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1	A dual birdcage coil for proton and fluorine 7 Tesla MRI
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29 Abstract

30 **Object:** Given the growing interest in fluorine, it is necessary to develop new multi-tuned RF 31 coils. Therefore, our objective is to design a simple and versatile double-tuned RF coil that can 32 be used as a transmitter and receiver double-tuned coil (¹H and ¹⁹F) or as transmitter-only double-33 tuned coil.

Materials and Methods: A high-pass eight-element birdcage coil was built for ¹H and ¹⁹F for a 34 35 7T scanner. PIN diodes and cable traps to block unwanted common mode currents in cables were introduced to confer more flexibility to the coil. S-parameters and quality factor were measured 36 37 in workbench and signal to noise ratio as well as signal intensity profiles in imaging experiments. 38 Results: Bench measurements show S11 values less than -33 dB, S21 lower than -13 dB and 39 quality factors ratio of the order of 1.8 that are in agreement with good performances of a RF coil, as well as values of -39 dB for ¹⁹F and -30 dB for ¹H as good detuning values. Signal intensity 40 profiles prove excellent homogeneity at ¹H and ¹⁹F. 41 42 Discussion: We present a simple structure of a double tuned high-pass birdcage coil tuned to ¹H and ¹⁹F that shows a great uniformity and sensitivity for ¹⁹F. 43

44

45 Keywords: High-pass birdcage; Double-tuned; Fluorine; PIN diode

46

48 Introduction

49 Magnetic Resonance Imaging (MRI) is a widely used clinical diagnostic tool because it is non-50 invasive, has no tissue depth penetration limitations, no ionizing radiation issues, and provides 51 the combination of structural and functional imaging in the same study at reasonably high spatial 52 resolution. Most MRI studies use ¹H as the nucleus of choice for imaging, but other nuclei, such 53 as sodium (^{23}Na) or fluorine (^{19}F) can be imaged even using simultaneous multinuclear acquisition 54 methods. Imaging with these nuclei introduces the possibility of using MRI for molecular imaging with higher specificity than conventional proton MRI. ¹⁹F MRI imaging allows direct 55 56 visualization of molecules of interest containing ¹⁹F nuclei. Since MRI signal from endogenous 57 ¹⁹F in tissues is negligible, and ¹⁹F is a nucleus with similar sensitivity to proton, molecules 58 containing ¹⁹F with the concentration limits of milli- to micromolar typical for NMR, results in a 59 hot-spot, with very high contrast and specificity characteristics.

60 Important applications of ¹⁹F MRI are lung imaging using perfluorinated gases [1], cell tracking using perfluorocarbons [2, 3], inflammatory processes (such as atherosclerosis) [4]. Lung imaging 61 using ¹⁹F MRI, together with hyperpolarized gas MRI, has provided insights in lung structure and 62 63 function.¹⁹F gas MRI offers very low signal compared to hyperpolarized gas MRI, due to the lack 64 of hyperpolarization. However, imaging with fluorinated gases is much easier and cheaper, they can be mixed with oxygen and do not need hyperpolarization. ¹⁹F gas imaging has used SF₆ [5, 65 66 6], C_2F_6 [7] and C_3F_8 [8] to measure diffusion, which is a proxy for airspace size [6, 7], ventilation/perfusion ratios [9] and 3D gas density maps [8]. 67

Another important ¹⁹F MRI application is imaging of liquid perfluorocarbons [10]. These have been used for cell tracking [2, 3, 11–16], visualization of pulmonary inflammation [4, 17], evaluation of response to antibiotic therapy [18], to assess the relationship between folate receptor expression and tumor proliferation [19] and to assess tumor oxygenation [20].

