

Acoustic characterization of absorbing materials using dynamic mode decomposition techniques

Gonzalo Carazo Barbero



Companies Involved

- **ITMATI** (Thechnological Institute for Industrial Mathematics)
- **Microflown Technologies**
- **ROMSOC Project** (Reduced Order Modeling, Simulation and Optimization of Coupled Systems)



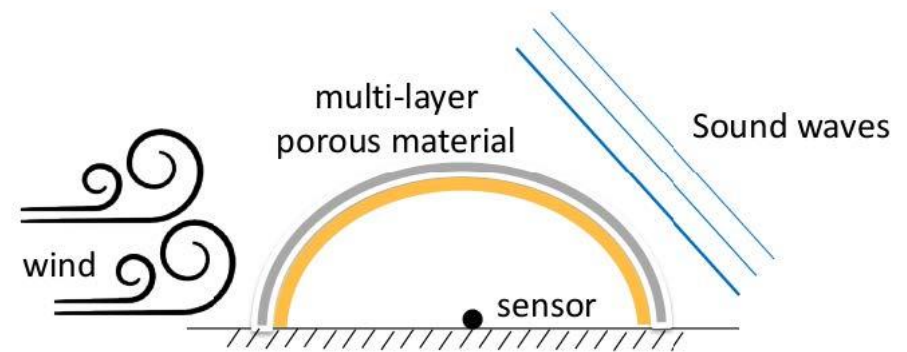
Introduction

Ashwin Nayak's PhD Thesis:
3D unbounded coupled model
in the frequency domain

Simplified Problem:
1D acoustic coupled
model in the time domain

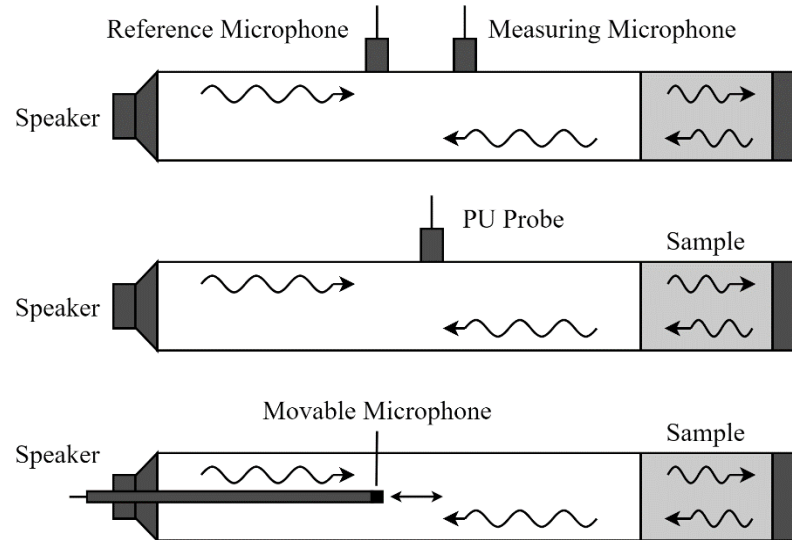
Phases of the project:

1. Numerical simulation
2. Validating the models
3. Applying DMD

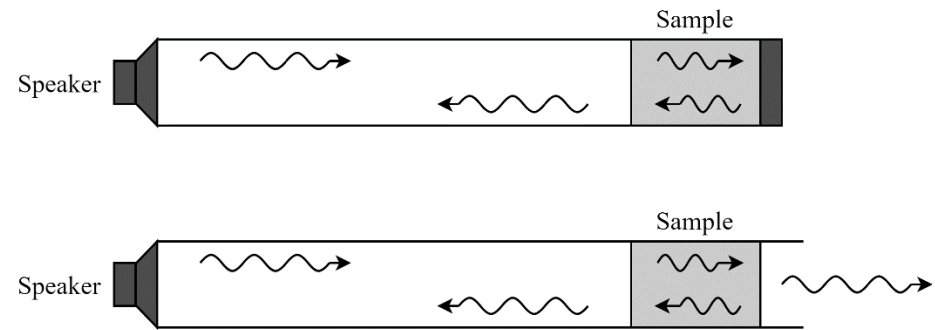


Motivation of the Physical Setting

Experimental Settings



Simulated settings



Holmarc Opto-Mechatronics Impedance tube*

Used Models

Fluid Models:

\mathcal{P}_1 : Fluid with rigid boundaries

\mathcal{P}_2 : Fluid with rigid-transparent boundaries

Rigid Porous Models:

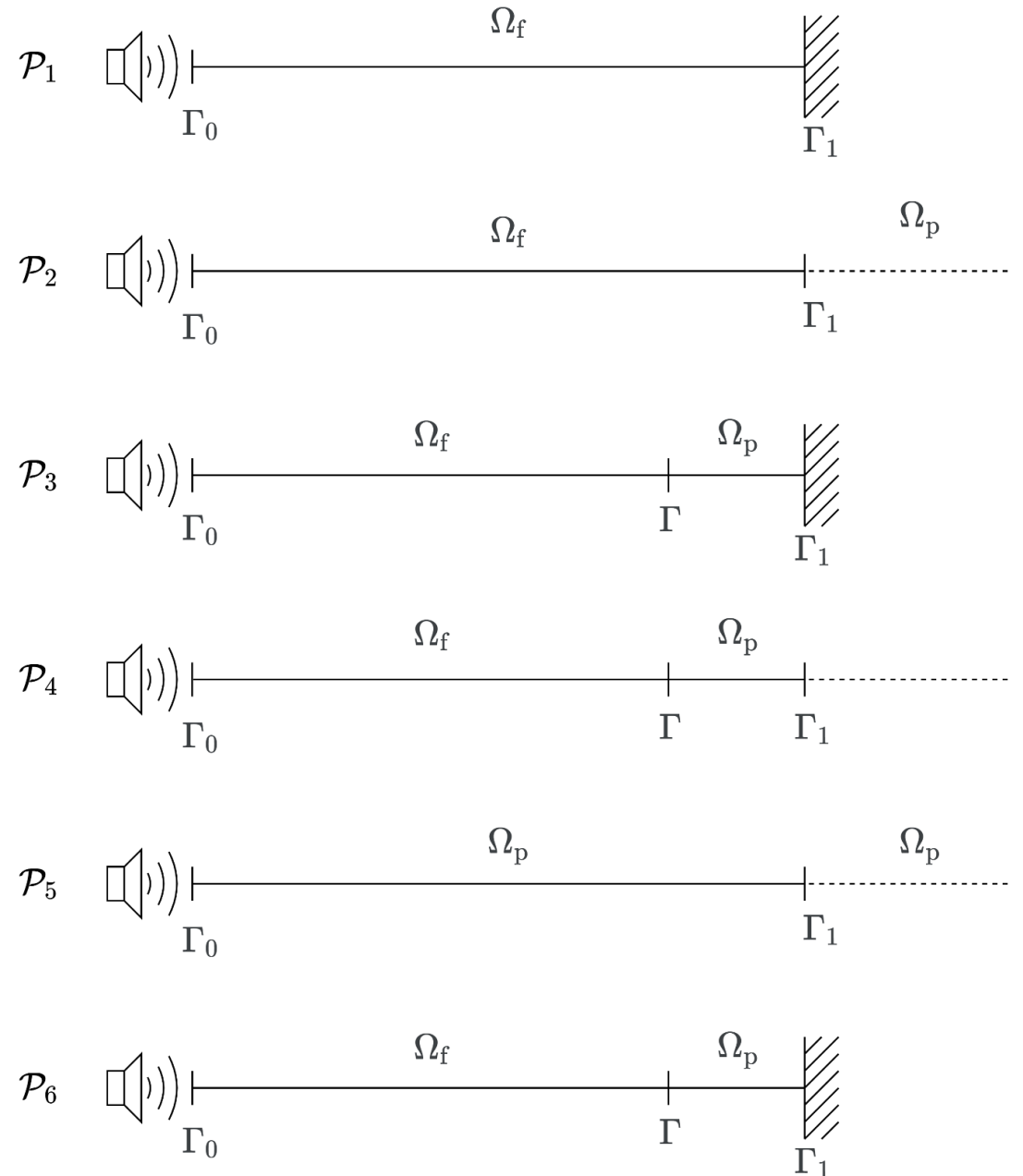
\mathcal{P}_3 : Coupled with rigid boundaries

