

## **Multi-Response Optimization of Turning Parameters on Vanadium Micro alloyed Steel using Taguchi based Grey Relational Analysis Coupled with Principal Component Analysis**

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### **Abstract**

*An experimental investigation of MAS38MnSiVS5 to investigate the effects of machining parameters, a turning test was designed using L<sub>27</sub> orthogonal array (OA) and machining was performed on the cylindrical bars using medium duty lathe of 7 kW spindle speed. The power consumption and surface roughness were measured. Grey Relational Analysis have been used for normalized the multi objective responses. Weighting values were evaluated by Principal Component Analysis (PCA) for each performance variables. The variability caused by the input parameters was apportioned using Analysis of Variance (ANOVA). Thus, the Taguchi method (TM) based GRA coupled with PCA was specifically adopted to determine the optimal combination of turning parameters. The confirmation experiment shows an average improved power consumed of 62.8 % and surface roughness of 65.4 %.*

**Keywords:** *Grey relational analysis, micro alloy, principal component analysis, power consumed, surface roughness, turning*

### **INTRODUCTION**

Development of light weight and high performance engineering materials like composites, alloys are one of the pioneering fields of research in material science and have been progressed through recent decades. Micro Alloy Steel (MAS) is one among them which possesses high strength to weight ratio, yield strength (above 550MPa) and zero heat treatment cycle when compared to carbon steels. Initially micro alloying technology has been utilized for developing the production of flat products and later for “long products” such as engineering bars, sections, forgings and wire rods [1]. During 1980’s the main rationale to use niobium bearing steel bars and wires was to eliminate the need for a hardening process [1,2]. The significant cost, weight reductions and energy savings features of micro alloyed steels find wider applications in automotive industry such as connecting rods, suspension components

and front axle beam, etc. for the replacement of conventional heat-treated steel materials.

Few research work was reported on machinability study of the micro alloy steels, Nakumara et al. (1993) made a research on the machining of free micro alloyed steel and the micro alloyed steel with best composition of alloy elements such as C, Mn, Cr, V, S, Pb, and Ca, and their impact on fatigue strength and machinability were found as 26% higher fatigue strength than conventional free machining microalloyed steel and 15% weight reduction resulted without any reduction of mechanical or fatigue strengths[7]. Cho W, et al. (1994) carried out research work on micro alloyed steel (0.4C-V Modified) intended for the production of connecting rods and wheel hubs. The research work focused on the evaluation of microstructures; tensile strength. It was found that machining

performance of the micro alloyed steel was dependent on cutting conditions [8]. VSivaramanaetal.(2011) conceded a research study on chip morphology during turning of Multiphase Ferrite (F-B-M) microalloyed steel. The turning experiment was performed using Taguchi orthogonal array. For different machining parameters such that cutting speed, depth of cut and feedrate, chip morphology were studied with optical and scanning electron microscope.[9]

VSivaramanaetal. (2012) reported that the machinability of multiphase (ferrite-bainite-martensite) microalloyed steel in a high speed lathe which is similar to the mechanical property of quenched and tempered steel. The results exposed that feed rate and depth of cut had persuade on cutting force and feed rate. The only parameter which shown that, the significant effect on the surface roughness[10].

AEbrahimi, MM Moshksar (2009), carried out an experimental investigation on micro alloyed steel (30MnVS6) and quenched-tempered (QT) steels (AISI 1045 and AISI 5140), to assess the effects of factors such as hardness, feed rate and work piece material cutting force, the tool flank wear and life of coated cemented carbide inserts in the hard turning process employed with statistical analysis. Also, investigations were carried out on chips characteristics and chip/tool contact length. Chips structure was studied through Scanning Electron Microscope (SEM) images. Shear planes and micro cracks of the chips in micro alloyed steel showed that the chips of regular and discontinuous in micro alloyed steel. Using video microscope crater wear of the tool in turning process was carried out by video microscope. The results indicated that the tool life and machinability of the micro alloyed steel is improved than the QT steels at identical cutting condition [11]. Muniraj and Muthukrishnan (2014) carried out the optimized machining parameters on

surface roughness and power consumption at the spindle of the lathe with a specimen of MAS38MnSiVS5 with Multilayer coated K20 carbide insert. The results indicated that cutting speed had estimable inverse effect on surface roughness. Higher cutting speed produced low value of surface roughness. But at advanced cutting speed increases the power consumption[12].

