

A shape optimization problem for stationary Navier-Stokes flows in 3D tubes



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RG8

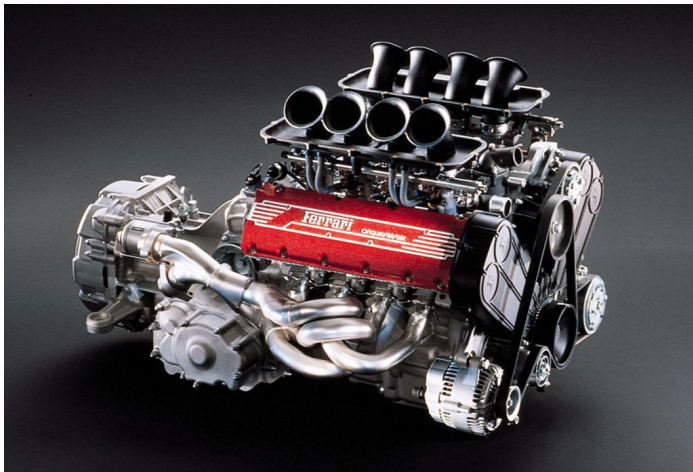
Combustion Engines



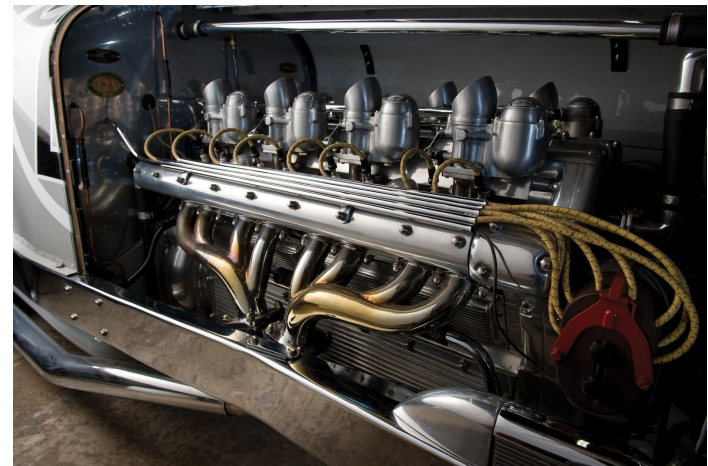
(a) lexusenthusiast.com.



(b) BMW Combustion Engine (bmwblog.com).



(c) Ferrari Combustion Engine.



(d) A beautiful combustion engine.

Figure: Various Combustion Engines.

Modeling Air Ducts

A schematic geometry and its boundary:

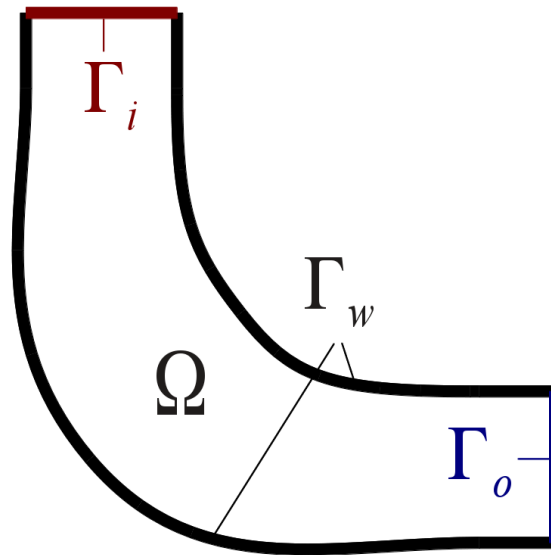


Figure: Simple sketch of an air duct.

Target: *Optimize the shape of air ducts.*

Stationary Navier-Stokes Equations

Stationary NSEs for *velocity* \mathbf{u} and *kinematic pressure* p :

$$\left\{ \begin{array}{ll} -\nu \Delta \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u} + \nabla p = \mathbf{f} & \text{in } \Omega, \\ \nabla \cdot \mathbf{u} = 0 & \text{in } \Omega, \\ \mathbf{u} = \mathbf{f}_{\text{in}} & \text{on } \Gamma_{\text{in}}, \\ \mathbf{u} = \mathbf{0} & \text{on } \Gamma_{\text{wall}}, \\ -\nu \partial_{\mathbf{n}} \mathbf{u} + p \mathbf{n} = \mathbf{0} & \text{on } \Gamma_{\text{out}}, \end{array} \right. \quad (\text{NSEs})$$

where

- ν : kinematic viscosity
- \mathbf{f} : source term
- \mathbf{f}_{in} : inflow profile at Γ_{in}

Main Problem. Find an $\Omega \in \mathcal{O}_{\text{ad}}$ s.t. 2 criteria are considered:

1. Flow Uniformity at the Outlet.

- The uniformity of the flow upon leaving the outlet plane is an important design criterion of e.g. *automotive air ducts*.
- Other use: Efficiency of distributing fresh air inside the car.

