Optimal operation of thermal system based on optimum power flow

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Article Info	ABSTRACT					
Article history: Received Nov 15, 2019 Revised Feb 6, 2020 Accepted Apr 29, 2021	This paper has demonstrated that the Newton-Raphsin (NR) load flow technique can be stretched out to produce optimal load flow (OPF) arrangement that is achievable as for all significant disparity imperatives. These arrangements are frequently desired for arranging and activity. We were examined how the load ought to be shared among different plants, when line misfortunes are represented to limit the absolute activity cost with					
Keywords:	optimal power flow computation with thought about penalty factors, steady fuel cost, and coefficient factors. The IEEE three-machines and nine- Bus					
Economic dispatch Newton-Raphsin technique Optimal power flow Optimal scheduling Power system control	bars system was a tested system. The obtained results were compared by initial operation and equality distribution through the saving cost (\$/year). The comparison of results showed saving more than 1.6 million \$/year under MATLAB V.18a environment.					
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INTRODUCTION 1.

The transmission misfortunes may fluctuate from 5-15% of the complete load, it is fundamental to represent misfortunes while building up a monetary load dispatch arrangement. It will be less expensive to draw more power from the generator which is nearer to the loads. The principle point in the financial dispatch is to limit the complete eighth of generator genuine power at different stations while fulfilling the loads and misfortunes in the transmission lines [1-3]. To start with the economic factor in power system operation, we will focus attention on optimum allocation of generation to each station for various system load level. The transmission loss was expressed in term of B-coefficients [4].

The optimal power flow program (OPF) is utilized to optimize the power flow arrangement of enormous scale power framework. This is finished by limiting chosen objective capacities while keeping up an adequate framework execution as far as generator ability limits and the yield of the repaying capacities, may exhibit financial cost, framework security, or different objectives. Effective reactive power arranging upgrades financial activity just as framework security [5]. The OPF has been examined by numerous analysts and numerous calculations utilizing diverse objective capacities and methods have been displayed [6-8].

MATHEMATICAL MODELING 2.

2.1. Transmission loss coefficient

One of the major steps of the optimal dispatch of generation is to express the system losses in terms of the generator's real power output.

$$P_L = P_{G1}^T H P_{G1}^*$$
(1)

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$$H = \begin{bmatrix} B_{11} & B_{12} & \dots & \dots & B_{1n} & B_{o1}/2 \\ B_{21} & B_{22} & \dots & \dots & B_{2n} & B_{o2}/2 \\ \vdots & \vdots & \dots & \vdots & \vdots \\ B_{ng1} & B_{ng2} & \dots & B_{ngng} & B_{ong}/2 \\ B_{o1}/2 & B_{o2}/2 & \dots & B_{ong}/2 & B_{oo} \end{bmatrix}$$
(2)

The B-coefficients are elements of the framework working state. In the event that new scheduling of generation isn't radically not quite the same as the underlying working condition, the misfortunes coefficient might be expected steady.

2.2. Optimal load flow solution method

The arrangement strategy presented here was initially by Domle and Trinney [3]. It dependent on NR load flow method, a first request angle alteration calculation for limiting the objective capacity and utilization of penalty capacity to represent imbalance requirements on subordinate factors [9-13]. The objective capacity to be limited is the operating cost:

$$C = \sum_{i=1}^{n} C_i P_{Gi} \tag{3}$$

$$P_i + \sum_{j=1}^{n} P_{Gi} V_i V_j Y_{ij} \cos(\theta_{ij} + \delta_i - \delta_j) = 0 \text{ for each PQ bus}$$
(4)

$$Q_i + \sum_{j=1}^{n} P_{Gi} V_i V_j Y_{ij} \cos(\theta_{ij} + \delta_i - \delta_j) = 0 \text{ for each PQ bus}$$
(5)

$$P_i - \sum_{j=1}^{n} P_{Gi} V_i V_j Y_{ij} \cos(\theta_{ij} + \delta_i - \delta_j) = 0 \text{ for each PQ bus}$$
(6)

In (4)-(6) can be expressed in vector form:

$$f(x,y) \rightarrow \begin{bmatrix} x = \{V_i, \delta_i \text{ for } PQ \text{ bus}; \delta_i \text{ for } PV \text{ bus}\} \\ y = \begin{cases} V_1, \delta_1 \text{ for } slack \text{ bus} \\ P_i, Q_i \text{ for } PQ \text{ bus} \\ P_i, V_i \text{ for } PV \text{ bus} \end{cases} \end{bmatrix}$$
(7)

The free factor vector (y) can be apportioned to two sections: the control factor vector (u) which is shifted to accomplish optimum estimation of the target capacity and the vector (p) of fixed or wild parameters. The optimization problem can be restated as [14-16]:

$$min_{u}\mathcal{C}(x,u) \tag{8}$$

Subjected to equality constraints:

$$f(x,u,p) = 0 \tag{9}$$

To solve the streamlining issue, characterize the Lagrangian function as:

$$L(x,u,p) = C(x,u) + \lambda^T f(x,u,p)$$
⁽¹⁰⁾

where *L* Lagrangian function; u: Vector of control variables; x: Vector of dependent variable; p=Vector of uncontrollable variables.