\mathcal{P}_4 : Coupled with rigid-transparent boundaries

Poro-Elastic Models:

\mathcal{P}_5 : Umnova's low frequency approx. on porous

\mathcal{P}_6 : Umnova's low frequency approx. Coupled



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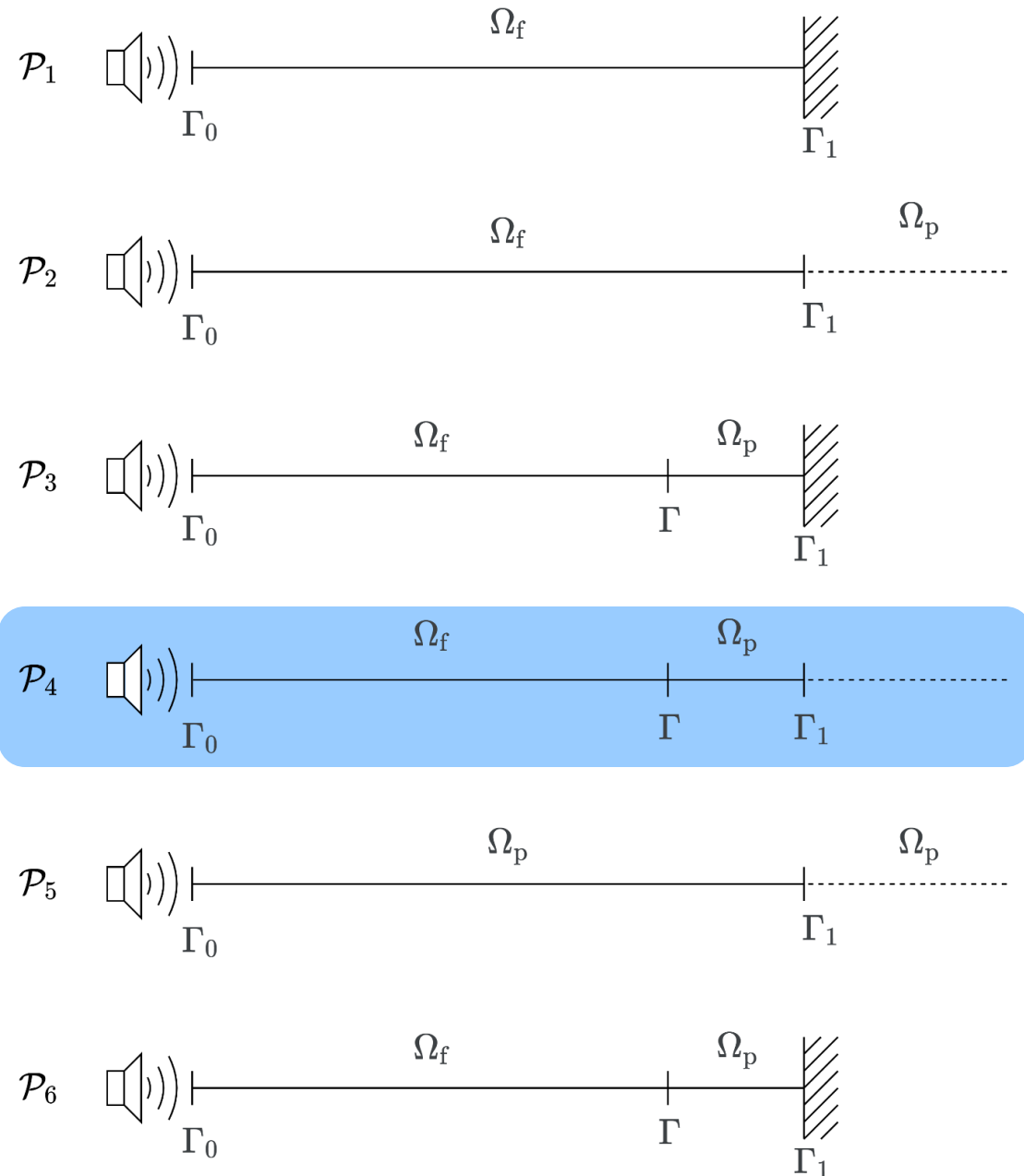
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Porosity-Elastic Models:

\mathcal{P}_5 : Umnova's low frequency approx. on porous

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Differential Formulation

Fluid – Rigid Porous Coupled Model



{	$\rho_f \partial_t^2 u_f - \rho_f c_f^2 \partial_x^2 u_f = f \quad \text{in } (0, T) \times \Omega_f,$	Interior domain
	$\rho_p \partial_t^2 u_p - \frac{\rho_p c_p^2}{\phi \gamma_p} \partial_x^2 u_p + \sigma \partial_t u_p = 0 \quad \text{in } (0, T) \times \Omega_p,$	
	$u_f = \phi u_p \quad \text{on } (0, T) \times \Gamma,$	Coupling boundary
	$\rho_f c_f^2 \partial_x u_f = \frac{\rho_p c_p^2}{\phi \gamma_p} \partial_x u_p \quad \text{on } (0, T) \times \Gamma,$	
	$u_f = 0 \quad \text{on } (0, T) \times \Gamma_0,$	Exterior boundaries
	$u_f = \phi u_p \quad \text{on } (0, T) \times \Gamma_1,$	
	$\rho_f c_f^2 \partial_x u_f = \frac{\rho_p c_p^2}{\phi \gamma_p} \partial_x u_p \quad \text{on } (0, T) \times \Gamma_1,$	
$\partial_t u_f + c_f \partial_x u_f = 0 \quad \text{on } (0, T) \times \Gamma_1.$		

