Enrico's Chart of Phase Noise and Two-Sample Variances

Enrico Rubiola – http://rubiola.org
European Frequency and Time Seminar – http://efts.eu
Oscillator Instability Measurement Platform http://oscillator-imp.com

Oscillator IMP

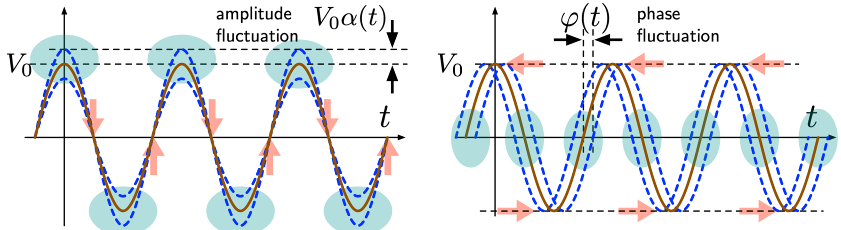
Thanks to FIRST-TF https://first-tf.com

Download the Vademecum

Place for the QR code of a companion article, in progress

Download the Enrico's Chart

Clock signal $v(t) = V_0[1+\alpha(t)]\cos[2\pi\nu_0 t + \varphi(t)]$



Boldface notation

total = nominal + fluctuation

$\boldsymbol{\varphi}(t) = 2\pi\nu_0 t + \varphi(t)$ phase

$\boldsymbol{\nu}(t) = \nu_0 + (\Delta\nu)(t)$ frequency

$\mathbf{x}(t) = t + \mathrm{x}(t)$ time

$\mathbf{y}(t) = 1 + \mathrm{y}(t)$ fractional frequency

Phase noise spectrum

Definition

$S_\varphi(f)$ [rad^2/Hz] is the one-sided PSD ($f>0$) of $\varphi(t)$

$$S_\varphi(f) = 2\mathcal{F}\{\mathbb{E}\{\varphi(t)\varphi(t+\tau)\}\}, \quad f>0$$

Evaluation

$$S_\varphi(f) = \frac{2}{T}\langle \Phi_T(f)\,\Phi_T^*(f)\rangle_m$$

avg on m data, $\Phi_T(f)$ = DFT of $\varphi(t)$ truncated on T

Usage

most often, 'phase noise' refers to $\mathscr{L}(f)$

Only $10\log_{10}[\mathscr{L}(f)]$ is used, given in dBc/Hz

Definition: $\mathscr{L}(f) = \frac{1}{2}S_\varphi(f)$ [the unit c/Hz never used]

Literally, the unit 'c' is a squared angle, $\sqrt{\mathrm{c}} = \sqrt{2}$ rad $\simeq 81°$

Two-sample (Allan-like) variances

Definition

$$\sigma_y^2(\tau) = \mathbb{E}\left\{\frac{1}{2}\left[\bar{\mathrm{y}}_2 - \bar{\mathrm{y}}_1\right]^2\right\}$$

$\mathrm{y}(t) \to \bar{\mathrm{y}}$ averaged over τ

$\bar{\mathrm{y}}_2$ and $\bar{\mathrm{y}}_1$ are contiguous

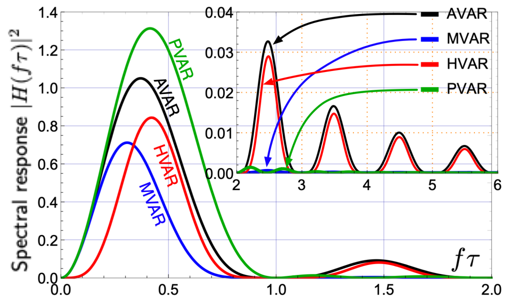
Bare mean $\bar{\mathrm{y}} \to$ Allan variance AVAR

Weighted averages $\to$ MVAR, PVAR, etc.