Consider:

$$\mathcal{J}_1(\mathbf{u}(\Omega)) := \frac{1}{2} \int_{\Gamma_{\text{out}}} (\mathbf{u} \cdot \mathbf{n} - u_d)^2,$$

where u_d is the *desire velocity* in the outlet plane.

Cost Functionals (2)

2. Dissipated Power. Compute power dissipated by a fluid dynamic device as the net inward flux of energy.

I.e., total pressure, through the device boundaries for smooth pressure p :

$$\mathcal{J}_2((\mathbf{u}, p)(\Omega)) := - \int_{\Gamma} \left(p + \frac{1}{2} |\mathbf{u}|^2 \right) \mathbf{u} \cdot \mathbf{n} d\Gamma.$$

But $p \in L^2(\Omega)$ only, consider an approximation of \mathcal{J}_2 instead:

$$\mathcal{J}_2^\varepsilon((\mathbf{u}, p)(\Omega)) := - \frac{|\Gamma_{\text{in}}|}{|\Gamma_{\text{in}}^\varepsilon|} \int_{\Gamma_{\text{in}}^\varepsilon} \left(p + \frac{1}{2} |\mathbf{u}|^2 \right) \mathbf{u} \cdot \mathbf{n} - \frac{|\Gamma_{\text{out}}|}{|\Gamma_{\text{out}}^\varepsilon|} \int_{\Gamma_{\text{out}}^\varepsilon} \left(p + \frac{1}{2} |\mathbf{u}|^2 \right) \mathbf{u} \cdot \mathbf{n}.$$

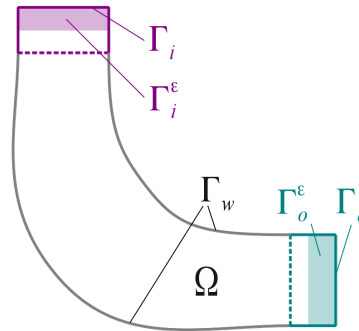


Figure: Simple sketch of Geometry Ω with Modified Inlet $\Gamma_{\text{in}}^\varepsilon$ and Outlet $\Gamma_{\text{out}}^\varepsilon$.

Note. Different measures are applied for Γ_{in} and $\Gamma_{\text{in}}^\varepsilon$.

Mixed Cost Functional & Optimization problem

Mixed cost functional. Take both criteria into effect, with the *weighting parameter* $\gamma \in [0, 1]$:

$$\mathcal{J}_{12}^{\varepsilon, \gamma}((\mathbf{u}, p)(\Omega)) := \gamma \mathcal{J}_1(\mathbf{u}(\Omega)) + (1 - \gamma) \mathcal{J}_2^{\varepsilon}((\mathbf{u}, p)(\Omega)). \quad (\mathcal{J}_{12})$$

Shape Optimization Problem.

Objective: Minimize the cost functional $\mathcal{J}_{12}^{\varepsilon, \gamma} : \mathcal{O}_{\text{ad}} \rightarrow \mathbb{R}$ over some *admissible subset* \mathcal{O}_{ad} of $2^{\mathbb{R}^d} := \{\Omega; \Omega \subset \mathbb{R}^d\}$, i.e.

$$\min_{\Omega \in \mathcal{O}_{\text{ad}}} \mathcal{J}_{12}^{\varepsilon, \gamma}((\mathbf{u}, p)(\Omega)) \text{ s.t. } (\mathbf{u}, p) \text{ solves (NSEs), } \text{Vol}(\Omega) = V_0. \quad (\text{SOP})$$