Differential Formulation

Fluid – Rigid Porous Coupled Model



$$\tilde{u}_p = \phi u_p$$

{	$\rho_f \partial_t^2 u_f - \rho_f c_f^2 \partial_x^2 u_f = f \quad \text{in } (0, T) \times \Omega_f,$	Interior domain
	$\frac{\rho_p}{\phi} \partial_t^2 \tilde{u}_p - \frac{\rho_p c_p^2}{\phi^2 \gamma_p} \partial_x^2 \tilde{u}_p + \frac{\sigma}{\phi} \partial_t \tilde{u}_p = 0 \quad \text{in } (0, T) \times \Omega_p,$	
	$u_f = \tilde{u}_p \quad \text{on } (0, T) \times \Gamma,$	Coupling boundary
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	$u_f = 0 \quad \text{on } (0, T) \times \Gamma_0,$	Exterior boundaries
	$\partial_t \tilde{u}_p + \frac{\rho_p c_p^2}{\rho_f c_f \phi^2 \gamma_p} \partial_x \tilde{u}_p = 0 \quad \text{on } (0, T) \times \Gamma_1.$	

Variational Formulation

Fluid – Rigid Porous Coupled Model



$$\begin{aligned}
 & \int_{\Omega_f} \rho_f \partial_t^2 u_f \cdot w \, dx + \int_{\Omega_p} \frac{\rho_p}{\phi} \partial_t^2 \tilde{u}_p \cdot w \, dx && \longrightarrow \text{Mass term} \\
 & + \int_{\Omega_p} \frac{\sigma}{\phi} \partial_t \tilde{u}_p \cdot w \, dx + (\rho_f c_f \partial_t \tilde{u}_p \cdot w)|_{\Gamma_1} && \longrightarrow \text{Damping term} \\
 & + \int_{\Omega_f} \rho_f c_f^2 \partial_x u_f \cdot \partial_x w \, dx + \int_{\Omega_p} \frac{\rho_p c_p^2}{\phi^2 \gamma_p} \partial_x \tilde{u}_p \cdot \partial_x w \, dx && \longrightarrow \text{Stiffness term} \\
 & = \int_{\Omega_f} f \cdot w \, dx. && \longrightarrow \text{External forces}
 \end{aligned}$$

Discretization Algorithms

Finite Element Method

Spatial Discretization: Piecewise linear finite element method

Basis functions

$$\psi_i(x) = \begin{cases} \frac{x - x_{i-1}}{\Delta x} & \text{in } x_{i-1} < x \leq x_i, \\ -\frac{x - x_{i+1}}{\Delta x} & \text{in } x_i < x \leq x_{i+1}, \\ 0 & \text{elsewhere,} \end{cases}$$

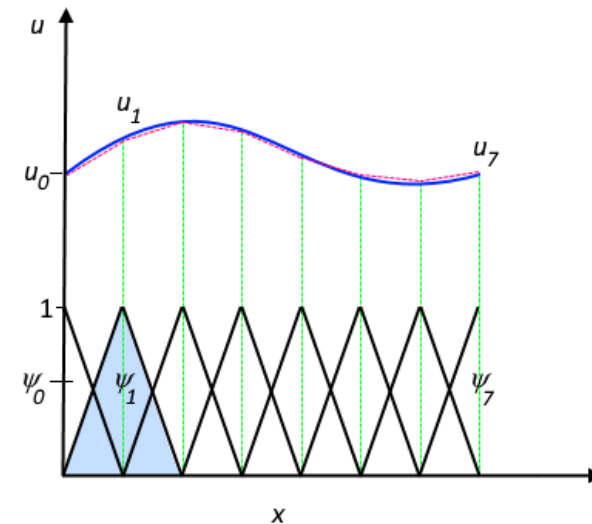
Finite Element method discretization

$$\underbrace{\sum_{i=0}^N M_{j,i} \ddot{u}_i^h}_{\text{Mass}} + \underbrace{\sum_{i=0}^N C_{j,i} \dot{u}_i^h}_{\text{Damping}} + \underbrace{\sum_{i=0}^N K_{j,i} u_i^h}_{\text{Stiffness}} = \underbrace{f_j}_{\text{External Forces}}$$

Discrete solution

$$u^h(t, x) = \sum_{i=0}^N u_i^h(t) \psi_i(x),$$

$$w^h(x) = \sum_{i=0}^N w_i^h \psi_i(x).$$



Discretization Algorithms

Newmark-Beta Method

Time Discretization: Newmark-beta integration method

$$M\ddot{u} + C\dot{u} + Ku = f$$

$$\begin{cases} u^{n+1} = u^n + \Delta t \dot{u}^n + \left(\frac{1}{2} - \beta\right) \Delta t^2 \ddot{u}^n + \beta \Delta t^2 \ddot{u}^{n+1}, \\ \dot{u}^{n+1} = \dot{u}^n + (1 - \gamma) \Delta t \ddot{u}^n + \gamma \Delta t \ddot{u}^{n+1}, \\ M\ddot{u}^{n+1} + C\dot{u}^{n+1} + Ku^{n+1} = f^{n+1}. \end{cases}$$

In the implementation it is divided in **initialization**, **explicit approximation** and **prediction**.

In order to get accurate results it meets the CFL condition:

$$C = \frac{\Delta t}{\Delta x} c_f \leq C_{\max}.$$

Reduced Order Methods

Singular Value Decomposition

- **Singular Value Decomposition (SVD):** Exact decomposition

$$A = U\Sigma V^T$$

$$A = \underbrace{\begin{bmatrix} | & | & \dots & | \\ u_1 & u_2 & \dots & u_n \\ | & | & \dots & | \end{bmatrix}}_{n \times n} \underbrace{\begin{bmatrix} \sigma_1 & & & \\ & \sigma_2 & & \\ & & \ddots & \\ & & & \sigma_{\min(n,m)} \end{bmatrix}}_{n \times m} \underbrace{\begin{bmatrix} - & v_1 & - \\ - & v_2 & - \\ & \vdots & \\ - & v_m & - \end{bmatrix}}_{m \times m} .$$

Singular left vectors
Singular values
Singular right vectors

- **Truncated SVD:** Approximated decomposition

$$A \approx U_r \Sigma_r V_r^T$$

$$A \approx \underbrace{\begin{bmatrix} | & | & \dots & | \\ u_1 & u_2 & \dots & u_r \\ | & | & \dots & | \end{bmatrix}}_{n \times r} \underbrace{\begin{bmatrix} \sigma_1 & & & \\ & \sigma_2 & & \\ & & \ddots & \\ & & & \sigma_r \end{bmatrix}}_{r \times r} \underbrace{\begin{bmatrix} - & v_1 & - \\ - & v_2 & - \\ & \vdots & \\ - & v_r & - \end{bmatrix}}_{r \times m} .$$

Singular left vectors
Singular values
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Reduced Order Methods

Dynamic Mode Decomposition

- **Dynamic Mode Decomposition (DMD):** Approximate prediction capabilities

1. Define data matrices

$$X = \begin{bmatrix} | & | & \dots & | \\ x_1 & x_2 & \dots & x_{m-1} \\ | & | & \dots & | \end{bmatrix}, \quad X' = \begin{bmatrix} | & | & \dots & | \\ x_2 & x_3 & \dots & x_m \\ | & | & \dots & | \end{bmatrix}.$$