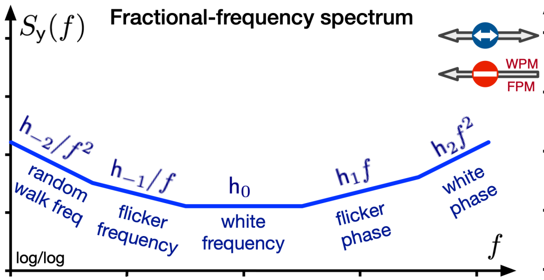
Evaluation

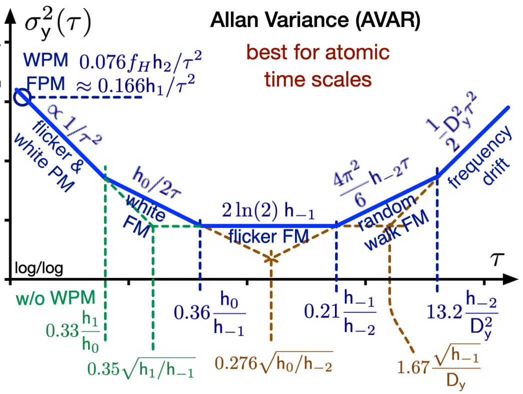
$$\sigma_y^2(\tau) = \frac{1}{2(M-1)}\sum_{k=1}^{M-1}\left[\bar{\mathrm{y}}_{k+1} - \bar{\mathrm{y}}_k\right]^2$$

M contiguous samples of $\bar{\mathrm{y}}$



Frequency fluctuation PSD <—> Allan Variance



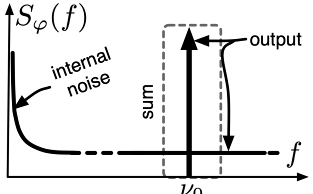


DOI: 10.5281/zenodo.4399218 (latest version)

