

Dual Feeding Antenna for Performance Enhancement of Next-Generation of Mobile Networks against Self-Interference

Ehab A. Hegazy, Mohamed Bakry El Mashade

Abstract: Actually, the interference phenomena appear in all current wireless communication systems. Generally, conventional wireless communication systems use two separate channels; one of them for transmitting and the other one for receiving. Achieving single channel full duplex (FD) represents one of the key challenges for the implementation of 5G. Single channel FD permits the capability of wireless communication system to transmit and get concurrently on the identical channel, as well as the assurance of an efficient utilization of the current spectrum. With this newest technology, another sort of interference, which is called self-interference, will be generated. Therefore, self-interference cancellation strategies have an awesome solution for the development of the next generation. Passive and active cancellation techniques can be used to remedy such type of interference. In this regard, a dual feeding antenna approach is regarded as passive cancellation. This paper is concerned with this type of self-interference cancellation. A patch antenna is simulated and tested for two resonance frequencies; 2.45 and 28 GHz. Both of these frequencies are frequency channel candidates proposed by international telecommunication union (ITU) for the fifth generation of mobile networks.

Keywords: Self-Interference Elimination, Mobile network generations, Frequency as well as time division duplex, Antenna Design.

I. INTRODUCTION

Through its technologies and devices, communication through cordless has become an ubiquitous part of recent life, from global cellular telephone systems to local and even personal-area networks. This strategy of communication involves the sending of information over a distance without the help of wires, cables or any other forms of electrical conductors. It is a broad term that incorporates all scenarios and styles of connecting and communicating between two or more devices using a wireless signal.

The world has witnessed significant progress through several generations of mobile communication technology. In these specified forms, each new one enlarging the capabilities and promoting the end-user experience in comparison with the previous strategy, as Fig.(1) demonstrates. On the other hand, the key drivers behind the success of the telecom industry include the rapid adaptation of telecommunication

techniques and services by different sectors of society, as well as parallel development of advanced technologies from both hardware and software framework points of view. This success has come a long way from the appearance of the first approach (1G) cellular technology to the present day's strategy of this technology (4G).

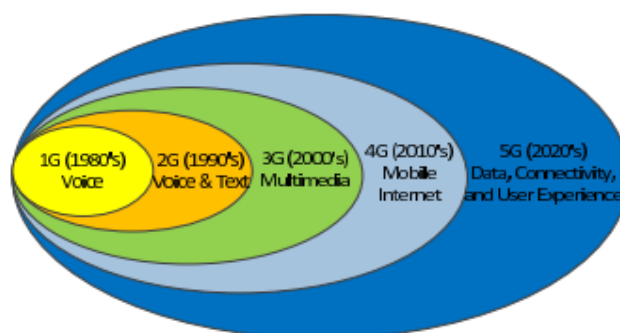


Fig.(1) Service classes evolution over wireless mobile generations

Recently, since we are dealing with “internet of things”, 5G is anticipated to accomplish the entire demands that have not been fulfilled by 4G. As shown in Fig.(2), 5G technologies are expected to prepare ultra-high bandwidth, extremely-high data rate, extra-low latency, highly speed mobility, and high energy efficiency. In other words, 5G will allow the use of much greater spectrum allocations at untapped mm-wave frequency bands, much higher bit rates in larger portions of the coverage area, higher aggregate capacity for many simultaneous users in both licensed and unlicensed spectrum, lower outage probability, longer battery life, lower infrastructure costs, and highly directional beam forming antennas at both the mobile device and base station. Additionally, the 5G backbone networks will replace copper and fiber communications with mm-wave wireless connections, which lead to rapid deployment as well as mesh-like connectivity with cooperation among base stations.

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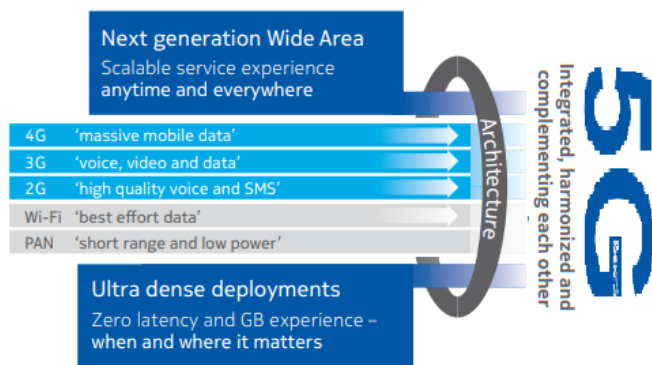


Fig.(2) Integration of existing and new services

As in all available mobile systems, the existing wireless communication systems employ two different channels to establish the transceiver process. They can't transmit and receive on the identical frequency channel per time slot. Additionally, transmission mode is not evolved, even long term evolution (LTE) still continuing via frequency division or time division duplex (FDD or TDD). Thus, achieving single full duplex will give us a great chance to enhance the future of 5G. In addition, it allows the current spectrum to be adequately utilized. Moreover, it eliminates the frequency and time constraints. However, through exploitation of the pronounced merits of single channel, self-interference (SI) will be generated. Transmitted antenna represents the main source of such type of interference due to its high power [3]. In telecommunication, a micro strip antenna refers to an antenna fabricated with micro strip mechanism on a printed circuit board. This type of antennas is usually employed at microwave frequencies. From the fabrication point of view, a micro strip antenna is composed of a patch of metal foil on the surface of a printed circuit board, with a metal foil ground plane on the other side of the board. The patch style is the most common type of micro strip antenna. A patch antenna is usually of narrowband [4].