2. Perform **Truncated SVD** to get U , Σ and V .
3. Calculate $\tilde{A} = U^T X' V \Sigma^{-1}$.
4. Calculate **eigenvalues** (in Λ) and **eigenvectors** (in W) of \tilde{A} .
5. Calculate

$$\Phi = X' V \Sigma^{-1} W, \quad \longrightarrow \quad \text{Modes}$$

$$b = \Phi^* x_1, \quad \longrightarrow \quad \text{Initial amplitude}$$

$$\Omega = \text{diag}(\omega_k), \quad \omega_k = \log(\lambda_k) / \Delta t. \quad \longrightarrow \quad \text{Continuous time eigenvalues}$$

6. Reconstruct data:

$$x(t) \approx \Phi e^{\Omega t} b$$

↓ Modes ↓ Dynamics

Software

- **FEniCS Project:** Finite element method
- **PyDMD:** Dynamic mode decomposition
- **Other Software:** ParaView, scikit-learn package, Docker, MATLAB...



Test Cases

- **Error Control Through Space and Time Step Size**

Validates discretization methods (FEM and Newmark) using:

\mathcal{P}_1 in smooth impulse response.	\mathcal{P}_2 in smooth impulse response
\mathcal{P}_1 in sharp impulse response	\mathcal{P}_2 in sharp impulse response
\mathcal{P}_1 in harmonic regime	\mathcal{P}_2 in harmonic regime

- **Exact Result Using d'Alembert's Solution**

Validates fluid models with null Dirichlet condition on Γ_0 :

\mathcal{P}_1 in smooth impulse response	\mathcal{P}_2 in smooth impulse response
\mathcal{P}_1 in sharp impulse response	\mathcal{P}_2 in sharp impulse response

- **Exact Result Using Harmonic Solution**

Validates fluid models with non-zero Dirichlet condition on Γ_0 :

\mathcal{P}_1 in harmonic regime	\mathcal{P}_2 in harmonic regime
------------------------------------	------------------------------------

Validates fluid - rigid porous coupled models with non-zero Dirichlet condition on Γ_0 :

\mathcal{P}_3 in harmonic regime	\mathcal{P}_4 in harmonic regime
------------------------------------	------------------------------------

- **Umnova's Low Frequency Approximation Comparison**

Validates poro-elastic model: \mathcal{P}_5

Test Cases

- **Error Control Through Space and Time Step Size**

Validates discretization methods (FEM and Newmark) using:

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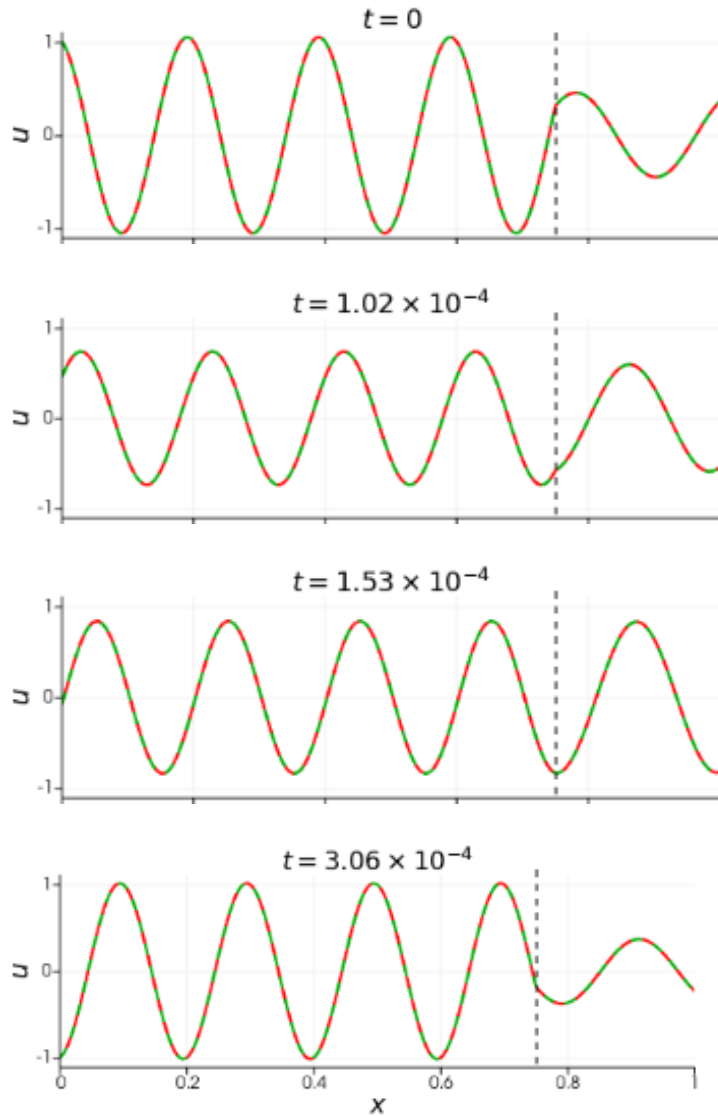
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- **Umnova's Low Frequency Approximation Comparison**