Lagrangian & Adjoint Method

Lagrangian:

$$\begin{aligned}\mathcal{L}(\mathbf{u}, p, \Omega, \mathbf{v}, q, \mathbf{v}_{\text{in}}, \mathbf{v}_{\text{wall}}, \mathbf{v}_{\text{out}}, v_{\text{Vol}}) &:= \mathcal{J}_{12}^{\varepsilon, \gamma}((\mathbf{u}, p)(\Omega)) \\ &+ \int_{\Omega} \mathbf{v} \cdot (-\nu \Delta \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u} + \nabla p - \mathbf{f}) d\mathbf{x} + \int_{\Omega} q \nabla \cdot \mathbf{u} d\mathbf{x} \\ &+ \int_{\Gamma_{\text{in}}} \mathbf{v}_{\text{in}} \cdot (\mathbf{u} - \mathbf{f}_{\text{in}}) d\Gamma_{\text{in}} + \int_{\Gamma_{\text{wall}}} \mathbf{v}_{\text{wall}} \cdot \mathbf{u} d\Gamma_{\text{wall}} \\ &+ \int_{\Gamma_{\text{out}}} \mathbf{v}_{\text{out}} \cdot (-\nu \partial_{\mathbf{n}} \mathbf{u} + p \mathbf{n}) d\Gamma_{\text{out}} + v_{\text{Vol}} (\text{Vol}(\Omega) - V_0). \quad (\mathcal{L})\end{aligned}$$

Total variation of \mathcal{L} :

$$\delta \mathcal{L} = \frac{\delta \mathcal{L}}{\delta \Omega} + \frac{\delta \mathcal{L}}{\delta \mathbf{u}} + \frac{\delta \mathcal{L}}{\delta p}.$$

Adjoint method. Choose Lagrange multiplier \mathbf{v}, q s.t.

$$\frac{\delta \mathcal{L}}{\delta \mathbf{u}} + \frac{\delta \mathcal{L}}{\delta p} = 0,$$

then the total variation $\delta \mathcal{L}$ can be computed *simply* as:

$$\delta \mathcal{L} = \frac{\delta \mathcal{L}}{\delta \Omega}.$$

Derive Adjoint Systems

Expand $\frac{\delta \mathcal{L}}{\delta \mathbf{u}} + \frac{\delta \mathcal{L}}{\delta p} = 0$ as

$$\begin{aligned} \frac{\partial \mathcal{J}_{12}^{\varepsilon, \gamma}}{\partial \mathbf{u}} \delta \mathbf{u} + \frac{\partial \mathcal{J}_{12}^{\varepsilon, \gamma}}{\partial p} \delta p + \int_{\Omega} \mathbf{v} \cdot [(\delta \mathbf{u} \cdot \nabla) \mathbf{u} + (\mathbf{u} \cdot \nabla) \delta \mathbf{u} - \nu \Delta \delta \mathbf{u}] d\mathbf{x} \\ - \int_{\Omega} q \nabla \cdot \delta \mathbf{u} d\mathbf{x} + \int_{\Omega} \mathbf{v} \cdot \nabla \delta p d\mathbf{x} + \int_{\Gamma_{\text{in}}} \mathbf{v}_{\text{in}} \cdot \delta \mathbf{u} d\Gamma_{\text{in}} \\ + \int_{\Gamma_{\text{wall}}} \mathbf{v}_{\text{wall}} \cdot \delta \mathbf{u} d\Gamma_{\text{wall}} + \int_{\Gamma_{\text{out}}} (-\nu \mathbf{v}_{\text{out}} \cdot \partial_{\mathbf{n}}(\delta \mathbf{u}) + \mathbf{v}_{\text{out}} \cdot \delta p \mathbf{n}) d\Gamma = 0. \end{aligned}$$

Decompose: $\mathcal{J}_{12}^{\varepsilon, \gamma} = \int_{\Gamma} J_{\Gamma} d\Gamma + \int_{\Omega} J_{\Omega} d\Omega$.

Integrate by parts:

$$\begin{aligned} \int_{\Omega} (-\nabla \cdot \mathbf{v} + \partial_p \mathcal{J}_{\Omega}) \delta p d\mathbf{x} \\ + \int_{\Omega} [-\nabla \mathbf{v} \cdot \mathbf{u} - (\mathbf{u} \cdot \nabla) \mathbf{v} - \nu \Delta \mathbf{v} + \nabla q + \partial_{\mathbf{u}} \mathcal{J}_{\Omega}] \cdot \delta \mathbf{u} \\ + \text{Boundary integral terms} = 0, \end{aligned}$$

for any variation $\delta \mathbf{u}$ and δp .