The greatest part of micro strip antennas composed of several patches in a 2-D array. In recent decades, micro strip antenna has become very popular owing to its thin planar profile which allows it to be incorporated into the surfaces of consumer products, aircraft and missiles. Additionally, the ease of its fabrication using printed circuit techniques; the ease of integrating it on the same board with the rest of the circuit, and the possibility of adding active devices to the antenna itself to produce active ones makes it widely used in practical applications [5].

The intensity of SI is a crucial parameter owing to its influence on the performance of any wireless communication system. Hence, the proposed self-interference cancellation (SIC) technique depends upon a smart approach to overcome this problem which in turn will enhance the usage of the current spectrum. Generally, SIC scenario acts as a backbone for the deployment of single channel in the forthcoming version of mobile networks. The cancellation of SI should be achieved via antenna scheme, RF fragment, and analogue & digital signal processing. This achievement can be formulated in two main scenarios; the first one is related to electromagnetic separation which is termed as passive cancellation, whilst the other one can called as active cancellation [6]. The remaining part of this paper is organized

as follows. In section II self-interference cancellation techniques are overviewed. Section III is concerned with discussing the antenna technique of interference cancellation. Our proposed design procedure along with its simulation results is the objective of section IV. Finally, section V extracts our concluded remarks.

II. SIC TECHNIQUES

Wireless communications have been associated with cellular telephony for long time and have their highest impact on everyday lives. In recent times, wireless computer networks have led to a significant change in working routines and mobility of workers. Besides these widely publicized cases, wireless sensor networks monitor factories, wireless links replace the cables between computers and keyboards, and wireless positioning systems monitor the location of trucks that have goods identified by wireless RF labels. This variety of novel applications creates technical challenges for the wireless designers to become bigger with each day.

SI cancellation procedures familiarize a best solution in upcoming of the next generation of mobile communication through realizing single channel. Traditional editions of mobile communication systems have the proficiency of choice since it can turn as transceiver concurrently either on the same frequency segment with time varying (TDD) or on another frequency resource (FDD). The algorithms of SIC have several forms. However, most research work announced that cancellation techniques can be classified into two basic forms: passive and active. Passive cancellation technique takes place on the level of an antenna module. Meanwhile, the active strategy of cancellation is dependent on both analogue and digital processes. Active cancellation can be implemented via combination of RF segment along with some digital processing. This scenario of cancellation is based on subtracting the SI signals from the received signal. The subtraction process will be performed through digital samples and analogue signal. Several types of active SIC are essentially exist [5-6]. In full duplex (FD) system, an active SIC can be accomplished via balanced to unbalanced transformation which is entitled as a balun. An inverse SI signal, which is produced by balun, is an expedient to revoke SI. Balun will obtain a positive signal from transmitted antenna which is the causing of SI signal. In order to match the received signal, a combination process will be executed for both the received and inversed signals. Additionally, some adjustments, such as delay and attenuation, can be employed in the preparation of an inverse signal [7]. According to [6, 8] Table I displays a brief summary of RF solution for SIC approaches.

Table I Antenna used according to each technique

RF SIC Technique	NO of Antennas
Combination of a variable attenuator and phase shifter	One general
Fed-forward cancellation with two fed	One specific
Balanced/unbalanced (balun) transformer	Two
Antenna cancellation using two transmit and one receive antennas	Three
1) QHx220 noise cancellers 2) A nulling transmit antenna	Two
1) QHx220 noise cancellers 2) Transmit antenna 3) Digital cancellation	Three

QHx 220 noise dominance chip is used to remove a known analogue interference from received signal. The transmitted signal of the antenna feeds the QHx220 via a wire. Through the use of QHx220 noise canceller, a subtraction process is applied to both interfering signal and received signal in order to improve the beneficial signal [6, 8]. Other methods for SIC can be implemented by eliminating SI, in the analogue signal stage, in accordance with the phase of the two signals [8].