Validates poro-elastic model: \mathcal{P}_5

Harmonic Solution

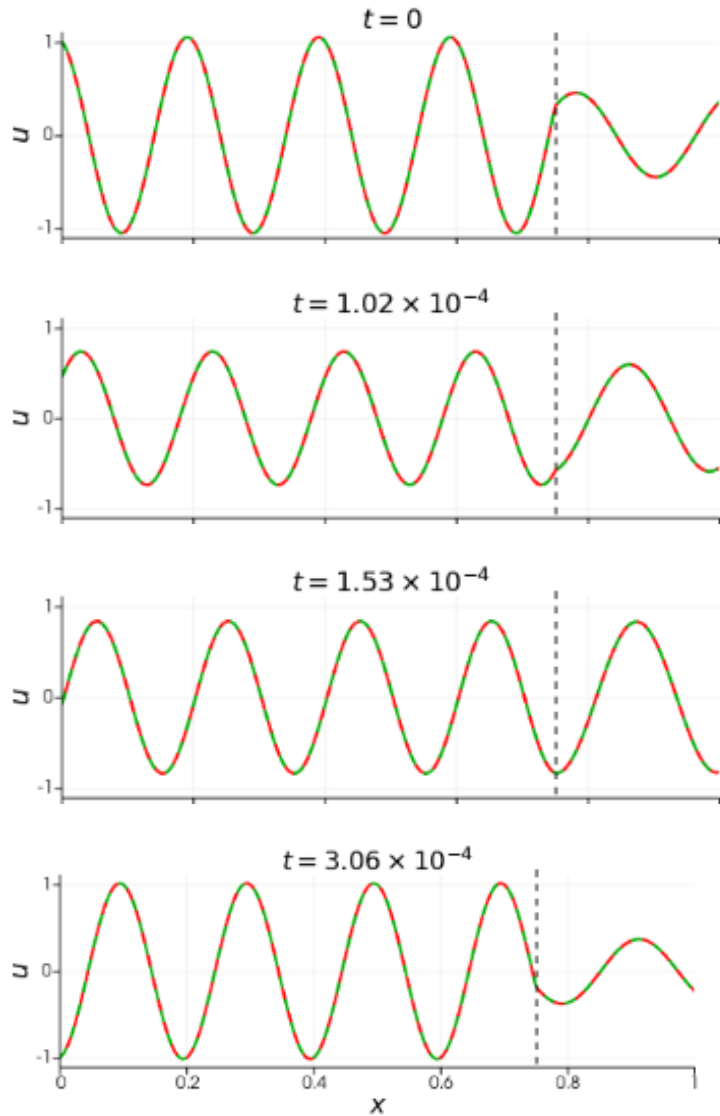


1. Transform the time domain equations to the frequency domain.
2. Solve the Helmholtz problem.
3. Transform back the exact solution to the time domain.
4. Find the initial conditions for the simulation.

$$\begin{cases}
 -\omega^2 \rho_f U_f - \rho_f c_f^2 \partial_x^2 U_f = 0 & \text{in } \Omega_f, \\
 -(\omega^2 \rho_p + i\omega\sigma) \tilde{U}_p - \frac{\rho_p c_p^2}{\phi \gamma_p} \partial_x^2 \tilde{U}_p = 0 & \text{in } \Omega_p, \\
 U_f = \tilde{U}_p & \text{on } \Gamma, \\
 \rho_f c_f^2 \partial_x U_f = \frac{\rho_p c_p^2}{\phi \gamma_p} \partial_x \tilde{U}_p & \text{on } \Gamma, \\
 U_f = 1 & \text{on } \Gamma_0, \\
 -i\omega \tilde{U}_p + \frac{\rho_p c_p^2}{\rho_f c_f \phi^2 \gamma_p} \partial_x \tilde{U}_p & \text{on } \Gamma_1.
 \end{cases}$$

Fluid – rigid porous coupled model with rigid-transparent boundaries.

Harmonic Solution



1. Transform the time domain equations to the frequency domain.
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3. Transform back the exact solution to the time domain.
4. Find the initial conditions for the simulation.

Sound speed in fluid	c_f	343 m/s
Fluid density	ρ_f	1.21 kg/m ³
Sound speed in porous	c_p	350 m/s
Porous density	ρ_p	1.5 kg/m ³
Porosity	ϕ	0.5
Specific heat capacity ratio	γ_p	1.4
Flux resistivity	σ	100 N s/m ⁴
Time step	Δt	7.29×10^{-6} s
Space step	Δx	2.5×10^{-3} m

Fluid – rigid porous coupled model with rigid-transparent boundaries.

Numerical Results

- Harmonic Waves
 - Reconstruction and prediction of harmonic waves.
 - Test: Reducing the number of snapshots.
 - Test: Increasing the discretization size.
- Periodic Impulse Responses
 - Reconstruction and prediction of periodic impulse responses.
 - Test: Reducing the number of snapshots.
 - Test: Reducing the DMD rank.
- Non-Periodic Impulse Responses
 - Reconstruction and prediction of non-periodic impulse responses.
- Other Approaches
 - Test: DMD vs. HODMD.
 - Test: DMD vs. SVD.
 - Simulation mixing.
 - Shifted DMD.

Numerical Results

- Harmonic Waves

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Reconstruction and prediction of non-periodic impulse responses.

- Other Approaches

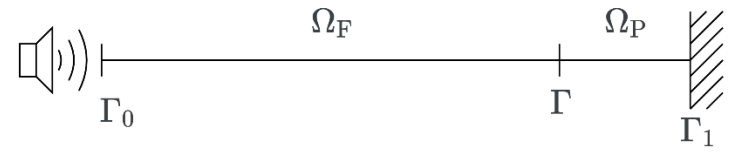
Test: DMD vs. HODMD.

Test: DMD vs. SVD.

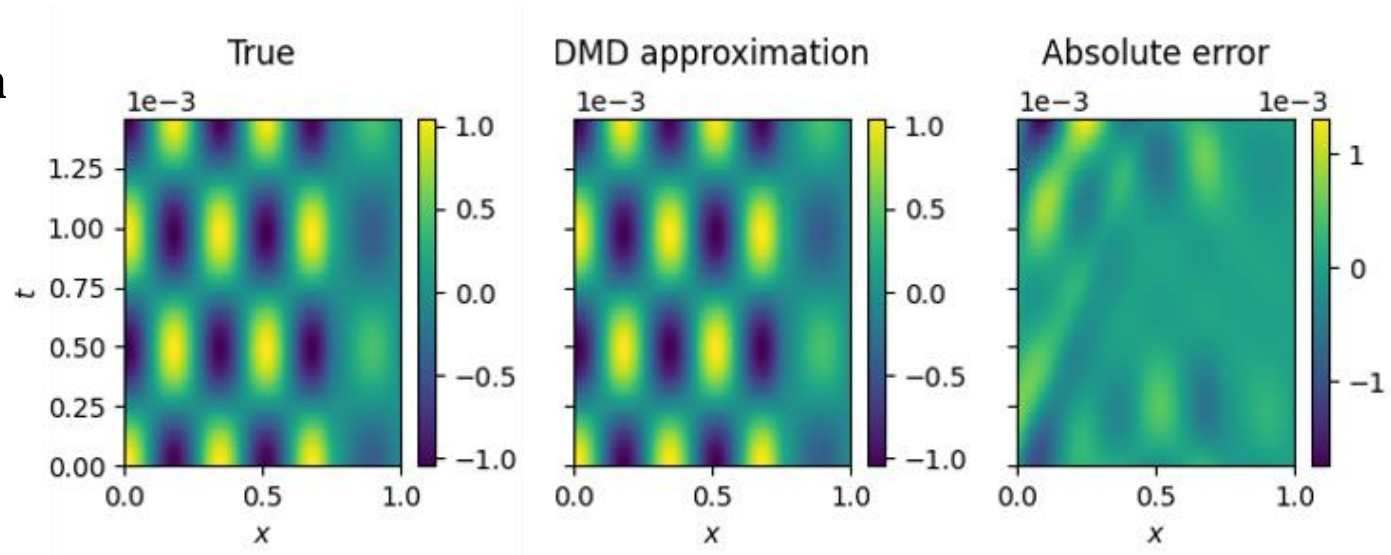
Simulation mixing.

Shifted DMD.