The important conditions to limit the unconstrained Lagrangian function are differentiation of matrix functions:

$$\frac{\partial L}{\partial x} = \frac{\partial C}{\partial x} + \left[\frac{\partial f}{\partial x}\right]^T \lambda = 0 \tag{11}$$

$$\frac{\partial L}{\partial u} = \frac{\partial C}{\partial u} + \left[\frac{\partial f}{\partial u}\right]^{T} \lambda = 0 \tag{12}$$

$$\frac{\partial L}{\partial \lambda} = f(x, u, p) = 0 \tag{13}$$

)

In (11)-(13) are nonlinear algebraic equations and it can be solved by iteration.

3. PROCEDURES OF GRANDIENT METHOD

The computational strategy for nonlinear logarithmic method with applicable detail is given underneath [17-19]:

- a. Make an underlying theory for u, the control factor
- b. Locate a possible NR load flow method from (13) iteratively. Its progressively improves the arrangement x as pursues:

$$X^{(r+1)} = X^{(r)} + \Delta X$$
(14)

$$\Delta X = -(j^{(r)})^{-1} f(X^{(r)}, y$$
(15)

c. Solve (11) for:

$$\lambda = -\left[\left[\frac{\partial f}{\partial u}\right]^T\right]^{-1} \frac{\partial c}{\partial x} \tag{16}$$

d. Compute the gradient;

$$\Delta \tau = \frac{\partial c}{\partial u} + \left[\frac{\partial f}{\partial u}\right]^T \lambda \tag{17}$$

- e. If equals to the prescribed tolerance then, a minimum value has been reached. Else,
- f. Evaluate a new set of control variables:

 $u_{new} = u_{old} + \Delta u \tag{18}$

$$\Delta u = -\alpha \,\Delta \tau \tag{19}$$

Here Δu is the opposite direction step in the gradient:

$$u_{\min \le u \le u_{\max}} \tag{20}$$

$$P_{Gi,min} \le P_{Gi} \le P_{Gi,max} \tag{21}$$

$$u_{i,new} = \begin{bmatrix} u_{i,max} \ if u_{i,old} + \Delta u > u_{i,max} \\ u_{i,min} \ if u_{i,old} + \Delta u < u_{i,min} \\ u_{i,old} + \Delta u \ if \ otherwise \end{bmatrix}$$
(22)

The minimization of L undergoing of constraint (21) are:

$$\frac{\partial L}{\partial ui} \begin{bmatrix} = 0 & if \ u_{ij,min} < u_i < u_{i,max} \\ \le 0 & if \ u_i = u_{ij,max} \\ \ge 0 & if \ u_i = u_{ij,min} \end{bmatrix}$$
(23)

There, presently, in stage (5) for the computational calculation the inclination vector needs to fulfill the optimum condition (23).

 $V_{min} \leq V \leq V_{max}$ on PQ bus (24)

The new objective function becomes:

$$C' = C(X, u) + \sum \omega_j \tag{25}$$

where ω_i is the penalty of each inequality constraint. It can become as:

(

$$\omega_{j} = \begin{bmatrix} g_{j} (X_{j} - X_{j}, max)^{2}; & \text{whenever } X_{j} > X_{j}, max \\ g_{i} (X_{i} - X_{i}, min)^{2}; & \text{whenever } X_{i} > X_{i}, min \end{bmatrix}$$
(26)

$$\frac{\partial L}{\partial x} = \frac{\partial C}{\partial x} + \sum_{j=1}^{n} \frac{\partial \omega_j}{\partial x} + \left[\frac{\partial f}{\partial x}\right]^T \lambda = 0$$
(27)

$$\frac{\partial L}{\partial u} = \frac{\partial C}{\partial u} + \sum_{j=1}^{n} \frac{\partial \omega_j}{\partial u} + \left[\frac{\partial f}{\partial u}\right]^T \lambda = 0$$
(28)

A decent plan is to begin with a low estimation of γj and to build it during the streamlining procedure, if the arrangement surpasses a specific resistance limit. This solution is often required for system planning and operation. [20-24].

4. CASE STUDIES

An OPF was used for the power framework of Figure 1 to get the optimum activity state for the system to lessen unit cost and resolve the active power flow problem. All details of the information data in appendix A, Table A.1 and A.2 [8, 25].