72

This renewed interest in non-proton MRI has brought the need to develop new designs of multituned radiofrequency (RF) coil configurations. Multinuclear studies typically require more than one RF coil to acquire all required information. In the case of fluorine, whose resonance frequency ⁷⁶ is close to the proton one, a double-tuned RF coil allows co-registration of both information, i.e.
¹H MRI is used to localize anatomical structures and ¹⁹F, depending on the application, for
⁷⁸ functional or molecular imaging. This double configuration is mandatory to reduce unpleasant
⁷⁹ situations to the subject of study, such as replacing or retuning RF coils, and to prevent subsequent
⁸⁰ co-registration issues with proton-based anatomical imaging.

81

82 Several designs for double-tuned RF coils have been reported. Each of these solutions present 83 advantages and disadvantages mainly related to the compromise to minimize the effect of 84 complicated manufacturing and annoying tuning processes. One of the first double-tuned 85 configuration used variable length transmission line [21], but this solution is not optimal due to 86 size constraints. The replacement of the transmission line with discrete elements, inductors and 87 capacitors, results in the well-known RF coil with trap circuits (LC circuit) [22-26], although this 88 solution requires a large frequency separation and is not suitable for dual proton and fluorine MRI 89 applications. LC circuit has a high impedance at lower resonance frequencies, which is equivalent 90 to an inductor, whereas at higher frequencies presents a low impedance and is then equivalent to 91 a capacitor, i.e. allowing a double-tuned RF coil. This trap circuit has been widely used in 92 combination with birdcage coils [27–29]. Different shield radius is another method to achieve a 93 double-tuned RF coil [30] when frequencies are close, as in this case, or to tune RF coil moving 94 RF shield along the coil [31]. The need to reassemble the coil with each frequency limits its use. 95 Another approach to manufacture a double-tuned coil is through two coaxial structures [32–35]; 96 however, signal to noise ratio (SNR) can decrease significantly due to the coupling effect. The 97 use of varicaps is an alternative to switch both frequencies [36, 37] but due to its low quality 98 factor it reduces the performances of the RF coil. Nowadays, active components (PIN diodes) 99 have been used in many RF coil designs to reduce coupling or switching between RF coils[38]. 100 PIN diodes are an alternative to replace trap circuits [39]. This solution plays an important role 101 for active detuning and switching between transmit and receive coils [40, 41]. However, SNR 102 could be decreased due to the resistance of the PIN diodes, especially when they are placed in 103 series with the coil and they are forward-biased. Finally, recent research in microelectromechanical systems (MEMS) open new developments in double-tuned RF coils [42] but it
is still in development. The switch technology in MEMS allows increased switching speed and
reduced insertion loss. This solution is not only valid for double-tuned RF coils but in array coils
to switch conductive elements and reconfigure coil field of view [43].

108

109 It is well known that the birdcage coil is one of the most versatile RF coils. It can perform double 110 resonant or quadrature excitations, as well as generate highly homogenous radiofrequency 111 magnetic fields [44–46]. Birdcage coils have the wires uniformly spaced in azimuthal angle. In 112 transmission mode, a current is passed through providing an ideal cosine current distribution 113 along the coil surface, which generates a homogeneous magnetic field. A birdcage coil has two orthogonal resonant modes [47]. Since ¹H and ¹⁹F nuclei have close resonant frequencies (300 114 115 MHz and 282 MHz, respectively at 7T) one can take advantage of these two channels and tune 116 each of them to a different frequency [48, 49]. Therefore, the coil assures almost identical B_1 117 profiles for the two nuclei.

118

119 In this work, we have designed and constructed a versatile design of a dedicated RF volume coil 120 that can be used in many configurations, for instance, as a transmitter and receiver (TX/RX) double-tuned coil (¹H and ¹⁹F) or as transmitter-only (TX) double-tuned coil to operate together 121 122 with an array coil tuned in proton or fluorine. The configuration of our double-tuned volume RF 123 coil is based on the advantage of the quadrature mode of the birdcage coil into two separate linear 124 modes and tune it into each frequency to achieve double resonance. The configuration as 125 transmitter coil uses active components, PIN diodes, to switch between the transmission and 126 reception coils. The PIN diodes are located in parallel to each capacitor placed in the end-ring of 127 the high-pass birdcage coil to reduce additional resistance when they are forward-biased and 128 therefore do not degrade its performance. This versatile home-made RF coil is optimized for 129 fluorine and can still acquire good quality proton MR images for anatomical information. Due to 130 this versatility, the proposed design is suitable for use either as a double-tuned RF coil or in 131 combination with an array coil for both the proton or fluorine frequencies.