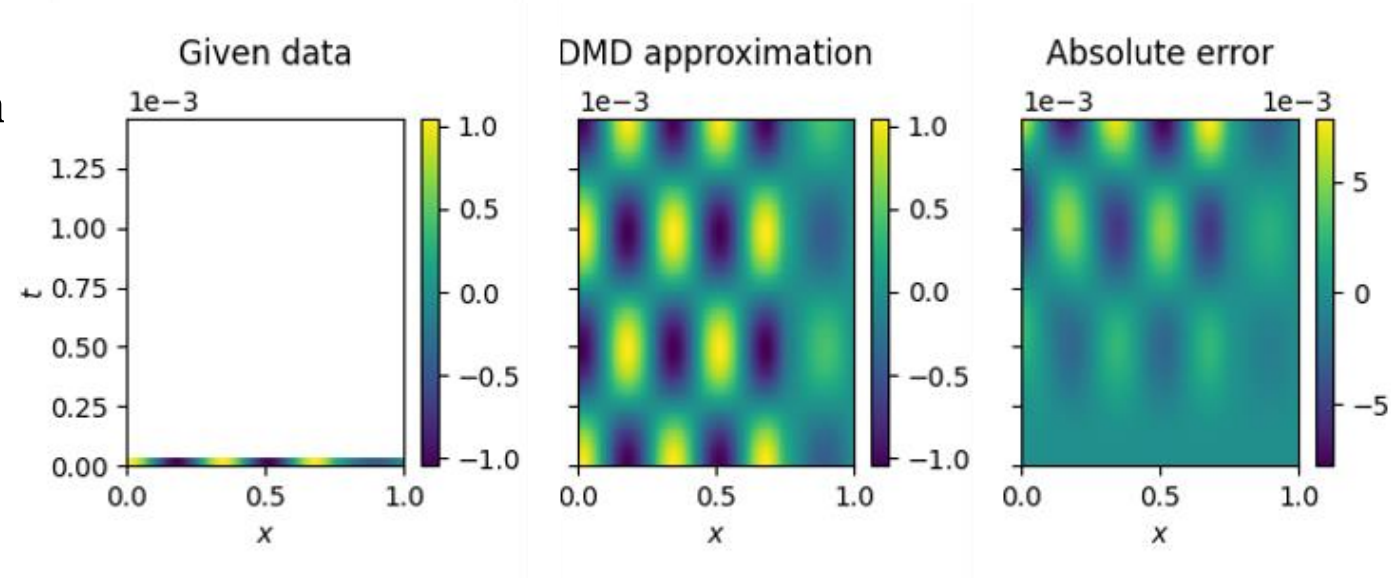
Harmonic Waves



Reconstruction



Prediction

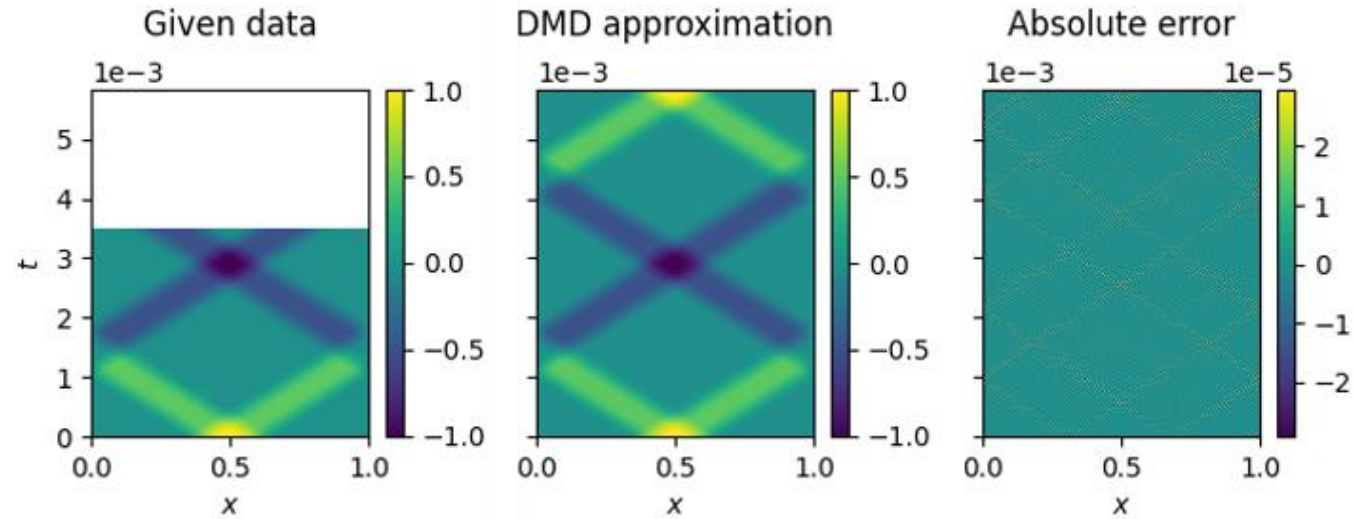


Δt	1.46×10^{-5} s
Δx	5×10^{-3} m
r	2
d	5

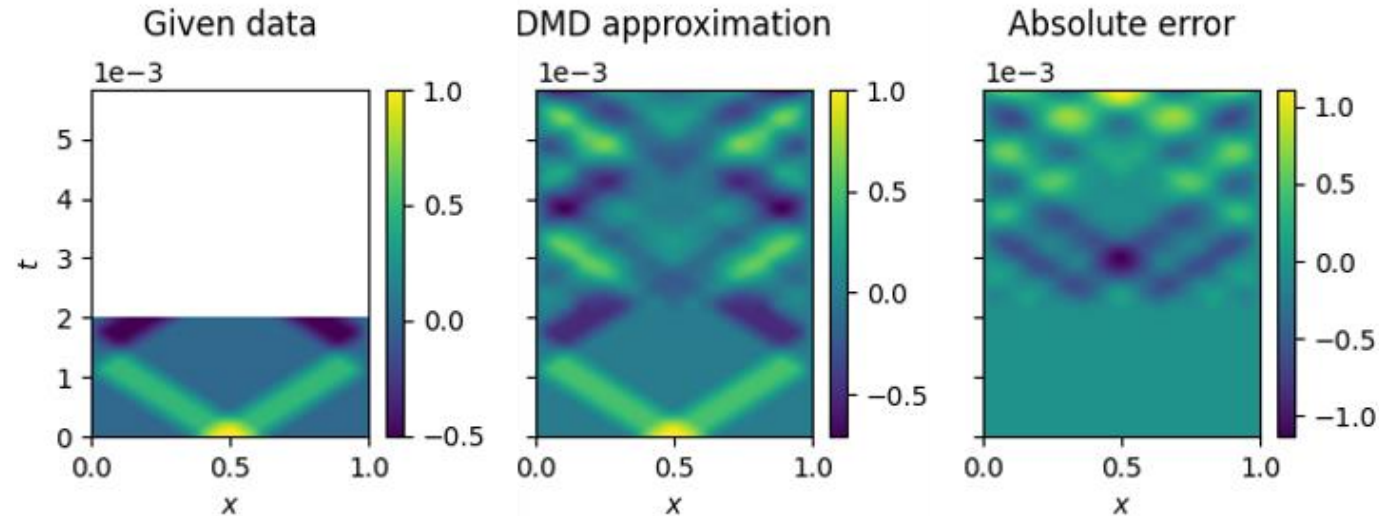
Periodic Impulses



Over a period

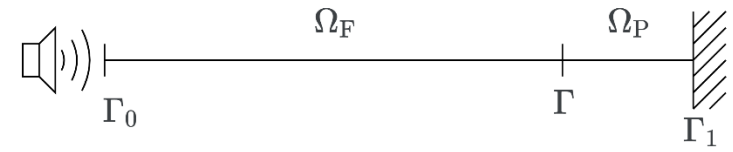


Under a period

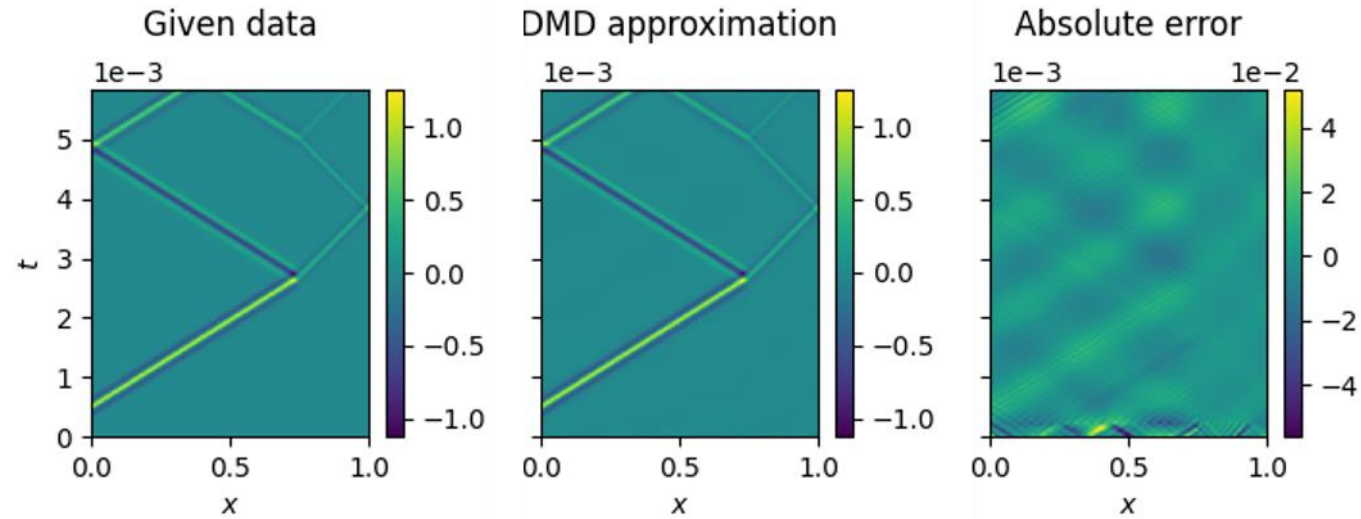


Δt	5.83×10^{-6} s
Δx	2×10^{-3} m
r	100
d	5

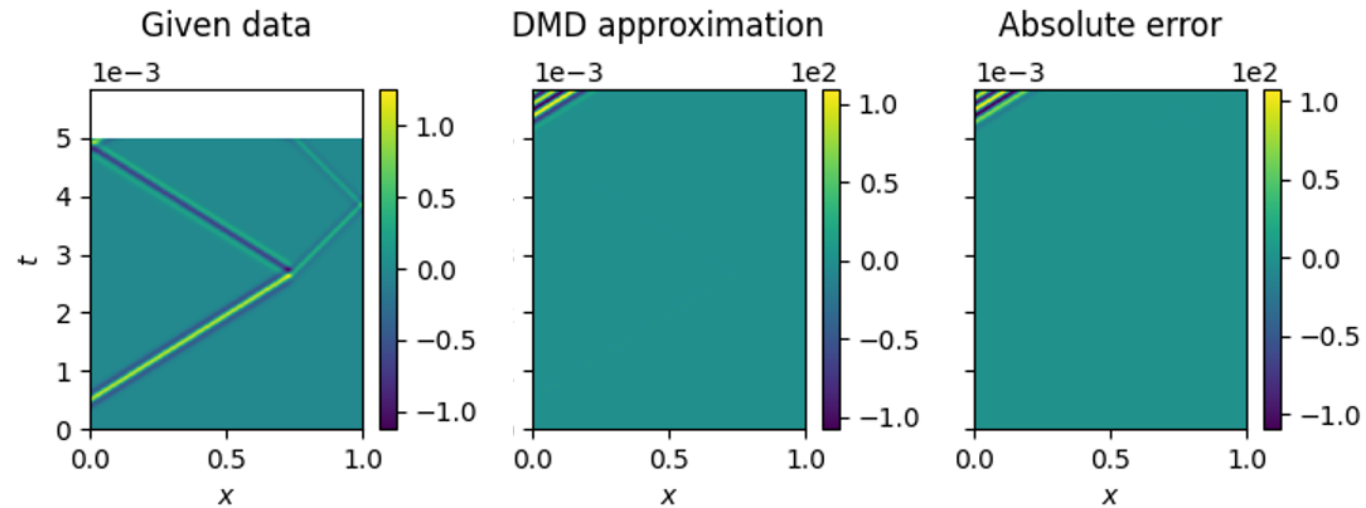
Non-Periodic Impulses



Reconstruction

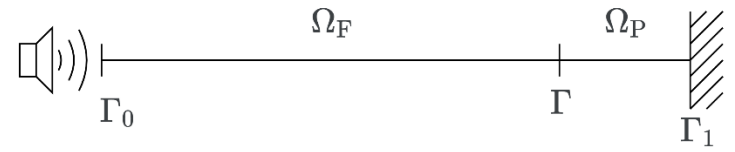


Prediction

