

Supplement to: Electron energy partition across interplanetary shocks

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ABSTRACT

This is supplemental material to the multi-part papers entitled, “Electron energy partition across interplanetary shocks”

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11 1. PARAMETERS AND SHOCK ANALYSIS

12 We use the following notations for any quantity, Q ,
13 throughout this paper: Q_o , δQ , and $\langle Q \rangle_j$, where Q_o is any
14 quasi-static quantity, δQ is any fluctuating or high pass
15 filtered quantity, $\Delta Q = \langle Q \rangle_{dn} - \langle Q \rangle_{up}$, and $\langle Q \rangle_j$ is the
16 time average of any quantity over region j = upstream
17 (up) or downstream (dn). Note that Q_o is not the same
18 as $\langle Q \rangle_j$ in this context.

19 Herein we use the following parameter definitions: \mathbf{B}_o
20 is the quasi-static magnetic field vector [nT]; \mathbf{V}_{bulk} is
21 the bulk flow velocity vector [$km\ s^{-1}$]; n_s is the number
22 density of species s [cm^{-3}]; m_s is the mass of species
23 s [kg]; T_s is the scalar temperature of species s [eV];
24 $W_s = \sqrt{k_B T_s / m_s}$ is the rms thermal speed of species
25 s ; $V_A = B_o / \sqrt{\mu_0 m_i n_i}$ is the Alfvén speed [$km\ s^{-1}$];
26 $\delta\mathbf{B}$ is the high pass filtered fluctuating magnetic field
27 due to a whistler precursor [nT]; $\Delta|\mathbf{B}_o|$ is the change in
28 the magnetic field magnitude across a shock ramp [nT];
29 SCF is the spacecraft rest frame; and SHF is the shock
30 rest frame.

31 All shock parameters used herein were taken from
32 the Harvard Smithsonian Center for Astrophysics’ Wind
33 shock database (WSDB), which can be found at:
34 https://www.cfa.harvard.edu/shocks/wi_data/.

35 The WSDB provides tables of numerical solutions to the
36 Rankine-Hugoniot relations (e.g., Koval & Szabo 2008;
37 Szabo 1994; Vinas & Scudder 1986) for eight different
38 methods (see Section 1.1 for definitions). The first table,

39 titled *General Information*, on each event webpage lists
40 the selected best method from which we take the values
41 for all events examined herein (e.g., second column of
42 Table 1).

43 In the tables that follow on each event webpage of
44 WSDB, some parameters are listed by name while
45 others use symbols or abbreviations. In the following
46 we will state our definition followed by the WSDB
47 equivalent label in parentheses and italicized text.
48 Rather than repeated state that $\langle Q \rangle_j$ corresponds to
49 the quantity Q averaged over the j^{th} region, we will
50 simply imply it for brevity. These parameters we used
51 are: $\langle W_s \rangle_j$ (W_s) is the rms thermal speed of species s
52 [$km\ s^{-1}$]; $\langle V_A \rangle_j$ (*Alfvén Speed*) is the Alfvén speed av-
53 eraged [$km\ s^{-1}$]; $\langle C_s \rangle_j$ (*Sound Speed*) is the sound or
54 ion-acoustic sound speed, defined here as $\sqrt{\frac{5}{3}} \langle W_i \rangle_j$;
55 $\langle \beta_{Tot} \rangle_j$ (*Plasma Beta*) is the “total” plasma beta, define
56 here as $(3/5)C_s^2/V_A^2$; \hat{n} (N_x , N_y , and N_z) is the shock
57 normal unit vector [GSE]; \mathcal{R} (*Compression*) is the shock
58 density compression ratio, defined as $\langle n_i \rangle_{down} / \langle n_i \rangle_{up}$;
59 $\langle \theta_{Bn} \rangle_{up}$ (*ThetaBn*) is the shock normal angle, defined
60 as the acute reference angle between $\langle \mathbf{B}_o \rangle_{up}$ and \hat{n} ;
61 $|V_{shn}|$ (*Shock Speed*) is the upstream shock normal speed
62 in the SCF (determined numerically from Equation 4d);
63 $\langle U_{shn} \rangle_j$ (*dV*) flow speed along shock normal in the SHF
64 [$km\ s^{-1}$] (defined in Equation 7); $\langle M_A \rangle_j$ (not shown) is
65 the Alfvénic Mach number, defined as $\langle |U_{shn}| \rangle_j / \langle V_A \rangle_j$;
66 and $\langle M_f \rangle_j$ (*Fast Mach*) is the fast mode Mach number,

defined as $\langle |U_{shn}| \rangle_j / \langle V_f \rangle_j$ where V_f is the MHD fast mode phase speed given by:

$$2V_f^2 = (C_s^2 + V_A^2) + \sqrt{(C_s^2 - V_A^2)^2 + 4C_s^2V_A^2 \sin^2 \theta_{Bn}} \quad (1a)$$

$$= (C_s^2 + V_A^2) + \sqrt{(C_s^2 + V_A^2)^2 - 4C_s^2V_A^2 \cos^2 \theta_{Bn}} \quad (1b)$$

where C_s is the sound speed (e.g., see Equation 1.9.1 in Krall & Trivelpiece 1973), which is formally defined as:

$$C_s^2 \equiv \frac{\partial P}{\partial \rho_m} \quad (2a)$$

which is often approximated by assuming an adiabatic equation of state to give:

$$= \frac{\gamma P}{\rho_m} \quad (2b)$$

and in a plasma where the ions and electrons carry different polytrope indices, we have the ion-acoustic sound speed:

$$C_s^2 = \frac{k_B(Z_i \gamma_e T_e + \gamma_i T_i)}{M_i + m_e} \quad (2c)$$

where k_B = Boltzmann constant, Z_i = ion charge state, and one generally assumes that either $\gamma_e = 1$ (isothermal) and $\gamma_i = 2$ or 3, or $T_e \gg T_i$ and $\gamma_e = 1$ such that $C_s^2 \sim \frac{k_B T_e}{M_i}$.

The sound speed reported on the WSDB is, as stated above, give by $\langle C_s \rangle_j = \sqrt{\frac{5}{3}} \langle W_i \rangle_j$, the total plasma beta relies only upon ion data.

1.1. Conservation Relations

In the case of a planar shock, we can define the conservation relations called the Rankine-Hugoniot relations across the shock ramp. If we define $\Delta[X] = \langle X \rangle_{dn} - \langle X \rangle_{up}$, where the subscript u(d) corresponds to upstream(downstream). Then we have the following Rankine-Hugoniot relations (Koval & Szabo 2008; Szabo 1994; Vinas & Scudder 1986):

$$\Delta[G_n] \equiv \Delta[\rho(V_n - V_{shn})] = 0 \quad (3a)$$

$$\Delta[B_n] \equiv \Delta[\hat{n} \cdot \mathbf{B}] = 0 \quad (3b)$$

$$\Delta[\mathbf{S}_t] \equiv \Delta\left[\rho(V_n - V_{shn}) \mathbf{V}_t - \frac{B_n}{\mu_o} \mathbf{B}_t\right] = 0 \quad (3c)$$

$$\Delta[\mathbf{E}_t] \equiv \Delta[(\hat{n} \times \mathbf{V}_t) B_n - (V_n - V_{shn})(\hat{n} \times \mathbf{B}_t)] = 0 \quad (3d)$$

$$\Delta[S_n] \equiv \Delta\left[P + \frac{\mathbf{B}_t \cdot \mathbf{B}_t}{2 \mu_o} + \rho(V_n - V_{shn})^2\right] = 0 \quad (3e)$$

$$\Delta[\varepsilon] \equiv \Delta\left[\rho(V_n - V_{shn}) \left\{ \frac{1}{2} (\mathbf{V}_{sw} - V_{shn} \hat{n})^2 + \frac{\gamma}{\gamma - 1} \frac{P}{\rho} + \frac{\mathbf{B} \cdot \mathbf{B}}{\rho \mu_o} \right\} - \frac{B_n (\mathbf{V}_{sw} - V_{shn} \hat{n}) \cdot \mathbf{B}}{\mu_o} \right] = 0 \quad (3f)$$

where we have defined:

$$Q_n = \mathbf{Q} \cdot \hat{n} \quad (4a)$$

$$\mathbf{Q}_t = (\hat{n} \times \mathbf{Q}) \times \hat{n} \quad (4b)$$

$$= \mathbf{Q} \cdot (\mathbb{I} - \hat{n}\hat{n}) \quad (4c)$$

$$V_{shn} = \frac{\Delta[\rho \mathbf{V}_{sw}]}{\Delta[\rho]} \cdot \hat{n} \quad (4d)$$

and ρ is the mass density, P is scalar total (ion plus electron) thermal pressure, and γ is the ratio of specific heats or polytrope index. We note that $P = \hat{n} \cdot \mathbb{P} \cdot \hat{n} = 1/3 \text{Tr}[\mathbb{P}] \sim n_o k_B (T_e + T_i)$ for an ideal gas.

The Harvard Smithsonian Center for Astrophysics' Wind shock database (WSDB), which can be found at: https://www.cfa.harvard.edu/shocks/wi_data/

provides tables of numerical solutions to the Rankine-Hugoniot relations (e.g., Koval & Szabo 2008; Szabo 1994; Vinas & Scudder 1986) for eight different methods, where the labels are defined as:

1. **MC:** Magnetic Coplanarity (e.g., Abraham-Shrauner & Yun 1976; Russell et al. 1983; Vinas & Scudder 1986);
2. **VC:** Velocity Coplanarity (e.g., Abraham-Shrauner & Yun 1976; Russell et al. 1983; Vinas & Scudder 1986);
3. **MX1:** Mixed Mode Normal 1 (e.g., Abraham-Shrauner & Yun 1976; Russell et al. 1983);
4. **MX2:** Mixed Mode Normal 2 (e.g., Abraham-Shrauner & Yun 1976; Russell et al. 1983);
5. **MX3:** Mixed Mode Normal 3 (e.g., Abraham-Shrauner & Yun 1976; Russell et al. 1983);

- 110 6. **RH08:** Rankine-Hugoniot with 8 Equations (e.g.,
 111 Abraham-Shrauner & Yun 1976; Koval & Szabo
 112 2008; Russell et al. 1983; Szabo 1994; Vinas &
 113 Scudder 1986);
- 114 7. **RH09:** Rankine-Hugoniot with 9 Equations (e.g.,
 115 Abraham-Shrauner & Yun 1976; Koval & Szabo
 116 2008; Russell et al. 1983; Szabo 1994; Vinas &
 117 Scudder 1986); and
- 118 8. **RH10:** Rankine-Hugoniot with 10 Equations
 119 (e.g., Abraham-Shrauner & Yun 1976; Koval &
 120 Szabo 2008; Russell et al. 1983; Szabo 1994; Vinas
 121 & Scudder 1986).