133 Materials and Methods

134 A versatile home-made RF coil was built and optimized for rat imaging. A double resonant high-135 pass birdcage coil for ¹H and ¹⁹F was designed for imaging at 7T, resonant frequency of 300 MHz 136 and 282 MHz respectively. The length of the coil was 11.4 cm, the radius 3.6 cm and the RF 137 shield radius was 5.6 cm. The coil dimensions were adjusted to fit the samples and enhance a 138 good filling factor. Adhesive copper tape (3M Corporation, St Paul, MN, USA) of 5 mm width 139 was used to construct a high-pass eight-element birdcage coil. An eight-element high-pass 140 birdcage coil was chosen to achieve enough homogenous radiofrequency magnetic field without 141 compromising its facile adjustment. This seems an optimal balance between adding more 142 elements to yield a better B_1 homogeneity and the complexity of construction. Non-magnetic 143 fixed capacitors (Series 100B, American Technical Ceramics, USA) were used in the eight 144 elements and placed at each end-rings. High voltage variable (1-25 pF) capacitors (Voltronics, 145 USA) were used to perform fine tuning and matching adjustment when high-pass birdcage coil is 146 loaded by the samples for both ¹H and ¹⁹F nuclei. The high-pass birdcage coil was optimized for 147 fluorine experiments with the capacitor distribution shown in Figure 1. To achieve double (¹H, 148 ¹⁹F) resonance, as birdcage coils have a cosine current distribution, C_0 and C_4 capacitors, which 149 correspond to the minimum current distributions, can be modified without changing B_1 profiles. 150 Balanced capacitive matching circuits were used to match the coil's impedances to the real values 151 of 50 Ω in each channel (¹H and ¹⁹F).

152

Active decoupling was performed by using a MA4P7006F-1072T PIN diode (MACOM, Lowell, MA, USA) in series with an inductor L (~ 64 nH or 44 nH) that is introduced in parallel to the capacitor (4.7 pF or 6.8 pF, respectively) of each element of the high-pass birdcage resonator. Thus, it can be used together with an array coil tuned either in ¹H or ¹⁹F. Each PIN diode was powered by a voltage source via 1.2 μ H RF chokes (Coilcraft. IL, USA). During the operation of the high-pass birdcage coil, in transmission mode, all PIN diodes were reverse-biased by -36 V 159 (PIN diode OFF), forming an open circuit and the inductor L is disconnected, so it works as a 160 conventional double-tuned high-pass birdcage coil (Figure 1B). In receive mode, the PIN diodes 161 are forward-biased by 5 V (PIN diode ON), inductor L is connected to the capacitor and the 162 parallel LC circuit is on resonance, forming a high impedance circuit that blocked current flowing 163 in the coil and detuned the high-pass birdcage coil (Figure 1C). As the PIN diode are in parallel 164 to the high-pass birdcage coil, no additional resistance is introduced and therefore SNR does not 165 decrease. This LC circuit (PIN diode ON) is tuned to a middle frequency between proton and 166 fluorine to be able to detune the high-pass birdcage coil at both frequencies. A series-parallel 167 combination of the PIN diode is chosen to achieve better detuning of our high-pass birdcage coil. 168 A total of 5 V and a required current of 400 mA is applied to switch on all PIN diodes.