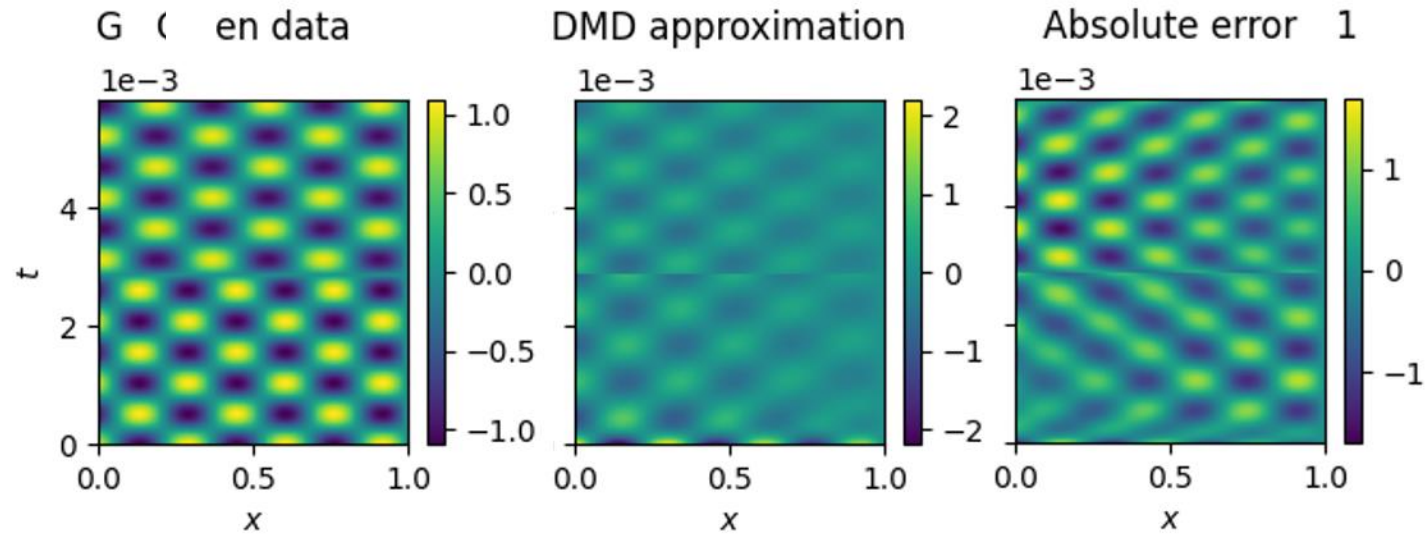


Δt	7.29×10^{-6} s
Δx	2.5×10^{-3} m
r	100
d	5

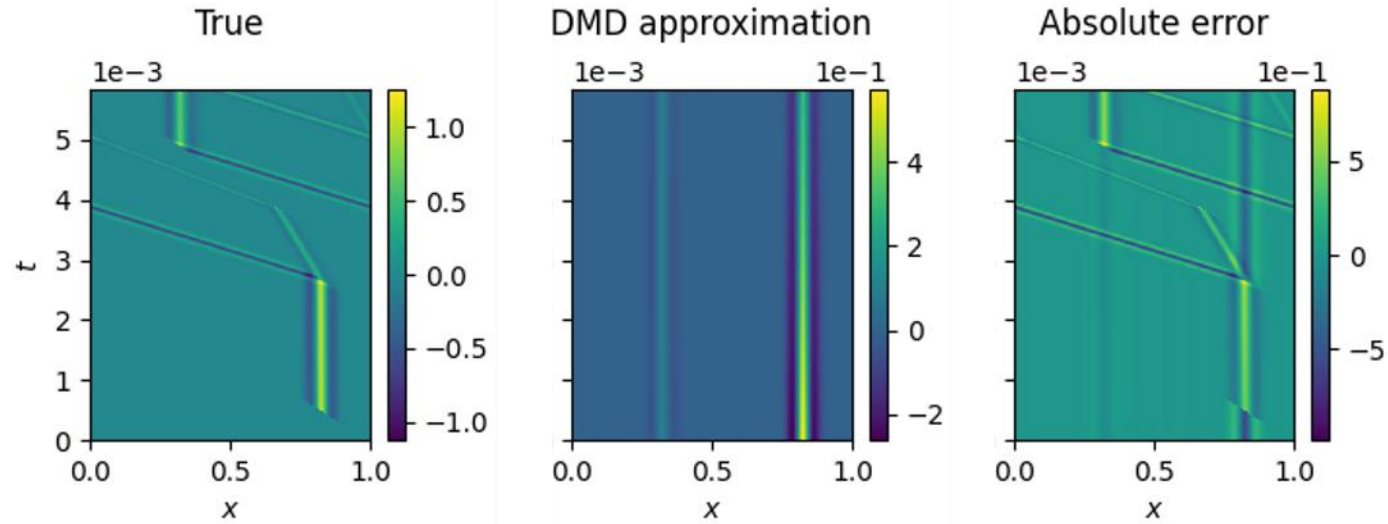
Other approaches



Simulation Mixing



Shifted DMD



Summary

- **Work completed:**

- 6 Acoustic models

- 15 Test cases

- 11 ROMs scenarios

- **Conclusions:**

- Accurate** results in **harmonic** cases: only 3 snapshots needed.

- Accurate** results in **periodic impulse response** cases: a single wave cycle needed.

- Unfeasible** use in **non-periodic impulse response** cases: unable to make predictions.