Collect terms on each $\int_{\Omega}(\cdots)\delta\mathbf{u}$, $\int_{\Omega}(\cdots)\delta p$, $\int_{\Gamma}(\cdots)\delta\mathbf{u}$, $\int_{\Gamma}(\cdots)\delta p$, obtain:

Adjoint Navier-Stokes equations.

$$\left\{ \begin{array}{ll} -(\nabla \mathbf{v})^{\top} \mathbf{u} - \nabla \mathbf{v} \cdot \mathbf{u} + \nabla q - \nu \Delta \mathbf{v} = (\gamma - 1)k_{\varepsilon} \left[\left(p + \frac{1}{2}|\mathbf{u}|^2 \right) \mathbf{n} + (\mathbf{u} \cdot \mathbf{n})\mathbf{u} \right], & \text{in } \Omega, \\ -\nabla \cdot \mathbf{v} = (\gamma - 1)k_{\varepsilon} \mathbf{u} \cdot \mathbf{n} & \text{in } \Omega, \\ \mathbf{v} = 0 & \text{on } \Gamma_{\text{in}} \cup \Gamma_{\text{wall}}, \\ -\nu \partial_{\mathbf{n}} \mathbf{v} - \mathbf{n}(\mathbf{u} \cdot \mathbf{v}) - (\mathbf{u} \cdot \mathbf{n})\mathbf{v} + q\mathbf{n} = \gamma(\mathbf{u} \cdot \mathbf{n} - \bar{u}) & \text{on } \Gamma_{\text{out}}, \end{array} \right.$$

with

$$k_{\varepsilon}(x) := \frac{|\Gamma_{\text{in}}|}{|\Gamma_{\text{in}}^{\varepsilon}|} \chi_{\overline{\Gamma_{\text{in}}^{\varepsilon}}}(x) + \frac{|\Gamma_{\text{out}}|}{|\Gamma_{\text{out}}^{\varepsilon}|} \chi_{\overline{\Gamma_{\text{out}}^{\varepsilon}}}(x), \quad \forall x \in \Omega,$$

Shape Derivatives

Describe *perturbed domains* via a *reference domain* Ω :

$$\Omega_t := T_t[V](\Omega) := \{x + tV(x); x \in \Omega\}.$$

Definition (Shape derivative (Sokolowski Zolesio 1992))

Let $D \subset \mathbb{R}^d$. A function $J : 2^D \rightarrow \mathbb{R}$ is said to be *shape differentiable*, if the limit

$$dJ(\Omega)[V] := \lim_{t \downarrow 0} \frac{J(T_t[V](\Omega)) - J(\Omega)}{t}$$

exists for all directions V and if the mapping $V \mapsto dJ(\Omega)[V]$ is linear and continuous.

Typical choices for $T_t[V]$.

- *Perturbation of Identity*: $T_t[V](x) = x + tV(x)$, $t \geq 0$, $x \in \Omega$.
- *Speed method*: $T_t[V](x) = \varphi(t, x)$ where φ solves the ODE

$$\frac{\partial \varphi}{\partial t}(t, x) = V(t, x), \quad \varphi(0, x) = x, \quad \forall (t, x) \in [0, \infty) \times \Omega.$$

Applied above formulas, obtain:

$$d\mathcal{J}_{12}^{\varepsilon,\gamma}(\Omega)[V] = \int_{\Gamma_{\text{wall}}} (\partial_{\mathbf{n}}\mathbf{u} \cdot \partial_{\mathbf{n}}\mathbf{v})(V \cdot \mathbf{n}).$$

Shape gradient:

$$D\mathcal{J}_{12}^{\varepsilon,\gamma}(\Omega) = -(\partial_{\mathbf{n}}\mathbf{u} \cdot \partial_{\mathbf{n}}\mathbf{v})\mathbf{n}|_{\Gamma_{\text{wall}}}.$$

Geometrical Constraints (1)

Impose further restrictions on the possible design by geometrical constraints:

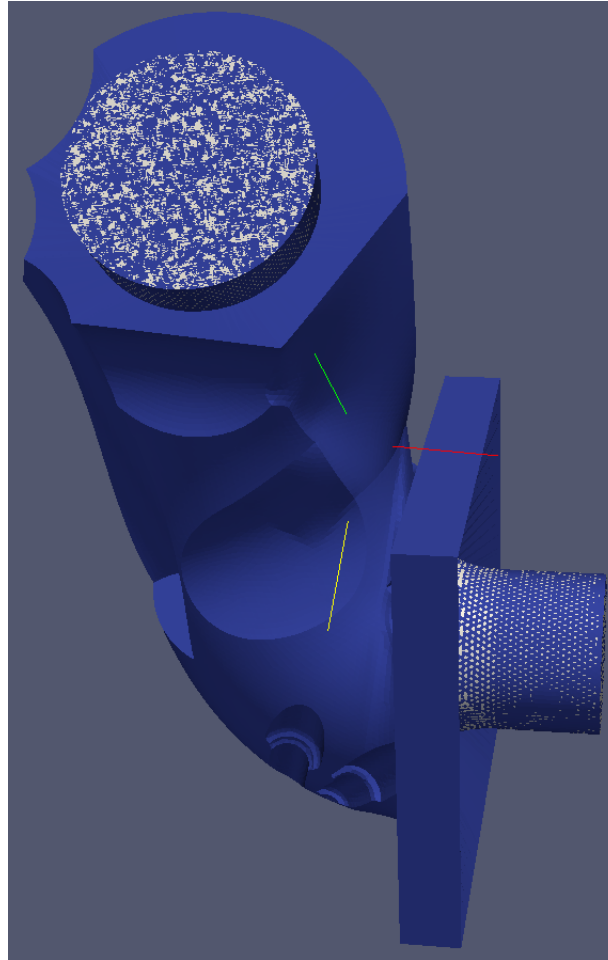


Figure: A design space (blue) contains a tube.

Geometrical Constraints (2)

Minimization problem with **geometrical constraint G** :

$$\min_{\Omega \subset \mathcal{O}_{\text{ad}} \cap G} \mathcal{J}_{12}^{\varepsilon, \gamma}((\mathbf{u}, \mathbf{p})(\Omega)) + \alpha \mathcal{G}(\Omega) \text{ s.t. } (\mathbf{u}, p) \text{ solves (NSEs), } \text{Vol}(\Omega) = V_0,$$

with $\alpha > 0$ and $\mathcal{G}(\Omega) := \int_{\Omega} l_G(x)$.

- **Barrier method.** $l_G(x) := |\log d(x, G^c)|$ with $G^c = \mathbb{R}^d \setminus G$.
- **Penalty method.** $l_G(x) := (d(x, G))^{\beta}$ with $\beta \geq 1$ and the distance function $d(x, G) := \min_{y \in G} |x - y|$.

Additional shape derivative term:

$$d\mathcal{G}(\Omega)[V] = \int_{\Gamma_{\text{wall}}} (V \cdot \mathbf{n}) l_G(s) ds.$$

Gradient Descent Algorithm (1)

A gradient descent algorithm using Armijo linesearch:

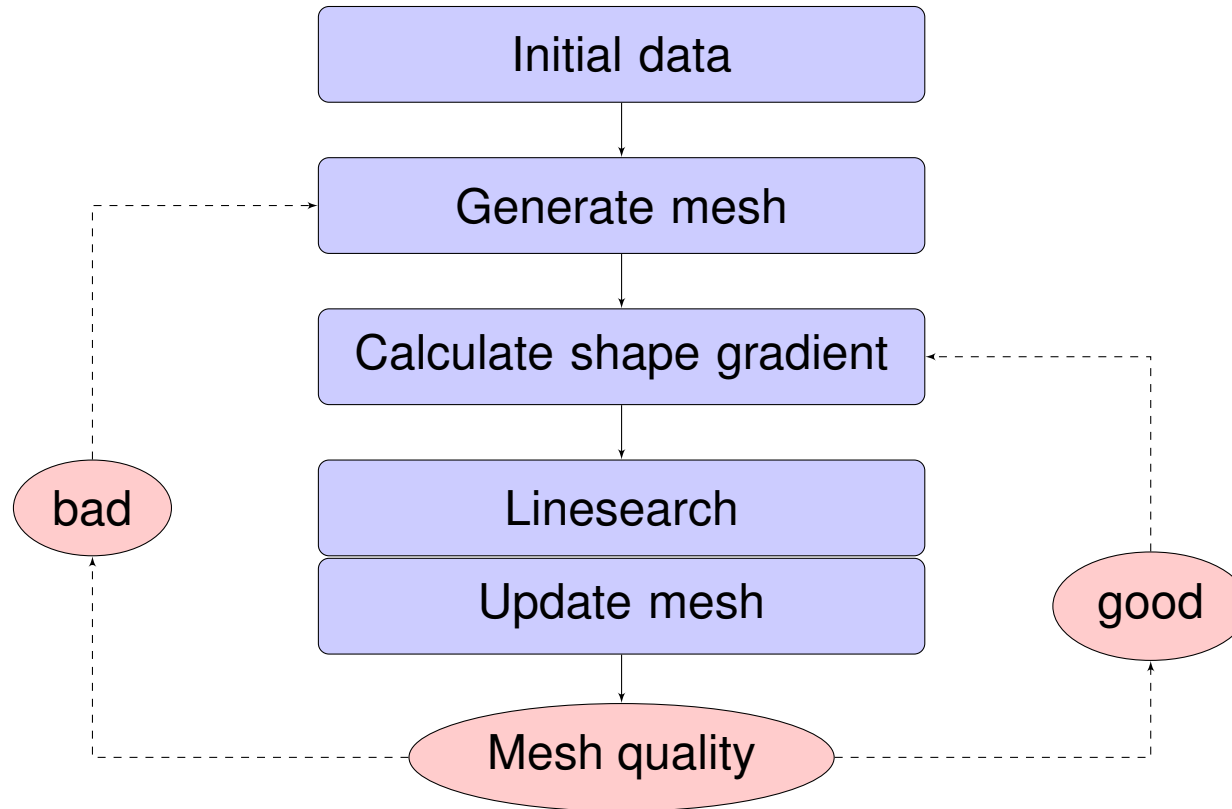


Figure: A Gradient Descent Algorithm.

- Kinematic viscosity $\nu \approx 1.56659 \times 10^{-5}$.
- Weighting parameter $\gamma = 0$: Only consider $\mathcal{J}_2^\varepsilon$.

Numerical Results (1)

Choose the weighting parameter $\gamma = 0$.

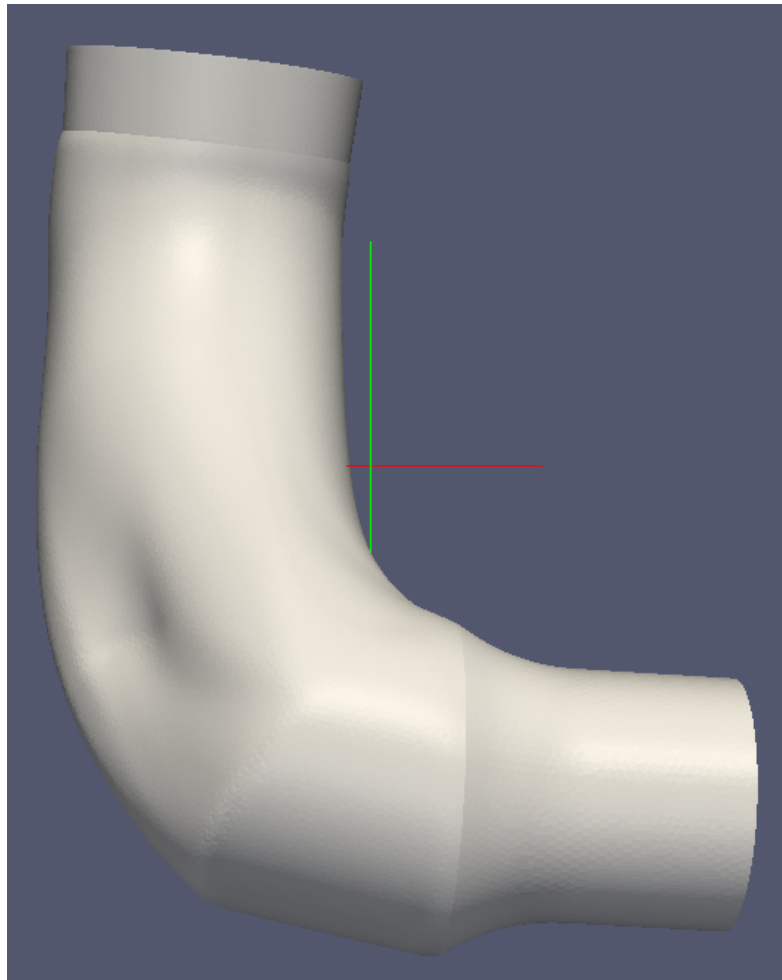
Run 30 gradient-descent iterations (≈ 10 days).