MunirajS, MuthukrishnanN(2015), investigated about a study on optimum levels of turning parameters on MAS using single layer coated K20 Insert. It shown that the influences of cutting speed, feed rate and depth of cut on the surface finish and the spindle power consumption[13]. MunirajS, MuthukrishnanN(2015), studied the machining performance of MAS38MnSiVS5 using uncoated K20 insert. The results showed the optimized cutting parameters of turning operation for the better surface value of the MAS micro alloyed steel bar[14]. Chang NC Hwang, CT Chung(2009), who conducted a research work on rough cutting process of high-speed end milling on SKD61 tool steel. The major characteristics selected to evaluate the performance indexes were tool life and metal removal rate, and the corresponding cutting parameters are milling type, spindle speed, feed per tooth, radial depth of cut, and axial depth of cut. Grey relation analysis grey relation grade adapted for optimal machining parameters combination. Principal component analysis was employed for weighing the performance index. This study concluded that this approach got hold of the optimal cutting parameters combinations[15]. RRamanujam, K Venkatesan, Vimal Saxena, Rachit Pandey(2014), investigated minimum machinability properties in turning operation of Inconel 625 by using fuzzy based principal component function coupled with Taguchi's design of experiment is used for optimization of machining parameters for minimum surface roughness, and power

consumption, and maximum material removal rate[16].SanjitMoshat (2010) investigated the optimization of CNC end milling process parameters to provide better surface finish as well as high MRR. The GRA based Taguchi method has been applied to multi objective optimization problem. Successfully used for simultaneous optimization of large number of responses[17].Tzeng et al. (2009), investigated the optimization of CNC turning operation for SKD11 using GRA based Taguchi method. In this study the GRA is applied to find how the turning operation parameter influences the quality target of work piece. Additionally the ANOVA is also applied to identify the most significant factor[18].Hag AN, MarimuthuP, Jeyapaul R(2008), employed

the grey relational analysis in Taguchi method to evaluate the optimized machining parameters in drilling of Al/SiC metal matrix composites. It was concluded that the method is most effective one[19].

In the view of above machining problems, the main objective of the present work is to investigate the influence of different cutting parameters on surface finish and power consumed criterion. The Taguchi L<sub>27</sub> orthogonal array is utilized for experimental planning for turning of MAS 38MnSiVS5. Fig.1a shows the microstructure of the specimen, shows uniform grains of pearlite in ferrite matrix.Fig. 1b shows the experimental setup.Table 1 shows the chemical composition of the work piece.

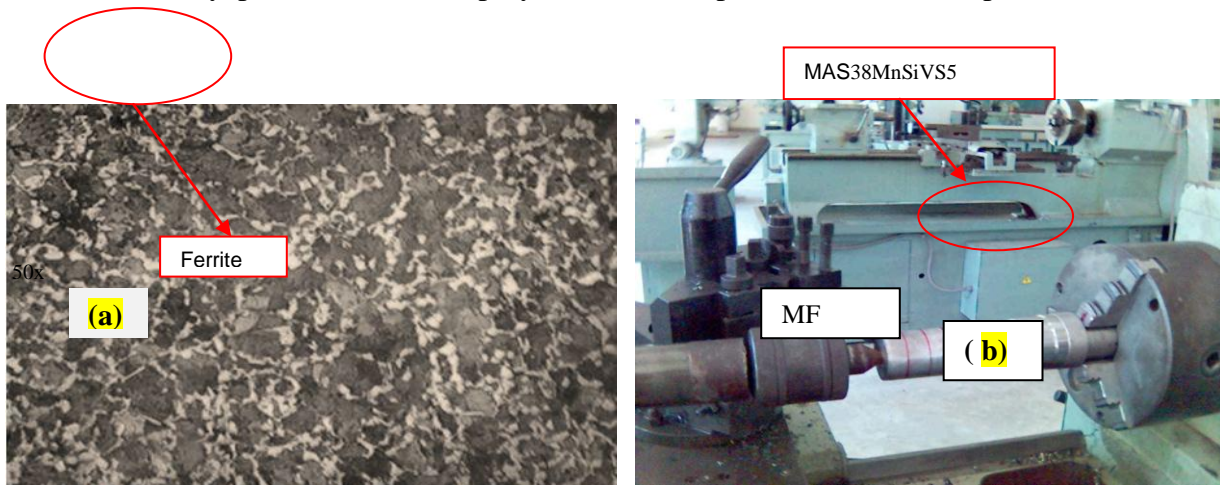


Figure 1:a) Microstructure of MAS 38MnSiVS5.b) Experimental set up.