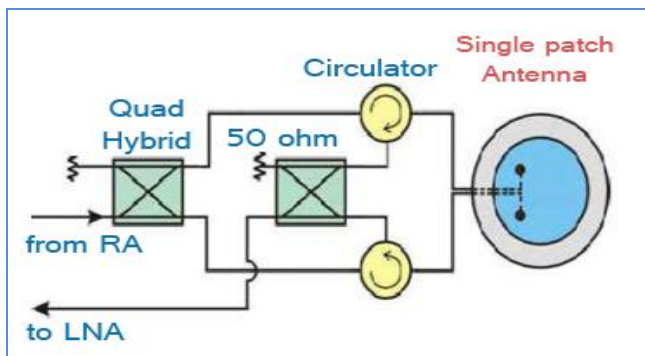


Fig.(3) Two-fed patch antenna for passive cancellation

III. ANTENNA CANCELLATION

An antenna system can be considered as the eye of each wireless communication system. Through the existence of self-interference problem, an antenna acts as a foremost part in passive SIC procedure, as Table I demonstrates.

Here, the proposed work offers one of the existing mechanisms which includes an antenna with dual feed in order to enhance the intensity of SIC. As Fig.(3) depicts, the existing antenna has the ability of transmitting and getting signals by means of polarization diversity. It is significant to note that feeding spots are orthogonal and have similar amplitudes. In our research, we select two resonance frequencies of values 2.45 GHz and 28GHz. Aiming that our proposed strategy will be useful for the future of 5G.

IV. ANTENNA DESIGN, SIMULATION RESULTS

In wireless communication, antenna plays the most prominent part in radiating the information of interest. In this regard, micro strip patch antenna is well known to have positive features for cost-effective, low profile and

broadband. Additionally, it is an evident choice for wireless devices due to its practical characteristics like low fabrication cost, light weight and volume, and a low profile configuration in comparison with the other bulky type of antennas. Moreover, it can be easily mounted on rockets, missiles and any conformal shaped satellites without major modification. Furthermore, arrays of these antennas can simply be produced. Owing to these important merits, this type of antenna is of practical use in many applications.

Now, we are going to design the suggested antenna following the micro strip patch antenna rules [9-11].

A. Proposed Antenna Design Configuration

The design specification of a patch antenna is characterized by three vital factors. These parameters are: the operative frequency (f_r), substrate dielectric constant (ϵ_r), and the dielectric substrate height (h). In the subsequent text, the design procedure is tabulated. Firstly, the antenna width can be calculated with the aid of the following formula:

$$W = \frac{c_0}{2 f_r} \sqrt{\frac{2}{\epsilon_r + 1}} \quad (1)$$

where c_0 denotes is the free-space velocity of light.

One the other hand, the effective dielectric constant has a mathematical expression given by:

$$\epsilon_{r_{eff}} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \sqrt{\frac{1}{1 + 12h/W}} \quad \& \quad \frac{W}{h} \gg 1 \quad (2)$$

For a given resonance frequency f_r , the effective length takes the form:

$$L_{eff} = \frac{c_0}{2 f_r} \sqrt{\frac{1}{\epsilon_{r_{eff}}}} \quad (3)$$

The normalized extension in the antenna length can be obtained via the formula:

$$\frac{\Delta L_{eff}}{h} = 0.412 \frac{(\epsilon_{r_{eff}} + 0.3)(W/h + 0.264)}{(\epsilon_{r_{eff}} - 0.258)(W/h + 0.8)} \quad (4)$$

As a function of L_{eff} & ΔL_{eff} , the actual length of the designed antenna can be evaluated as:

$$L_{eff} = L + 2 \Delta L \quad (5)$$

The proposed antenna feeding is accomplished through a micro strip line technique. In our design procedure, we will calculate the length and width of matching transmission line which are indicated as L_{m1} & W_{m1} for port one, as Fig.(4) depicts. Meanwhile, the length and width of feed micro strip line are computed and are denoted as L_{t1} & W_{t1} for port one. The design is performed in accordance with micro strip patch antenna rules [11, 12]. Additionally, similar calculations are performed for the second port.

B. Simulation results and Discussion

The performance analysis of the underlined antenna is carried out using CST software [12].



Subdivision 1

The proposed patch antenna working at 2.45GHz is of 1.5mm substrate height.

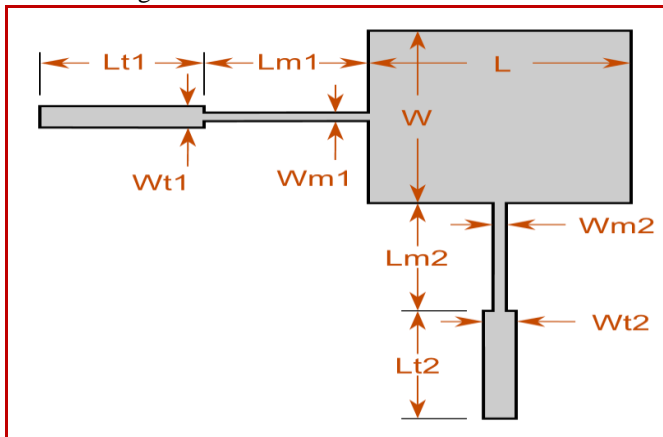


Fig.(4) Dual micro strip-edge-fed circularly polarised rectangular patch antenna

We confer to the design specifications in order to complete the plan of the under examination patch antenna. These parameters are listed in Table II which shows dual-fed circularly polarized patch design objectives. Moreover, Table III outlines the physical parameters of our proposed design.