122 The shock normals for the first five methods are given
 123 by:

Magnetic Coplanarity (MC)

$$\hat{\mathbf{n}} = \pm \frac{(\langle \mathbf{B}_o \rangle_{up} \times \langle \mathbf{B}_o \rangle_{dn}) \times (-\Delta \mathbf{B}_o)}{|(\langle \mathbf{B}_o \rangle_{up} \times \langle \mathbf{B}_o \rangle_{dn}) \times (-\Delta \mathbf{B}_o)|} \quad (5a)$$

Velocity Coplanarity (VC)

$$\hat{\mathbf{n}} = \pm \frac{\Delta \mathbf{V}_{bulk}}{|\Delta \mathbf{V}_{bulk}|} \quad (5b)$$

Mixed Mode Normal 1 (MX1)

$$\hat{\mathbf{n}} = \pm \frac{(\Delta \mathbf{V}_{bulk} \times \langle \mathbf{B}_o \rangle_{up}) \times \Delta \mathbf{B}_o}{|(\Delta \mathbf{V}_{bulk} \times \langle \mathbf{B}_o \rangle_{up}) \times \Delta \mathbf{B}_o|} \quad (5c)$$

Mixed Mode Normal 2 (MX2)

$$\hat{\mathbf{n}} = \pm \frac{(\Delta \mathbf{V}_{bulk} \times \langle \mathbf{B}_o \rangle_{dn}) \times \Delta \mathbf{B}_o}{|(\Delta \mathbf{V}_{bulk} \times \langle \mathbf{B}_o \rangle_{dn}) \times \Delta \mathbf{B}_o|} \quad (5d)$$

Mixed Mode Normal 3 (MX3)

$$\hat{\mathbf{n}} = \pm \frac{-\Delta \mathbf{B}_o \times (\Delta \mathbf{V}_{bulk} \times \Delta \mathbf{B}_o)}{|\Delta \mathbf{B}_o \times (\Delta \mathbf{V}_{bulk} \times \Delta \mathbf{B}_o)|} \quad (5e)$$

124 1.2. Field Transformations

125 We can define the velocity transformation from any
 126 arbitrary frame of reference (e.g. spacecraft frame) to
 127 the shock frame of reference as:

$$\mathbf{V}_{sh}^{rest} = \mathbf{V}^{arb.} - (\mathbf{V}_{sh}^{arb.} \cdot \hat{\mathbf{n}}) \hat{\mathbf{n}} \quad (6)$$

128 where $\hat{\mathbf{n}}$ is the vector normal to the assumed planar
 129 shock front (see Appendix 1.1). For an experimentalist's
 130 purposes, $\mathbf{V}^{arb.} \rightarrow \mathbf{V}_{sw}^{SCF}$, where \mathbf{V}_{sw}^{SCF} is the bulk
 131 flow velocity (e.g., solar wind velocity) in the spacecraft
 132 frame (SCF) of reference. Therefore, let us define V_{shn}
 133 as the shock normal speed in the SCF and $\langle U_{shn} \rangle_j$ as the
 134 flow speed along shock normal in the shock rest frame
 135 (SHF) averaged over the j^{th} region. Therefore, Equation
 136 6 goes to:

$$\langle U_{shn} \rangle_j = [\langle \mathbf{V}_{sw}^{SCF} \rangle_j - (V_{shn} \hat{\mathbf{n}})] \cdot \hat{\mathbf{n}}. \quad (7)$$

137 For many applications, one may want to know the
 138 upstream incident bulk flow speed in the shock frame,
 139 which is given by:

$$\mathbf{V}_u^{SHF} = \mathbf{V}_{sw} - (V_{shn} \hat{\mathbf{n}}). \quad (8)$$

2. SHOCK PARAMETER TABLES

Table 1. IP Shock Parameters

Ramp Time [UTC]	RH a Meth.	$\langle V_{shn} \rangle_{up}$ [km/s]	$\langle n_i \rangle_{up}$ [cm $^{-3}$]	$\langle \mathbf{B}_o \rangle_{up}$ [nT]	$\langle M_A \rangle_{up}$ ^c	$\langle M_{cs} \rangle_{up}$ ^e	$\langle M_f \rangle_{up}$ ^f	$\langle M_f \rangle_{up}$ ^g
1995-02-26/02:55:41.125	RH08	285.90 \pm 4.60	21.3 \pm 0.70	8.62 \pm 8.66	1.43 \pm 0.03	2.54 \pm 0.06	1.35 \pm 0.03	
1995-07-24/02:23:13.000	RH08	375.20 \pm 6.20	8.80 \pm 0.20	1.91 \pm 1.96	6.24 \pm 0.37	4.41 \pm 0.19	4.00 \pm 0.15	
1995-08-17/02:47:21.925	RH08	463.90 \pm 4.80	2.50 \pm 0.20	2.00 \pm 2.31	2.50 \pm 0.20	2.07 \pm 0.14	1.74 \pm 0.10	
1995-08-22/12:56:49.250	RH08	381.00 \pm 5.30	3.40 \pm 0.20	2.11 \pm 2.17	2.57 \pm 0.13	2.47 \pm 0.16	1.82 \pm 0.04	
1995-12-24/05:57:35.375	RH08	422.80 \pm 11.50	16.4 \pm 1.50	6.33 \pm 6.52	2.95 \pm 0.26	4.30 \pm 0.23	2.52 \pm 0.17	
1996-02-06/19:14:23.700	RH08	383.40 \pm 5.90	7.60 \pm 0.30	3.88 \pm 4.25	1.71 \pm 0.10	2.06 \pm 0.07	1.40 \pm 0.06	
1996-04-02/10:07:57.525	RH09	155.20 \pm 5.70	12.1 \pm 0.30	2.55 \pm 2.77	2.29 \pm 0.19	1.51 \pm 0.05	1.27 \pm 0.07	
1996-04-03/09:47:17.152	RH08	379.20 \pm 3.80	14.5 \pm 0.50	4.24 \pm 4.26	2.02 \pm 0.06	2.52 \pm 0.07	1.59 \pm 0.02	
1996-04-08/02:41:09.765	RH08	182.30 \pm 4.00	15.8 \pm 0.20	5.69 \pm 5.85	2.42 \pm 0.04	3.89 \pm 0.06	2.08 \pm 0.03	
1997-02-09/12:50:21.125	RH08	635.90 \pm 12.50	3.90 \pm 0.20	3.38 \pm 3.63	3.14 \pm 0.16	2.09 \pm 0.09	1.86 \pm 0.06	
1997-02-27/17:29:09.087	RH08	557.40 \pm 30.20	1.80 \pm 0.10	3.99 \pm 4.09	1.83 \pm 0.06	3.42 \pm 0.16	1.71 \pm 0.04	
1997-05-15/01:15:21.945	RH08	449.00 \pm 11.50	18.6 \pm 0.40	7.29 \pm 7.34	3.99 \pm 0.14	5.06 \pm 0.11	3.14 \pm 0.07	
1997-05-20/05:10:47.400	RH08	349.60 \pm 2.60	8.60 \pm 0.30	3.39 \pm 3.52	1.92 \pm 0.13	2.02 \pm 0.16	1.50 \pm 0.08	
1997-10-24/11:18:09.966	RH08	490.90 \pm 13.00	11.0 \pm 0.70	9.14 \pm 9.91	1.92 \pm 0.07	3.71 \pm 0.23	1.73 \pm 0.06	
1997-11-30/07:15:44.250	RH08	360.60 \pm 4.40	19.2 \pm 0.50	4.81 \pm 5.00	3.01 \pm 0.08	3.67 \pm 0.08	2.48 \pm 0.05	
1997-12-10/04:33:14.664	RH08	391.20 \pm 12.40	10.2 \pm 0.90	7.10 \pm 7.35	2.73 \pm 0.17	3.89 \pm 0.26	2.26 \pm 0.10	
1997-12-30/01:13:43.921	RH08	423.40 \pm 8.10	7.70 \pm 0.20	5.37 \pm 5.82	2.47 \pm 0.07	2.94 \pm 0.07	1.89 \pm 0.03	
1998-01-06/13:29:00.368	RH08	408.40 \pm 10.00	9.70 \pm 0.40	6.53 \pm 6.86	2.41 \pm 0.07	3.40 \pm 0.29	1.97 \pm 0.05	
1998-01-31/15:53:43.500	RH09	418.50 \pm 20.20	6.70 \pm 0.50	9.81 \pm 9.87	1.06 \pm 0.06	3.62 \pm 0.37	1.04 \pm 0.02	
1998-03-04/11:02:45.500	MX3	455.50 \pm 3170	4.70 \pm 0.20	3.17 \pm 3.20	3.48 \pm 0.15	3.18 \pm 0.16	2.57 \pm 0.04	
1998-04-07/16:53:35.700	RH08	368.80 \pm 4.00	9.30 \pm 0.30	6.87 \pm 6.94	2.02 \pm 0.04	3.98 \pm 0.15	1.92 \pm 0.03	
1998-04-23/17:29:02.500	RH08	401.70 \pm 9.80	14.3 \pm 0.80	4.18 \pm 4.22	3.22 \pm 0.10	2.32 \pm 0.06	1.98 \pm 0.05	
1998-04-30/08:43:15.291	RH08	331.20 \pm 6.30	11.6 \pm 0.60	1.04 \pm 1.57	15.61 \pm 4.14	6.91 \pm 0.37	6.39 \pm 0.34	
1998-05-03/17:02:20.425	RH08	499.60 \pm 11.10	3.80 \pm 0.40	3.50 \pm 3.72	1.91 \pm 0.11	5.50 \pm 0.42	1.85 \pm 0.09	
1998-05-15/13:53:46.000	RH08	328.50 \pm 2.10	12.3 \pm 0.10	2.85 \pm 2.87	4.61 \pm 0.06	4.51 \pm 0.15	3.40 \pm 0.04	
1998-06-13/19:18:10.950	MX2	257.70 \pm 8.00	3.70 \pm 0.40	4.45 \pm 4.50	1.86 \pm 0.13	4.70 \pm 0.47	1.83 \pm 0.08	
1998-08-06/07:16:07.587	RH08	478.80 \pm 36.50	10.9 \pm 1.00	10.3 \pm 10.4	1.66 \pm 0.10	5.11 \pm 0.39	1.58 \pm 0.08	
1998-08-19/18:40:41.450	RH08	334.70 \pm 6.20	7.80 \pm 0.30	3.54 \pm 3.91	2.80 \pm 0.17	3.35 \pm 0.17	2.32 \pm 0.13	
1998-08-26/06:40:24.972	RH08	687.40 \pm 26.80	4.90 \pm 0.40	6.48 \pm 6.64	6.20 \pm 0.39	7.30 \pm 0.28	4.74 \pm 0.18	
1998-10-02/07:06:02.475	RH08	620.30 \pm 77.00	2.80 \pm 1.10	6.48 \pm 7.15	2.88 \pm 0.91	4.02 \pm 0.94	2.66 \pm 0.41	
1998-10-23/12:58:20.505	RH09	584.60 \pm 7.90	2.60 \pm 0.10	4.22 \pm 4.53	2.27 \pm 0.11	2.08 \pm 0.10	1.66 \pm 0.05	
1998-11-08/04:41:17.290	RH08	644.50 \pm 64.30	4.40 \pm 0.70	17.4 \pm 17.6	1.51 \pm 0.14	6.47 \pm 1.11	1.49 \pm 0.14	
1998-12-28/18:20:16.211	RH08	465.20 \pm 30.20	6.90 \pm 0.90	6.88 \pm 8.53	1.75 \pm 0.27	2.28 \pm 0.55	1.42 \pm 0.16	
1999-01-13/10:47:45.119	RH08	433.10 \pm 22.40	9.70 \pm 1.10	5.06 \pm 6.24	2.48 \pm 0.27	2.69 \pm 0.27	1.85 \pm 0.20	
1999-01-22/20:21:37.150	RH08	668.90 \pm 146.50	2.90 \pm 0.10	9.56 \pm 10.1	1.44 \pm 0.04	2.31 \pm 0.10	1.40 \pm 0.03	
1999-02-18/02:48:15.800	RH08	699.00 \pm 19.70	3.30 \pm 0.40	7.08 \pm 7.43	3.55 \pm 0.25	5.05 \pm 1.16	3.05 \pm 0.38	
1999-04-16/11:14:11.089	RH09	479.80 \pm 14.50	4.00 \pm 0.50	6.60 \pm 6.63	1.60 \pm 0.11	3.62 \pm 0.37	1.49 \pm 0.08	
1999-05-18/00:32:39.625	RH08	442.40 \pm 3.80	8.00 \pm 0.50	5.56 \pm 5.66	2.37 \pm 0.11	3.38 \pm 0.19	2.25 \pm 0.07	
1999-06-26/19:30:58.154	RH08	467.20 \pm 9.70	15.6 \pm 1.00	11.9 \pm 12.9	2.22 \pm 0.07	2.93 \pm 0.14	1.83 \pm 0.03	
1999-07-02/00:27:24.060	RH08	635.90 \pm 36.00	1.30 \pm 0.00	4.59 \pm 5.05	2.05 \pm 0.07	2.83 \pm 0.29	1.81 \pm 0.04	

