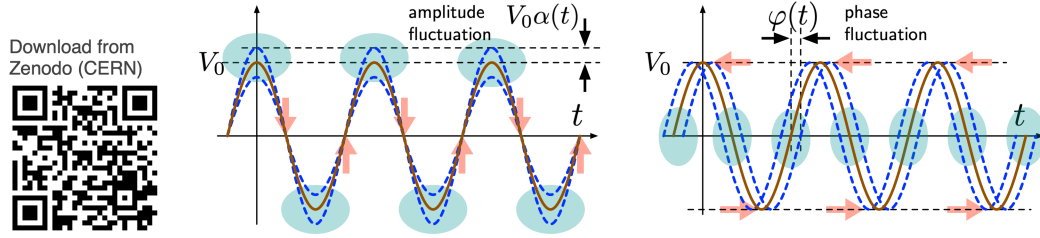


Thanks to FIRST-TF <https://first-tf.com>

Clock signal $v(t) = V_0[1 + \alpha(t)] \cos[2\pi\nu_0 t + \varphi(t)]$



Boldface notation

- total** = nominal + fluctuation
- $\varphi(t) = 2\pi\nu_0 t + \varphi(t)$ phase
- $\nu(t) = \nu_0 + (\Delta\nu)(t)$ frequency
- $x(t) = t + x(t)$ time
- $y(t) = 1 + y(t)$ fractional frequency

Phase noise spectrum

Definition
 $S_\varphi(f)$ [rad^2/Hz] is the one-sided PSD ($f > 0$) of $\varphi(t)$
 $S_\varphi(f) = 2\mathcal{F}\{\mathbb{E}\{\varphi(t)\varphi(t+\tau)\}\}, f > 0$

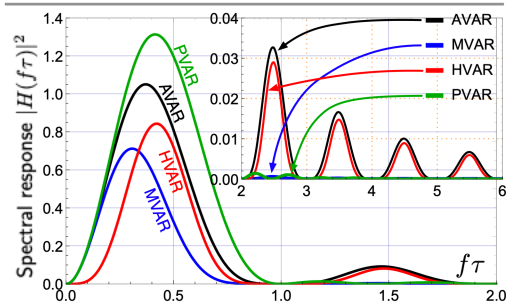
Evaluation
 $S_\varphi(f) = \frac{2}{T} \langle \Phi_T(f) \Phi_T^*(f) \rangle_m$
 avg on m data, $\Phi_T(f) = \text{DFT of } \varphi(t) \text{ truncated on } T$

Usage most often, 'phase noise' refers to $\mathcal{L}(f)$
 Only $10 \log_{10}[\mathcal{L}(f)]$ is used, given in dBc/Hz
 Definition: $\mathcal{L}(f) = \frac{1}{2} S_\varphi(f)$ [the unit c/Hz never used]
 The unit 'c' is a squared angle, $\sqrt{c} = \sqrt{2} \text{ rad} \approx 81^\circ$

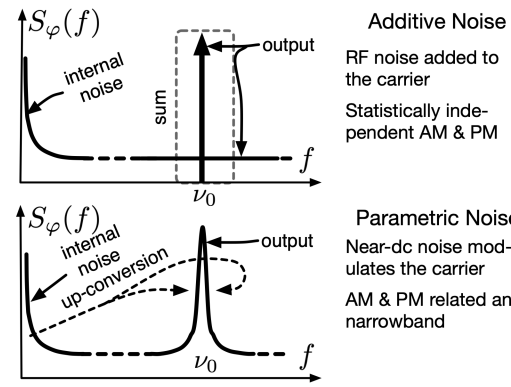
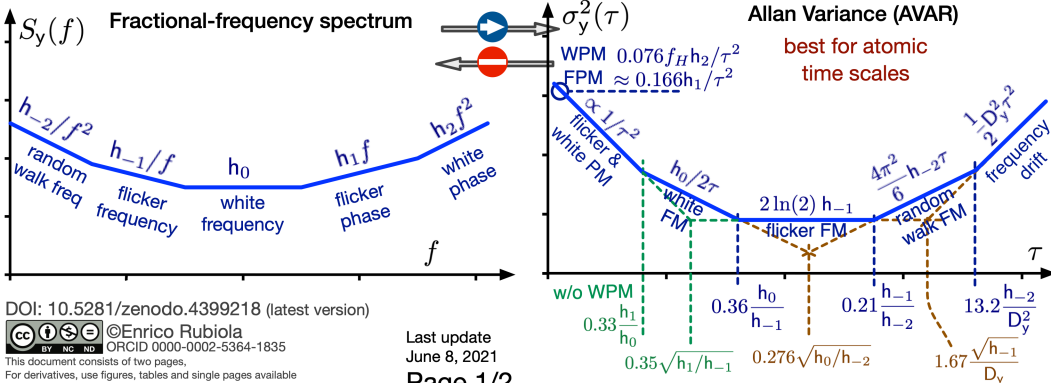
Two-sample (Allan-like) variances

