

Effect of retarders on the early hydration mechanisms of calcium-sulpho-aluminate (CSA) type cements

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Abstract

The retardation of calcium-sulpho-aluminate (CSA) type cements by three common retarders – sodium gluconate, sodium-potassium tartrate and borax is investigated. The results show that each of the retarder has a different effect on the early-age hydrates assemblage as shown by quantitative X-ray diffraction, thermogravimetric analysis, scanning electron microscopy and pore solution analysis. Regardless the retarder used, the hydration starts with the formation of ettringite and of some X-ray amorphous hydrates. The ettringite-forming reaction is delayed specifically, depending on the retarder used. The results showed that the retardation is caused either by calcium complexation preventing hydrates formation or surface adsorption of inhibitors or by the formation of a semipermeable layer on the cement grains in the case of tartrate and gluconate. Borax retards the hydration by lowering the initial pH that destabilizes ettringite. Furthermore, the morphology of ettringite is altered depending on the type of the retarder used.

Keywords: Sulfoaluminate (D), Pore solution (B), Retardation (A), SEM (B), X-ray Diffraction (B)

23 1. Introduction

24 In recent years, calcium-sulpho-aluminate cements (CSA) [1], [2] have attracted the attention of
25 scientists [3] [4] as well as of industry [5] [6] [7] [8]. In general, this type of cements may exhibit broadly
26 similar performance as the ordinary Portland cements (OPC), such as good early and late strength, good
27 protection of steel reinforcement from corrosion and controllable volume stability [1] [4] [9]. However,
28 the CSA cements can achieve even higher strengths at early age while keeping the compressive strength
29 at 28 days comparable to that of a standard OPC [10]. In addition, a very good resistance to sulphate-rich
30 environments has been reported [11]. Besides these technical advantages, the production of CSA clinkers
31 has attracted interest as it generates lower CO₂ emissions than the production of the OPC clinker [6]
32 [12]. For those reasons, CSA type cements represent an interesting and promising alternative to the
33 traditional Portland cements.

34 The mechanism of a CSA cement hydration depends mainly on the cement clinker composition [13] [14],
35 the amount and reactivity of the added calcium sulphate [15] [16] and on the processing conditions [17].
36 In comparison to the OPC, the CSA cement reacts faster and most of the hydration heat is released
37 between 2 and 12 h [18], [19]. The primary hydration products are ettringite and monosulphate formed
38 together with amorphous aluminium hydroxide. Depending on the clinker and cement composition,
39 various other hydrates such as strätlingite, C-S-H, monocarboaluminate or hydrogarnet may also
40 precipitate [7], [13], [18], [20], [21].

41 The fast reaction of the CSA-type cements often requires the use of a retarder to obtain a sufficient open
42 time [1], [22], [23]. Hydroxylic organic compounds such as sugars or citric, tartaric or gluconic acids and
43 their salts are powerful retarders in high alumina cements or calcium alumina cements [24] [25]. It was
44 shown that citric acid [26], [27] and gluconate [28] efficiently retard the early hydration reactions, such
45 as the ettringite formation in CSA - anhydrite - OPC ternary binders. Carboxylic acids can bind to calcium
46 ions on the crystal surfaces and prevent further growth on these surfaces [29]. Citrate and tartrate ions
47 are also powerful chelators of solution Ca²⁺ and Al³⁺ and would be expected to influence the nucleation
48 and growth of phases containing these ions [29]. Similarly, sugars are capable of complexing calcium and
49 possibly also aluminium since they contain numerous hydroxyl groups that deprotonate to form
50 multidentate, negatively charged molecules, which in turn tightly bind positively charged solution ions
51 [29]. Effect of these compounds on the hydration of the CSA and of the OPC is qualitatively comparable.
52 However, chloride salts, which are powerful accelerators in OPC, normally have retarding effects in CSA,
53 somewhat depending on dosage and temperature [25], [30]. Another inorganic retarder applied for CSA

54 type cements is Borax (sodium tetraborate) [10], [31]. Both boric acid and its sodium salt inhibited the
55 nucleation of ettringite, but instead allowed six-sided plates of the metastable AFm phase to form [29].