Table II Dual-fed circularly polarised patch design objective

Name	Description	Value
f_0	Centre frequency	2.45 GHz
R1	Input resistance at port 1	50 Ω
R2	Input resistance at port 2	50 Ω
P	Polarization (transmitting)	linear
Name	Substrate: The substrate name.	FR-4

Table III Dual-fed circularly polarised design parameters for 2.45GHz antenna

Name	Description	Value
L	Length of the patch element	26.19 mm
W	Width of the patch element	29.01 mm
Lm1	Length of matching transmission line (port 1)	18.18 mm
Wm1	Width of matching transmission line (port 1)	159.7 μ m
Lt1	Length of feed microstrip line (port 1)	16.84 mm
Wt1	Width of feed microstrip line (port 1)	2.892 mm
Lm2	Length of matching transmission line (port 2)	18.18 mm
Wm2	Width of matching transmission line (port 2)	159.7 μ m
Lt2	Length of feed microstrip line (port 2)	16.84 mm
Wt2	Width of feed microstrip line (port 2)	2.892 mm

For an antenna, the most interesting parameter to be investigated is the maximum power transferring, which is considered as an indication about the matching between the feed line and the input impedance of the antenna. In this situation, S11 represents the insertion loss of an antenna. It designates the amount of power that is lost to the load and doesn't return as a reflection. It clarifies how well the matching between the transmitter and antenna has taken place. In other words, insertion loss is consistent with the ratio of the reflected power to that of input of an antenna.

Generally, antenna radiates efficiently for particular range of frequencies. At these frequencies, the radiated power is almost equal to the input power, which means that the reflected power is of negligible value. Based on this principal background, a graph of S11 of an antenna versus frequency represents its return loss. For optimum operating conditions, such a graph must exhibit a dip at the operating frequency, i.e., a minimum dB value at this frequency. So, the expected behavior of S11 for an antenna would be a flat line throughout the frequency scale with deep dip at its operating frequency range. On the other hand, scattering parameters of an antenna can be defined as the correlation or the relationship between its ports [14]. For case in point, S12 represents the power transferred from port 2 to port 1 whilst S21 indicates the reverse, i.e.; it refers to the power transferred from port 1 to port 2. Fig.(5) illustrates the estimated result of the reference antenna. It plots S12 and S21 versus frequency indicating the fundamental resonance frequency. In other words, Fig.(5) demonstrates a high isolation between the two ports of the examined antenna.

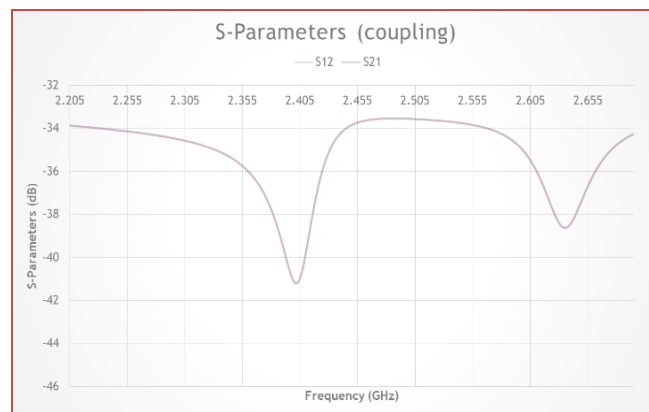


Fig.(5) S12 and S21 of the patch antenna resonating at 2.45 GHz.

Table IV Average S-parameters of dual-fed circularly polarised Antenna

Dual port Antenna 2.45GHz		
	S12	S21
Average S-parameters	-35.17 dB	-35.17 dB
Bandwidth below(-10dB level)	490MHZ	490MHZ



The radiation pattern of an antenna is a description of its far-field radiation characteristics as a three-dimensional plot in which θ denotes the angle of elevation and ϕ represents the azimuth angle. More specifically, it is a plot of the radiated power of an antenna per unit solid angle [11]. Figs.(6 & 7) depict the far field gain of the underlined antenna at $\phi=0^\circ$ and $\phi=90^\circ$, respectively. As demonstrated in Fig.(8), the proposed antenna achieve an accepted radiation pattern with directivity of about 7.221dBi.