169

A cable trap was placed in each of the two channels to minimize the coupling between cables by
blocking unwanted common mode currents [50, 51]. It consists in a parallel resonant circuit and
it was built with a capacitor and an inductor formed by a semi-rigid cable UT47C-TP-LL (MicroCoax, PA, USA). The cable traps were tuned to ¹H and ¹⁹F frequency.

174

175 Bench measurements were performed in an 8712ET Network Analyzer (Agilent Technologies, 176 Palo Alto, USA). The reflection (S11) and transmission (S21) coefficient were measured for both 177 nuclei. Quality factor (Q) measurements were used to characterize the performance of the coil. Q 178 factors were measured without (Q_u) and with (Q_i) sample load (a home-made phantom, described 179 below) at both frequencies.

180

A proton-¹⁹F phantom was manufactured in house consisting of 5 lab tubes of 15 mm diameter filled with different solutions of 2,2,2-trifluorethanol (3 equivalent ¹⁹F nuclei per molecule) dissolved in water: 79.5, 53, 26, 13 mM and 5 mM. All MRI experiments were performed on a 7 T MR scanner, Bruker Biospec 70/30 USR (Bruker BioSpin, Rheinstetten, Germany) for small animals located at CIC BiomaGUNE (San Sebastian, Spain). Axial images were acquired using a Multi Slice Multi Echo (MSME) sequence. Acquisition parameters for ¹H imaging were: repetition time (TR) = 1151 ms, echo time (TE) = 11.77 ms, 1 average, field of view of 6 x 6 cm², and acquisition matrix of 256 x 256. Parameters for ¹⁹F images were: repetition time (TR) = 1151 ms, echo time (TE) = 8.65 ms, 1 average, field of view of 6 x 6 cm², and acquisition matrix of 64 x 64 for a total acquisition time of 3 minutes and 12 seconds. Shimming and pulse calibration were performed using the standard adjustment tools of the scanner. Paravision PV 6.0.1 (Bruker BioSpin, Rheinstetten, Germany) and ImageJ 1.52 (National Institutes of Health, Bethesda, Maryland, United States) software were used to show the profiles and to calculate SNR.

194

For SNR calculation, five regions of interest (ROIs) were drawn inside the tubes and one ROI in the background (Figure 2). In the tube's regions (SNR>0), pixel intensity follows a Rice distribution with two parameters, the noise σ and the SNR [52]. For this case, the first moment of the distribution is [53]:

199

$$\overline{M} = \sigma \cdot \sqrt{\pi/2} \cdot L_{1/2} \left(-SNR^2/2\right) \tag{1.1}$$

In the background, SNR = 0 and the pixel intensity follows a Rayleigh distribution with mean and
 standard deviation

202

$$\overline{M} = \sigma \cdot \sqrt{\pi/2} \qquad \sigma_M = \sigma \cdot \sqrt{(4-\pi)/2}$$
 (1.2)

Here, \overline{M} is the average of the magnitude signal, σ_M is the standard deviation of the magnitude signal and $L_{1/2}(x)$ is a Laguerre L polynomial.

The SNR calculation proceeds as follows. First, a quantile plot of pixel intensity in the background ROI using R (https://www.r-project.org) confirms that the background ROI is Rayleigh distributed. If this is not the case, another background ROI is drawn. Then, Equation 1.2 gives two different estimations of the noise σ , which are averaged. Then, a numerical solution of equation 1.1 using Mathematica (Wolfram Research, Champaign, Illinois, United States) provides the SNR in a straightforward way.