56 To better understand the hydration mechanisms of CSA cements in the presence of different retarders,
57 the composition of the solid and the liquid phase during hydration of two CSA cements was followed.
58 The ionic composition of the liquid phase was linked to the precipitation of hydrates, which control the
59 setting, hardening and the evolution of the early mechanical properties. The focus of this study is on the
60 evolution of the properties at the early times, i.e. at times lower than 7 days of hydration. The effects of
61 three retarders with supposedly different ways of retardation were investigated: sodium gluconate
62 (labelled G, $\text{NaC}_6\text{H}_{11}\text{O}_7$), tartrate (T, $(\text{K,Na})_2\text{C}_4\text{H}_4\text{O}_6 \cdot 4\text{H}_2\text{O}$) and borax (B, $\text{Na}_2\text{B}_4\text{O}_7\text{H}_2\text{O}_8$).

63 In the paper the cement notation is used: C = CaO, S = SiO_2 , A = Al_2O_3 , F = Fe_2O_3 , S;⁻ = SO_3 , N = Na_2O , K =
64 K_2O .

65 2. Materials

66 CSA clinker and natural anhydrite (AH) were used to prepare the cements. The chemical composition as
67 determined by the XRF is given in **Table 1**. The mineralogical composition determined by the quantitative
68 XRD Rietveld analysis is given in **Table 2**.

69 The particle size distributions of ground clinker (C) and anhydrite determined by laser granulometry
70 using a Malvern Mastersizer 2000 (Fraunhofer model, propanol-2-ol (dispersant)) are given in **Figure 1**.

71 The experimental matrix is given in Table 3. Two cements were prepared: ground clinker (labelled C) and
72 ground clinker blended with 10 wt.-% of the anhydrite in a laboratory mixer (labelled CAH). The
73 experiments were conducted at the water to cement (W/C) ratio of 2.0. Performing the hydration study
74 at the high W/C ratio allowed performing the pore solution analyses and the phase assemblage
75 investigations on a single sample even at 7 days of hydration. The retarders were pre-dissolved in the
76 mixing water (deionized). This procedure assured a homogeneous distribution of the retarder in the
77 sample as well as an easy and reproducible sample preparation. The retarders' solutions were added on
78 top of the cement mass, i.e. the mass of the retarders was not included in the W/C ratios.

79 Additional samples were prepared at W/B =0.5 for microstructural investigations by SEM.

80 **3. Methods**

81 To investigate the hydration of the two cements, all sample preparations and investigations were carried
82 out at 20 °C if not stated otherwise.

83 A conduction calorimeter (Thermometric TAM Air) was used to determine the rate of hydration heat
84 release during the first 7 days. 6.0 g of cement was weighed into a flask and the corresponding amount
85 of retarder solution was added and mixed externally for about 1 minute before inserting the sample into
86 the calorimeter.

87 For the X-ray diffraction (XRD), thermogravimetric (TGA) and pore solution analyses, about 50 g of
88 cement was mixed with the retarder solution in a plastic container. A single sample was prepared for
89 each time investigated. The cement pastes were mixed using a laboratory mixer. The plastic containers
90 were stored sealed. During the curing time, samples were regularly shaken. The pore solutions were
91 obtained by a pressure-filtration using a 0.45 µm Nylon filter. For further analyses, one part of the
92 solution was diluted by 1:20 with deionized water to prevent any precipitation of solids. The total
93 concentrations of elements were determined using inductively coupled plasma optical emission
94 spectroscopy (ICP-OES Varian Vista-Pro). The other part of the pore solution (i.e. as extracted, not
95 diluted) was used for pH measurements. The pH electrode was calibrated against KOH solutions of
96 known concentrations. The measurements were performed not later than 2 hours after the solution
97 extraction. For the XRD and the TGA measurements, the samples were ground and the hydration was
98 stopped by solvent exchange with isopropanol for 15 min followed by flushing with diethyl ether.
99 TGA/DTG (NETZSCH STA F449 F3 Jupiter) was carried out on 30±2 mg of the stopped cement paste. Open
100 vessels in N₂ atmosphere and a heating rate of 20 °C/min up to 1050 °C were used.