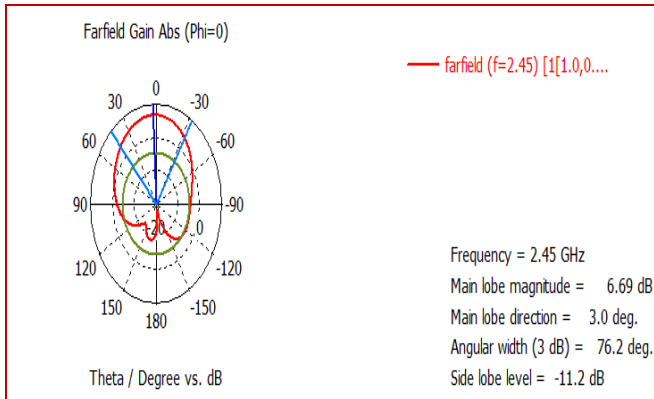


Fig.(6) Dual microstrip-edge-fed circularly polarised patch antenna radiation pattern at 2.45GHz, for $\phi=0^\circ$

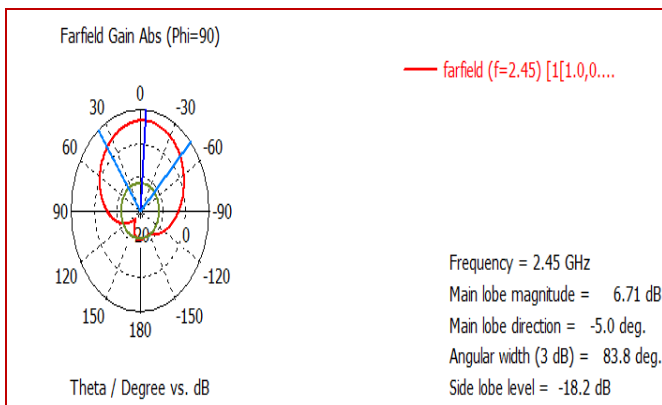


Fig.(7) Dual microstrip-edge-fed circularly polarised patch antenna radiation pattern at 2.45GHz, for $\phi=90^\circ$

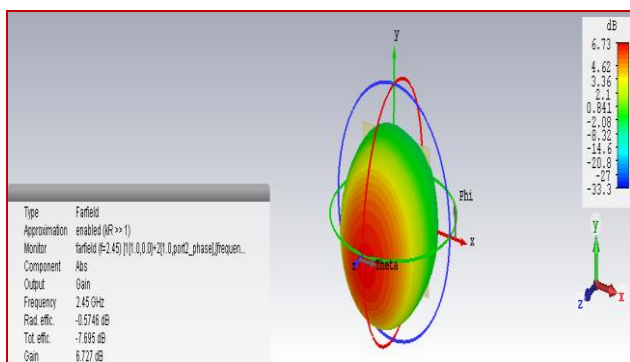


Fig.(8) Dual micro strip-edge-fed CP radiation pattern plot

Fig.(9) shows far field versus angle at the designed frequency for $\phi=0^\circ$. Fig.(10) illustrates the same thing as Fig.(9) for $\phi=90^\circ$.

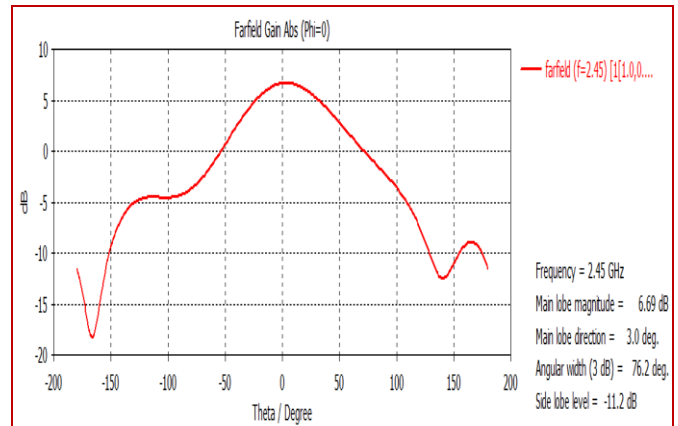


Fig.(9) Far field versus angle plot for $\phi=0^\circ$

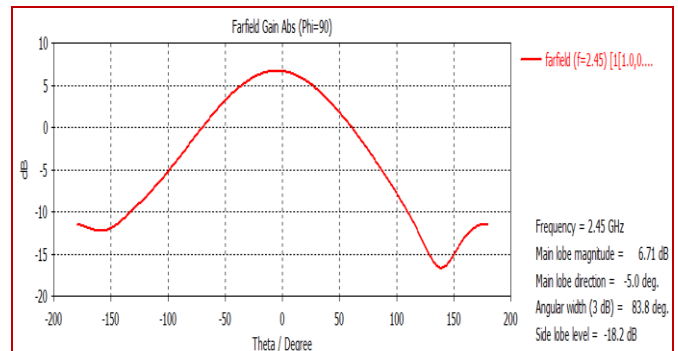


Fig.(10) Far field plot as a function of angle for $\phi=90^\circ$

Commonly the axial ratio (AR) is deployed in order to determine the quality of antenna polarization with dual feed [15]. Figs.(11 & 12) clarify the polar and 3D plot for axial ratio of the suggested antenna.

