

Liquid Si-rich Si-Zr alloys in contact with C and SiC: Wettability and Interaction phenomena

About

GOAL

Collecting knowledge on the occurring interfacial phenomena between liquid Si-rich Si-Zr alloys in contact with C and SiC substrates.

WHY?

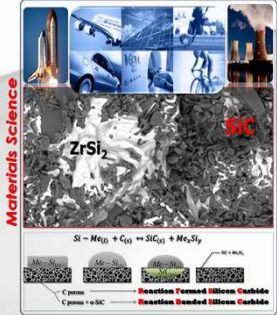
Targeted wettability and reactivity studies can easily provide useful indications for solving many technological problems affecting the reactive infiltration mechanisms, such as pore closure/narrowing phenomena.

HOW

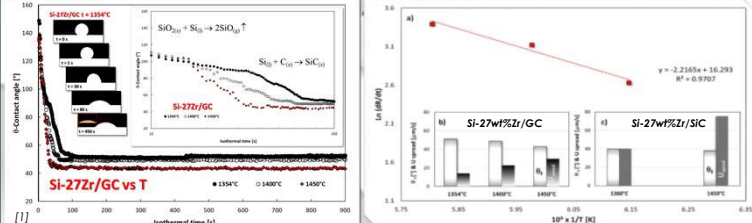
The contact heating sessile drop method (CH-SD) was applied for better understanding the interfacial phenomena occurring between 3 liquid Si-rich Si-Zr alloys in contact with Glassy Carbon (GC) and SiC substrates. Specifically, the contact angles behaviors as a function of time were obtained over the temperature range of $T = 1354\text{--}1500^\circ\text{C}$ under an Ar atmosphere.

IMPACT

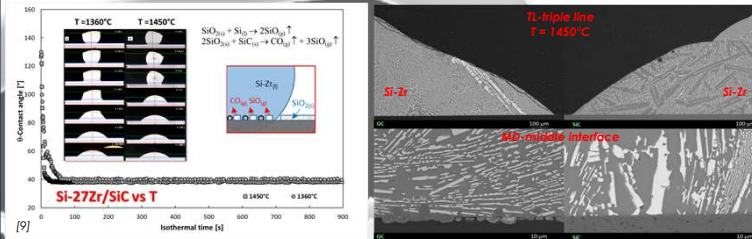
- Computational models are enabling in the design of advanced refractory materials such as SiC-based composites for highly demanding applications (thermal barriers, structural materials and chemically stable components for assembling re-entry space vehicles and fission/fusion nuclear, etc.).
- The fabrication of tailored SiC/ZrSi₂-based composites via cost-less reactive infiltration of Si-rich Si-Zr alloys into C- and SiC-based preforms, is currently one of the main goals of materials science and design.



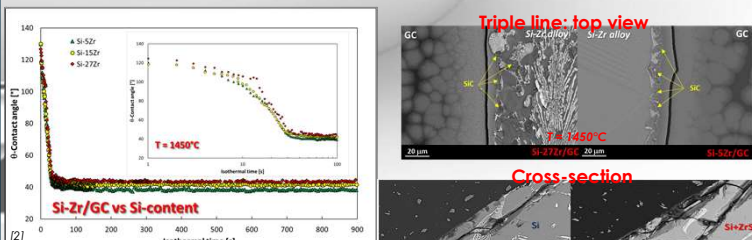
Results



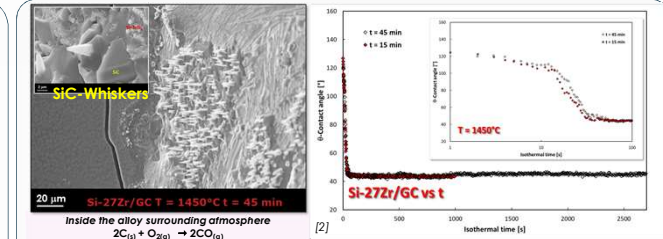
- $U_{spread}(1354^\circ\text{C}) < U_{spread}(1400^\circ\text{C}) < U_{spread}(1450^\circ\text{C})$
 $\theta_c(1354^\circ\text{C}) > \theta_c(1400^\circ\text{C}) > \theta_c(1450^\circ\text{C})$
- Equilibrium contact angle values in good agreement with the literature [3-8]
- Reactive wetting at the Si-27Zr/GC triple line ($E_a = 222\text{ kJ/mol}$)
- Early stage of spreading affected by SiO₂-native oxide at the alloy surface



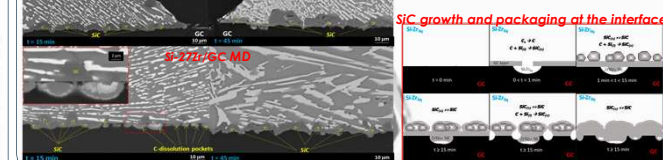
- $U_{spread}(\text{SiC } 1360^\circ\text{C}) < U_{spread}(\text{SiC } 1450^\circ\text{C})$
 $\theta_c(\text{SiC } 1450^\circ\text{C}) < \theta_c(\text{GC } 1450^\circ\text{C})$
- Equilibrium contact angle values in good agreement with the literature [1,2,3].
- Spreading kinetics affected by the presence of SiO₂-native oxide at the surface of both SiC substrate and Si-Zr alloy.