Table 1:Chemical composition of MAS 38MnSiVS5.

Elements	%C	%Cr	%Si	%Mn	%Ni	%Cu	%Mb	%Zn	%Ti	%V	%Fe
Micro Alloyed Steel 38MnSiVS5	0.41	0.002	0.40	1.38	0.001	0.08	0.02	0.08	0.05	0.18	Balance

Table 2:Machining parameters and their levels.

Symbol	Machining parameter	Unit	Level 1	Level 2	Level 3
A	Cutting Speed	rpm	500	775	1200
B	Feed	mm/rev	0.04	0.042	0.046
C	Depth of cut	mm	0.5	1.0	1.5

### Grey Relation Analysis

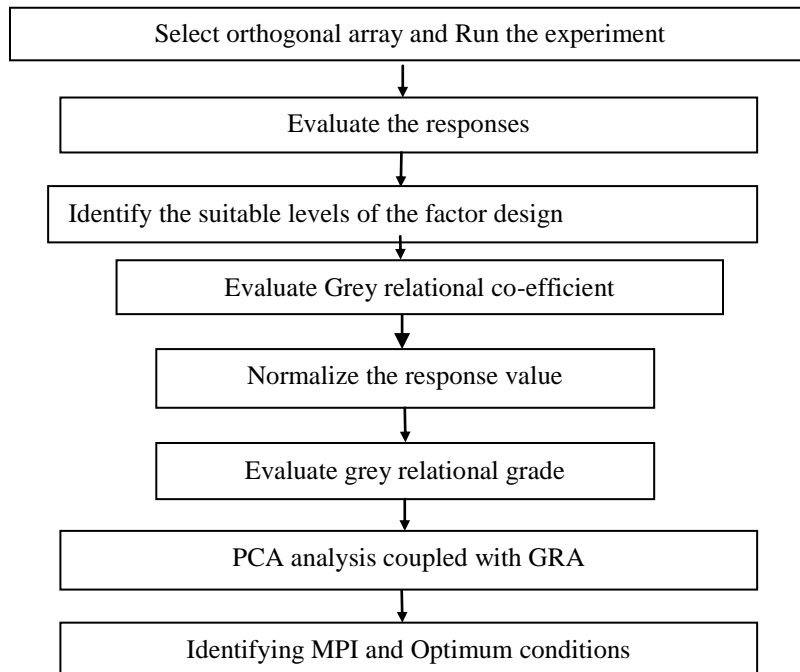
The grey relational theory provides an efficient management upon the uncertainty, multi input and discrete data. A grey relational grade is obtained to evaluate the

multi responses. As a result, optimization of the responses can be converted into optimization of a single relational grade [19–21]. A flow chart for the grey relational analysis procedure is shown in Fig.2.

In GRA, when the range of a response variable is large or the standard value is enormous, the fluctuation of variables may be neglected. Since the response variables and their units are different, it is necessary to preprocess the data so that they can be normalized in the range between zero and one. The normalization was done to the

response variables using Eqns. (1) and (2). For smaller the better, the normalized the experimental results  $x_{ij}$  can be expressed as:

$$x_{ij} = \frac{\max_j y_{ij} - y_{ij}}{\max_j y_{ij} - \min_j y_{ij}} \quad (1)$$



**Figure 2:** Flow diagram for grey relational analysis and PCA.

For higher – the –better, the normalized experimental results  $X_{ij}$  can be expressed as:

$$x_{ij} = \frac{y_{ij} - \min_j y_{ij}}{\max_j y_{ij} - \min_j y_{ij}} \quad (2)$$