101 The quantitative phase compositions of the unhydrated cements and of cement pastes were evaluated
102 using the XRD analysis coupled with the Rietveld refinement method. The XRD patterns were obtained at
103 room temperature (24±2 °C) using Bruker D-8 Advance in a θ -2 θ configuration with a monochromatic
104 CuK α radiation ($\lambda = 1.54059 \text{ \AA}$) and equipped with the LYNXEYE (1-d) detector. The generator settings
105 were 40 kV and 40 mA. The measurement range was 5° to 70° 2 θ with a step-size of approximately 0.02°.
106 10 wt.-% of zincite (ZnO) was added as the internal standard. A more detailed description of the test
107 procedure used is available in [17].

108 Additional samples were prepared for the microstructure observations. The cement pastes were
109 prepared at W/C = 0.5 using the same solutions as for the samples prepared at W/C = 2.0. The fragments

110 of cement pastes were immersed in isopropanol and subsequently dried at 40 °C for 24 h. The fractured
111 surfaces of the samples were gold coated and examined using Hitachi S450 scanning electron microscope
112 (SEM).

113 For the calculation of the supersaturating indexes, GEMS-PSI, a geochemical speciation code [32],
114 involving a thermodynamic database [33] [34] which has been updated with the cement-specific data
115 [35] [36] was used.

116 **4. Results**

117 ***4.1. Hydration of the reference samples***

118 ***4.1.1. Kinetics of hydration***

119 The results of the isothermal conduction calorimetry are shown in Figure 2. Heat flow curves differ for
120 the two investigated reference samples. Both reference cements show a very short induction period
121 after the initial peak. After that, sample C is characterized by three overlapping peaks with their maxima
122 at 2.5 h, 4.7 h and 53 h, respectively. The peak at 4.7 h has a shoulder after its maximum. Sample CAH
123 shows the main hydration peak at 5.5 h with a shoulder at 3.5 h. The later peak(s) were not observed up
124 to 7 days of hydration. The multi-peak evolution of the heat release is consistent with former studies
125 [18] [14] [16].

126 The cumulative heat, as shown in Figure 3, agrees very well with the evolution of the hydration degree of
127 cement clinker, calculated based on the Rietveld quantification (Figure 8). In general, the cumulative
128 heat is believed to be proportional to the hydration degree of hydraulic cement [14] [25]. In the case of
129 the reference samples, a substantial degree of hydration is already observed after 30 minutes. Between
130 30 minutes and about 2 hours, the hydration progresses slowly. The hydration significantly accelerates
131 between 2 and 10 hours. After 10 hours, the hydration slows down again. After 10 hours, the C sample
132 shows a faster hydration than CAH.

133 Table 4 and 5 depict the dissolution of major cement clinker phases in C and CAH samples. It is seen that
134 the fast progress of the hydration between 2 and 10 hours is related to the dissolution of aluminium
135 bearing phases, i.e. $C_4A_3S_7^-$, CA and C_4AF that react fast with water and the available sulphate [13] [18].
136 The XRD and TG data suggest that a significant amount of $C_4A_3S_7^-$ reacts during the first 30 minutes in

137 samples C and CAH (first measurement point, see as well Figure 9). Both cements contain anhydrite. In
138 the samples C, anhydrite is not detectable after 4 h of hydration. In the CAH sample, about a half of the
139 anhydrite reacts up to the first day of hydration. At 7 days, anhydrite is no more detectable. Belite reacts
140 significantly slower than the aluminate bearing phases during the investigated period [19].