Table 1 continued

Table 1 (*continued*)

Ramp Time [UTC]	RH Meth.	$\langle V_{shn} \rangle_{up}$ [km/s]	$\langle n_i \rangle_{up}$ [cm $^{-3}$]	$\langle \mathbf{B}_o \rangle_{up}$ [nT]	$\langle M_A \rangle_{up}$ ^d	$\langle M_{cs} \rangle_{up}$ ^e	$\langle M_f \rangle_{up}$ ^f	$\langle M_f \rangle_{up}$ ^g
1999-07-06/14:24:56.625	RH08	475.70± 20.80	2.90±0.20	5.59±5.99	1.86±0.07	6.50± 0.55	1.83±0.05	
1999-07-26/23:50:17.327	RH08	426.80± 8.80	2.30±0.20	3.85±4.06	1.33±0.24	1.39± 0.17	1.15±0.05	
1999-08-04/01:44:38.601	RH08	418.10± 6.90	8.70±0.20	6.23±6.39	2.07±0.08	4.91± 0.27	1.95±0.04	
1999-08-15/10:33:45.975	RH09	424.30± 8.90	15.5±0.60	4.49±5.49	3.73±0.26	2.35± 0.10	1.99±0.05	
1999-08-23/15:41:34.980	MX2	506.20± 25.10	8.70±0.40	10.6±10.7	1.17±0.05	1.98± 0.11	1.01±0.04	
1999-09-12/03:57:56.062	RH08	534.90± 8.00	3.70±0.20	4.04±4.35	3.15±0.10	3.41± 0.12	2.35±0.06	
1999-09-15/07:43:49.625	RH08	665.50± 16.30	2.60±0.10	5.69±7.01	2.04±0.12	1.93± 0.07	1.42±0.06	
1999-09-22/12:09:25.567	RH08	510.70± 37.20	17.0±0.70	11.3±13.8	2.44±0.10	2.85± 0.11	1.88±0.08	
1999-10-21/02:20:51.968	RH08	477.30± 28.60	13.4±0.40	9.17±9.64	2.46±0.07	4.71± 0.16	2.21±0.06	
1999-12-12/15:54:27.750	RH08	564.00± 39.90	0.60±0.10	4.71±4.83	1.51±0.19	7.20± 1.40	1.51±0.20	
2000-02-11/23:33:55.710	RH08	641.40± 13.20	5.00±0.40	6.70±6.94	3.98±0.12	5.62± 0.25	3.25±0.08	
2000-02-20/21:03:45.795	RH08	474.50± 13.40	8.60±0.50	7.64±7.70	3.06±0.10	5.48± 0.32	2.67±0.05	

^aRankine-Hugoniot^bshock normal speed in SCF^cupstream ion number density^dupstream magnetic field magnitude^eupstream Alfvénic Mach number^fupstream sound Mach number^gupstream fast mode Mach number

NOTE—For symbol definitions, see Section 1.

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3. CRITICAL MACH NUMBERS

142 For each crossing, we estimated four different critical
 143 Mach numbers. The first critical Mach number,
 144 M_{cr} , defines the maximum Mach number above which
 145 an ion sound wave could not phase stand within the
 146 shock ramp, thus for $\langle M_f/M_{cr} \rangle_{up} \geq 1$ the shock cannot
 147 rely upon resistive dissipation effects to maintain a sta-
 148 ble discontinuity (e.g., Edmiston & Kennel 1984; Kennel
 149 et al. 1985). We also estimated three whistler critical
 150 Mach numbers (Krasnoselskikh et al. 2002), defined as:
 151 M_{ww} is the maximum Mach number for which a linear
 152 whistler can phase stand upstream of the shock ramp;
 153 M_{gr} is similar to M_{ww} but depends upon the whistler
 154 group velocity, thus determines the cutoff where a lin-
 155 ear precursor can no longer carry energy into the up-
 156 stream; and M_{nw} defines the separation between a sta-
 157 ble/stationary and “breaking” shock front.

158 The ratios between the upstream fast mode Mach
 159 number and each critical Mach number is shown in Ta-
 160 ble 2 along with the upstream average beta and shock
 161 normal angle for the 145 good shocks. All values are re-
 162 ported with associated uncertainties. Notice that only

163 12($\sim 8\%$) satisfy $\langle M_f/M_{cr} \rangle_{up} \geq 1$, thus most of these
 164 shocks are subcritical.

165 As a side note, for all 250 quasi-perpendicular shocks
 166 in the WSDB, 104($\sim 42\%$) satisfy $\langle M_f/M_{cr} \rangle_{up} \geq 1$ thus
 167 slightly less than half are supercritical. Further, only
 168 40($\sim 16\%$) satisfy $\langle M_f/M_{ww} \rangle_{up} \geq 1$, thus most quasi-
 169 perpendicular interplanetary shocks should exhibit up-
 170 stream whistler precursor waves, assuming cold plasma
 171 and a dispersion-only dissipation mechanism (e.g., Kras-
 172 noselskikh et al. 2002).

Table 2. IP Shock Critical Mach Number Ratios

Ramp Time [UTC]	$\langle U_{shn} \rangle_{up}$ [km/s]	$\langle \beta_{Tot} \rangle_{up}$ ^a	$\langle \theta_{Bn} \rangle_{up}$ ^b	$\langle M_f/M_{cr} \rangle_{up}$ ^c	$\langle M_f/M_{ww} \rangle_{up}$ ^d	$\langle M_f/M_{gr} \rangle_{up}$ ^e	$\langle M_f/M_{nw} \rangle_{up}$ ^f	$\langle M_f/M_{nw} \rangle_{up}$ ^g
1995-02-26/02:55:41.125	58.60± 1.00	0.19±0.19	34.80±1.50	0.67±0.05	0.08±0.00	0.06±0.00	0.05±0.00	
1995-07-24/02:23:13.000	90.70± 1.10	1.21±1.27	33.80±7.00	2.62±0.85	0.23±0.02	0.17±0.02	0.16±0.01	
1995-08-17/02:47:21.925	70.10± 4.40	0.89±0.94	41.90±4.10	1.03±0.31	0.11±0.01	0.08±0.01	0.08±0.01	
1995-08-22/12:56:49.250	66.10± 2.50	0.65±0.67	66.10±7.40	0.91±0.24	0.21±0.06	0.16±0.05	0.15±0.04	
1995-12-24/05:57:35.375	101.50± 2.30	0.29±0.26	58.40±3.30	1.14±0.16	0.22±0.03	0.17±0.02	0.16±0.02	
1996-02-06/19:14:23.700	52.90± 1.30	0.42±0.43	48.40±4.60	0.70±0.13	0.10±0.01	0.08±0.01	0.07±0.01	
1996-04-02/10:07:57.525	36.90± 1.00	1.39±1.47	74.00±3.10	0.71±0.27	0.22±0.04	0.17±0.03	0.15±0.03	
1996-04-03/09:47:17.152	49.60± 0.80	0.39±0.38	75.70±1.40	0.71±0.12	0.30±0.03	0.23±0.02	0.21±0.02	
1996-04-08/02:41:09.765	76.40± 0.70	0.23±0.23	73.30±1.10	0.87±0.10	0.34±0.02	0.26±0.02	0.24±0.02	
1997-02-09/12:50:21.125	122.90± 3.50	1.37±1.30	42.70±10.2	1.19±0.40	0.12±0.02	0.09±0.02	0.08±0.01	
1997-02-27/17:29:09.087	122.50± 2.50	0.17±0.18	42.20±3.50	0.80±0.06	0.11±0.01	0.08±0.00	0.08±0.00	
1997-05-15/01:15:21.945	147.00± 0.80	0.38±0.38	85.30±2.20	1.38±0.24	1.79±0.84	1.38±0.64	1.27±0.59	
1997-05-20/05:10:47.400	49.50± 3.20	0.54±0.54	46.00±11.3	0.80±0.18	0.10±0.02	0.08±0.02	0.07±0.02	
1997-10-24/11:18:09.966	117.40± 2.40	0.16±0.16	68.30±4.50	0.71±0.06	0.22±0.04	0.17±0.03	0.15±0.03	
1997-11-30/07:15:44.250	71.90± 1.20	0.41±0.40	49.10±2.10	1.24±0.21	0.18±0.01	0.14±0.01	0.13±0.01	
1997-12-10/04:33:14.664	132.30± 2.30	0.30±0.28	70.90±1.60	0.99±0.14	0.32±0.03	0.25±0.02	0.23±0.02	
1997-12-30/01:13:43.921	107.20± 1.30	0.42±0.41	87.40±8.10	0.85±0.16	0.81±0.53	0.62±0.41	0.57±0.37	
1998-01-06/13:29:00.368	111.00± 2.60	0.30±0.30	82.30±6.20	0.84±0.12	0.69±0.55	0.53±0.43	0.49±0.39	
1998-01-31/15:53:43.500	87.30± 3.50	0.05±0.05	37.50±2.50	0.48±0.02	0.06±0.00	0.05±0.00	0.04±0.00	
1998-03-04/11:02:45.500	110.40± 0.30	0.73±0.76	41.70±3.00	1.48±0.39	0.16±0.01	0.12±0.01	0.11±0.01	
1998-04-07/16:53:35.700	99.70± 0.70	0.16±0.16	37.10±0.90	0.93±0.06	0.11±0.00	0.09±0.00	0.08±0.00	
1998-04-23/17:29:02.500	77.70± 1.20	1.15±1.17	51.70±1.60	1.16±0.39	0.15±0.01	0.11±0.00	0.11±0.00	
1998-04-30/08:43:15.291	114.40± 1.80	3.86±2.65	64.60±9.30	5.14±0.89	0.70±0.24	0.54±0.19	0.50±0.17	
1998-05-03/17:02:20.425	76.80± 2.90	0.07±0.08	52.30±2.00	0.78±0.05	0.14±0.01	0.11±0.01	0.10±0.01	
1998-05-15/13:53:46.000	83.30± 0.60	0.63±0.62	52.70±1.80	1.79±0.43	0.26±0.01	0.20±0.01	0.19±0.01	
1998-06-13/19:18:10.950	95.20± 2.20	0.10±0.08	27.20±2.50	0.93±0.05	0.10±0.00	0.07±0.00	0.07±0.00	
1998-08-06/07:16:07.587	113.90± 1.90	0.06±0.07	80.80±3.90	0.60±0.04	0.46±0.20	0.36±0.15	0.33±0.14	
1998-08-19/18:40:41.450	78.10± 2.80	0.42±0.41	45.50±8.10	1.19±0.22	0.16±0.02	0.12±0.02	0.11±0.02	
1998-08-26/06:40:24.972	401.30± 3.80	0.44±0.42	82.20±3.00	2.15±0.41	1.63±0.63	1.26±0.48	1.15±0.44	
1998-10-02/07:06:02.475	270.70± 10.10	0.44±0.37	26.20±9.90	1.58±0.35	0.14±0.02	0.11±0.02	0.10±0.02	
1998-10-23/12:58:20.505	131.30± 5.40	0.72±0.74	43.60±8.40	0.94±0.25	0.11±0.02	0.08±0.01	0.08±0.01	
1998-11-08/04:41:17.290	275.10± 6.10	0.03±0.03	54.60±1.40	0.61±0.06	0.12±0.01	0.09±0.01	0.08±0.01	
1998-12-28/18:20:16.211	105.90± 10.90	0.41±0.43	60.70±12.9	0.68±0.15	0.14±0.06	0.11±0.04	0.10±0.04	
1999-01-13/10:47:45.119	92.90± 7.30	0.52±0.49	70.90±12.7	0.89±0.21	0.27±0.18	0.21±0.14	0.19±0.12	
1999-01-22/20:21:37.150	180.20± 3.50	0.23±0.23	17.10±5.70	0.83±0.08	0.07±0.00	0.05±0.00	0.05±0.00	
1999-02-18/02:48:15.800	304.40± 20.30	0.31±0.23	51.30±6.80	1.45±0.24	0.23±0.04	0.18±0.03	0.16±0.03	
1999-04-16/11:14:11.089	116.30± 4.20	0.12±0.11	62.30±3.40	0.61±0.05	0.15±0.02	0.12±0.01	0.11±0.01	
1999-05-18/00:32:39.625	102.20± 0.60	0.30±0.28	22.20±1.00	1.31±0.15	0.11±0.00	0.09±0.00	0.08±0.00	
1999-06-26/19:30:58.154	145.40± 1.70	0.34±0.36	59.40±3.70	0.85±0.13	0.17±0.02	0.13±0.01	0.12±0.01	
1999-07-02/00:27:24.060	178.80± 5.30	0.32±0.31	39.30±6.60	0.93±0.13	0.11±0.01	0.08±0.01	0.08±0.01	
1999-07-06/14:24:56.625	135.80± 3.10	0.05±0.05	44.80±6.60	0.80±0.04	0.12±0.01	0.09±0.01	0.09±0.01	
1999-07-26/23:50:17.327	75.80± 7.60	0.60±0.79	18.50±9.10	0.77±0.18	0.06±0.00	0.04±0.00	0.04±0.00	

