

FUZZY BASED STATOR FLUX OPTIMIZER DESIGN FOR DIRECT TORQUE CONTROL

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ABSTRACT

Direct Torque Control (DTC) is well known as an effective control technique for high performance drives in a wide variety of industrial applications and conventional DTC technique uses two constant reference value: torque and stator flux. In this paper, a new fuzzy based stator flux optimizer has been proposed for DTC controlled induction motor drivers and simulation studies have been carried out with Matlab/Simulink to compare the proposed system behaviours at vary load conditions. The most important feature of the proposed fuzzy logic based stator flux optimizer that it self-regulates the stator flux reference value using the motor load situation without need of any motor parameters. Simulation results show that the performance of the proposed DTC technique has been improved and especially at low-load conditions torque ripples are greatly reduced with respect to the conventional DTC.

KEYWORDS

Induction motor control, Direct torque control, Fuzzy logic optimization, Vector control

1. INTRODUCTION

Vector controls are well-known control techniques in high performance variable speed - load applications for induction motor drivers and can be grouped as field oriented control (FOC) and direct torque control (DTC). The basic idea of vector control is the control of motor flux and torque separately as dc motors. For this aim, motor currents converted two phase vector components using park or Clarke transformations. One of these is the component control flux vector, and the other one is the control torque vector, separately. The main difference between the two methods is that the FOC controls by a rotor or stator field orientation while the DTC controls by stator field observation[1].

FOC was first introduced by Blaschke[2] in the 1970's. It was unrivalled in industrial induction motor drivers until DTC was introduced by Takahashi[3] in the middle of the 1980's. It was a good alternative to FOC due to some well known advantages, such as simple control structure, no need much motor parameters so independency of parameter changes, fast dynamic response. Beside these advantages, DTC scheme still had some disadvantages like high torque and current ripples, variable switching frequency behavior and implementaiton difficulties owing to necessity of low sampling time.

Instantaneous values of the flux and the torque are calculated by using the transformation of the measured currents and the voltages of the motor. In these calculations, all measured electrical values of motor must be converted to stationary α - β reference frame on DTC scheme and conversation matrix as given in (1-3).

$$i_{\alpha\beta 0} = [T] i_{abc} \quad (1)$$

$$V_{\alpha\beta 0} = [T] V_{abc} \quad (2)$$

i_{abc} , v_{abc} measured and $i_{\alpha\beta 0}$, $v_{\alpha\beta 0}$ calculated phase currents and voltages respectively. T is transformation matrix as given in (3).

$$T = \frac{2}{3} \begin{bmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & -\frac{\sqrt{3}}{2} & \frac{\sqrt{3}}{2} \\ \frac{1}{2} & \frac{1}{2} & \frac{1}{2} \end{bmatrix} \quad (3)$$

Stator flux vector can be calculated using the measured current and voltage vectors as given in (4-6).

$$\lambda_{\alpha} = \int (V_{\alpha} - R_s i_{\alpha}) dt \quad (4)$$

$$\lambda_{\beta} = \int (V_{\beta} - R_s i_{\beta}) dt \quad (5)$$

$$\lambda = \sqrt{\lambda_{\alpha}^2 + \lambda_{\beta}^2} \quad (6)$$

Where λ is stator flux space vector, v_{ds} and v_{qs} stator voltage, i_{ds} and i_{qs} line currents in α - β reference frame and R_s stator resistance. The electromagnetic torque of an induction machine is usually estimated as given in (7).

$$T_e = \frac{3}{2} p (\lambda_{\alpha} i_{\beta} - \lambda_{\beta} i_{\alpha}) \quad (7)$$

Where p is the number of pole pairs. An important control parameter on DTC is stator flux vector sector. Stator flux rotate trajectory divided six sector and calculation of stator flux vector sector as given in (8).

$$\theta_{\lambda} = \tan^{-1} \left(\frac{\lambda_{\beta}}{\lambda_{\alpha}} \right) \quad (8)$$

Two different hysteresis comparator generates other control parameters on DTC scheme. Flux hysteresis comparator is two level type while torque comparator is tree level type. These comparators use flux and torque instantaneous error values as input and generates control signals as output. Switching selector unit generates inverter switching states with use of hysteresis comparator outputs and stator flux vector sector.

3. FUZZY FLUX OPTIMIZATION BASED DTC SYSTEM

As can be seen in Fig.1., conventional DTC scheme not only uses speed/torque reference value, but also a stator flux reference value as control parameters. Usually, motors are designed to work their maximum efficiency in their nominal operating point. However, for many industrial control applications motor loading situations can vary from time to time. So, it has been investigated in this paper what if flux reference value is adjusted regarding to the motor load. The value of motor flux should be readjusted when the load is less than the rated value.