Where,  $y_{ij}$  is the experimental result of the  $i^{\text{th}}$  run for the  $j^{\text{th}}$  response variable. The larger normalized results correspond to the

better performance and the best-normalized results are equal to one. Next, the grey relational coefficient (GRC) is calculated to display the relationship between the optimal and actual normalized experimental results,  $\xi_{ij}$  can be expressed as:

$$\xi_{ij} = \frac{\min_i \min_j |x_i^o - x_{ij}| + \xi \max_i \max_j |x_i^o - x_{ij}|}{|x_i^o - x_{ij}| + \xi \max_i \max_j |x_i^o - x_{ij}|} \quad (3)$$

Where  $X_i^o$  is the ideal normalized results for  $i^{\text{th}}$  response variable and  $\xi$  is the distinguishing coefficient and lies

between 0 and 1. In general it is set as 0.5. Table 3 shows the experimental layout.

**Table 3: Experimental layout and the response variables using L27 OA.**

Exp.No	Machining parameters and their levels			Response variable		
	A	B	C	Ra	Rz	Pc
1	1	1	1	3.4433	17.8167	0.1300
2	1	1	2	3.4920	17.8020	0.1300
3	1	1	3	2.9160	16.3320	0.1400
4	1	2	1	2.9867	15.6067	0.1400
5	1	2	2	3.4380	19.5080	0.1400
6	1	2	3	2.8920	16.4460	0.1400
7	1	3	1	3.4133	20.2600	0.1400
8	1	3	2	2.9840	17.2280	0.1400
9	1	3	3	2.7760	16.8320	0.1500
10	2	1	1	2.2300	12.6533	0.2300
11	2	1	2	3.1320	17.4860	0.2000
12	2	1	3	3.0920	17.5120	0.1900
13	2	2	1	2.3433	13.0267	0.2400
14	2	2	2	3.4500	17.9720	0.2000
15	2	2	3	2.9560	16.8360	0.2000
16	2	3	1	2.2600	11.9067	0.2300
17	2	3	2	3.7000	19.5500	0.2100
18	2	3	3	3.3340	18.2600	0.2000
19	3	1	1	1.4500	7.4000	0.3400
20	3	1	2	2.6980	14.5780	0.2900
21	3	1	3	2.9980	15.3680	0.2900
22	3	2	1	1.2700	6.6300	0.3500
23	3	2	2	2.7540	14.1140	0.3000
24	3	2	3	2.8140	16.0340	0.3000
25	3	3	1	1.4500	7.4933	0.3500
26	3	3	2	3.2400	16.5600	0.3100
27	3	3	3	2.9340	15.6840	0.3200

**Table 4: Results of grey with principle component analysis(PCA).**

Exp. No	Normalized Ra	Normalized Rz	Normalized Pc	Grey coefficientRa	Grey coefficientRz	Grey coefficientPc	MPI	Rank
1	0.1056	0.1793	1.0000	0.3586	0.3786	1.0000	0.3658	22
2	0.0856	0.1803	1.0000	0.3535	0.3789	1.0000	0.3615	25
3	0.3226	0.2882	0.9545	0.4247	0.4126	0.9167	0.4265	12
4	0.2936	0.3414	0.9545	0.4144	0.4316	0.9167	0.4203	14
5	0.1078	0.0552	0.9545	0.3591	0.3461	0.9167	0.3612	26
6	0.3325	0.2798	0.9545	0.4283	0.4098	0.9167	0.4291	11
7	0.1180	0.0000	0.9545	0.3618	0.3333	0.9167	0.3617	24
8	0.2947	0.2225	0.9545	0.4148	0.3914	0.9167	0.4151	17
9	0.3802	0.2515	0.9091	0.4465	0.4005	0.8462	0.4430	9
10	0.6049	0.5581	0.5455	0.5586	0.5308	0.5238	0.5545	4
11	0.2337	0.2035	0.6818	0.3949	0.3857	0.6111	0.3951	19
12	0.2502	0.2016	0.7273	0.4001	0.3851	0.6471	0.3997	18
13	0.5583	0.5307	0.5000	0.5310	0.5158	0.5000	0.5287	6
14	0.1029	0.1679	0.6818	0.3579	0.3753	0.6111	0.3621	23
15	0.3062	0.2512	0.6818	0.4188	0.4004	0.6111	0.4176	15
16	0.5926	0.6129	0.5455	0.5510	0.5636	0.5238	0.5526	5
17	0.0000	0.0521	0.6364	0.3333	0.3453	0.5789	0.3367	27
18	0.1506	0.1467	0.6818	0.3705	0.3695	0.6111	0.3721	21
19	0.9259	0.9435	0.0455	0.8710	0.8985	0.3438	0.8711	2
20	0.4123	0.4169	0.2727	0.4597	0.4616	0.4074	0.4596	7
21	0.2889	0.3589	0.2727	0.4128	0.4382	0.4074	0.4163	16
22	1.0000	1.0000	0.0000	1.0000	1.0000	0.3333	0.9953	1
23	0.3893	0.4509	0.2273	0.4502	0.4766	0.3929	0.4534	8
24	0.3646	0.3101	0.2273	0.4404	0.4202	0.3929	0.4373	10
25	0.9259	0.9367	0.0000	0.8710	0.8876	0.3333	0.8695	3
26	0.1893	0.2715	0.1818	0.3815	0.4070	0.3793	0.3850	20
27	0.3152	0.3357	0.1364	0.4220	0.4295	0.3667	0.4227	13