Definition
 $\sigma_y^2(\tau) = \mathbb{E}\left\{\frac{1}{2}[\bar{y}_2 - \bar{y}_1]^2\right\}$ $y(t) \rightarrow \bar{y}$ averaged over τ
 \bar{y}_2 and \bar{y}_1 are contiguous
 Bare mean $\bar{y} \rightarrow$ Allan variance AVAR
 Weighted averages \rightarrow MVAR, PVAR, etc.

Evaluation
 $\sigma_y^2(\tau) = \frac{1}{2(M-1)} \sum_{k=1}^{M-1} [\bar{y}_{k+1} - \bar{y}_k]^2$ M contiguous samples of \bar{y}

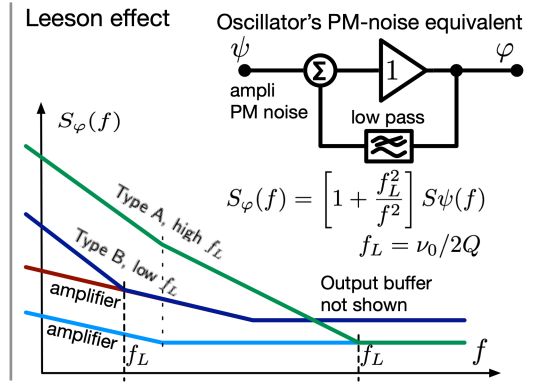


Frequency fluctuation PSD \leftrightarrow Allan Variance

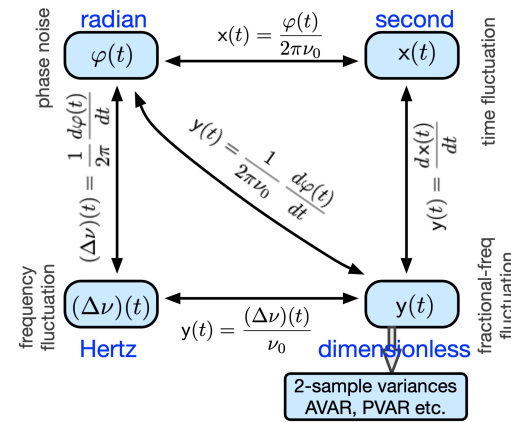


Additive Noise
 RF noise added to the carrier
 Statistically independent AM & PM

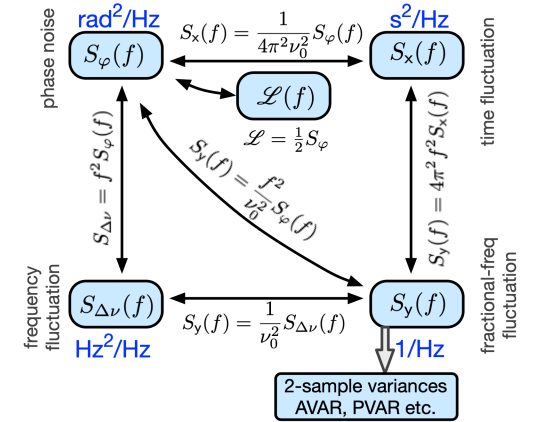
Parametric Noise
 Near-dc noise modulates the carrier
 AM & PM related and narrowband