Adaptation of flux to load variations can be done in three ways: flux control as a function of torque, flux control based on loss model and flux control by a minimum loss search controller. In this paper, the first way have been preferred. It means that flux controlled as a function of torque but without need of any motor parameters by using fuzzy algorithm. Simulink block diagram of the proposed DTC scheme is given in Fig. 2.

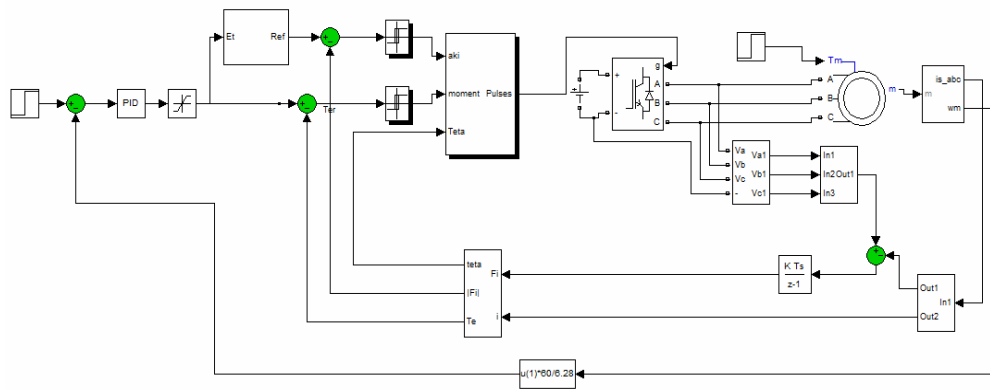
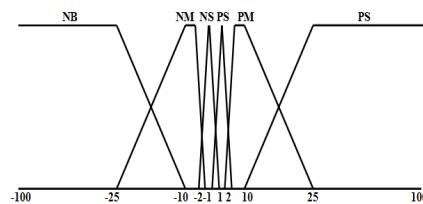
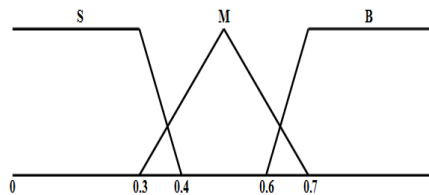


Figure 2. Simulink block diagram of proposed DTC

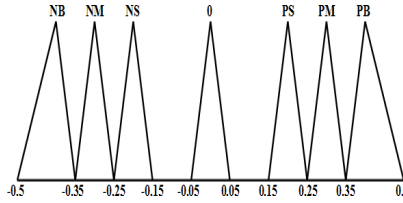
FL controller, which used in proposed DTC scheme, utilizes the torque error and initial value of stator flux reference as control variable and generates amount of change on stator flux reference for next step as output.



(a) Torque error



(b) Initial value of stator flux reference



(c) Change on stator flux reference
Figure. 3. Membership functions

Membership functions of purposed fuzzy control scheme are given in Fig 3. Fuzzy control rules of purposed fuzzy control scheme are designed to minimize torque ripples and rules can be obtained based on prior experience of investigators about DTC scheme. The FL rules shown in Table 1.

Table 1. Rule Table

		Torque error					
		NB	NM	NS	PS	PM	PB
λ_{ref}^{-1}	S	0	PS	PB	0	PS	PB
	M	NS	0	PM	NS	0	PM
	B	NB	NM	0	NB	NM	0

4. SIMULATIONS

Numerical simulations have been carried out to investigate the effects the proposed fuzzy stator flux controller based DTC scheme. Its developed using Matlab/Simulink®. The parameter of the induction motor and simulation used in research as follows:

Table 2. Parameters of Motor and Simulations

Rated Power (kW)	7.5
Rated Voltage (V)	400
Frequency (Hz)	50
Rated speed (rpm)	1440
Stator Resistance (Ω)	0.7334
Pole pairs (p)	2
DC bus voltage (V)	400
Reference speed (rpm)	1500
Cycle period (μ s)	50

In the first step of simulation studies, motor has worked with 0 N.m. reference torque value to compare unloaded behaviors of the motor on conventional and proposed DTC. The torque response curves of conventional DTC and proposed fuzzy stator flux optimizer based DTC are shown Fig 4.