The GRC for the present study were calculated and listed in Table 4. The GRG for each experimental run is computed from the average GRC of the response variable. GRG is used to show the relationship among the experimental runs. Higher the GRG more important the experimental run which is given in the Eqn.4.

$$\gamma_i = \frac{1}{n} \sum_{j=1}^n w_j \xi_{ij} \text{ where } \sum_{j=1}^n w_j = 1 \quad (4)$$

Where,  $\gamma_i$  is the weighted – Grey relation grade (GRG) for the  $i^{\text{th}}$  experiment,  $n$  is the number of response variables and  $w_j$  represents the normalized weighting value of the  $j^{\text{th}}$  response variable.

**Principle Component Analysis Coupled With Grey**

This is a most effective statistical approach to make linear combinations of response variables into structured variance-covariance [16,24,25]. The multi objective response matrix is formed by Eqn.4.

$$X = \begin{bmatrix} x_1(1) & x_1(2) & \dots & x_1(n) \\ \vdots & \ddots & & \vdots \\ x_m(1) & x_m(2) & \dots & x_m(n) \end{bmatrix} \quad (4)$$

Where  $x_i(j)$ ,  $i = 1, 2, \dots, m$  number of

experiments,  $j=1, 2, \dots, n$  number of response variable. In this study,  $m=27$ ,  $n=3$  and  $x$  is the GRC response variable from Table 4. The correlation coefficient matrix is obtained by the Eqn.(5).

$$R_{jl} = \left( \frac{\text{Cov}(x_i(j), x_i(l))}{\sigma_{x_i(j)} \times \sigma_{x_i(l)}} \right) \quad (5)$$

Where,  $\text{Cov}(x_i(j), x_i(l))$  is the covariance of sequences of  $x_i(j)$  and  $x_i(l)$  is the standard deviation of the sequence of  $x_i(j)$  and  $\sigma_{x_i(l)}$  standard deviation of the sequence  $x_i(l)$ . Then the eigen values and eigen vectors are estimated from the correlation coefficient matrix by Eqn.(6).

$$(R - \lambda_k I_m) V_{ik} = 0 \quad (6)$$

Where,

$$\sum_{k=1}^n \lambda_k = n, \quad k = 1, 2, 3,$$

$V_{ik} = [a_{k1} a_{k2} \dots a_{kn}]^T$  Eigenvectors corresponding to the eigenvalue  $\lambda_k$  the uncorrelated principal component (PC) is formulated as:

$$Y_{mk} = \sum_{i=1}^n X_m(i) \cdot V_{ik} \quad (7)$$

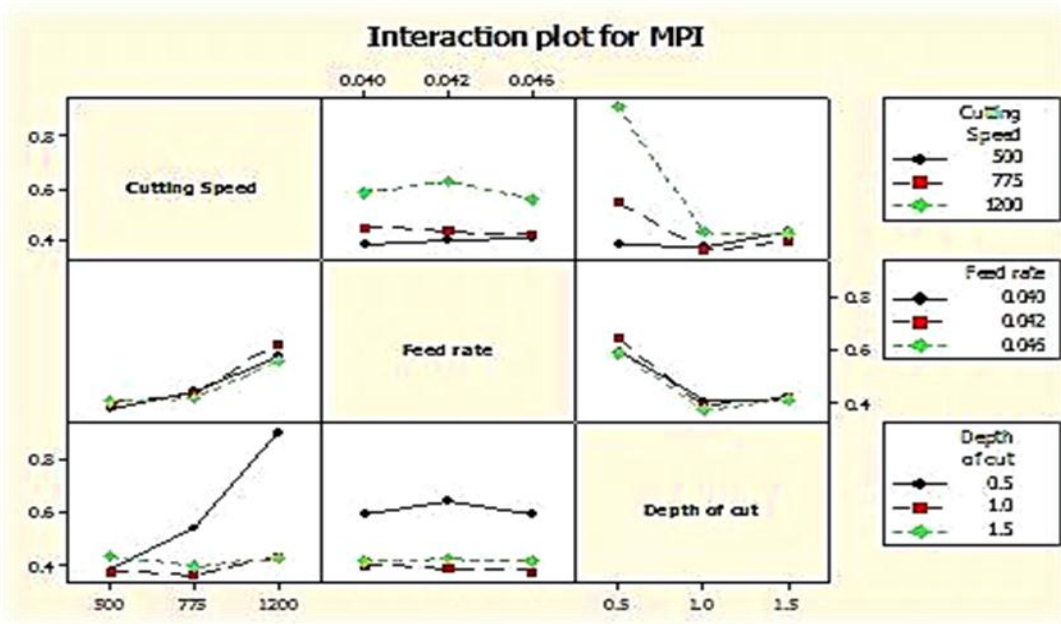


Figure 3: Interaction plot for MPI.

Where  $Y_{mk}$  is called the first PC,  $Y_{m2}$  is called the second PC, and soon. For the present study,  $w_j$  were obtained from the PCA. In this study, the elements GRC and the results Grey coupled with Principal component analysis listed in

Table 5. Interaction plot for Multi performance index is shown in Fig.3, for three levels of cutting speed, feed rate and depth of cut. The response table for the MPI is given in Table 5.

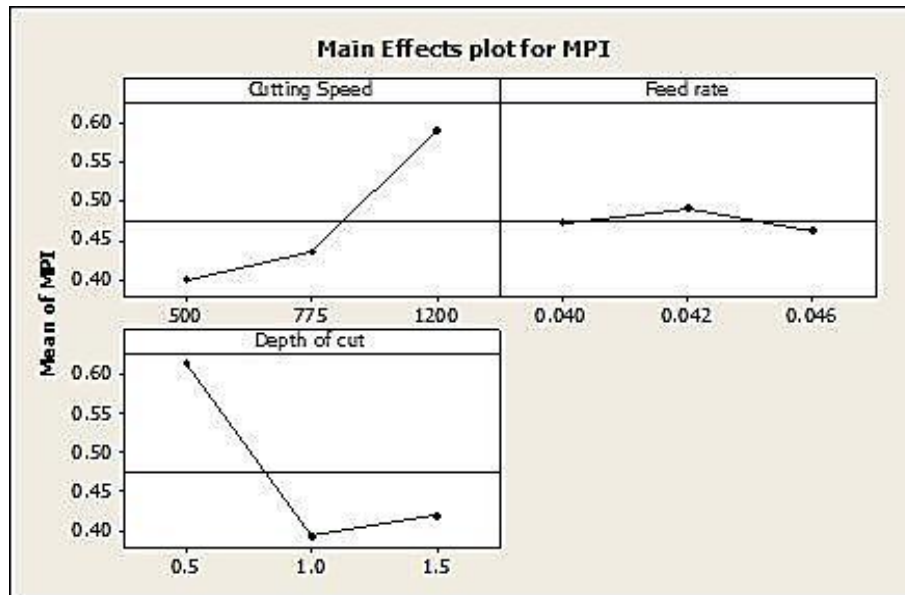


Figure 4: Main effect plot for multi performance index.

Table 5: Response table for multi performance index.