141 **4.1.2. Hydrates assemblage**

142 Rietveld calculations were performed to follow the evolution of the ettringite content as well as the
143 content of the XRD – amorphous hydrates in the investigated samples. AFm and strätlingite were
144 considered as parts of the amorphous phase due to their low level of crystallinity. The XRD data shown in
145 Figure 4,5 and9 show that ettringite is the main hydration product at early times. The XRD results are
146 confirmed by the TGA data (Figure6 and7). In C and CAH samples, substantial amounts of ettringite are
147 formed already after 30 minutes. This is in agreement with the qualitative analysis of the XRD and DTG
148 data (Figure 9). It is noticeable that almost the same amount of ettringite is formed up to 2 hours. The
149 ettringite content increases slowly up to 2 hours and 3 hours for C and CAH, respectively. Afterwards, the
150 ettringite formation accelerates and reaches its final content at around 1 day. The final ettringite content
151 is considerably higher in the sample CAH when compared to the sample C. This is obviously a result of
152 the additional anhydrite. The evolution of the XRD amorphous phase content (Table 4 and 5 follows the
153 trend shown for the hydration degree (Figure 8). The nature of hydrates cannot be exactly identified
154 either form the XRD or TGA results. The corresponding broad and flat weight loss between 200 °C and
155 400 °C could be related to the presence of several phases like AFm, strätlingite and aluminium hydroxide.
156 The XRD data, in agreement with the TGA data, suggest that the content of these phases is considerably
157 higher in the samples C than in the CAH samples at 1 day and later.

158 Figure 10 shows the SEM images of the fractured samples after 1 day. In the CAH sample, ettringite
159 intermixed with aluminium hydroxide is visible confirming that the ettringite is the main hydration
160 product. Needles of ettringite display a range of sizes – from large needles with cross-sections up to 5
161 µm down to needles with cross-sections in the range of tenths of µm. The needles have irregular shape.
162 Ettringite in sample C had a similar morphology. However, only CAH samples are presented due to their
163 higher ettringite contents allowing an easier comparison of the effects of retarders on the ettringite
164 morphology.

165 **4.1.3. Pore solution chemistry**

166 The results obtained from the chemical analyses of the extracted pore solutions, i.e. elemental
167 concentrations (Ca, Al, S, Si, Fe and alkalis) and pH, are presented in Table 6 and 7 . For the reference
168 samples and the investigated period, the pore solution concentration is dominated by alkalis, calcium,
169 aluminium and sulphate. Silica and iron concentrations are under detection limits for both samples.
170 Sodium and potassium concentrations are relatively stable over the studied period. The calcium
171 concentration decreases rapidly from ~17 mmol/l at 5 minutes to less than 1 mmol/l at 1 day. After that,
172 the calcium concentration is relatively stable. The sulphate concentration (strictly speaking, the sulphur
173 concentration is measured by the ICP) decreases over the hydration time from 50 mmol/l to 0.1 mmol/l
174 in the case of C and to ~2 mmol/l in the case of CAH cement after 7 days. Aluminium concentration
175 increases initially, up to 8 hours and 4 hours for C and CAH, respectively, reaching ~60 mmol/l. Then the
176 aluminium concentration starts to decrease. The pH of the cement pore solution is close to 11 at the
177 beginning of the hydration and increases up to 13. In the sample CAH, the pH reaches a lower level
178 confirming that the pH is reversibly proportional to the concentration of sulphate. Winnefeld al. [13]
179 and Li et al. [20] analysed the liquid phase of reacting CSA cements. Their results show similar
180 concentrations of Ca and sulphate as well as similar trends as presented here, i.e. the drop of both
181 concentrations during the course of hydration, despite the differences in the experimental approach.
182 They also report the increase of aluminium concentration followed by the drop after some time.
183 Contrary to their experiments, the continuing increase of the alkalis concentration was not observed,
184 probably due to the higher W/B ratio used here.

185 A closer analysis of the pore solution results revealed that the charge balance is not exact. This can be
186 expected since the measurements of alkali and alumina with ICP are associated with considerable errors
187 of measurements. Moreover, a carbonation of the solutions during pH measurements cannot be fully
188 avoided [37].