Iteration	\mathcal{J}_{12}	Reduce
0	182.07227883754	0%
1	180.929940529294	0.63%
2	180.136772627044	1.06%
3	179.571215644196	1.37%
4	179.091345594335	1.64%
5	178.804927417778	1.79%
6	178.048912220916	2.2%
7	177.935313457448	2.27%
8	177.907822689922	2.29%
9	177.368528982915	2.58%
10	177.354503052929	2.59%
11	177.353679949393	2.59%
12	176.874239498098	2.85%
13	176.872879859059	2.86%
14	176.872793330895	2.86%

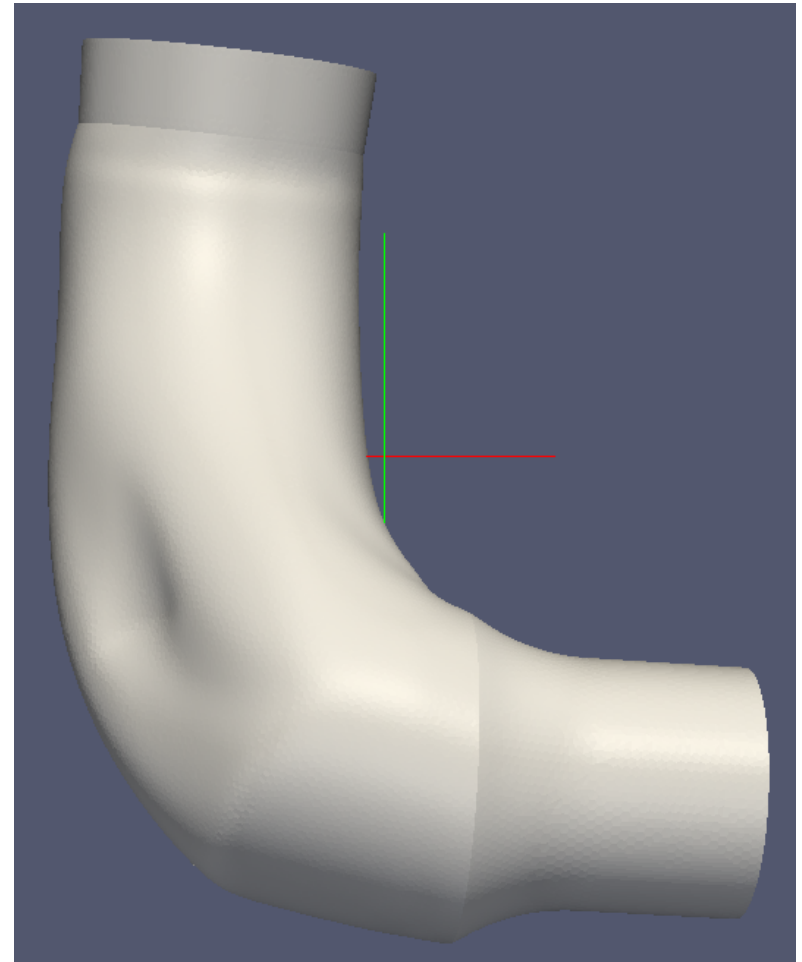
Numerical Results (2)

Iteration	\mathcal{J}_{12}	Improvement
15	176.397008800941	3.12%
16	176.39201327152	3.12%
17	176.391228177362	3.12%
18	176.027299330372	3.32%
19	176.025503228316	3.32%
20	176.025478930617	3.32%
21	175.583524795214	3.56%
22	175.580539111237	3.57%
23	175.580538614767	3.57%
24	175.377206316433	3.68%
25	175.375696397475	3.68%
26	175.375696266596	3.68%
27	175.117224921322	3.82%
28	175.115844803727	3.82%
29	174.771828640699	4.01%
30	174.656762605995	4.07%