Cutting Speed(rpm)	Mean
500	0.3982
775	0.4355
1200	0.5900
Feed rate(mm/rev)	Mean
0.040	0.4722
0.042	0.4894
0.046	0.4620
Depth of cut(mm)	Mean
0.5	0.6133
1.0	0.3922
1.5	0.4183

By using this table main effect plot for Multi performance index(MPI) is drawn as shown below Fig.4.

Table 6: Eigen values for the principle components.

Principle Components	First Component	Second Component	Third Component
Eigen Values	2.5642	0.4138	0.0221
Contribution in %	85.5	13.8	0.7

Table 6 showed the Eigenvalues for the three principle components which are Ra, Rz and Pc respectively. The contributions

of these components revealed that the first component has greater influence on the performances. The second and third

components are also showing their significance on the work as in their order.

**ANALYSIS OF VARIANCE FOR MULTI PERFORMANCE INDEX**

It is a statistical tool for apportioning the variability of an output to various inputs. It is used to determine which input parameter significantly influences the output [26,27]. The total variability among weighted GRG measured by the sum of squared deviations from the total men of weighted –GRG are

decomposed into two sources: the sum of squared deviations due to each machining parameter are the sum of squared error. The fisher’s F –test can be used to identify which machining parameter have significantly effect on the weighted –GRG. The results of ANOVA for the weighted – GRG were tabulated as shown in Table 7. It shows that three machining parameters are found to be the most influential on the power consumed and surface roughness.

*Table 7: Analysis of variance MPI, using adjusted SS for tests.*

Factor	Degrees of Freedom	Sum of squares	Mean Squares	Test F	Contribution %
Cutting Speed (V)	2	0.18613	0.093065	89.58	25.31
Feed (f)	2	0.003452	0.001726	1.66	0.4694
Depth of cut (D)	2	0.262780	0.131390	126.48	35.75
V*f	4	0.006222	0.001555	1.49	0.8461
V*D	4	0.264909	0.066227	63.75	36.02
f*D	4	0.003496	0.000874	8.41	0.4754
Error	8	0.008311	0.0010388		1.13
Total	26	0.735332			100

**Confirmation Experiment**

Once the optimal level of machining parameters is selected (A<sub>1</sub>B<sub>1</sub>C<sub>1</sub>), the final step is to predict and verify the improvement of the performance characteristics using the optimal level of the machining parameters. The estimated grey relational grade  $\hat{\gamma}$  using the optimum level of the machining parameters can be calculated as:

$$\hat{\gamma} = \gamma_m + \sum_{i=1}^q (\bar{\gamma}_j - \gamma_m) \quad (8)$$

Where,  $\gamma_m$  is the total mean of the grade,

$\bar{\gamma}_j$  is the mean of the Grey relational grade at the optimum level and q is the number of machining parameters that significantly affects the multiple performance characteristics.

Based on Eqn. (5) the estimated grey relational grade using the optimal machining parameters can then be obtained. Table8 shows the results of the confirmation experiment using the optimal machining parameters. As shown inTable8 predicted values of combined grey relational grade is 1.188.

*Table 8: Results of confirmation experiment.*

	Initial machining parameters	Optimal machining parameters	
		Prediction	Experiment
Setting level	A <sub>1</sub> B <sub>1</sub> C <sub>1</sub>	A <sub>3</sub> B <sub>2</sub> C <sub>1</sub>	A <sub>3</sub> B <sub>2</sub> C <sub>1</sub>
Surface roughness (Ra) in μm	3.44	-----	1.27
Power consumed (kW)	0.13	-----	0.35
Multi performance index	-----	0.741	0.949



## CONCLUSION

In this investigation, Taguchi method based GRA coupled with PCA was used for optimizing the machining parameters of machining micro alloy steel using single layer(TiN) coated K 20 carbide insert.

The micro alloy MAS38MnSiVS5 was chosen for the study. The power consumed by main spindle and the surface roughness that are measured were considered as multi-objective response variables.

GRA was used to convert these multi-objectives into a single weighted-GRG where PCA was used to determine the weighting values of each response variable and thereby the multi objectives were converted into a weighted-GRG. Thus, optimization of complicated multi-objective response variables can be greatly simplified through this method.

From the proposed method, it is found that improved power consumed and surface roughness can be obtained by setting the optimal combination of the forming parameters as  $A_3 B_2 C_1$ .

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