ORCID 0000-0002-5364-1835

Last update August 31, 2021

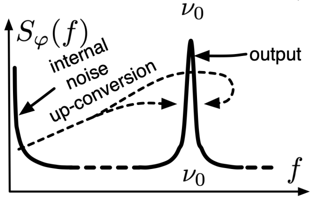
Additive Noise



RF noise added to the carrier

Statistically independent AM & PM

Parametric Noise

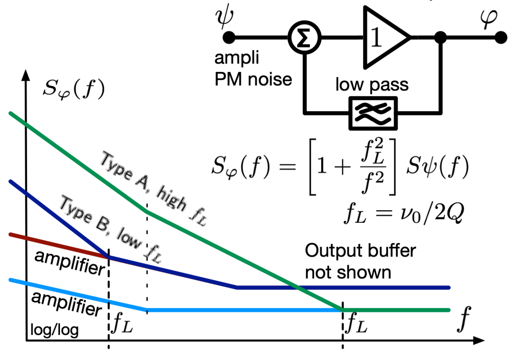


Near-dc noise modulates the carrier

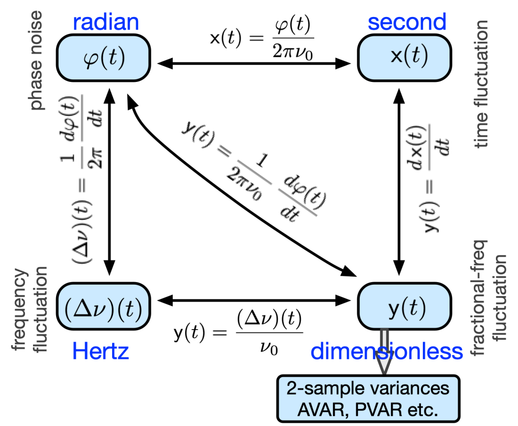
AM & PM related and narrowband

Leeson effect

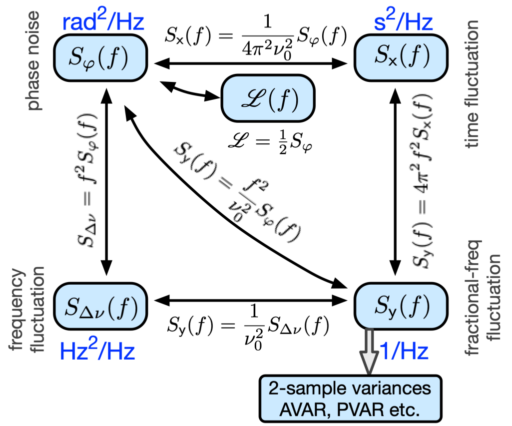
