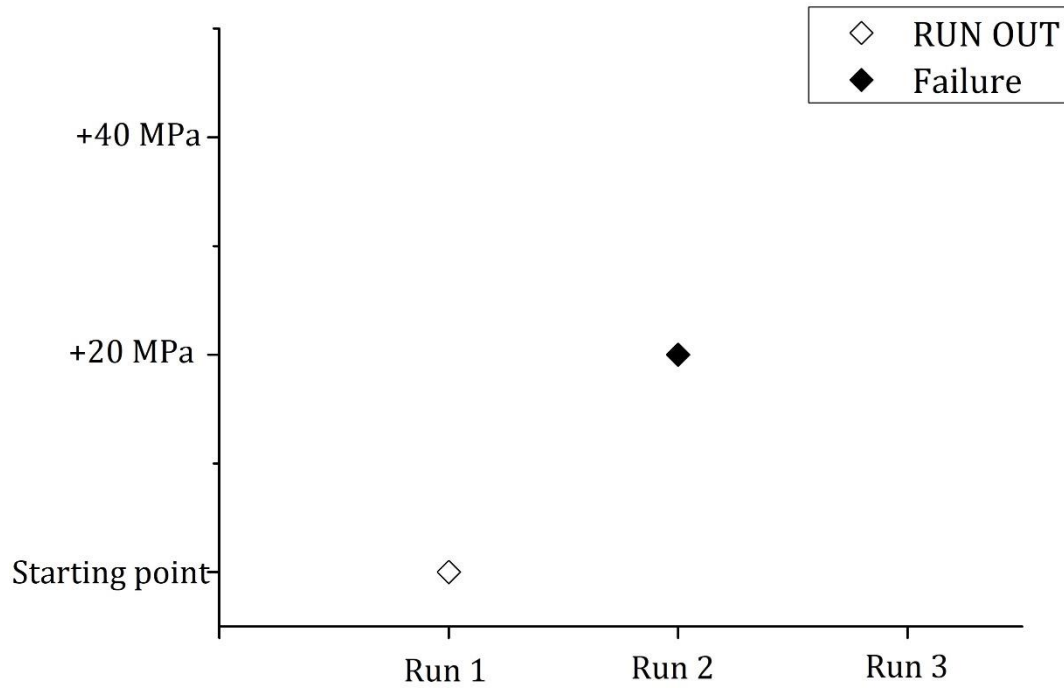


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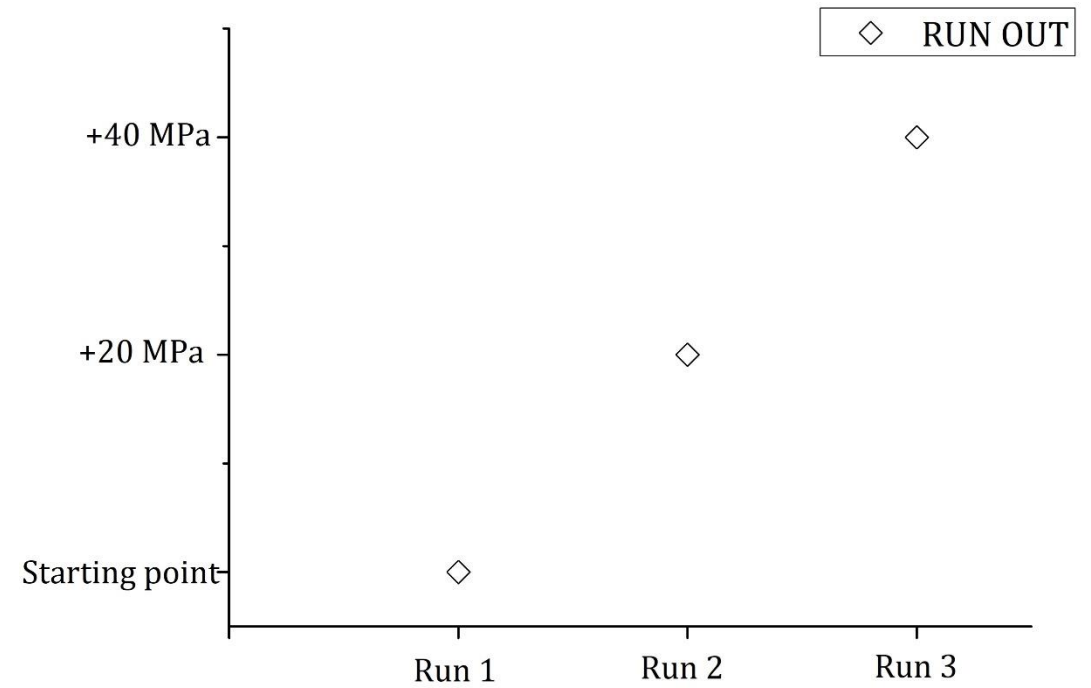