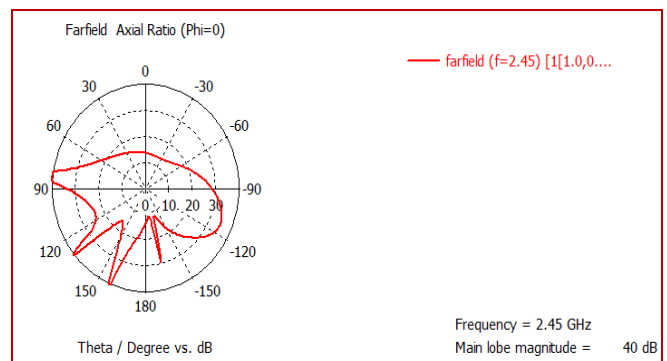


Fig.(11) Polar plot of axial ratio pattern for proposed antenna

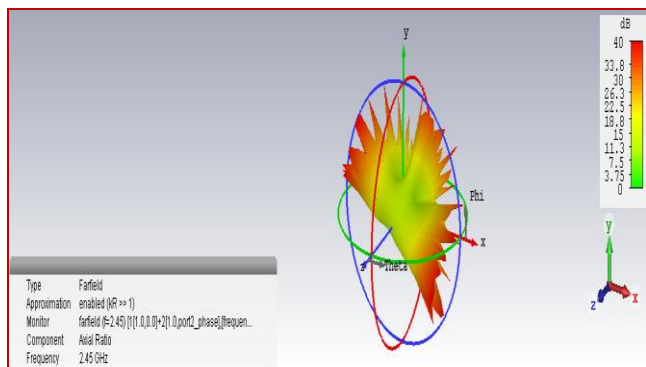


Fig.(12) Axial ratio pattern of the tested antenna

Subdivision II

Now, we turn our attention to the proposed patch antenna with 100µm substrate height and designed for operating at 28GHz resonance frequency through the same design objectives of 2.45GHz. This antenna has a preview displayed in Fig.(13).

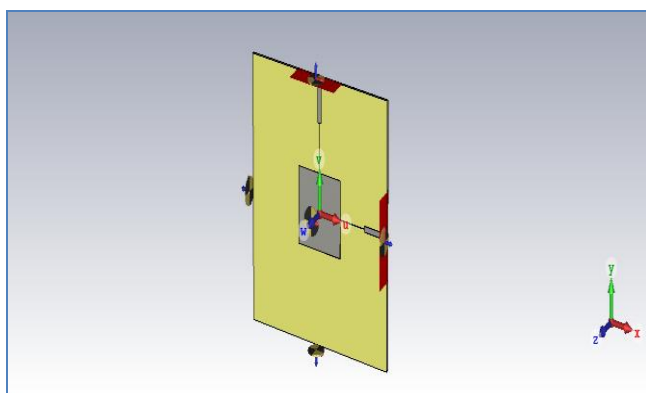


Fig.(13) Dual microstrip-edge-fed CP patch antenna preview

The physical parameters of the second proposed antenna are listed in Table V.

Table V Dual-fed circularly polarised design parameters for 28GHz antenna

Name	Description	Value
L	Length of the patch element	2.500 mm
W	Width of the patch element	2.750 mm
Lm1	Length of matching transmission line (port 1)	1.592 mm
Wm1	Width of matching transmission line (port 1)	10.14 µm
Lt1	Length of feed microstrip line (port 1)	1.474 mm
Wt1	Width of feed microstrip line (port 1)	192.8 µm
Lm2	Length of matching transmission line (port 2)	1.592 mm
Wm2	Width of matching transmission line (port 2)	10.14 µm
Lt2	Length of feed microstrip line (port 2)	1.474 mm
Wt2	Width of feed microstrip line (port 2)	192.8 µm

Fig.(14) clarifies the estimated scattering parameters, such as S12 and S21, of the proposed patch antenna versus frequency indicating its fundamental resonance frequency. S12 and S21 are around 36.762dB.

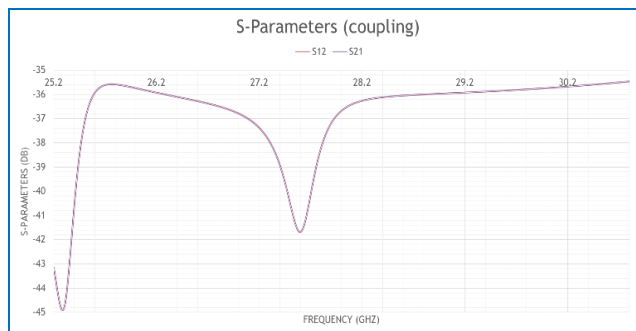


Fig.(14) Scattering parameters, S12 & S21, of circularly polarised patch antenna radiation pattern at 28GHz

Table VI Average S-parameters of dual-fed circularly polarised Antenna

Dual port Antenna 28 GHZ		
	S12	S21
Average S-parameters	-36.75 dB	-36.75 dB
Bandwidth below(-10dB level)	5.6GHZ	5.6GHZ

Table VI indicates the antenna bandwidth and average values of S12 and S21. The polar plots at $\phi=0^\circ$ and $\phi=90^\circ$ are shown in Figs.(15 & 16), respectively.