Oscillator's PM-noise equivalent



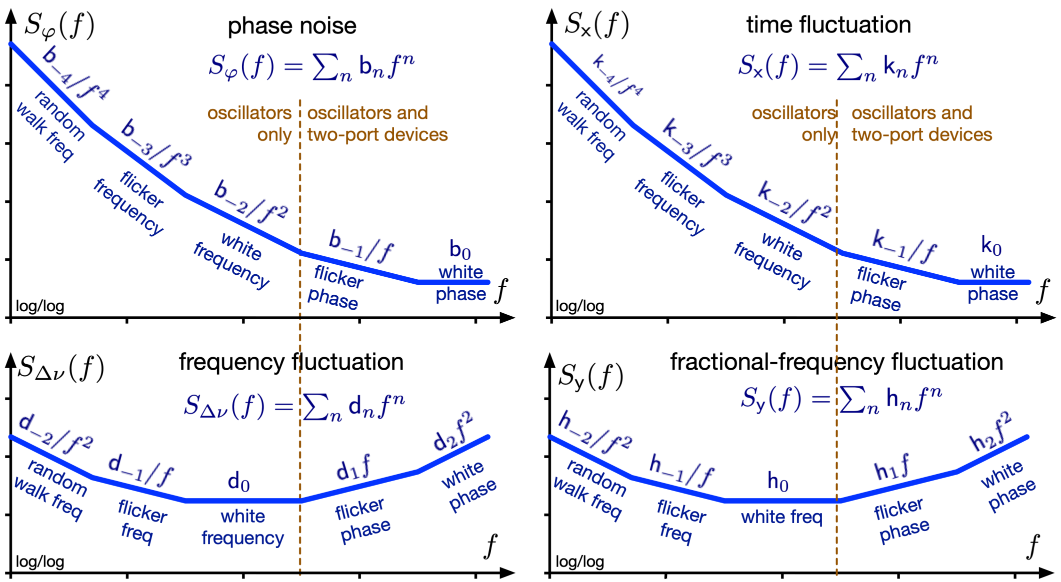
Time Domain



Frequency Domain



Spectra and Polynomial Law



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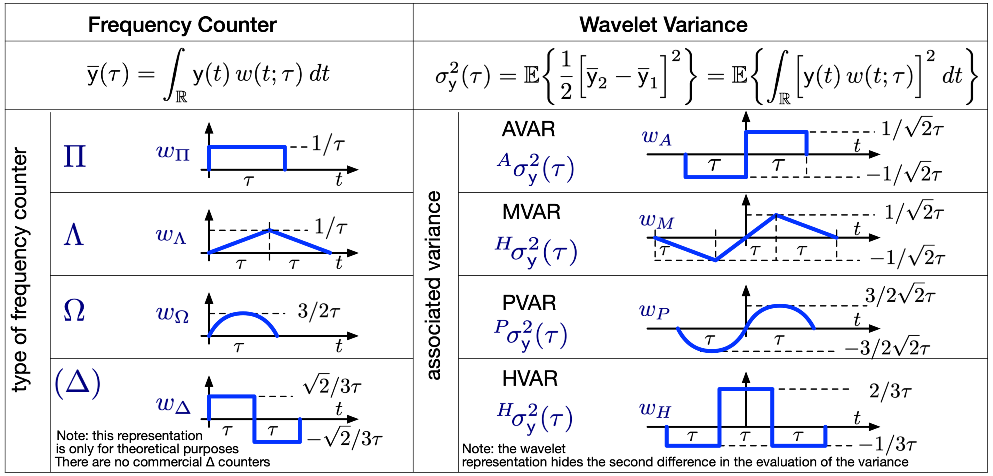
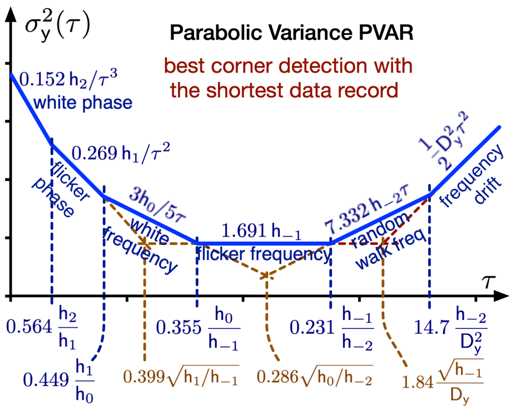
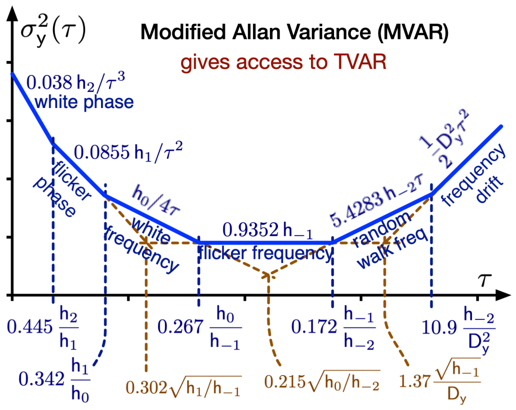
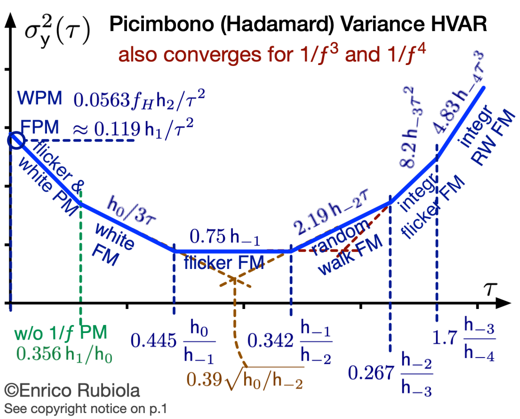
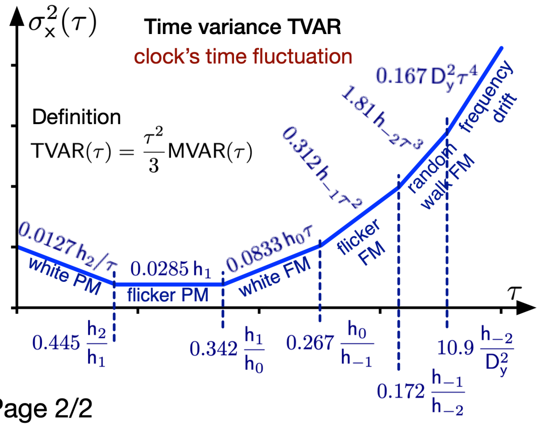


