

Multiplexing and transient estimates in lung EIT instruments

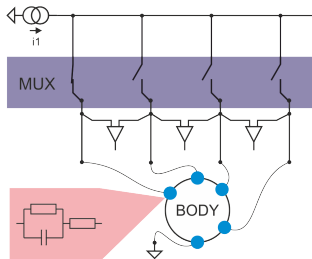
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Multiplexing in EIT instruments I

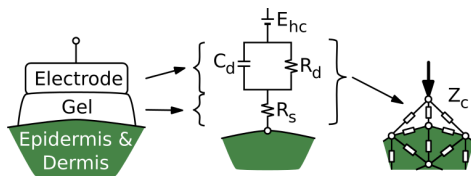
- Multiplexing is inherent to EIT. During current change, voltage amplitudes change and a transient can appear.



- Traditional approach is to settle to steady state. To achieve high frame rates, settling time after multiplexing is significant.
- Transient may not only take up significant amount of signal power, but also contain useful information about electrodes.

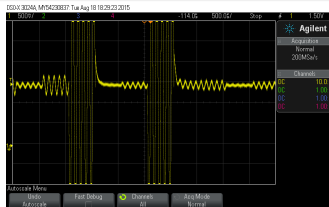
Contact impedance modelling I

- Model electrode as lumped capacitance (dead skin layer) C , in parallel with lumped resistance (ionic gel) R i.e. a parallel RC circuit [1, 2].



- 64 electrode system, $f > 10$ kHz injection and 30 fps, implies < 0.5 ms measurement time (5 full cycles per measurement).
- Typically $\tau \approx 0.1$ - 0.2 ms, and significant amount of useful energy is lost.

Contact impedance modelling II



- In practice, contact may have several characteristic time constants, inductive effects, or imperfect capacitors ($Z(\omega) = \frac{1}{iC(\omega)^\beta}$, $0 < \beta < 1$), which will not have single exponential behaviours.
- Explore fitting exponential and polynomial transient models

$$U_A^{\text{EXP}}(t) = A_1 \cos(\omega t) + A_2 \exp\left(-\frac{t}{A_3}\right) \quad (1)$$

$$U_A^{\text{POLY}}(t) = A_1 \cos(\omega t) + \sum_{i=2}^N A_i t^i. \quad (2)$$

Simulating transients with Fourier series

- Assuming linear constitutive relations $D = \epsilon E$, $J = \sigma E$, and negligible magnetic induction. Maxwell's equations:

$$\nabla \cdot \left(\epsilon \frac{\partial E}{\partial t} + \sigma E \right) = 0, \quad E = \nabla u \quad \text{for some } u.$$

$$\text{Let } u(x, t) = \sum_{\omega} u(x, \omega) e^{i\omega t},$$

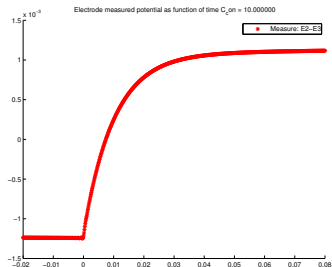
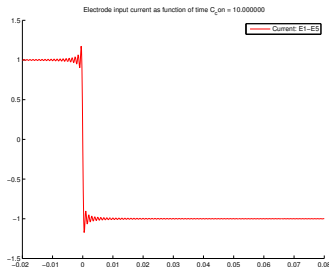
$$\nabla \cdot ((\sigma + i\omega\epsilon)\nabla u(x, \omega)) = 0, \quad \text{for each } \omega \quad (3)$$

- Generalise CEM with frequency dependent impedance e.g. $\frac{1}{z(\omega)} = \frac{1}{R} + i(\omega)^{\beta} C$, $\beta \geq 0$.
- Given current $I(t) : [-T, T] \rightarrow \mathbb{R}$, decompose using Fourier series into modes $\tilde{I}(\omega)$, solve (static) (3) with $\tilde{I}(\omega)$, and sum resulting $u(x, \omega)$ weighted by $e^{i\omega t}$

Square wave current simulation

- Conductive ($\sigma = 1$)/permittive ($\epsilon = 0.01$) medium and current

$$I(t) = \begin{cases} 1 & t \leq 0 \\ -1 & t > 0. \end{cases}$$



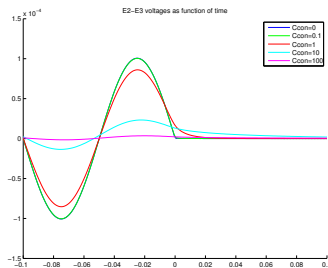
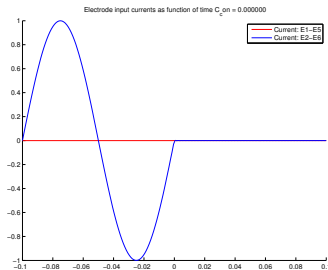
- Current discontinuity at $t = 0$ generates exponential decay in typical measured voltage, due to permittivity.