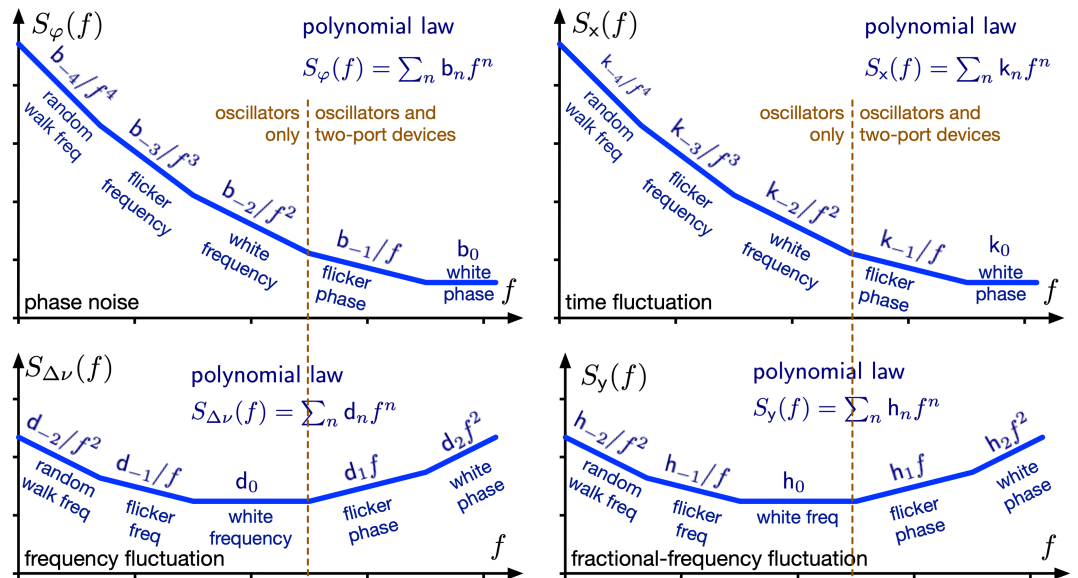
Time Domain



Frequency Domain

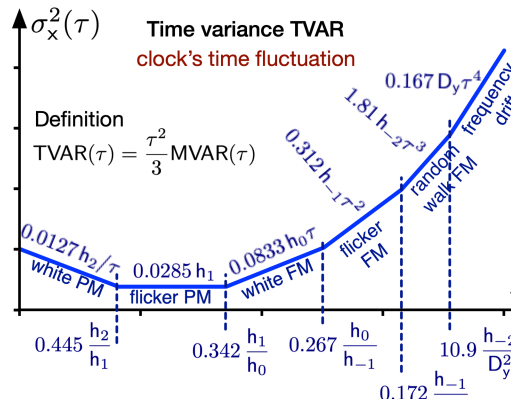
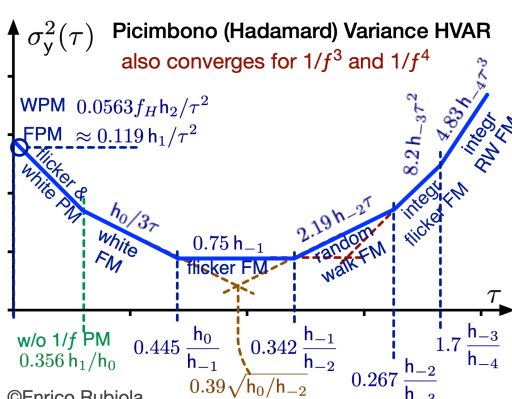
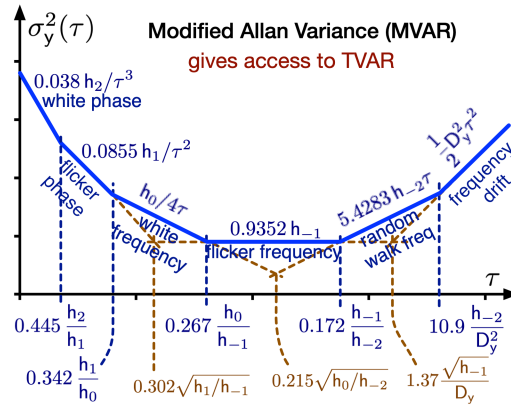
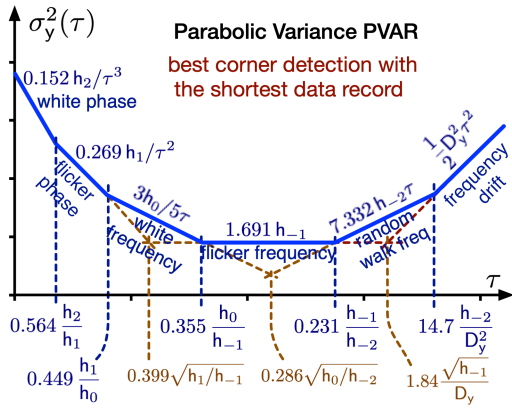


Spectra and Polynomial Law



Frequency Counter		Wavelet Variance	
$\bar{y}(\tau) = \int_{\mathbb{R}} y(t) w(t; \tau) dt$		$\sigma_y^2(\tau) = \mathbb{E} \left\{ \frac{1}{2} [\bar{y}_2 - \bar{y}_1]^2 \right\} = \mathbb{E} \left\{ \int_{\mathbb{R}} [y(t) w(t; \tau)]^2 dt \right\}$	
type of frequency counter	Π	associated variance	AVAR $A \sigma_y^2(\tau)$
	Λ		MVAR $H \sigma_y^2(\tau)$
	Ω		PVAR $P \sigma_y^2(\tau)$
	Δ		HVAR $H \sigma_y^2(\tau)$
Note: this representation is only for theoretical purposes. There are no commercial Δ counters		Note: the wavelet representation hides the second difference in the evaluation of the variance	