189 **4.2. Effect of Tartrate**

190 **4.2.1. Kinetics of hydration**

191 The addition of tartrate has a pronounced effect on the hydration kinetics. Tartrate-retarded system
192 produces a small peak around 5.5 hours after the initial dissolution peak followed by a very low heat flow
193 for C-T and CAH-T samples (Figure 2). The characteristic multi-peak heat evolution seen for the reference

194 sample is not visible. Figure 3 reveals that the dormant period is strongly prolonged; hydration is strongly
195 accelerated only after about 4 h. At 7 days, the hydration degrees of reference samples and samples with
196 tartrate are similar. However, the cumulative heat is significantly lowered. QXRD data (Table 4 and 5)
197 reveal that tartrate strongly retards the hydration of ye'elimite and the dissolution of anhydrite.
198 Nevertheless, ye'elimite and gypsum are fully consumed after 7 days of reaction. The data suggest that
199 also the hydration of C₄AF is retarded.

200 **4.2.2. Hydrates assemblage**

201 In C-T sample, tartrate delays the formation of ettringite; it is firstly detected after 8 hours (Figure 4 and
202 Table 4). The formation of strätlingite is observed after 7 days by the XRD and TG (Figure 6), whereas no
203 AFm phase could be detected by means of the XRD analysis. In the case of CAH samples mixed with the
204 tartrate solution, similar phenomena are observed: tartrate delays the formation of hydrates. Later on,
205 the crystalline hydrates assemblage is similar as for the reference sample CAH, however, at 7 days, small
206 reflexion of strätlingite are visible in the XRD. The TGA data shown in Figure 7 confirms that the main
207 hydration product of the CAH-T system is ettringite and aluminium hydroxide.

208 Microstructure observations reveal that in the CAH-T sample, similarly to the CAH sample, the ettringite
209 needles of various sizes are intermixed with AH₃. The shape of the needles is, however, better defined
210 showing the typical hexagonal crystals. The smallest needles observed in the CAH sample, are not
211 present in the CAH-T.

212 **4.2.3. Pore solution chemistry**

213 Tartrate has a similar effect on the pore solution concentration in both two investigated cements.
214 Tartrate results in higher calcium and sulphate concentrations than in the reference samples up to one
215 day of hydration. These two concentrations decrease over time. At the beginning of hydration, the
216 concentration of aluminium is very low <0.01 mmol/l and it increases rapidly between 4th and 8th hour of
217 hydration reaching ~40 mmol/l. Afterwards, up to 7 days, the aluminium concentration decreases. Since
218 (K,Na)₂C₄H₄O₆·4H₂O was used in this study, the initial sodium and potassium concentrations are higher as
219 is also the pH. Additionally, in the sample CAH-T, the concentration of silicon increases above the
220 detection limit up to ~0.03 mmol/l.

221 **4.3. Effect of borax.**

222 **4.3.1. Kinetics of hydration**

223 The addition of borax results in a similar shape of the calorimetry curves of both cements as shown in
224 Figure 2. The main hydration peak starts after 24 hours and have its maximum at 33 hours. However, the
225 heat flow increases already after 12 hours of reaction. The cumulative heat (Figure 2) as well as the
226 hydration degree evolution (Figure 8) shows that borax strongly retards the hydration up to one day.
227 After that, the hydration proceeds significantly faster than for the references. Between 1 and 2 days, the
228 hydration degree of borax samples reaches the level of reference samples and evolves similarly to them
229 up to 7 days.

230 **4.3.2. Hydrates assemblage**

231 Borax retards the formation of XRD-detectable hydrates up to one day of hydration (Figure 4 and 5,
232 Table 4 and 5). Instead, the precipitation of gypsum is observed. Between 1 and 2 days, a massive
233 formation of ettringite and strätlingite is observed in addition to the depletion of gypsum. At 7 days, the
234 difference between C-B and CAH-B samples is similar as the difference between C and CAH samples,
235 respectively. In the C-B samples, a massive formation of AFm phases is observed whereas in the sample
236 CAH-B, ettringite and alumina hydroxide are the main hydration products (Figure 6 and 7).

237 The morphology of ettringite of the CAH-B sample (Figure 10) differs significantly when compared to the
238 reference and the tartrate-retarded sample. Contrary to both CAH and CAH-T, the range of ettringite
239 sizes is much narrower; all needles have their cross-section within ~ 0.1 and $1 \mu\text{m}$. Ettringite needles have
240 a well-defined shape.