Figure 1. Single line diagram of IEEE 9-Bus power system [20]

5. RESULTS AND DISCUSSION

Figure 2 shows the unit gradual operating cost versus unit yield Pi, assume one unit is operating at a higher steady operating cost than different units. Optimal loading of generators corresponds to the equal incremental cost of all generators (8.1) MWh to redistribute the power generation of three generators and there is a difference between the origin case, before applying optimal power flow calculation, and the new case, after applying optimal power flow calculation as show in Table 1. The main advantage of this concept is to know the saving of total operation cost in (h) or (y/year) as shown in Table 2. The total generation cost of the initial condition is 3326.77 h and the total generation cost with the optimal dispatch is 3515.74 h. This result in a saving of 188.97 h, annually saving =1655377.2 y/year. The total generation cost for the equal load distribution between the generation units is 3255 h, this result in a saving of 60.74 h, annually saving =532082.4 y/year as shown in Table 2. At final iteration the B coefficients are as below:

$$B = \begin{array}{c} 0.0108 & 0.0011 & -0.0006 \\ B = 0.0011 & 0.0308 & -0.0006 \\ -0.0006 & -0.0010 & 0.0078 \\ B0 = 0.0000143 & 0.0002625 & 0.0000096 \\ B00 = 0.0000014232 \end{array}$$



Figure 2. The unit gradual operating cost versus unit yield Pi (MW)

Due No	Voltage	Angle	Load		Gener	Injected	
Bus NO.	Mag.(P.U)	Degree	MW	Mvar	MW	Mvar	Mvar
1	1.040	0.000	0.000	0.000	72.145	27.245	0.000
2	1.025	11.301	0.000	0.000	163.000	-6.432	0.000
3	1.025	2.082	0.000	0.000	85.000	4.738	0.000
4	1.004	-2.759	0.000	0.000	0.000	0.000	0.000
5	0.988	-4.141	90.000	30.000	0.000	0.000	0.000
6	0.991	-0.376	100.000	35.000	0.000	0.000	0.000
7	1.010	3.637	0.000	0.000	0.000	0.000	0.000
8	1.001	5.289	0.000	0.000	0.000	0.000	0.000
9	1.004	-3.100	125.000	50.000	0.000	0.000	0.000
	Total		315.000	115.000	320.145	25.551	0.000

Table 1. Power flow solution by newton-raphson method

Table 2. Saving with deferent operation methods

		0				
Item	Initial operation		Optima	l operation	Equal operation	
	P _i MW	λ \$/MWh	P _i MW	λ \$/MWh	P _i MW	λ \$/MWh
P ₁	150	11.050	96.3	8.434016	117.985	6.947
P_2	80	9.400	230	8.434016	117.985	8.370
P_3	120	10.390	118.8	8.434016	117.985	12.289
Total cost \$/h	3515.74		3326.77		3455	
Saving \$/h			188.97		60.74	
Saving \$/y			1655377.2		532082.4	

6. CONCLUSION

After running OPF the results will appear in Tables 1-2. The total generation cost of the initial condition is 3515.74 \$/h and the total generation cost with the optimal dispatch is 3326.77 \$/h. Result of saving is 188.97 \$/h. That is, with this loading, the total annual saving is over one million \$. In the event that the yield power of that unit is diminished and moved to units with lower steady operating costs, at that point the complete operating cost diminishes. That is, lessening the yield of the unit with higher gradual cost brings about a more prominent cost decline than the cost increment of adding that equivalent yield decreases to units with lower steady costs. Along these lines, all units must work at the equivalent gradual operating costs (the financial dispatch paradigm).

Appendix A

Table A.1. Line data								
Bus	Bus	R	Х	1/2 B	E(II-)			
NO.	NO.	(p.u)	(p.u)	(p.u)	F(HZ)			
1	4	0.00	0.0576	0.000	60			
2	8	0.00	0.0625	0.000	60			
3	6	0.00	0.0586	0.000	60			
4	5	0.017	0.092	0.079	60			
5	6	0.039	0.170	0.179	60			
6	7	0.0119	0.1008	0.1045	60			
7	8	0.0085	0.072	0.0745	60			
8	9	0.032	0.161	0.153	60			
9	4	0.010	0.085	0.088	60			

Table A.2. Bus data

Bus V			GEN	VERATO	LOAD		
Dus	type	(p.u)	P _G (MW)	\mathbf{Q}_{\min}	Q _{max}	P _L (MW)	Q _L (Mvar)
1	Slack	1.04	0.0	-300.0	300.0	0.0	0.0
2	PV	1.025	163.0	-300.0	300.0	0.0	10.0
3	PV	1.025	85.0	-300.0	300.0	0.0	15.0
4	PQ	1.0	0.0	0.0	0.0	0.0	5.0
5	PQ	1.0	0.0	0.0	0.0	90.0	30.0
6	PQ	1.0	0.0	0.0	0.0	0.0	0.0
7	PQ	1.0	0.0	0.0	0.0	100.0	35.0
8	PQ	1.0	0.0	0.0	0.0	0.0	0.0
9	PQ	1.0	0.0	0.0	0.0	125.0	50.0

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