Other Two-Sample Variances









Spectra to Variances Conversion

noise type	$S_y(f)$	AVAR $^A\sigma_y^2(\tau)$	MVAR $^M\sigma_y^2(\tau)$	HVAR $^H\sigma_y^2(\tau)$	PVAR $^P\sigma_y^2(\tau)$	TVAR $^T\sigma_x^2(\tau)$
white PM	$h_2 f^2$	$\frac{3f_H}{4\pi^2}\frac{h_2}{\tau^2}$ $0.0760\, f_H h_2/\tau^2$	$\frac{3}{8\pi^2}\frac{h_2}{\tau^3}$ $0.0380\, h_2/\tau^3$	$\frac{5f_H}{9\pi^2}\frac{h_2}{\tau^2}$ $0.0563\, f_H h_2/\tau^2$	$\frac{3}{2\pi^2}\frac{h_2}{\tau^3}$ $0.1520\, h_2/\tau^3$	$\frac{1}{8\pi^2}\frac{h_2}{\tau}$ $0.0127\, h_2/\tau$
flicker PM	$h_1 f$	$\frac{3\gamma - \ln 2 + 3\ln(2\pi f_H\tau)}{4\pi^2}\frac{h_1}{\tau^2}$ $[3\gamma - \ln 2 + 3\ln 2\pi]/4\pi^2 = 0.166$	$\frac{(24\ln 2 - 9\ln 3)}{8\pi^2}\frac{h_1}{\tau^2}$ $0.0855\, h_1/\tau^2$	$\simeq \frac{5[\gamma + \ln(\sqrt[10]{48}\,\pi f_H\tau)]}{9\pi^2}\frac{h_1}{\tau^2}$ $5[\gamma + \ln(\sqrt[10]{48}\,\pi)]/9\pi^2 = 0.1187$	$\frac{3\,[\ln(16) - 1]}{2\pi^2}\frac{h_1}{\tau^2}$ $0.2694\, h_1/\tau^2$	$\frac{(8\ln 2 - 3\ln 3)}{8\pi^2}h_1$ $0.0285\, h_1$
white FM	h_0	$\frac{1}{2}\frac{h_0}{\tau}$	$\frac{1}{4}\frac{h_0}{\tau}$	$\frac{1}{3}\frac{h_0}{\tau}$	$\frac{3}{5}\frac{h_0}{\tau}$	$\frac{1}{12}h_0\tau$
flicker FM	$h_{-1} f^{-1}$	$2\ln(2)\, h_{-1}$ $1.386\, h_{-1}$	$\frac{27\ln 3 - 32\ln 2}{8}h_{-1}$ $0.935\, h_{-1}$	$\frac{8\ln 2 - 3\ln 3}{3}h_{-1}$ $0.750\, h_{-1}$	$\frac{2\,[7 - \ln(16)]}{5}h_{-1}$ $1.691\, h_{-1}$	$\frac{27\ln 3 - 32\ln 2}{24}h_{-1}\tau^2$ $0.312\, h_{-1}\tau^2$
random walk FM	$h_{-2} f^{-2}$	$\frac{2\pi^2}{3}h_{-2}\tau$ $6.58\, h_{-2}\tau$	$\frac{11\pi^2}{20}h_{-2}\tau$ $5.43\, h_{-2}\tau$	$\frac{2\pi^2}{9}h_{-2}\tau$ $2.19\, h_{-2}\tau$	$\frac{26\pi^2}{35}h_{-2}\tau$ $7.33\, h_{-2}\tau$	$\frac{11\pi^2}{60}h_{-2}\tau^3$ $1.81\, h_{-2}\tau^3$
integrated flicker FM	$h_{-3} f^{-3}$	not converging	not converging	$\frac{\pi^2[27\ln(3) - 32\ln(2)]}{9}h_{-3}\tau^2$ $8.205\, h_{-3}\tau^2$	not converging	not converging
integrated RW FM	$h_{-4} f^{-4}$	not converging	not converging	$\frac{44\pi^2}{90}h_{-4}\tau^3$ $4.825\, h_{-4}\tau^3$	not converging	not converging
linear drift D_y		$\frac{1}{2}D_y^2\tau^2$	$\frac{1}{2}D_y^2\tau^2$	0	$\frac{1}{2}D_y^2\tau^2$	$\frac{1}{6}D_y^2\tau^4$
spectral response $\lvert H(\theta)\rvert^2$, $\theta = \pi f\tau$		$\frac{2\sin^4(\theta)}{\theta^2}$	$\frac{2\sin^6(\theta)}{\theta^4}$	$\frac{16\sin^6(\theta)}{9\theta^2}$	$\frac{9\left[2\sin^2(\theta) - \theta\sin(2\theta)\right]^2}{2\theta^6}$	$\frac{\tau^2}{3}\frac{2\sin^6(\pi f\tau)}{(\pi f\tau)^4}$
The the cutoff frequency f_H is explicit in AVAR, and implicit in MVAR, PVAR and TVAR due to the sampling frequency $1/\tau_0$.						$^T\sigma_x^2(\tau) = \frac{\tau^2}{3}\, ^M\sigma_y^2(\tau)$