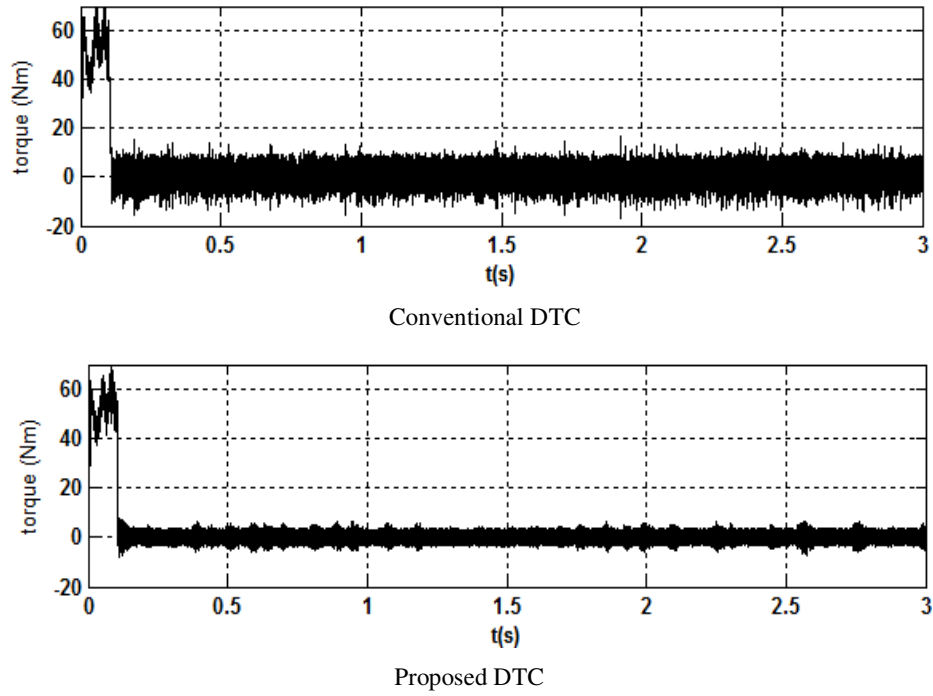


Figure 4. Torque response of conventional DTC and proposed DTC

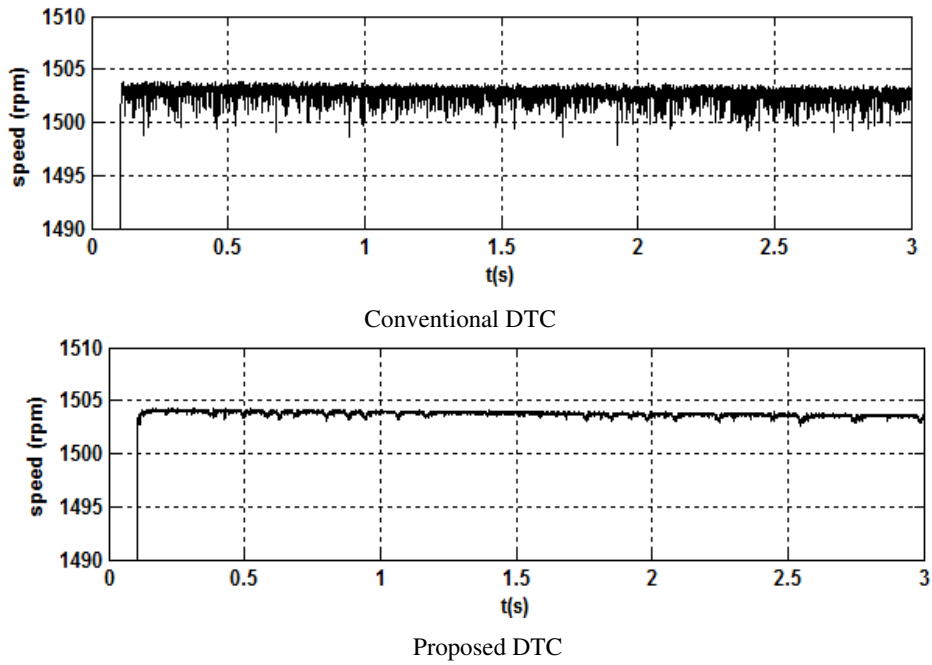
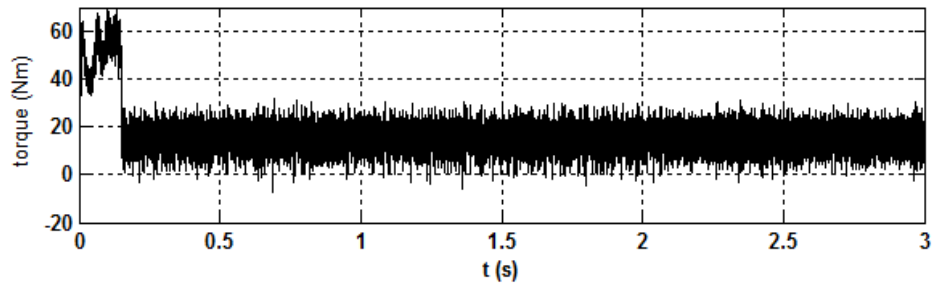