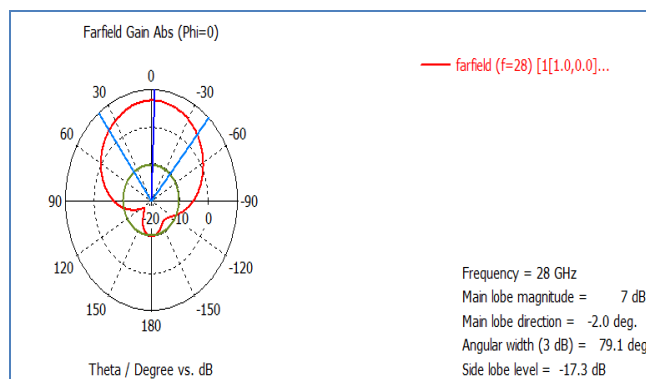


Fig.(15) Dual microstrip-edge-fed circularly polarised patch antenna radiation pattern at 28GHz, for $\phi=0^\circ$

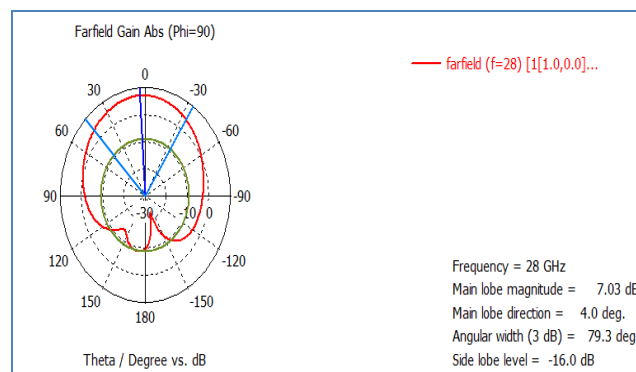


Fig.(16) Dual microstrip-edge-fed circularly polarised patch antenna radiation pattern at 28GHz, for $\phi=90^\circ$

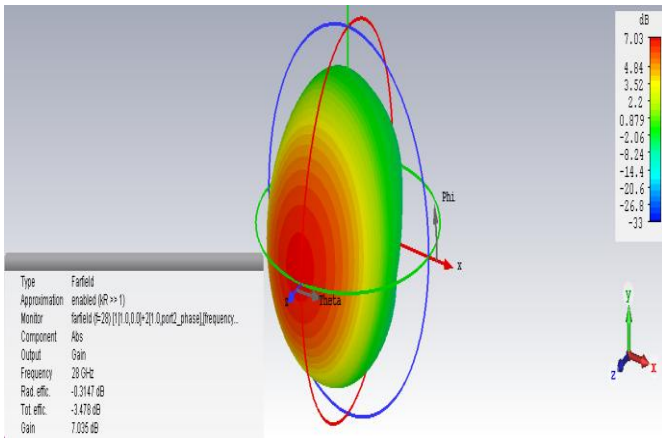


Fig.(17) Dual micro strip-edge-fed CP radiation pattern plot

As revealed in Fig.(17), the proposed antenna attains an accepted radiation pattern with directivity of about 7.329dBi. Fig.(18) shows the far field, as a function of angle, of the designed antenna at $\phi=0^\circ$. Fig.(19) illustrates the same thing as Fig.(18) for $\phi=90^\circ$.

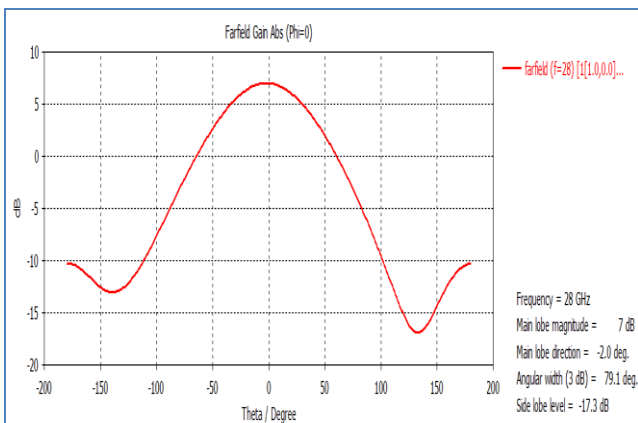


Fig.(18) Far field, as a function of angle, plot of 28GHz designed antenna for $\phi=0^\circ$