- Unfeasible** use using **simulation mixing**.

- **Other conclusions** (not included in the slides):

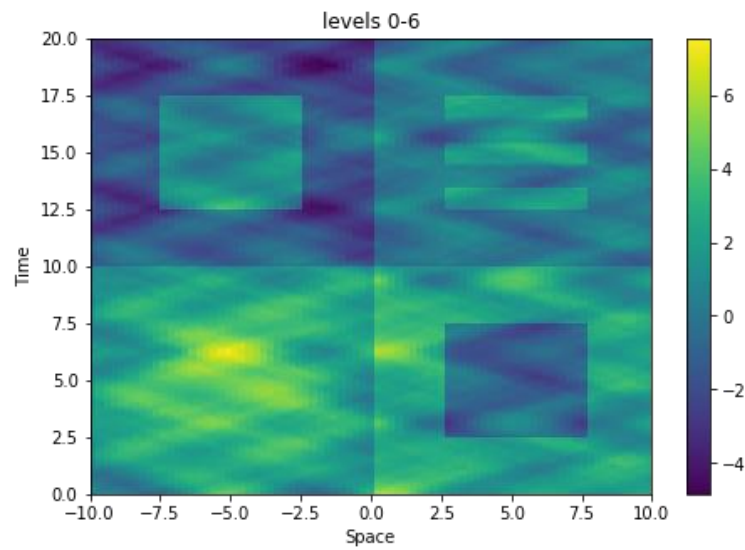
- Discretization size can affect results.

- Increased DMD rank improves predictions.

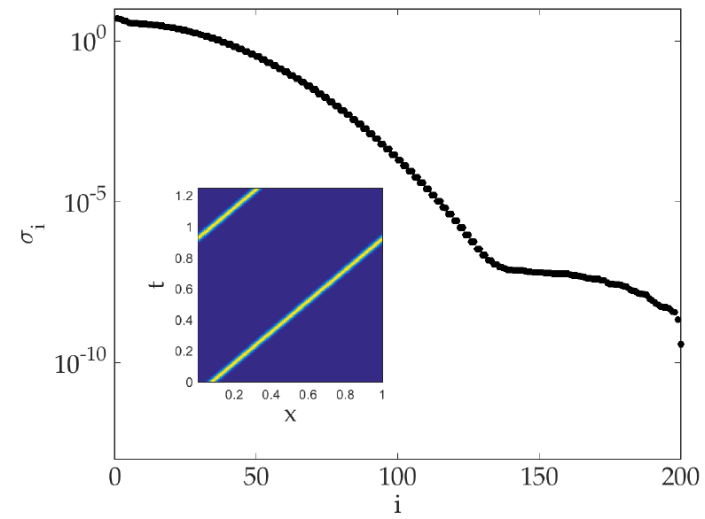
- HODMD is more versatile but requires tuning.

Next Steps

- Explore predictions using MrDMD.
- Extend to 3D models.
- Explore Shifted DMD for non-periodic impulse responses.
- Develop poro-elastic high frequency models.



MrDMD*



Shifted POD**