## High Cycle Fatigue at 760 °C with a R=0

Alloy 1



Alloy 2 and Alloy 3





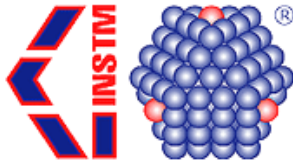
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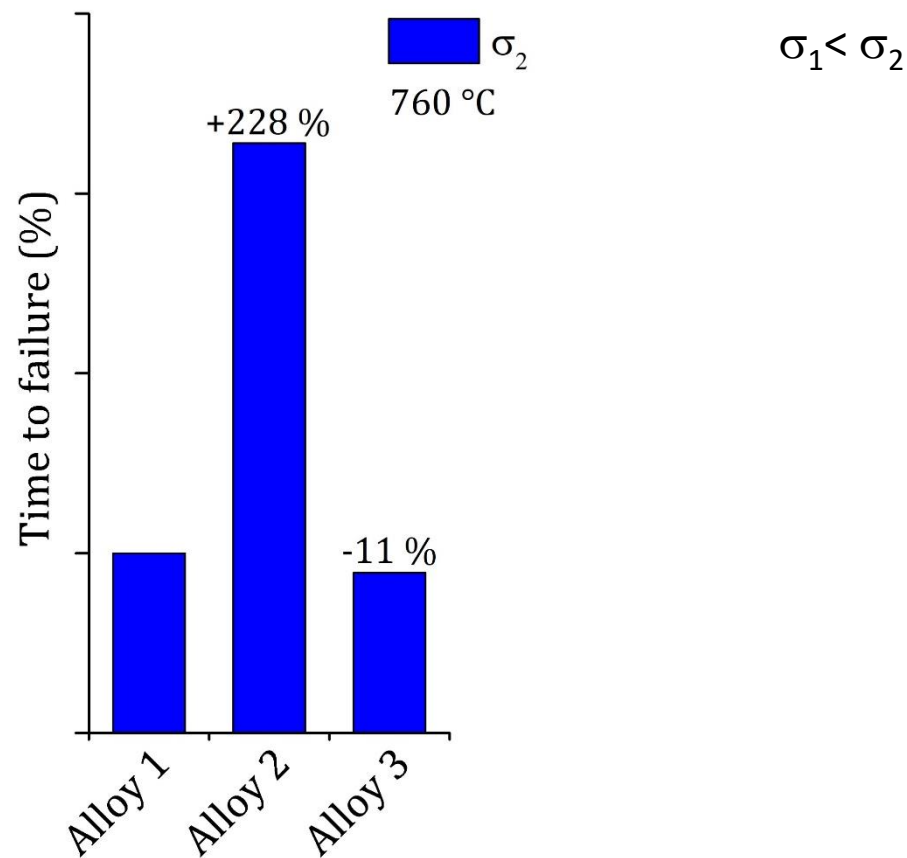
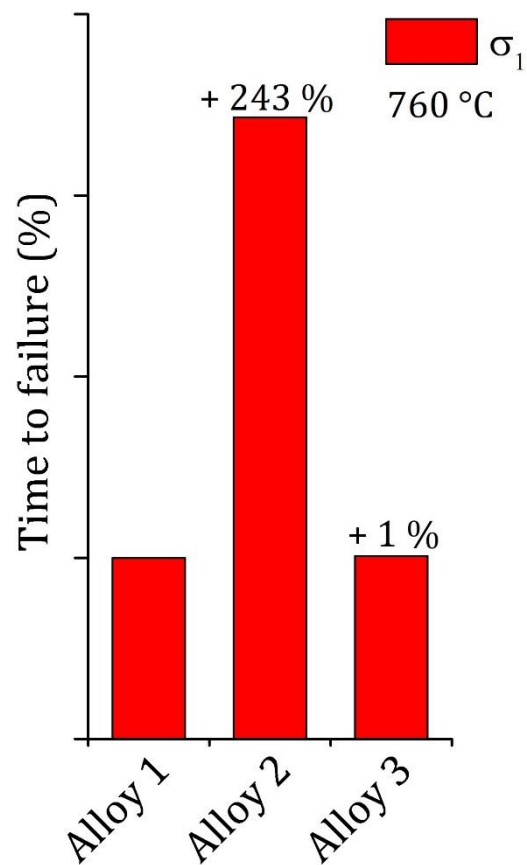
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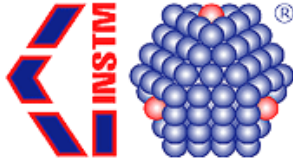


## Time to failure during creep test





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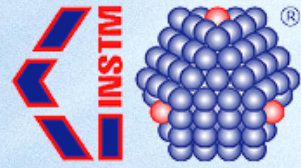


## Conclusion

- The characteristics of the EBM process have to be taken into account when **designing TiAl alloys for EBM**.
- The **simulation of the process** helped in understanding the effect of the process parameters on the final microstructure and aluminium content
- Thanks to the **process simulation** the optimisation of the process parameters from a simple cube to a complex shape has been speeded up.
- The process parameters influence the heat treatment and can be optimized for **reducing the inhomogeneity in Al distribution**.
- The two new chemical compositions exhibited **improved performances with respect to the reference alloy**.



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# A study on the chemical and microstructural optimization of the Ti-48-2-2 alloy processed by Electron Beam Melting

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