Table 2 continued

Table 2 (*continued*)

Ramp Time [UTC]	$\langle U_{shn} \rangle_{up}$ [km/s]	$\langle \beta_{Tot} \rangle_{up}$ ^a	$\langle \theta_{Bn} \rangle_{up}$ ^b	$\langle M_f/M_{cr} \rangle_{up}$ ^c	$\langle M_f/M_{ww} \rangle_{up}$ ^d	$\langle M_f/M_{gr} \rangle_{up}$ ^e	$\langle M_f/M_{nw} \rangle_{up}$ ^f	$\langle M_f/M_{nw} \rangle_{up}$ ^g
1999-08-04/01:44:38.601	95.90 ± 2.90	0.11 ± 0.11	54.10 ± 4.80	0.83 ± 0.05	0.16 ± 0.02	0.12 ± 0.01	0.11 ± 0.01	
1999-08-15/10:33:45.975	95.10 ± 1.30	1.55 ± 1.60	79.20 ± 4.30	1.11 ± 0.44	0.50 ± 0.20	0.38 ± 0.15	0.35 ± 0.14	
1999-08-23/15:41:34.980	92.30 ± 3.50	0.21 ± 0.21	88.60 ± 4.40	0.41 ± 0.05	0.80 ± 0.52	0.61 ± 0.40	0.56 ± 0.37	
1999-09-12/03:57:56.062	145.30 ± 3.50	0.51 ± 0.50	69.90 ± 5.40	1.12 ± 0.24	0.32 ± 0.08	0.25 ± 0.06	0.23 ± 0.06	
1999-09-15/07:43:49.625	163.70 ± 2.70	0.68 ± 0.73	73.60 ± 4.30	0.70 ± 0.19	0.24 ± 0.06	0.18 ± 0.05	0.17 ± 0.04	
1999-09-22/12:09:25.567	149.20 ± 3.40	0.44 ± 0.46	70.80 ± 3.40	0.87 ± 0.18	0.27 ± 0.05	0.21 ± 0.04	0.19 ± 0.03	
1999-10-21/02:20:51.968	135.80 ± 1.10	0.17 ± 0.16	69.40 ± 3.30	0.91 ± 0.08	0.29 ± 0.05	0.23 ± 0.04	0.21 ± 0.03	
1999-12-12/15:54:27.750	203.90 ± 8.50	0.03 ± 0.03	48.70 ± 3.00	0.63 ± 0.09	0.11 ± 0.02	0.08 ± 0.01	0.08 ± 0.01	
2000-02-11/23:33:55.710	263.60 ± 2.40	0.30 ± 0.30	86.50 ± 2.20	1.38 ± 0.20	2.49 ± 1.56	1.91 ± 1.20	1.76 ± 1.10	
2000-02-20/21:03:45.795	174.60 ± 2.70	0.19 ± 0.18	88.10 ± 4.60	1.08 ± 0.10	1.93 ± 1.28	1.49 ± 0.99	1.37 ± 0.91	

^a shock normal speed in SHF^b upstream plasma beta^c shock normal angle^d fast mode to first critical Mach number ratio^e fast mode to linear (phase) whistler critical Mach number^f fast mode to linear (group) whistler critical Mach number^g fast mode to nonlinear whistler critical Mach number

NOTE—For symbol definitions, see Section 1.

173 4. DATA AVAILABILITY

174 Most relevant *Wind* instrument data can be found on
175 CDAWeb at:
176 <http://cdaweb.gsfc.nasa.gov>
177 including quasi-static magnetic fields from *Wind*/MFI
178 (Lepping et al. 1995) and solar wind plasma parame-
179 ters from the *Wind*/SWE Faraday Cups (FCs) (Ogilvie
180 et al. 1995). The remaining *Wind*/3DP level-zero (lz)
181 data can be found at:
182 <http://sprg.ssl.berkeley.edu/wind3dp/data/wi/3dp/lz/>.

183
184 The Harvard Smithsonian Center for Astrophysics'
185 *Wind* interplanetary shock list can be found at:
186 https://www.cfa.harvard.edu/shocks/wi_data/.

187
188 The critical Mach number analysis software can be
189 found at:
190 <https://github.com/pulupa/Critical-Mach>.

191
192 Any additional analysis software can be found at:
193 https://github.com/lynnbwilsoniii/wind_3dp_pros.

195 5. EXTRA STATISTICAL RESULTS

196 In the following one-variable statistics and distribu-
197 tions of $T_{s,j}$, n_s , $\beta_{es,j}$, and $(T_s/T_{s'})_j$ are presented that
198 are not directly shown in the main multi-part papers.
199 Given that none of the parameters have Gaussian dis-
200 tributions, the median (\tilde{X}) and lower ($X_{25\%}$) and upper
201 quartile ($\equiv X_{75\%}$) values in addition to the minimum
202 (X_{min}), maximum (X_{max}), and mean (\bar{X}) in the statis-
203 tical tables shown in the main paper. The distributions
204 for these parameters are shown in the histograms in Fig-
205 ures 1–8.

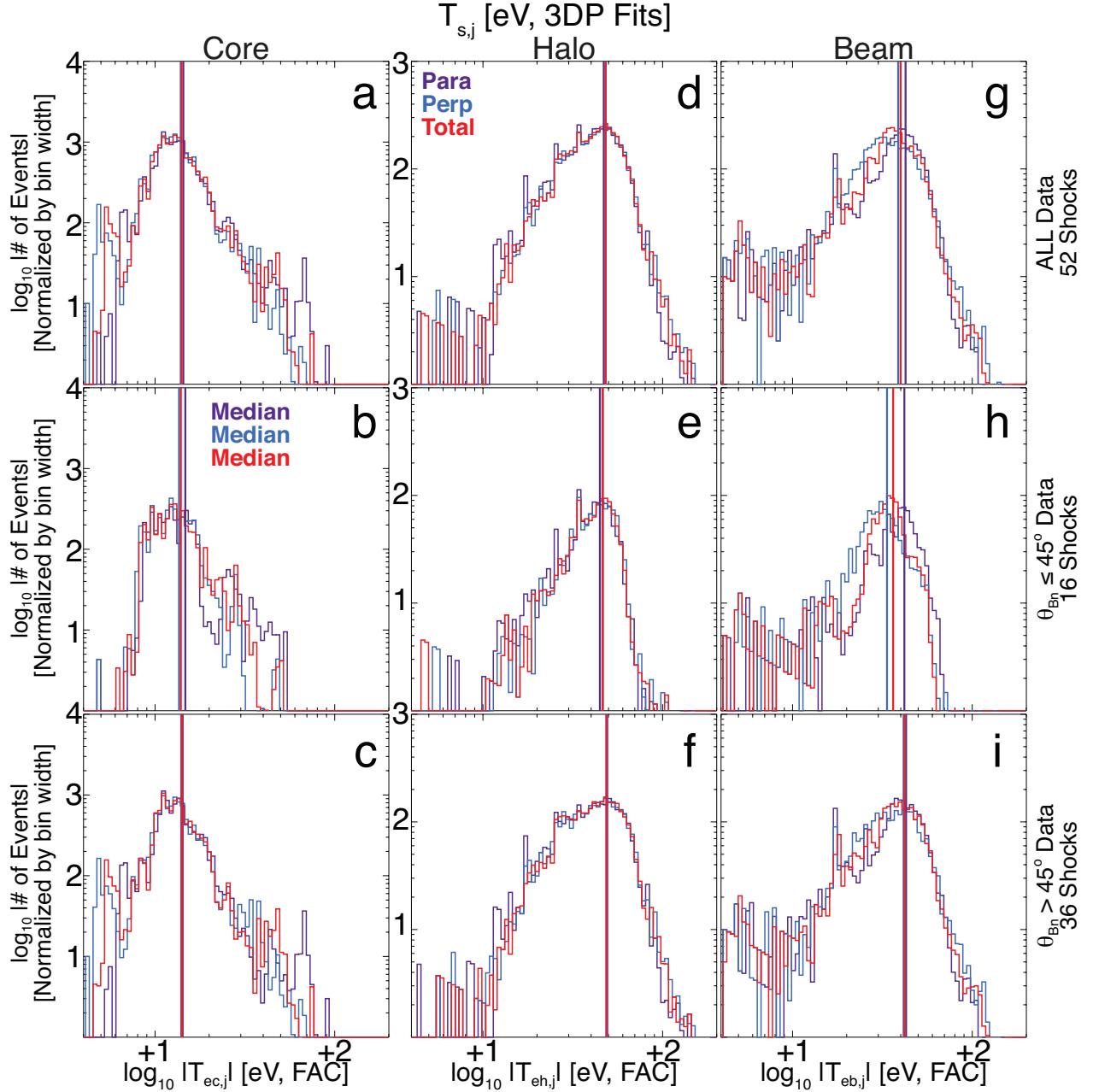


Figure 1. Temperatures [eV] for different electron components in each column and for the different shock geometries (i.e., rows) shown to the right. In each panel, there are three color-coded histograms for the different field-aligned components defined as follows: total (red); parallel (violet); and perpendicular (blue). The color-coded vertical lines are the median values of the regressed distributions for the corresponding color-coded histograms.