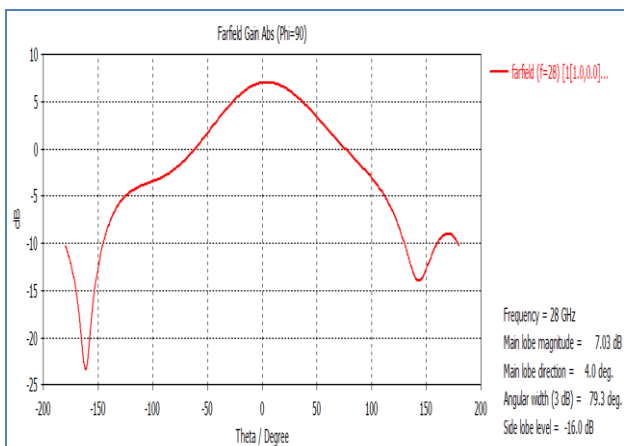


Fig.(19) Far field, as a function of angle, plot of 28GHz designed antenna for $\phi=90^\circ$

Subsequently, Figs.(20 & 21) demonstrate the polar and 3D, respectively, plots for axial ratio of the examined antenna.

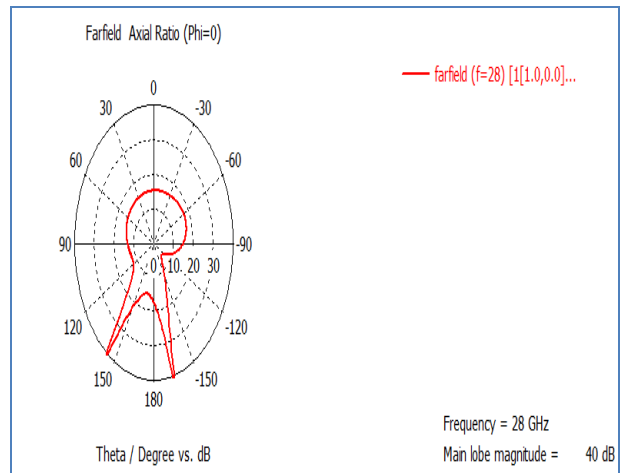


Fig.(20) Axial ratio pattern of 28GHz designed antenna

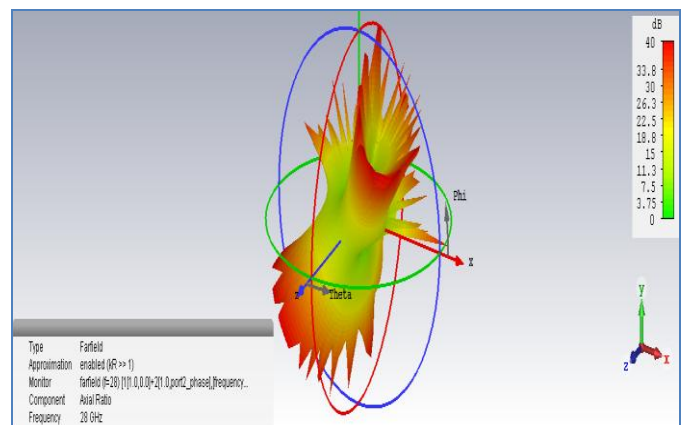


Fig.(21) Axial ratio pattern of the 28GHz tested antenna

C. Design Summary of Proposed Antenna

Our proposed antenna has the ability of transmitting and getting signals by means of polarization diversity. It is significant to note that feeding spots are orthogonal and have similar amplitude. Table VII summarizes the main parameters used in our design along with the gain of each antenna in terms of its resonance frequency.

Table VII Average S-parameters of Dual-fed circularly polarised Antenna

Dual port Antenna		
	2.45GHz	28GHz
Dielectric substrate	FR-4	FR-4
Substrate permittivity (ϵ_r)	4.35	4.35
substrate height	1.5mm	100 μ m
Antenna gain(directivity)	7.221dBi	7.329dBi

The proposed work is considered as one of SIC techniques which are already used to improve or reduce the intensity of SI in wireless systems and this in turn will overcome the limitations of full duplex communication via effective propagation isolation between transmitted and received signals. Numerous dissimilar cancellation approaches are outlined in [16-18].

In these literatures, it is indicated that through this type of SIC algorithms, which is called antenna isolation technique, an isolation of about 20-30 dB can be provided. In our proposed antenna, we succeeded to achieve an isolation, between ports of antenna, in the order of 34dB for resonance frequency of 2.45GHz and of 36dB in the case of 28GHz

V. CONCLUSION

5G is predicted to provide attractive landscapes such as huge connections, reducing the latency down to one millisecond and enhancing the data rate up to 10Gb/s. Extending full duplex communication to a longer range could remain a primary challenge owing to growing of the spectral efficiency along with more occupation of frequency spectrum. One of the major challenges in 5G future is the realizing of single channel full duplex. Self-interference cancellation is a mandatory and attractive solution for more utilization of the current spectrum. Several self-interference cancellation techniques are deployed in wireless systems. Our proposed work is applied to achieve such objective for 2.45 and 28GHz.

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