Simulation Results



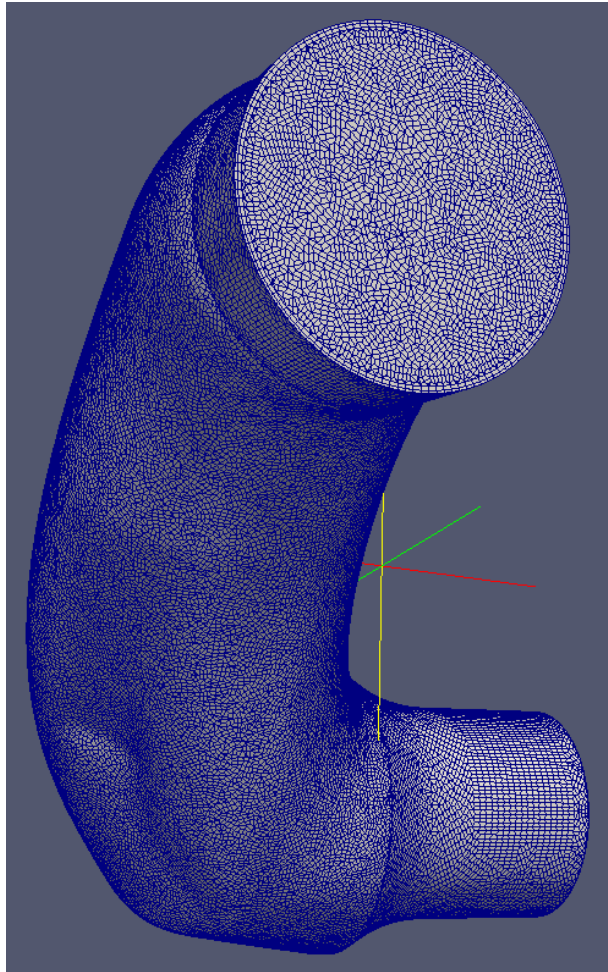
(a) Initial tube.



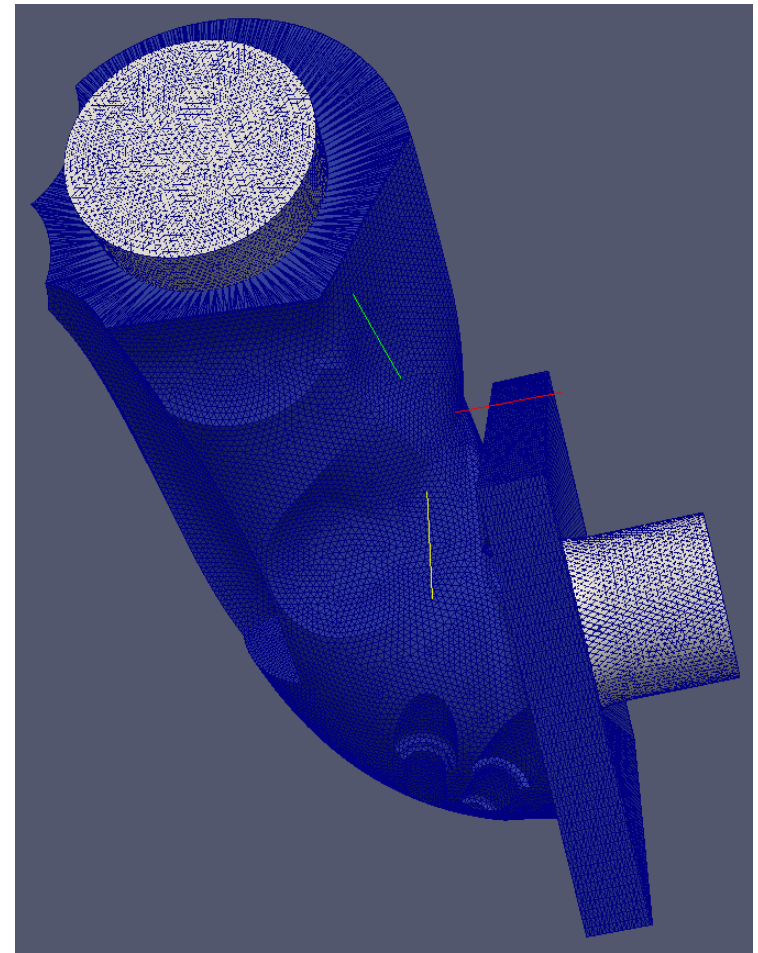
(b) Optimized tube after 30 gradient iterations.

Figure: Initial vs. Optimized Tubes.

Meshes



(a) Tube with Mesh.



(b) Geometrical Constraint with Mesh.

- **Model reduction:** Replace NSEs with high Reynolds number with turbulence models in 3D
- Small eddies resolution
- Time dependent case

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