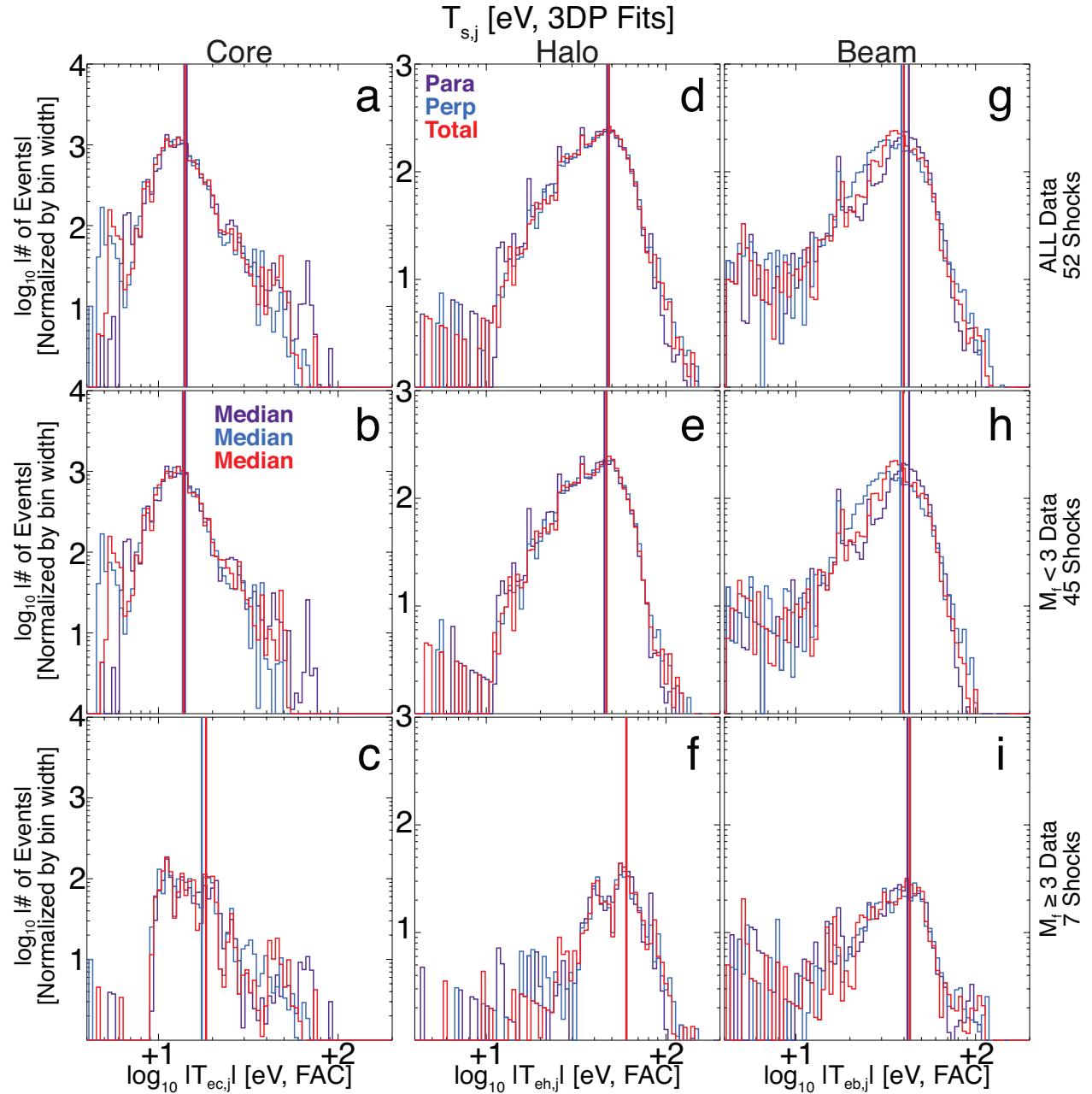


Figure 2. Temperatures [eV] for different electron components in each column and for the different Mach numbers (i.e., rows) shown to the right with the same format as Figure 1.

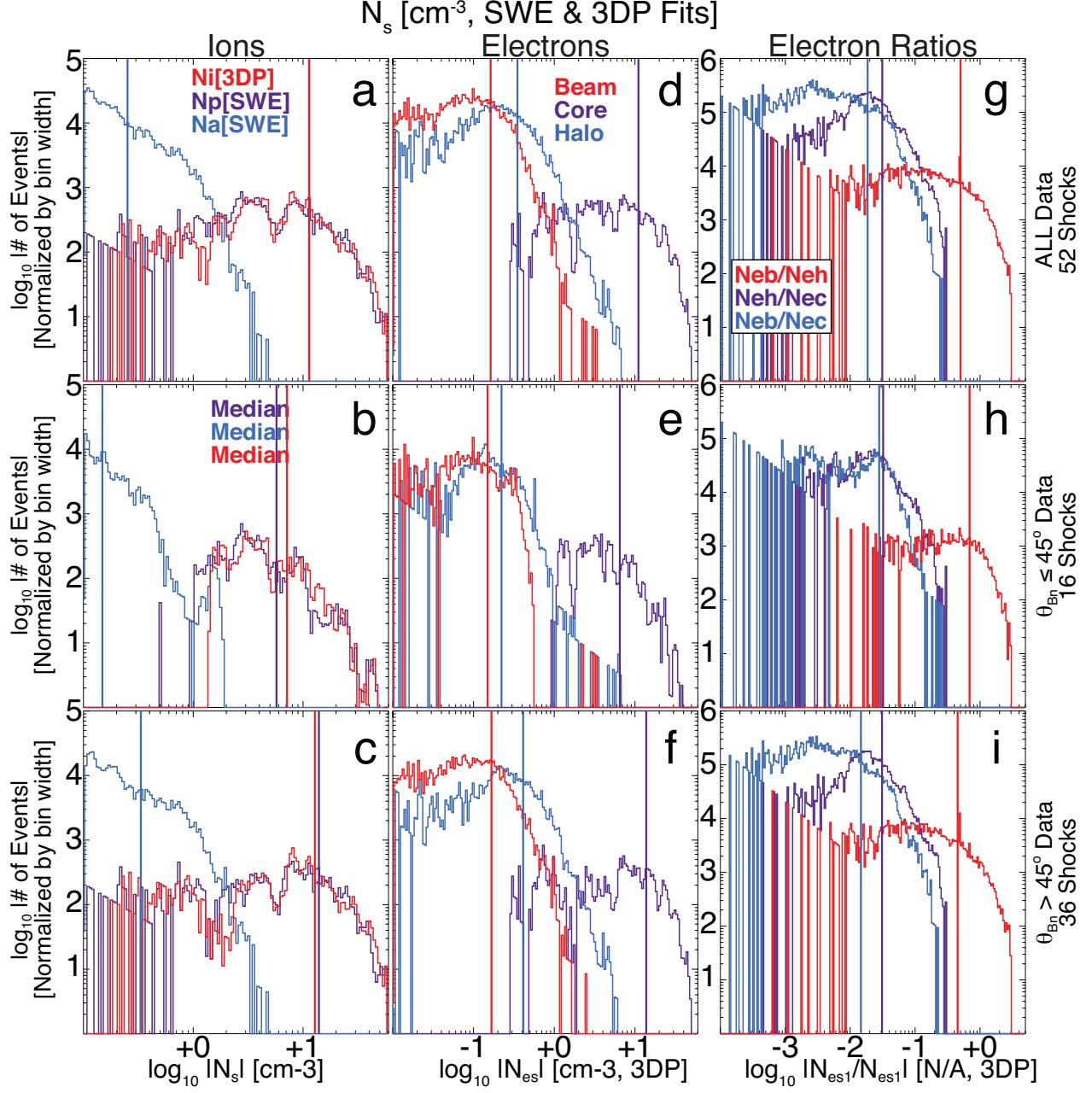


Figure 3. Densities [cm^{-3}] and density ratios for different ion and electron components. The format is similar to Figure 1 with the row organization but the columns differ. The first column here shows proton (violet) and alpha-particle (blue) density from *Wind*/SWE and total ion density from *Wind*/3DP (red). The second column shows n_{es} for the core (violet), halo (blue), and beam/strahl (red) components. The third column shows n_{es1}/n_{es2} for the halo-to-core (violet), beam-to-core (blue), and beam-to-halo (red) density ratios.

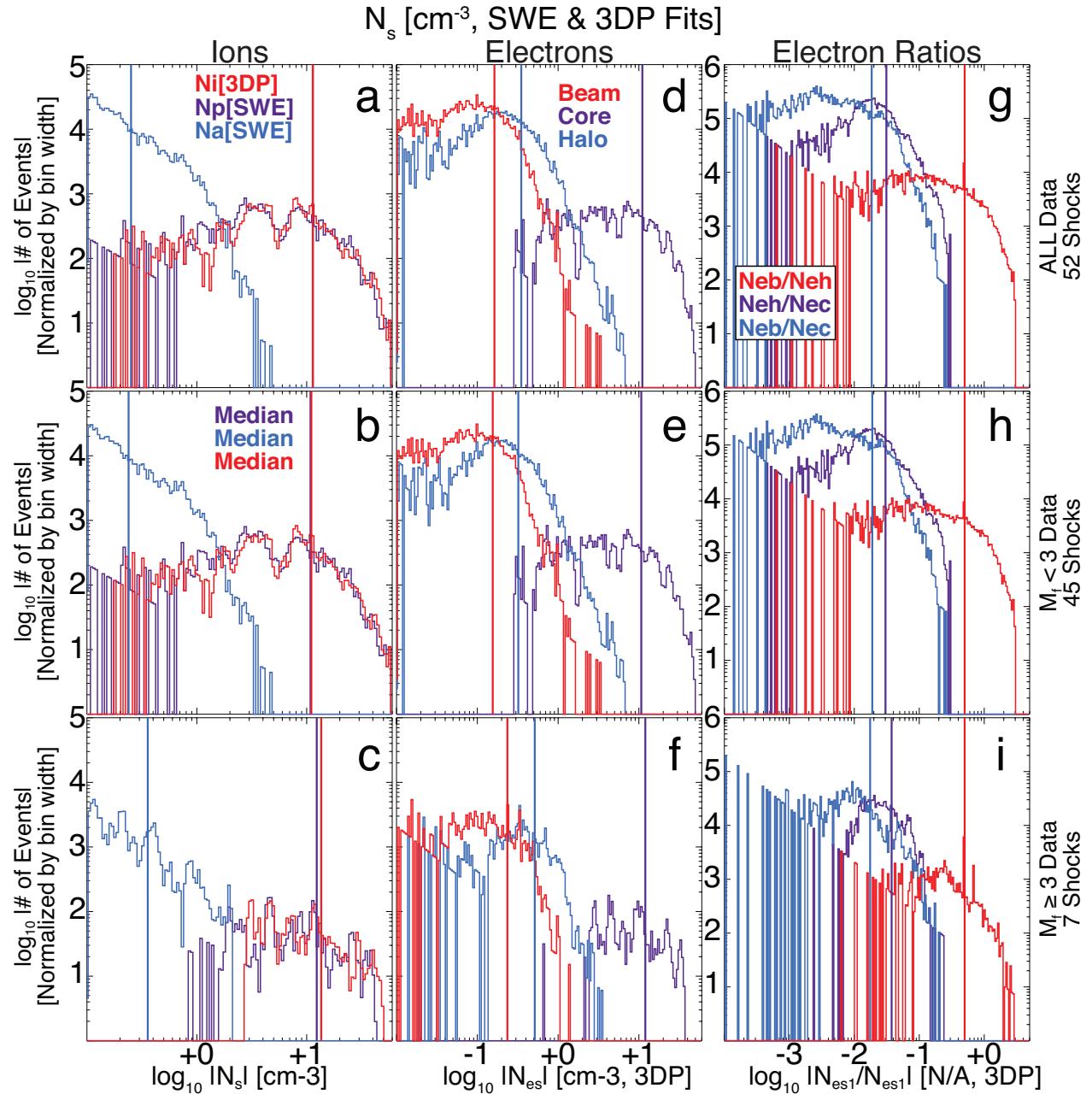


Figure 4. The same format and variables as in Figure 3 but for different Mach numbers instead of geometry.