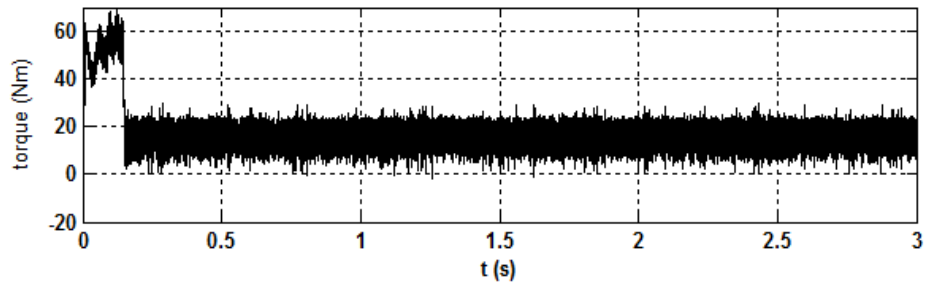
Figure 5. Speed response of conventional DTC and proposed DTC

It can be seen that the proposed stator flux optimization system finds the optimal flux value rapidly and has better performance. Obviously, proposed system with optimized command stator flux has much smaller ripple in torque with respect to the conventional DTC at all working conditions. When the speed responses of motor are compared, its clear that the motor speed ripples has reduced remarkably with proposed DTC controlled motor. The speed response curves of motor with unloaded conditions are given Fig. 5.

In the next step of simulation studies, motor has worked with 15 N.m. reference torque value to compare loaded behaviors of motor on conventional and proposed DTC. The torque and speed response curves of conventional DTC and proposed fuzzy stator flux optimizer based DTC are shown Fig 6. and Fig. 7.

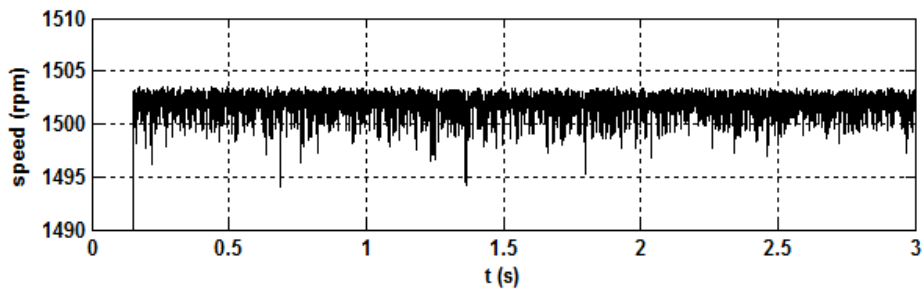


Conventional DTC

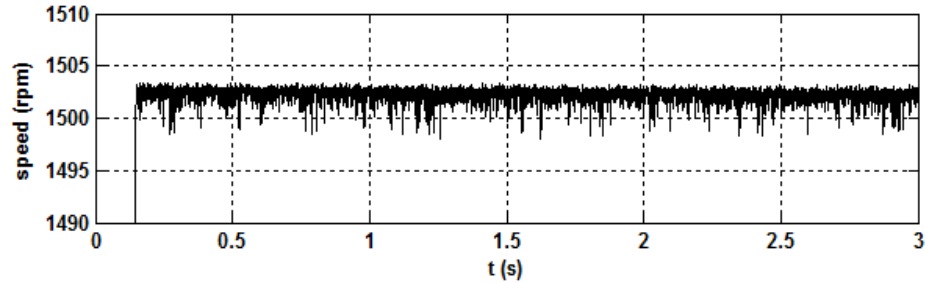


Proposed DTC

Figure 6. Torque response of conventional DTC and proposed DTC



Conventional DTC



Proposed DTC
Figure 7. Speed response of conventional DTC and proposed DTC

The torque and speed response curves show that proposed DTC controlled motor still has lesser torque and speed ripples regarding to conventional DTC controlled one. Transient working behaviors of both control technique are completely same due to optimizer unit works based instantaneous torque error and the torque error value is at largest value in transient working conditions. So, at transient working, the fuzzy optimizer unit creates rate flux value which used in conventional DTC.

6. CONCLUSION

A new fuzzy logic based stator flux control and optimization strategy for DTC controlled induction motors has been presented and investigated in this paper. Fuzzy logic based stator flux optimizer has been designed to determine the reference value. Fuzzy stator flux optimizer uses just torque error and change on torque error without need of any other motor parameter to determine the reference value on the DTC scheme. The proposed DTC system structure also has resistant to changes in motor parameters as conventional DTC due to use of any additionally motor parameters. So, the proposed DTC system can easily applicable every size of motors. The simulation results validate that fuzzy logic based control strategy for stator flux optimization can be successfully cooperated with conventional DTC scheme and achieves a reduction of torque ripple.

7. REFERENCES

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