- $\theta_c(\text{Si-27Zr}) > \theta_c(\text{Si-15Zr}) > \theta_c(\text{Si-5Zr})$
- More compact SiC-layer at the interface by increasing the Si-content.
- The presence of ZrSi₂ precipitates affects the melting of Si-27Zr alloy.
- Si-evaporation/condensation phenomena beyond the triple line.



- High reproducibility
- In agreement with [11], the SiC-reaction layer growth and packaging is time dependent phenomenon



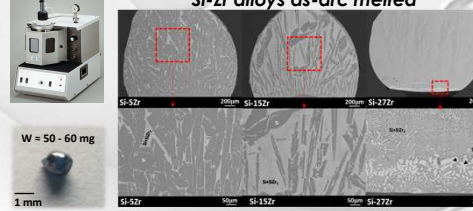
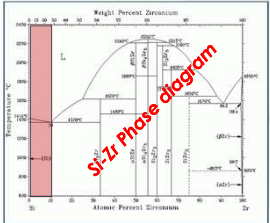
Summary and Conclusions

- For the first time, a comprehensive study of the interaction phenomena occurring when a liquid Si-rich Si-Zr alloy is in contact with amorphous C and SiC was performed.

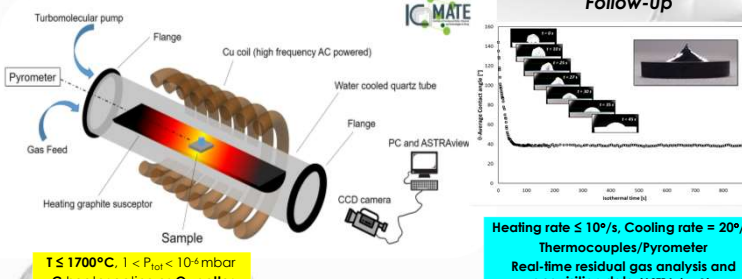
System	T [°C]	t [min]	$\theta_c \pm 2$ [°]	U_{spread} [$\mu\text{m/s}$]
Si-27Zr/GC	1354	15	51±52	13.9
	1400	15	49	22.7
	1450	15	43	29.7
	1450	45	45	28.6
	1360	15	40	40
Si-27Zr/SiC	1450	15	38	75
	1450	15	41	36.4
Si-15Zr/GC	1450	15	41	36.4
Si-5Zr/GC	1450	15	38	37.7

- Careful analyses of the θ -behaviors, spreading kinetics, reactivity and interfacial developed microstructures as a function of the Si-content at $T = 1450^\circ\text{C}$, were done.
- Wettability of GC by Si-rich Si-Zr alloys is controlled by the reactive mechanism.
- Despite the pronounced reactivity, the wetting characteristics are slightly composition-dependent.
- The wetting characteristics and spreading kinetics observed at the Si-rich Si-Zr alloys/GC triple lines at $T = 1450^\circ\text{C}$ are in a very good agreement with the results reported in literature.
- In view to provide knowledge for optimizing the infiltration process used to fabricate SiC/ZrSi₂ composites, except Si-27Zr alloy, the liquid Si-Zr alloys more enriched in Si, may not enhance the pore closure phenomenon for limited time of contact.
- The use of Si-Zr alloys with Si exceeding respect to the eutectic composition should be avoided for preserving the overall thermo-mechanical response of the produced composite.

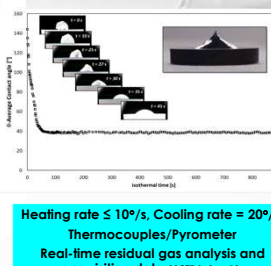
Methodology



Experimental set-up



Follow-up



Heating rate $\leq 10^\circ\text{S}^{-1}$, Cooling rate = 20°S^{-1}
 Thermocouples/Pyrometer
 Real-time residual gas analysis and acquisition data (ASTRAVIEW)

Acknowledgements

The NCN-National Science Center, Poland is greatly acknowledged for the financial support through the POLONEZ project number UMO-2016/23/P/ST8/01916. This project was carried out under POLONEZ-3 program which has received funding from European Union's Horizon 2020 research and innovation program under Marie Skłodowska-Curie grant agreement No 645778.

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