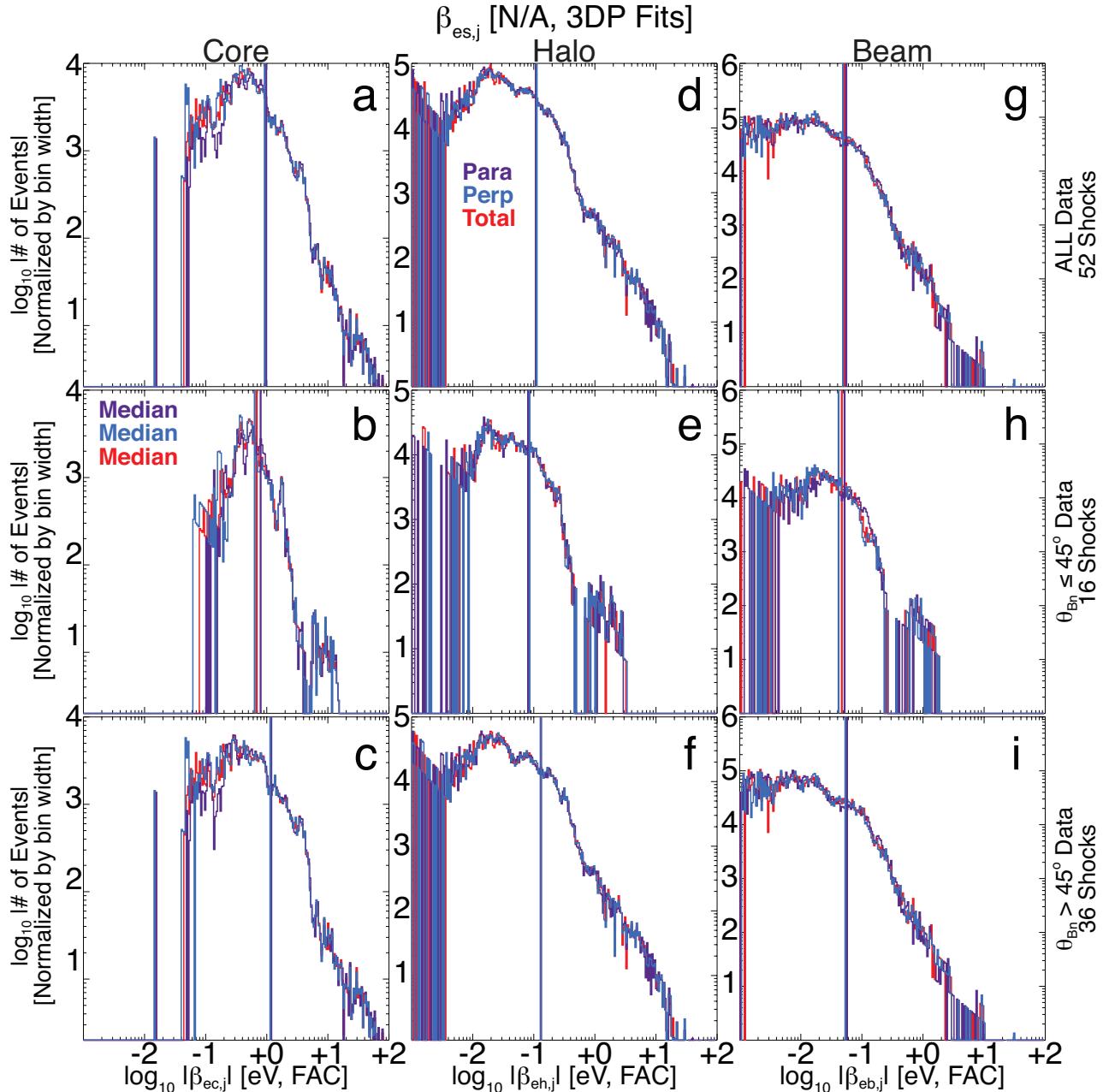


Figure 5. The same format as Figures 1 and 3 except for electron betas [N/A]. Note that all three components have different vertical axis scales.

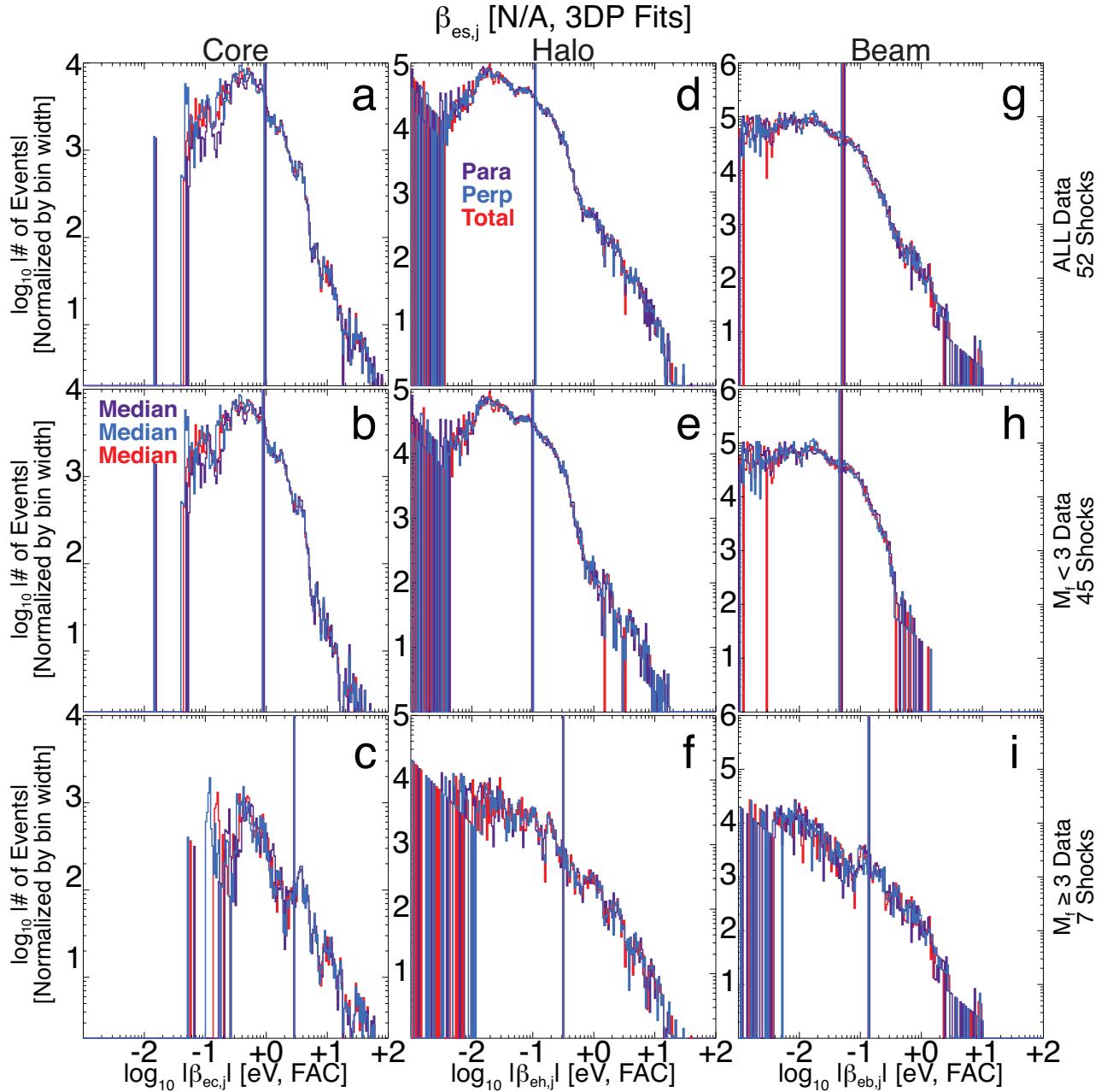


Figure 6. The same format as Figure 5 except for different Mach numbers (i.e., rows) instead of geometry. Note that all three components have different vertical axis scales.

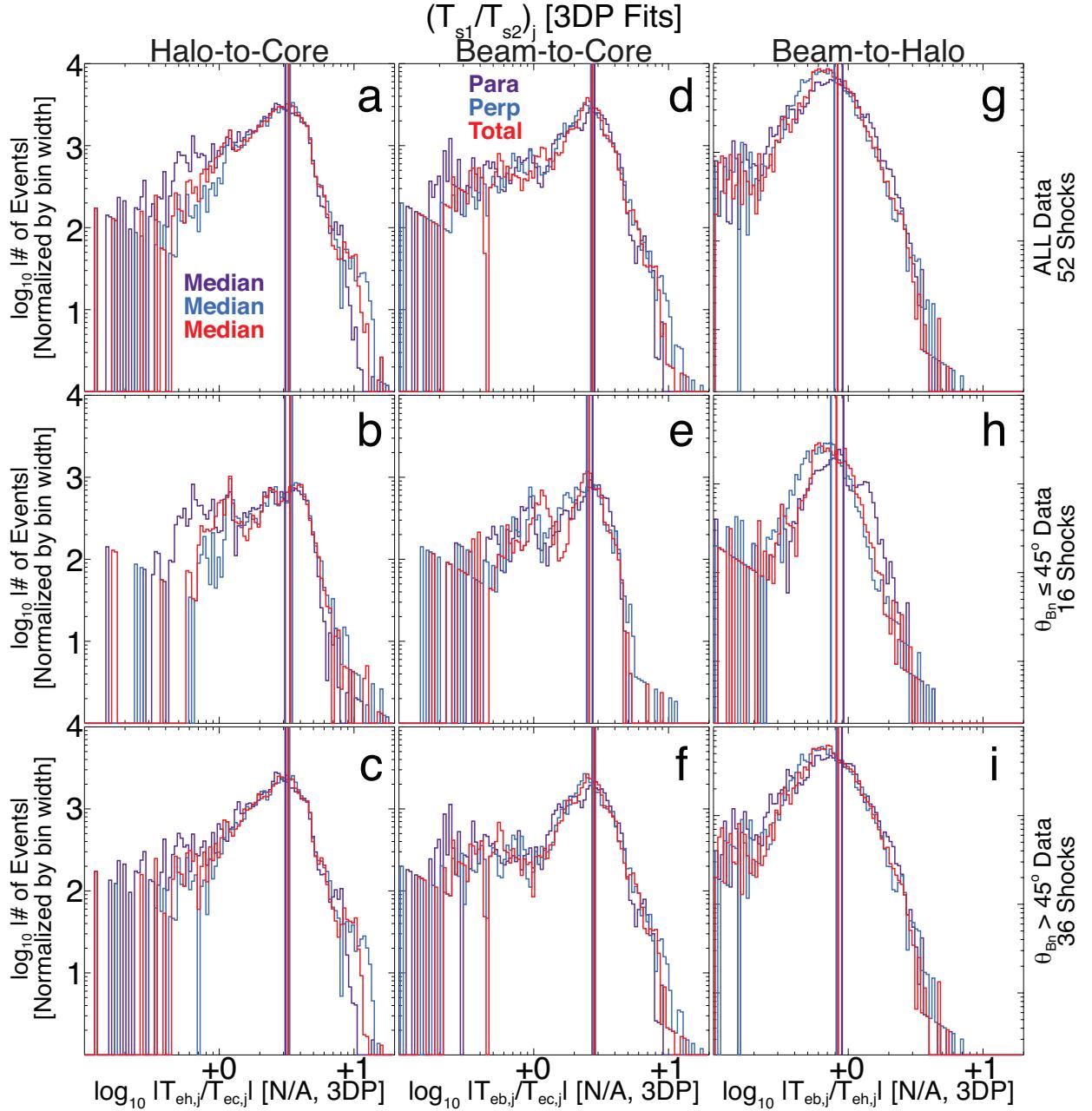


Figure 7. The same format as Figure 1 except for electron temperature ratios [N/A]. Note that all three components have a uniform vertical axis scale.