241 **4.3.3. Pore solution chemistry**

242 The addition of borax results in an increase of the initial concentrations of calcium, sulphate and silicon
243 for both investigated samples as shown in Table 6 and 7. The calcium and sulphate concentrations drop
244 significantly after the first day of hydration. Aluminium concentration stays below the detection limit.
245 Only at 2 days, an increased aluminium concentration was detected. Boron concentrations are initially
246 high at around 120 mmol/l . They decrease slowly up to one day and then drop to values below
247 0.01 mmol/l already at 2 days. This time correlates with the increase of the aluminium concentration and
248 with the sharp decrease of the calcium concentration. The addition of borax results in a significant drop

249 of the initial pH when compared to the reference samples. The pH is reversibly proportional to the boron
250 concentration. The measured sodium concentrations are comparable to the reference samples. These
251 are unexpected results since sodium was released from borax. Theoretically, the sodium ion
252 concentration needs to be approximately half of the borate concentration. This assumption was
253 confirmed by measurements of the concentrations in the solutions used for sample preparation. The
254 measured concentration of sodium and boron in this solution was 50 mmol/l and 115 mmol/l
255 respectively. Consequently, the very initial concentration of sodium in C-B and CAH-B samples around
256 65–70 mmol/l should be expected accounting for the alkalis from cement. However, in both investigated
257 cements, i.e. C-B and CAH-B, the sodium concentration is similar to the reference samples. The sodium
258 concentrations increase rapidly between the 1st and the 2nd day and drop once more afterwards.

259 **4.4. Effect of gluconate**

260 **4.4.1. Kinetics of hydration**

261 Gluconate strongly retards the hydration of C and CAH cements (Figure 2). After the first dissolution
262 peak, only a weak activity is observed by the calorimetry. This is confirmed by the evolution of the
263 hydration degree that evolves only slowly during the investigated period.

264 Gluconate retards the formation of ettringite less than the other investigated retarders; the first
265 ettringite is detectable already after 4 hours (Figure 4 and 5) in C-G, i.e. before the C-T and C-B.
266 According to the XRD, no other crystalline hydrates are present. These results are confirmed by the TGA
267 data shown in Figure 6 and 7. At one day of hydration, ettringite appears as the main hydration product
268 in C-G and CAH-G samples. No significant amounts of AFm or AH₃ can be detected. At 7 days, the TGA
269 reveals a presence of several phases: ettringite, strätlingite, AFm and AH₃ in the C-G sample. In the case
270 of CAH-G, ettringite is still the main hydration products. The amount of hydrates is clearly lower than in
271 the reference samples.

272 In the sulfate-rich gluconate-containing sample, CAH-G, large ettringite needles with cross-sections
273 greater than 1 μm are visible. The needles have rectangular cross-sections with aspect ratios of approx.
274 1:3 to 1:1. Partly-dissolved clinker grains as well as the aluminium hydroxide can be identified in the
275 images (Figure 10).

276 **4.4.2. Pore solution chemistry**

277 The addition of gluconate results in an increase of the calcium, silicate, alkali and sulphate
278 concentrations when compared to the reference samples (Table 6 and 7). Aluminium concentration is
279 low in the presence of gluconate at 5 min (3 mmol/l) and it increases continuously up to 7 days of
280 hydration, reaching 90 mmol/l for the C-G sample and 30 mmol/l for CAH sample at 7 days. The
281 concentrations of Si and Fe are higher when compared to the other samples. The pH evolution is
282 different as for reference cements. It is initially higher, reaching about 11.8 at 5 minutes and does not
283 significantly change significantly during the experiments.

284 **5. Saturation indices**

285 The experimental data of the pore solution concentrations of C and CAH were used to calculate the
286 saturation indices of possible hydrate phases in order to reveal which phases could precipitate. The
287 saturation indexes were not calculated for Si bearing phases (strätlingite, C-S-H) since the Si
288 concentration, in most cases, was under the detection limit.