Other Two-Sample Variances



Spectra to Variances Conversion

noise type	$S_y(f)$	AVAR $A \sigma_y^2(\tau)$	MVAR $M \sigma_y^2(\tau)$	HVAR $H \sigma_y^2(\tau)$	PVAR $P \sigma_y^2(\tau)$	TVAR $T \sigma_y^2(\tau)$
white PM	$h_2 f^2$	$\frac{3f_H h_2}{4\pi^2 \tau^2}$ $0.0760 f_H h_2 / \tau^2$	$\frac{3 h_2}{8\pi^2 \tau^3}$ $0.0380 h_2 / \tau^3$	$\frac{5f_H h_2}{9\pi^2 \tau^2}$ $0.0563 f_H h_2 / \tau^2$	$\frac{3 h_2}{2\pi^2 \tau^3}$ $0.1520 h_2 / \tau^3$	$\frac{1 h_2}{8\pi^2 \tau}$ $0.0127 h_2 / \tau$
flicker PM	$h_1 f$	$\frac{3\gamma - \ln 2 + 3 \ln(2\pi f_H \tau)}{4\pi^2}$ $[3\gamma - \ln 2 + 3 \ln(2\pi f_H \tau)] / 4\pi^2 = 0.166$	$\frac{(24 \ln 2 - 9 \ln 3) h_1}{8\pi^2 \tau^2}$ $0.0855 h_1 / \tau^2$	$\frac{5[\gamma + \ln(\frac{10}{48} \pi f_H \tau)] h_1}{9\pi^2 \tau^2}$ $\approx \frac{5[\gamma + \ln(\frac{10}{48} \pi)] h_1}{9\pi^2} = 0.1187$	$\frac{3[\ln(16) - 1] h_1}{2\pi^2 \tau^2}$ $0.2694 h_1 / \tau^2$	$\frac{(8 \ln 2 - 3 \ln 3) h_1}{8\pi^2}$ $0.0285 h_1$
white FM	h_0	$\frac{1 h_0}{2 \tau}$	$\frac{1 h_0}{4 \tau}$	$\frac{1 h_0}{3 \tau}$	$\frac{3 h_0}{5 \tau}$	$\frac{1 h_0 \tau}{12}$
flicker FM	$h_{-1} f^{-1}$	$2 \ln(2) h_{-1}$ $1.3863 h_{-1}$	$\frac{27 \ln 3 - 32 \ln 2}{8} h_{-1}$ $0.9352 h_{-1}$	$\frac{8 \ln 2 - 3 \ln 3}{3} h_{-1}$ $0.7498 h_{-1}$	$\frac{2[7 - \ln(16)] h_{-1}}{5}$ $1.691 h_{-1}$	$\frac{27 \ln 3 - 32 \ln 2}{24} h_{-1} \tau^2$ $0.312 h_{-1} \tau^2$
random walk FM	$h_{-2} f^{-2}$	$\frac{2\pi^2}{3} h_{-2} \tau$ $6.5797 h_{-2} \tau$	$\frac{11\pi^2}{20} h_{-2} \tau$ $5.4283 h_{-2} \tau$	$\frac{2\pi^2}{9} h_{-2} \tau$ $2.1933 h_{-2} \tau$	$\frac{26\pi^2}{35} h_{-2} \tau$ $7.3317 h_{-2} \tau$	$\frac{11\pi^2}{60} h_{-2} \tau^3$ $1.81 h_{-2} \tau^3$
integrated flicker FM	$h_{-3} f^{-3}$	not converging	not converging	not converging	not converging	not converging
integrated RW FM	$h_{-4} f^{-4}$	not converging	not converging	not converging	not converging	not converging
linear drift D_y		$\frac{1}{2} D_y^2 \tau^2$	$\frac{1}{2} D_y^2 \tau^2$	0	$\frac{1}{2} D_y^2 \tau^2$	$\frac{1}{6} D_y^2 \tau^2$
spectral response $ H(\theta) ^2, \theta = \pi f \tau$		$\frac{2 \sin^4(\theta)}{\theta^2}$	$\frac{2 \sin^6(\theta)}{\theta^4}$	$\frac{16 \sin^6(\theta)}{9\theta^2}$	$\frac{9 [2 \sin^2(\theta) - \theta \sin(2\theta)]^2}{2\theta^6}$	$\frac{\tau^2}{3} \frac{2 \sin^6(\pi f \tau)}{(\pi f \tau)^4}$
						$\sigma_x(\tau) = \frac{\tau^2}{3} M \sigma_y(\tau)$

MVAR, PVAR and TVAR formulas need $\tau > 1/f_H$, where $f_H < 1/2\tau_0$ is the cutoff frequency, and τ_0 is the sampling interval.