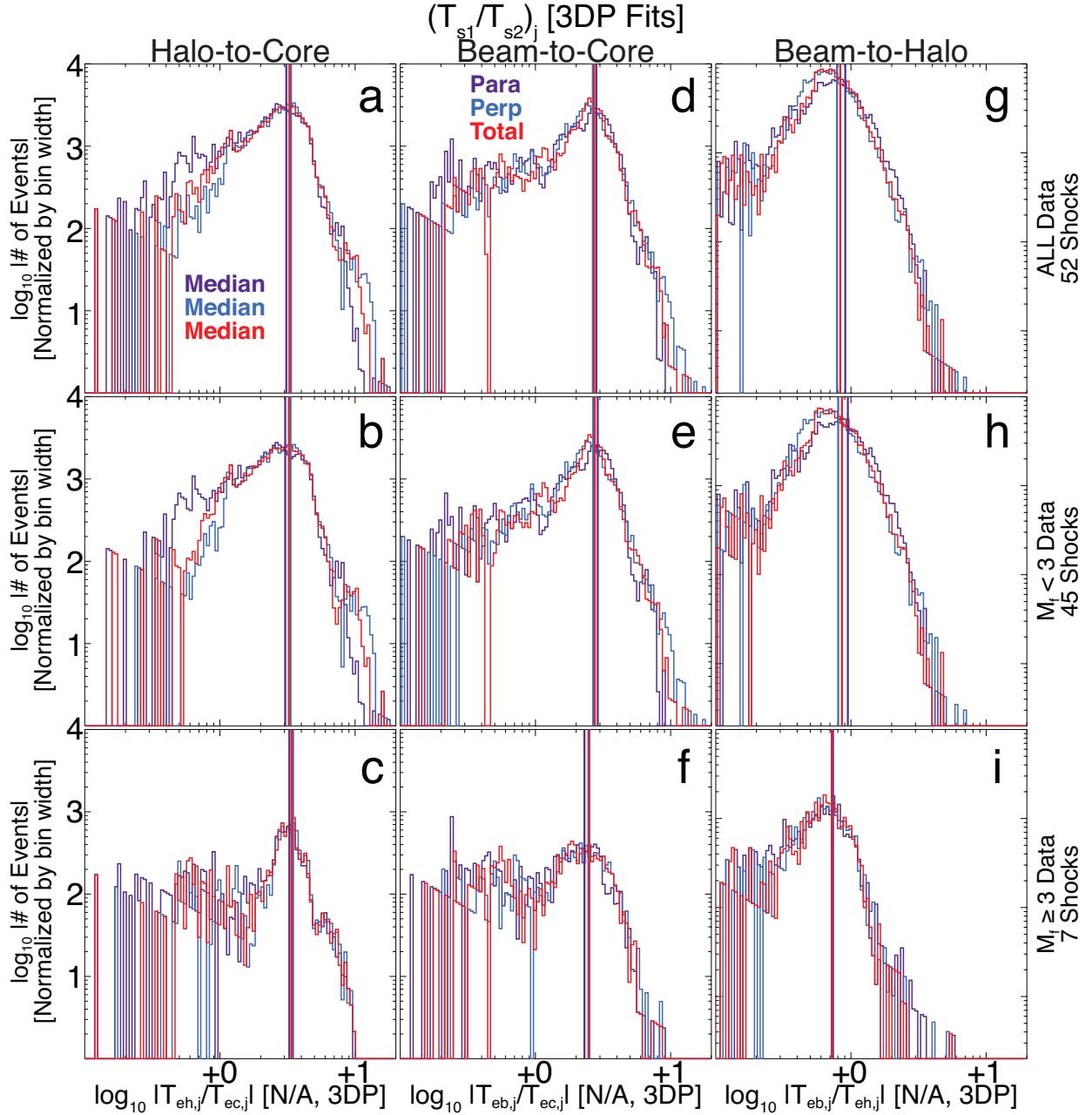


Figure 8. The same format as Figure 2 except for electron temperature ratios [N/A]. Note that all three components have a uniform vertical axis scale.

APPENDIX

A. VELOCITY DISTRIBUTION FUNCTIONS

208 A generalized Gaussian probability density function is defined as:

$$f_s(x) = \frac{A_o}{\sqrt{2\pi\sigma^2}} e^{-\frac{(x-x_o)^2}{2\sigma^2}} \quad (\text{A1})$$

209 where x_o is the displacement of the peak from $x = 0$, A_o is a normalization amplitude, s denotes the specific set (later
210 used for particle species) of data the distribution describes, and σ^2 is the variance. For this distribution, the Full
211 Width at Half Maximum (FWHM) is given by:

$$FWHM = 2\sqrt{2\ln 2} \sigma \quad (\text{A2})$$

212 Introducing the change of variable $x \rightarrow v$, where v is a velocity, then the distribution in Equation A1 becomes a
213 Maxwell-Boltzmann velocity distribution, or Maxwellian, given by:

$$f_s(v) = \frac{n_o}{\sqrt{\pi} V_{Ts}} e^{-\left(\frac{v-v_o}{V_{Ts}}\right)^2} \quad (\text{A3})$$

214 where v_o is the drift speed of the peak relative to zero, n_o is the particle number density, and $2\sigma^2 \rightarrow V_{Ts}^2$, i.e., the
215 thermal speed given by a one-dimensional most probable speed of a Gaussian distribution, which is related to the
216 FWHM by $2\sqrt{\ln 2} V_{Ts}$.

217 The general representation of a two dimensional multivariate distribution is given by the following:

$$f(x, y) = \alpha e^{-\left(\frac{\beta}{\sqrt{2(1-\rho^2)}}\right)^2} \quad (\text{A4a})$$

where α and β are given by

$$\alpha = \frac{A_o}{2\pi\sigma_x\sigma_y\sqrt{1-\rho^2}} \quad (\text{A4b})$$

$$\beta^2 = \left[\left(\frac{x-x_o}{\sigma_x} \right)^2 + \left(\frac{y-y_o}{\sigma_y} \right)^2 - \left(\frac{2\rho(x-x_o)(y-y_o)}{\sigma_x\sigma_y} \right) \right] \quad (\text{A4c})$$

and ρ and σ_j are defined in the following manner:

$$\rho = \frac{cov(x, y)}{\sigma_x\sigma_y} \quad (\text{A4d})$$

$$cov(x, y) = E[(x - \mu_x)(y - \mu_y)] \quad (\text{A4e})$$

218 Here ρ is the correlation between x and y , $\mu_x = E[X]$ is the expected value of the aggregate data set $X = \cup_i x_i$. In
219 the limit $\rho \rightarrow 0$ (i.e., x and y are uncorrelated), Equation A4a reduces to:

$$f(x, y) = \frac{A_x A_y}{2\pi\sigma_x\sigma_y} e^{-\frac{1}{2} \left[\left(\frac{x-\mu_x}{\sigma_x} \right)^2 + \left(\frac{y-\mu_y}{\sigma_y} \right)^2 \right]} \quad (\text{A5})$$

A.1. *Bi-Maxwellian Distributions*

²²¹ In general, for uncorrelated variables, one can write:

$$f(x, y, z) = f(x)f(y)f(z) \quad (\text{A6})$$

²²² and assuming gyrotropy one finds $V_x \rightarrow V_\perp \cos \phi$, $V_y \rightarrow V_\perp \sin \phi$, and $V_z \rightarrow V_{\parallel}$, where ϕ is the phase angle of the
²²³ velocity and $\partial f / \partial \phi = 0$. One can show that such a gyrotropic distribution satisfies $V_{T\perp,x} = V_{T\perp,y} \equiv V_{T\perp}$. Substituting
²²⁴ the following into Equation A5, $x \rightarrow V_{\parallel}$, $y \rightarrow V_\perp$, $\mu_j \rightarrow V_{o,j}$, and $\sigma_j \rightarrow V_{T,j}/\sqrt{2}$, yields a bi-Maxwellian velocity
²²⁵ distribution function (VDF) given by:

$$f(V_{\parallel}, V_\perp) = \frac{n_o}{\pi^{3/2} V_{T\perp}^2 V_{T\parallel}} e^{-\left[\left(\frac{V_{\parallel} - v_{o\parallel}}{V_{T\parallel}}\right)^2 + \left(\frac{V_\perp - v_{o\perp}}{V_{T\perp}}\right)^2\right]} \quad (\text{A7})$$

²²⁶ The bi-Maxwellian is the most commonly used VDF to model both ions and electrons in space plasmas (e.g., [Feldman et al. 1979b,a, 1983a; Kasper et al. 2006](#)).

A.1.1. *Derivatives of Parameters: Bi-Maxwellian Distributions*

²²⁹ In the use of numerical methods like the Levenberg-Marquardt algorithm (e.g., [Markwardt 2009](#)), it is useful to
²³⁰ define the derivatives of a function with respect to the free parameters. In the case of velocity distributions, these
²³¹ are the density, thermal speeds, drift speeds, and exponent (for self-similar and kappa distributions discussed below).
²³² First, some simplifying terms are defined for brevity, given by:

$$u_j = V_j - v_{o,j} \quad (\text{A8a})$$

$$w_j = \frac{u_j}{V_{T,j}} \quad (\text{A8b})$$

$$\psi(z) = \frac{\Gamma'(z)}{\Gamma(z)} \equiv \text{digamma function} \quad (\text{A8c})$$

²³³ where $\Gamma(z)$ is the Riemann gamma function of argument z . After denoting the VDF in Equation A7 as $f^{(m)}$, the
²³⁴ partial derivatives are given by:

$$\frac{\partial f^{(m)}}{\partial n_o} = \frac{f^{(m)}}{n_o} \quad (\text{A9a})$$

$$\frac{\partial f^{(m)}}{\partial V_{T\parallel}} = \left[\frac{2 (w_{\parallel}^2 - 1)}{V_{T\parallel}} \right] f^{(m)} \quad (\text{A9b})$$

$$\frac{\partial f^{(m)}}{\partial V_{T\perp}} = \left[\frac{2 (w_{\perp}^2 - 1)}{V_{T\perp}} \right] f^{(m)} \quad (\text{A9c})$$

$$\frac{\partial f^{(m)}}{\partial v_{o\parallel}} = \left(\frac{2 w_{\parallel}}{V_{T\parallel}} \right) f^{(m)} \quad (\text{A9d})$$

$$\frac{\partial f^{(m)}}{\partial v_{o\perp}} = \left(\frac{2 w_{\perp}}{V_{T\perp}} \right) f^{(m)} \quad (\text{A9e})$$

A.2. *Bi-Kappa Distributions*

²³⁵ A generalized power-law particle distribution is given by a bi-kappa VDF (e.g., [Livadiotis 2015; Mace & Sydora 2010](#)), for electrons here as:

$$f(V_\perp, V_{\parallel}) = A_\kappa \left\{ 1 + \frac{1}{(\kappa - \frac{3}{2})} \left[\left(\frac{V_{\parallel} - v_{o\parallel}}{V_{T\parallel}} \right)^2 + \left(\frac{V_\perp - v_{o\perp}}{V_{T\perp}} \right)^2 \right] \right\}^{-(\kappa+1)} \quad (\text{A10a})$$

where A_κ is given by

$$A_\kappa = \left[\frac{1}{\pi (\kappa - \frac{3}{2})} \right]^{3/2} \frac{n_o \Gamma(\kappa + 1)}{V_{T\perp}^2 V_{T\parallel} \Gamma(\kappa - \frac{1}{2})} \quad (\text{A10b})$$

$$(\text{A10c})$$

where $\Gamma(z)$ is the Riemann gamma function of argument z and V_{Tj} is again the most probable speed of a 1D Gaussian for consistency, i.e., it does not depend upon κ .

The kappa velocity distribution has gained popularity in recent years owing to improvements in particle detectors and the ubiquitous non-Maxwellian tails observed for both ions and electrons (e.g., Lazar et al. 2015b,a, 2016, 2017, 2018; Livadiotis 2015; Livadiotis et al. 2018; Mace & Sydora 2010; Pulupa et al. 2014; Saeed et al. 2017; Shaaban et al. 2018), but references to and use of kappa or kappa-like (e.g., modified Lorentzian) distributions have been around for decades (e.g., Feldman et al. 1983b; Maksimovic et al. 1997; Salem et al. 2003; Vasyliunas 1968). It is beyond the scope of this study to explain the physical interpretation/origin of this function but there are several detailed discussions already published on the topic (e.g., Livadiotis 2015; Livadiotis et al. 2018).