289
290 Ettringite is always highly oversaturated except for the borax retarded samples at early ages; the degree
291 of oversaturation decreases with time. Additionally, aluminium hydroxide, monosulphate and CAH_{10} are
292 oversaturated up to one day of hydration. Gypsum and portlandite are undersaturated. However, not
293 every oversaturated phase will precipitate. The amount and type of the phase precipitated depends on
294 the kinetic of the precipitation as well as on thermodynamic stability of other phases. The predicted
295 precipitation of ettringite, gypsum, AH_3 and monosulphate is in agreement with data of the solid phase
296 composition. The initially high concentration of calcium, sulphate and alkalis is a result of the very rapid
297 dissolution of readily soluble alkalis (Table 2) and ye'elimite. It demonstrates that at early age, the pore
298 solution concentrations are dominated by the hydration of ye'elimite and calcium aluminate phases with
299 readily soluble sulphates and anhydrite. As a result, ettringite, gibbsite and potentially monosulphate are
300 predicted to precipitate in agreement with the experimental data.

301 The addition of tartrate results in the increase of the calcium and sulphate concentration in the pore
302 solution already after 5 minutes. This is related to the dissolution of the readily soluble alkalis. The pore
303 solution concentrations of Ca^{2+} , $\text{Al}(\text{OH})_4^-$ and SO_4^{2-} are limited by the ettringite solubility. The very low
304 concentration of alumina allows further increase of the calcium and sulphate concentrations. The
305 calcium concentration is additionally increased by formation of complexes with tartrate. The high

306 concentrations of calcium and sulphate result in the supersaturation of the pore solution with respect to
307 gypsum. One notes that the solution is supersaturated with respect to ettringite and monosulphate, but
308 undersaturated with respect to alumina hydroxide (Figure 12). These results indicate that the ettringite
309 and monosulphate could precipitate. However, these phases did not form because their nucleation and
310 growth was poisoned by tartrate or because the dissolution of ye'elimite and calcium aluminates was
311 blocked which resulted in the lack of alumina. The high concentration of calcium and sulphate can have a
312 negative role on the dissolution rate of anhydrous calcium aluminates. It was proven that the high
313 concentration of calcium and sulphate slows down the dissolution of calcium aluminate phases in the
314 OPC [38] [39].

315 Due to the low pH in the boron retarded systems and to the low concentration of aluminium, the
316 solution is undersaturated with respect to ettringite and AFm phases (Figure 14). Because of the very
317 high concentration of calcium and sulphate, the dissolution of ye'elimite may be slowed down. However,
318 this cannot be verified since the solubility data for ye'elimite are not available.

319 The slow decrease of the boron concentration may be related to the precipitation of either calcium-
320 boron phases or AFm phases (however, the AFm is modelled to be undersaturated). It is known that
321 boron can substitute for sulphate in the AFm phase [40] [41]. The boron containing AFm may easily form
322 the solid solution with hemcarbonate, which complicates the investigated system even more. In both
323 cases, these phases may precipitate as XRD amorphous explaining the fact that they are not seen by the
324 XRD [51] [37]. However, one notes the significant amount of the XRD amorphous content in the samples
325 C-B and CAH-B (Table 4 and 5). Another possibility of borax absorption is alumina hydroxide. However,
326 data supporting or disproving this hypothesis are not available to authors' knowledge.

327 Once boron is consumed and its pH-buffering effect stops, the pH increases considerably followed by the
328 supersaturation with respect to ettringite. Further hydration proceeds very rapidly. This is confirmed by
329 the high increase of the alumina concentration as well as by the decrease of the sulphate and calcium
330 concentrations between 1 and 2 days of hydration (Table 6 and Table 7). During that time, the phase that
331 bound sodium decomposes which results in an increased sodium concentration. Consequently, the
332 released sodium is reabsorbed on the hydrates formed as discussed for the reference samples.

333 In the gluconate retarded system, the solution is strongly oversaturated with respect to ettringite and
334 monosulphate phases. Such a mechanism is comparable to that of tartrate. However, contrary to the
335 tartrate, portlandite is the only undersaturated phase. All the other phases are close to be saturated or
336 are strongly supersaturated.