211

212 **Results**

- A range of tests were performed on the RF coil both on the bench and imaging experiments to
 ensure good performances. These tests included quality factor measurements, checking B₁
 homogeneity and active decoupling. We present here both measurements.
- 216

217 Bench measurements:

218 S-parameters were measured on the bench using a network analyser and confirmed that tuning

220 both nuclei, ¹H and ¹⁹F, was less than -33 dB, indicating a good impedance matching.

and matching to 50 Ω was done at both frequencies considering the home-made phantom. S11 for

221 Transmission coefficients S21 were lower than -13 dB for each channel.

222

For optimal RF coil operation at high frequencies, the resistive losses of the coil must be smaller than the sample losses. Table 1 shows quality factor measurements of the double-tuned high-pass birdcage coil with and without sample load. High ratio values of Q_u / Q_l imply high coil sensitivity and low coil losses, which result in higher SNR. As we can see in this table, Q values are slightly higher at ¹⁹F since the high-pass birdcage coil has been optimized for fluorine.

228

229 When the PIN diode is forward-biased, the LC circuit is on resonance. The PIN diode and the 230 series inductor L are in parallel to each capacitor located in the end-ring of the high-pass birdcage. 231 No intrinsic resistance is added and thus Q values are not reduced. This parallel LC circuit was 232 tuned to a frequency between proton and fluorine, around 290 MHz. A value of -24 dB was measured for the transmission coefficient S21 in both frequencies (¹H and ¹⁹F), appropriate value 233 234 for a good detuning in the receive mode. Once all LC circuits were adjusted, a series-parallel 235 combination was implemented. A current intensity of 400 mA is applied to achieve the active 236 decoupling of the double-tuned high-pass birdcage coil. S21 values were calculated as the 237 difference between on-resonance and off-resonance states of the double-tuned high-pass birdcage. 238 In this case, values of -39 dB for fluorine and -30 dB for proton were achieved. These values 239 clearly display that the high-pass birdcage coil was sufficiently detuned with the PIN diodes 240 during acquisition to avoid interference.

242 Imaging Experiments

Figure 2 shows axial images for both nuclei, ¹H and ¹⁹F, obtained from the phantom using the 243 244 double-tuned high-pass birdcage coil and its corresponding profiles. In these images, we can see 245 the high homogeneity of B₁. Signal intensity profiles of this phantom are shown in Figure 2b for 246 ¹H image and Figure 2d for ¹⁹F image. Homogeneity within each tube, expressed using the Coefficient of Variation, are around 1.5% and 4.6% for ¹H and ¹⁹F respectively. The selected 247 248 configuration to tune each of the two orthogonal channels to proton and to fluorine in coexistence 249 with the introduction of the PIN diodes to detune the coil when operated together with a receiver-250 only array coil yielded good results. B₁ homogeneity profiles are preserved in both nuclei. This 251 design ensures high B₁ homogeneity within the RF coil.

252

In order to characterize the efficiency of the proposed coil, power consumption for a 90 degree pulse was measured for both nuclei and compared to a commercial coil. 3.8 W for ¹H and 3.6 W for ¹⁹F were measured for our coil, whereas 3.1 W was obtained for ¹H in a linear commercial one (single tuned birdcage coil of similar dimensions).

257

Since the phantom has five different concentrations, the SNR of the five tubes was calculated to find out how sensitive our RF coil is. The calculated SNR values of the phantom are given in table 2. We point out that a concentration as small as tube 3 (26 mM) or even tube 4 (13 mM) results in a Contrast-to-noise ratio (CNR) superior to 4. Tube 5 (5 mM) is discernible even if SNR is low, CNR close to 2. Since our voxel size is 4.4 mm³, a concentration of 22 nmol per voxel can be easily imaged in a short time (less than 4 minutes).

264

265 Discussion

In this study, we present an approach to a RF coil to be used in different configurations. We chose one of the most homogenous RF coils, a birdcage, and we took advantage of its performance in a 268 quadrature configuration. Each of the two linear modes was tuned to ¹H and ¹⁹F. PIN diodes were

added to be able to use it as a transmitter-only RF coil together with an array coil.

270

271 Due to the high B_1 homogeneity of birdcage coils, it is one of the most suitable for transmission 272 mode. Our results demonstrate that the double-tuned high-pass birdcage coil offers similar 273 homogeneity at both nuclei.