247 A.2.1. Derivatives of Parameters: Bi-Kappa Distributions

Similar to Appendix A.1.1, the analytical derivatives for the bi-kappa VDF are shown below. Again, the following simplifying terms are defined for brevity as:

$$u_j = V_j - v_{oj} \quad (\text{A11a})$$

$$w_j = \frac{u_j}{V_{Tj}} \quad (\text{A11b})$$

$$\psi(z) = \frac{\Gamma'(z)}{\Gamma(z)} \equiv \text{digamma function} \quad (\text{A11c})$$

$$D(w_\parallel, w_\perp, \kappa) = w_\parallel^2 + w_\perp^2 + (\kappa - \frac{3}{2}) \quad (\text{A11d})$$

where $\Gamma(z)$ is the Riemann gamma function of argument z . After denoting the VDF in Equation A10a as $f^{(\kappa)}$, the partial derivatives are given by:

$$\frac{\partial f^{(\kappa)}}{\partial n_o} = \frac{f^{(\kappa)}}{n_o} \quad (\text{A12a})$$

$$\frac{\partial f^{(\kappa)}}{\partial V_{T\parallel}} = \left[\frac{2 w_\parallel^2 (\kappa + \frac{1}{2}) - w_\perp^2 - (\kappa - \frac{3}{2})}{V_{T\parallel} D(w_\parallel, w_\perp, \kappa)} \right] f^{(\kappa)} \quad (\text{A12b})$$

$$\frac{\partial f^{(\kappa)}}{\partial V_{T\perp}} = \left\{ \frac{2 [\kappa w_\perp^2 - w_\parallel^2 - (\kappa - \frac{3}{2})]}{V_{T\perp} D(w_\parallel, w_\perp, \kappa)} \right\} f^{(\kappa)} \quad (\text{A12c})$$

$$\frac{\partial f^{(\kappa)}}{\partial V_{o\parallel}} = \left[\frac{2 w_\parallel (\kappa + 1)}{V_{T\parallel} D(w_\parallel, w_\perp, \kappa)} \right] f^{(\kappa)} \quad (\text{A12d})$$

$$\frac{\partial f^{(\kappa)}}{\partial V_{o\perp}} = \left[\frac{2 w_\perp (\kappa + 1)}{V_{T\perp} D(w_\parallel, w_\perp, \kappa)} \right] f^{(\kappa)} \quad (\text{A12e})$$

$$\frac{\partial f^{(\kappa)}}{\partial \kappa} = \left\{ \frac{(w_\parallel^2 + w_\perp^2) (\kappa - \frac{1}{2}) - \frac{3}{2} (\kappa - \frac{3}{2})}{(\kappa - \frac{3}{2}) D(w_\parallel, w_\perp, \kappa)} - \ln |1 + \frac{w_\parallel^2 + w_\perp^2}{(\kappa - \frac{3}{2})}| + \psi(\kappa + 1) - \psi(\kappa - \frac{1}{2}) \right\} f^{(\kappa)} \quad (\text{A12f})$$

252

A.3. Self-Similar Distributions

253 When a VDF evolves under the action of inelastic scattering (e.g., Dum et al. 1974; Dum 1975; Goldman 1984;
 254 Horton et al. 1976; Horton & Choi 1979; Jain & Sharma 1979) or flows through disordered porous media (e.g., Matyka
 255 et al. 2016), the result is called a *self-similar distribution*, which in one dimension is given by:

$$f_s(x, t) = C_o e^{-\left(\frac{x}{x_o}\right)^s} \quad (\text{A13})$$

256 The constant C_o is determined by defining:

$$n_o = \int_{-\infty}^{\infty} dv f_s(v, t) \quad (\text{A14a})$$

$$= 2 \int_0^{\infty} dv f_s(v, t) \quad (\text{if symmetric}) \quad (\text{A14b})$$

257 The general solution to Equation A14b is given by:

$$\int_0^{\infty} dx x^n e^{-\alpha x^s} = \frac{\Gamma(k)}{s \alpha^k} \quad (\text{A15})$$

258 for $n > -1$, $s > 0$, $\alpha > 0$, and $k = (n+1)/s$. For $n = 0$, the constant C_o reduces to:

$$C_o = \frac{n_o s \alpha^{1/s}}{2 \Gamma(1/s)} \quad (\text{A16})$$

259 Physically one can see that $\alpha \rightarrow V_{T_s}^{-s}$, which leads to the one dimensional form of the self-similar VDF can be given
 260 by:

$$f_s(v, t) = \frac{n_o s}{2 V_{T_s} \Gamma(1/s)} e^{-\left(\frac{v}{V_{T_s}}\right)^s} \quad (\text{A17})$$

261 Note that in the limit as $s \rightarrow 2$, Equation A17 reduces to a one-dimensional Maxwellian given by Equation A3. For
 262 the 3D case, the self-similar VDF, for even integer s , reduces to:

$$f(V_x, V_y, V_z) = \left[\frac{s}{2\Gamma\left(\frac{n+1}{s}\right)} \right]^3 \frac{n_o}{(V_{T_x} V_{T_y} V_{T_z})^{n+1}} e^{-\left[\left(\frac{V_x}{V_{T_x}}\right)^s + \left(\frac{V_y}{V_{T_y}}\right)^s + \left(\frac{V_z}{V_{T_z}}\right)^s\right]} \quad (\text{A18})$$

263 Following the same procedure that led to Equation A7, one finds (for $n \rightarrow 0$, i.e., the zeroth moment):

$$f(V_{\parallel}, V_{\perp}) = \left[\frac{s}{2\Gamma\left(\frac{1}{s}\right)} \right]^3 \frac{n_o}{V_{T_{\perp}}^2 V_{T_{\parallel}}} e^{-\left[\left(\frac{V_{\parallel}}{V_{T_{\parallel}}}\right)^s + \left(\frac{V_{\perp}}{V_{T_{\perp}}}\right)^s\right]} \quad (\text{A19})$$

264 After recalling that $\Gamma(1/s)/s = \Gamma(1+1/s)$ and letting $V_j \rightarrow V_j - v_{oj}$, Equation A19 reduces to:

$$f(V_{\parallel}, V_{\perp}) = \left[2\Gamma\left(\frac{1+s}{s}\right) \right]^{-3} \frac{n_o}{V_{T_{\perp}}^2 V_{T_{\parallel}}} e^{-\left[\left(\frac{V_{\parallel} - v_{o\parallel}}{V_{T_{\parallel}}}\right)^s + \left(\frac{V_{\perp} - v_{o\perp}}{V_{T_{\perp}}}\right)^s\right]} \quad (\text{A20})$$

²⁶⁵ Note that V_{Tj} is again the most probable speed of a 1D Gaussian for consistency, i.e., it does not depend upon s .
²⁶⁶ Further, one can see that Equation A20 reduces to Equation A7 in the limit where $s \rightarrow 2$. A slightly more general
²⁶⁷ approach can be taken where the exponents are not uniform, e.g., one assumes:

$$f(V_x, V_y, V_z) = C_o e^{-\left[\left(\frac{V_x}{V_{Tx}}\right)^p + \left(\frac{V_y}{V_{Ty}}\right)^q + \left(\frac{V_z}{V_{Tz}}\right)^r\right]} \quad (\text{A21})$$

²⁶⁸ The triple integral of Equation A21, still assuming we set the result equal to n_o and assuming the integrals are
²⁶⁹ symmetric about zero, results in the following:

$$n_o = 2^3 C_o V_{Tx} V_{Ty} V_{Tz} \Gamma(1+p^{-1}) \Gamma(1+q^{-1}) \Gamma(1+r^{-1}) \quad (\text{A22})$$

²⁷⁰ Equation A22 can be further reduced by assuming gyrotropy about the mean magnetic field direction such that $r \rightarrow q$,
²⁷¹ $V_{Tz} \rightarrow V_{Ty}$, $V_z \rightarrow V_y$, and $x \rightarrow \parallel$ and $y \rightarrow \perp$, then the expression for the normalization constant is given by:

$$C_o = \frac{p q^2 n_o}{2^3 V_{T\parallel} V_{T\perp}^2 \Gamma(p^{-1}) \Gamma^2(q^{-1})} \quad (\text{A23})$$

²⁷² Thus, the full bi-self-similar VDF for non-homogenous exponents is given by:

$$f(V_{\parallel}, V_{\perp}) = \frac{p q^2 n_o}{2^3 V_{T\parallel} V_{T\perp}^2 \Gamma(p^{-1}) \Gamma^2(q^{-1})} e^{-\left[\left(\frac{V_{\parallel} - v_{o\parallel}}{V_{T\parallel}}\right)^p + \left(\frac{V_{\perp} - v_{o\perp}}{V_{T\perp}}\right)^q\right]} \quad (\text{A24a})$$

or in another form as:

$$f(V_{\parallel}, V_{\perp}) = \frac{n_o \Gamma^{-1}\left(\frac{1+p}{p}\right) \Gamma^{-2}\left(\frac{1+q}{q}\right)}{2^3 V_{T\parallel} V_{T\perp}^2} e^{-\left[\left(\frac{V_{\parallel} - v_{o\parallel}}{V_{T\parallel}}\right)^p + \left(\frac{V_{\perp} - v_{o\perp}}{V_{T\perp}}\right)^q\right]} \quad (\text{A24b})$$

²⁷³ A.3.1. Derivatives of Parameters: Self-Similar Distributions

²⁷⁴ Similar to Appendix A.1.1, the analytical derivatives for the bi-self-similar VDF are shown below. Again, the
²⁷⁵ following simplifying terms are defined for brevity as:

$$u_j = V_j - v_{oj} \quad (\text{A25a})$$

$$w_j = \frac{u_j}{V_{Tj}} \quad (\text{A25b})$$

$$\psi(z) = \frac{\Gamma'(z)}{\Gamma(z)} \equiv \text{digamma function} \quad (\text{A25c})$$

²⁷⁶ where $\Gamma(z)$ is the Riemann gamma function of argument z . After denoting the VDF in Equation A20 as $f^{(ss)}$, the
²⁷⁷ partial derivatives are given by:

$$\frac{\partial f^{(ss)}}{\partial n_o} = \frac{f^{(ss)}}{n_o} \quad (\text{A26a})$$

$$\frac{\partial f^{(ss)}}{\partial V_{T\parallel}} = \left(\frac{s w_{\parallel}^s - 1}{V_{T\parallel}} \right) f^{(ss)} \quad (\text{A26b})$$

$$\frac{\partial f^{(ss)}}{\partial V_{T\perp}} = \left(\frac{s w_{\perp}^s - 2}{V_{T\perp}} \right) f^{(ss)} \quad (\text{A26c})$$

$$\frac{\partial f^{(ss)}}{\partial v_{o\parallel}} = \left(\frac{s w_{\parallel}^{s-1}}{V_{T\parallel}} \right) f^{(ss)} \quad (\text{A26d})$$

$$\frac{\partial f^{(ss)}}{\partial v_{o\perp}} = \left(\frac{s w_{\perp}^{s-1}}{V_{T\perp}} \right) f^{(ss)} \quad (\text{A26e})$$

$$\frac{\partial f^{(ss)}}{\partial s} = \left[\frac{3 \psi(\frac{1+s}{s})}{s^2} - w_{\parallel}^s \ln w_{\parallel} - w_{\perp}^s \ln w_{\perp} \right] f^{(ss)} \quad (\text{A26f})$$

²⁷⁸ After denoting the VDF in Equation A24b as $f^{(as)}$, the partial derivatives are given by:

$$\frac{1}{f^{(as)}} \frac{\partial f^{(as)}}{\partial n_o} = \frac{1}{n_o} \quad (\text{A27a})$$

$$\frac{1}{f^{(as)}} \frac{\partial f^{(as)}}{\partial V_{T\parallel}} = \left(\frac{p w_{\parallel}^p - 1}{V_{T\parallel}} \right) \quad (\text{A27b})$$

$$\frac{1}{f^{(as)}} \frac{\partial f^{(as)}}{\partial V_{T\perp}} = \left(\frac{q w_{\perp}^q - 2}{V_{T\perp}} \right) \quad (\text{A27c})$$

$$\frac{1}{f^{(as)}} \frac{\partial f^{(as)}}{\partial v_{o\parallel}} = \left(\frac{p w_{\parallel}^{p-1}}{V_{T\parallel}} \right) \quad (\text{A27d})$$

$$\frac{1}{f^{(as)}} \frac{\partial f^{(as)}}{\partial v_{o\perp}} = \left(\frac{q w_{\perp}^{q-1}}{V_{T\perp}} \right) \quad (\text{A27e})$$

$$\frac{1}{f^{(as)}} \frac{\partial f^{(as)}}{\partial p} = \frac{\psi(\frac{1+p}{p})}{p^2} - w_{\parallel}^p \ln w_{\parallel} \quad (\text{A27f})$$

$$\frac{1}{f^{(as)}} \frac{\partial f^{(as)}}{\partial q} = \frac{2 \psi(\frac{1+q}{q})}{q^2} - w_{\perp}^q \ln w_{\perp} \quad (\text{A27g})$$

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