Sinusoidal current simulation I

- Conductive ($\sigma = 1$)/permittive ($\epsilon = 0.01$) medium and current

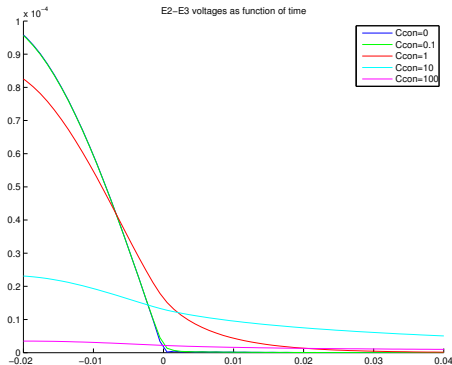
$$I(t) = \begin{cases} \sin(10\pi t/T) & t \leq 0 \\ 0 & t > 0. \end{cases}$$

- Left/Right represents input current/measurement at $t = 0$.
Note decay of measurement at $t = 0$.



Sinusoidal current simulation II

- Smooth current transition at $t = 0$, hence decay of measured voltages is due to non-zero electrode capacitance.



- Smaller capacitances have higher amplitude and faster decay, since $\tau \approx CR$ (approximate since effective τ will depend on bulk medium permittivity/conductivity.)

Signal Processing and data reduction

- Denote $U(t)$ be raw voltage data, sampled uniformly (2 MHz), and passed through 16-bit ADC.
- ≈ 3200 bits per cycle(0.1ms). 64 electrodes implies ≈ 2 Gbits/s data rate.
- Instead, typically compress data at FPGA e.g. at i^{th} -cycle

$$\begin{aligned} I_i &= \sum_{n=iT}^{(i+1)T} V(t_n) \sin(\omega t_n), & Q_i &= \sum_{n=iT}^{(i+1)T} V(t_n) \cos(\omega t_n), \\ D_i &= \sum_{n=iT}^{(i+1)T} V(t_n), & SS_i &= \sum_{n=iT}^{(i+1)T} V(t_n)^2. \end{aligned}$$

where $T = \frac{2\pi}{\omega}$. Assume saturation flag for each cycle.

- ≈ 22 bytes = 176 bits per cycle (0.1ms). 64 electrodes implies ≈ 0.1 Gbits/s data rate (50 times data reduction.)

- **Classical approach and FFT:** Reduce gain on current driven electrode just after measurement, and wait for a number of cycles until transient has effectively disappeared.
- **Exponential/Polynomial model:** Denote $M = \text{EXP}$ or POLY from in (2). Objective is to determine parameter $\{A_i\}_{i=1}^N$ and formulate as (non-linear) optimisation problem [3]

$$\mathbf{A} = \arg \min_{\mathbf{A}'} \sum_{i=1}^N (U(t_i) - U_{\mathbf{A}}^M(t_i))^2$$

- MATLAB function `lsqnonlin.m` is used to solve this (and subsequent) optimisation problems.

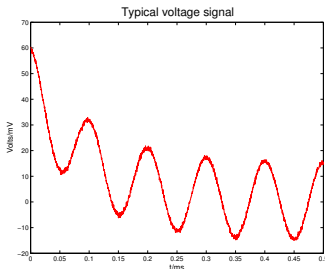
Simulated transient signal

- Without loss of generality consider phase-corrected signal

$$V(t) = A \cos(\omega t) + f(t) + n(t),$$

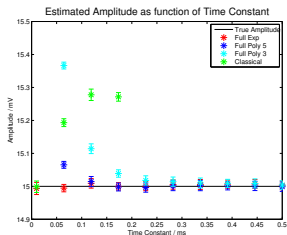
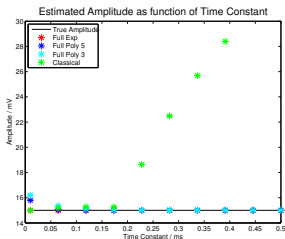
where $n(t)$ is white Gaussian noise and $f(t)$ is transient (assumed here to be $B \exp(-t/C)$).

- Simulation parameters:** Frequency $f = 10$ kHz, 5 full cycles (0.5ms measurement time), 2 MHz sampling rate, with 16-bit ADC. Initial/final amplitude 60/15 mV and noise variance $\sigma^2 = 0.5$ mV.