274

This simple and versatile design shows a great sensitivity even to detect a ¹⁹F concentration as 275 276 low as 5 mM in a few minutes averaging time, which is comparable to a typical in-vivo 277 concentration. Since our voxel size is 4.4 mm³, this is equivalent to a concentration of 22 nmol 278 per voxel. We decided to use this concentration to see the sensitivity of our measurements. Our 279 results can be compared to those from van Heeswijk et al. [54], who used a gradient echo pulse 280 sequence within a 10-minute measurement time limit for possible human applications. The final 281 concentration of the perfluoro-15-crown-5 ether emulsion in their work ranged from 10 to 0.4 282 mM. Considering that this molecule has 20 chemically equivalent fluorine atoms whilst 2,2,2-283 trifluoroethanol has only three, the minimum concentration described as detection limit of this 284 molecule for a typical gradient echo acquisition is about 0.4 mM, which is equivalent to 2.7 mM 285 in our case. In our case, we only accumulated half the time as these authors did, TR was different 286 in both cases and we did not use a quadrature coil.

287

Our design avoids the use of degrading trap circuits in series to the RF coil and therefore resulting in an improvement at both frequencies. The idea of tuning a trap circuit to a middle frequency provides good detuning values overall in ¹⁹F as the high-pass birdcage coil is optimized for ¹⁹F. The proposed design provides a simple and robust approach to a double-tuned RF coil design. Next studies will include the benefit of the TX mode with an array coil of four elements tuned to both frequencies.

294

295 Conclusion

296	For MRI with non-proton nuclei, it is necessary to develop some appropriate hardware such as
297	multi-tuned RF coils. In this paper, we suggest the idea of building a multi-tuned RF coil based
298	on one of the most homogenous RF coil design, the birdcage configuration, and take advantage
299	of its performance. We present here a versatile and simple structure of a double-tuned high-pass
300	birdcage coil tuned to ¹ H and ¹⁹ F to be used in transmission and reception mode or as a transmitter-
301	only RF coil with active component inside. High quality images for ¹ H and ¹⁹ F nuclei were
302	obtained using this RF coil.
303	

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310

311 Author contributions

- 312 Villa-Valverde: project development, analysis and interpretation of data, drafting of manuscript.
- 313 Rodriguez: analysis and interpretation of data, drafting of manuscript. Padró: acquisition of data.
- 314 Benito: acquisition of data. Garrido-Salmon: critical revision. Ruiz-Cabello: acquisition of data,
- 315 critical revision.
- 316

317 **Compliance with ethical standards**

- 318 **Conflict of interest:** The authors declare that they have no conflict of interest
- 319 Ethical approval: This article does not contain any studies with human participants or animals
- 320 performed by any of the authors.
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- 322
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470	Fig 1. A) Schematic of double-tuned eight-element high-pass birdcage coil. B) Schematic in the
471	transmitter and receiver mode. C) Schematic in the receiver mode, when the PIN diodes
472	are switched on. CM is a variable capacitor for matching and CT is a variable capacitor
473	for tuning.
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478	Fig 2. MSME images of the five tubes containing different concentrations of 2,2,2-
479	Trifluorethanol: a) ¹ H image and c) ¹⁹ F image; b) and d) Profiles of ¹ H and ¹⁹ F,
480	respectively.
481	
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483	

	¹ H	¹⁹ F
Qunloaded	166	192
Qloaded	97	104
Qratio	1.71	1.84

486	Table 1. Quality	factors of the d	louble-tuned high-	pass birdcage coil	for both nuclei.
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Nucleus	ROI 1	ROI 2	ROI 3	ROI 4	ROI 5
¹ H	180.45	181.22	173.70	172.94	166.85
¹⁹ F	29.26	19.68	10.23	4.82	1.41

491 Table 2. Calculated signal to noise ratio for both nuclei, ¹H and ¹⁹F. SNR is calculated from each

492 of the five tubes.