Full data results - Sinusoidal amplitude estimation

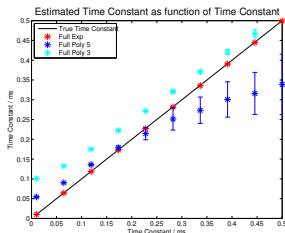
- Sinusoidal amplitude estimation as a function of $\tau \in [0, 0.5]$ over 20 noise realisations.
- Red/Blue/Magenta/Green - Exponential/ 3^{rd} order polynomial/ 5^{th} order polynomial models/FFT respectively.



- FFT gives poor estimates for $\tau > 0.05$. Exponential model estimates very well, and polynomial model estimates well for $\tau > 0.1$.
- Amplitude estimates at $\tau = 0.2278$ s:
 - Exponential - 15.001 ± 0.013 mV. 5^{th} order polynomial - 14.997 ± 0.014 mV. FFT - 18.637 ± 0.015 mV.

Full data results - Time constant estimation

- Time constant estimation as a function of $\tau \in [0, 0.5]$.



- Time constants also estimated very well with exponential model. 3rd and 5th order polynomial estimates time constants better for $\tau > 0.3$ and $\tau < 0.3$ respectively.
- Time constant estimates at $\tau = 0.2278$ s:
 - Exponential - 0.2272 ± 0.0002 ms. 5th order - 0.2144 ± 0.0156 ms.

Data reduction optimisation

- What information can be obtained given I, Q, S, D values (and saturation flags) from FPGA?
- Assume transient is purely exponential, integrating exponential model (2) analytically over i^{th} cycle gives

$$D(\mathbf{A})_i = -\frac{A_2}{A_3} \left(\exp\left(-\frac{T(i+1)}{A_3}\right) - \exp\left(-\frac{Ti}{A_3}\right) \right)$$

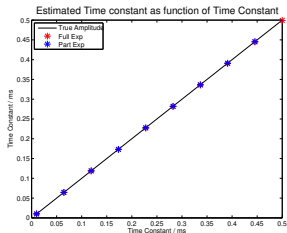
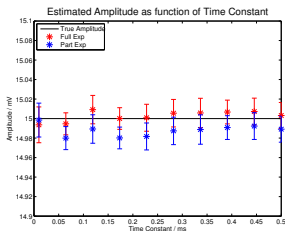
$$I(\mathbf{A})_i = A_2 A_3 \exp\left(-\frac{iT}{C}\right) (1 - \exp\left(-\frac{T}{A_3}\right)) / ((1/A_3)^2 + \omega^2) + A_1 T/2$$

- Equivalent integrals computable for n^{th} order polynomial model. However, n extra integrals $Vt_i^n := \int_{\text{cycle } i} V(t) t^n dt$ must be computed at FPGA, which will require, ≈ 48 bits per cycle per moment (≈ 30 Mbits/s).
- Let $M(\mathbf{A})_i = [D(\mathbf{A})_i, I(\mathbf{A})_i]$, and $M_i = [D_i, I_i]$ be measured data and s first cycle without saturation, then

$$\mathbf{A} = \arg \min_{\mathbf{A}'} \sum_{i=s} (M(\mathbf{A}')_i - M_i)^2$$

Partial data results - Amplitude estimation

- Left/Right represent amplitude/time constant estimation for exponential model over 20 noise realisations.
- Red/Blue represent Full/Partial data respectively.



- For exponential model partial data results are only marginally worse than full data results.
- Amplitude estimate for $\tau = 0.2278$ s:
 - Full - 15.001 ± 0.013 mV. Partial - 14.982 ± 0.018 mV.
- Time constant estimate for $\tau = 0.2278$ s:
 - Full - 0.2272 ± 0.0002 ms. Partial - 0.2277 ± 0.0002 ms.

Conclusions

- Transient behaviour is significant when attempting high frame rates at kHz frequencies.
- Given full time samples of voltage data, one can extract both sinusoidal amplitude and information of exponential transient, both with an exponential and polynomial model.
- Typically small set of data (e.g. I , Q , S , D) are computed per clock cycle, and sinusoidal amplitude can be extracted almost as well with this ≈ 50 times smaller data set.

Further Work

- Improved models of electrode-skin interfaces e.g. Jossinet *et al.* [2] to improve model fits.
- Algorithm presented here is inherently offline. Can fitting be performed on FPGA to extract sinusoidal component?



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McAdams E T, Jossinet J, Lacknermeier, Risacher F 1996, Factors affecting electrode-gel-skin interface impedance in electrical impedance tomography *Med. and Bio. Eng. and Comp.* **34**(6) pp. 397-408



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