337 **6. Discussions on retarders on mechanisms**

338 Three different cement hydration inhibiting mechanisms have been proposed to explain the action of
339 different retarders in cement [25]:

- 340 • Calcium complexation that involves either removing calcium from solution by forming insoluble
341 salts or chelating calcium in solution to prevent hydrates formation.
- 342 • Surface adsorption of inhibitors directly onto the surface of either the anhydrous or (more likely)
343 the partially hydrated mineral surfaces that blocks future reactions with water.
- 344 • Formation of a semipermeable layer on the cement grains that slows the migration of water and
345 extends the induction period.

346 Tartaric acid is a known calcium chelating ligand with the resulting complex only sparingly soluble in
347 water. The hypothesis that calcium is complexed by the tartrate can be valid since the calcium
348 concentration in the samples C-T and CAH-T is significantly higher than in the reference samples. In
349 addition to the calcium chelating, tartaric acid has a high affinity for aluminium. In moderately acidic
350 solutions, aluminium is capable of coordinating to the octahedral aluminium while the tetrahedral
351 aluminium is preferred in moderately basic solutions. Above pH of 11.5, the tetrahedral aluminium
352 tartrate complex dissociate into the free ligand and $\text{Al}(\text{OH})_4^-$ [42]. Bishop and Barron [43] studied
353 mechanisms of the C_3A reaction retardation by the tartrate. They proposed a mechanism in which
354 tartaric acid directly adsorbs onto the surface of hydrating C_3A and blocks by that its reaction with water.
355 The mechanism involves a dissolution of calcium by extraction with tartaric acid (exposing the residual
356 aluminium) followed by a precipitation of a layered calcium tartrate that binds to the surface of the C_3A
357 grains, inhibiting further hydration. On the other hand, Cody [29] noted that tartrate inhibits ettringite
358 nucleation and growth. Additionally, one notes that ettringite in natural or synthesized pore solutions
359 can adsorb high amounts of negatively charged polycarboxylate-based superplasticizers [44] [45]. Since
360 tartrate used in the present study is also negatively charged, it could also adsorb onto ettringite surfaces
361 and block its growth. The results presented in this study does not allow distinguishing whether the
362 tartrate retarders the hydration of CSA cement by limiting the clinker dissolution or by limiting the
363 growth of ettringite. Once the tartrate is consumed, e.g. by the ab- or adsorption on the surface of
364 hydrates during the slow initial hydration, the course of the reaction becomes the same as for the
365 reference samples. The tartrate consumption could be related e.g. to its adsorption to the slowly formed
366 ettringite or to the increase in the pH that became high enough to stabilize the aluminium–tartrate
367 complex.

368 The addition of borax results in the low pH of the cement pore solution. The low pH can be associated
369 with the presence of $B(OH)_4^-$ species in the cement pore solution. As the electro-neutrality of the pore
370 solution has to be ensured, the hydroxide concentration decreases and so does the pH. Boric acid is
371 a solid substance soluble in the water — with solubility of 55 g/l at 25 °C. As boron is an electron
372 deficient element, boric acid acts as a weak acid. Below 22 mg/l, mononuclear species $B(OH)_3$ and
373 $B(OH)_4^-$ are present. Polyborates appear at concentrations of boron higher than 1000 mg/l. In the pH
374 range above 7, the mole fraction of $B(OH)_3$ decreases while that of $B(OH)_4^-$ increases with increasing pH.
375 At pH values around 9, the $B(OH)_3$ and $B(OH)_4^-$ concentrations are practically equal, while at higher pH,
376 $B(OH)_4^-$ is the predominant species [46].

377 Additional factor that contributes to the decreased pH is that the sodium concentration is significantly
378 lower when compared to the expected one. Consequently, it is reasonable to assume a formation of
379 a metastable Na-rich phase:

- 380 • Sodium can precipitated to form the so called U-phase; i.e. a kind of AFm phase, which can be
381 formed in significant amounts in hydrating CSA cements. However, the formation of the U-phase
382 requires a high pH and a high concentration of the sodium sulphate [47] [48]. None of these
383 conditions is fulfilled in the investigated systems
- 384 • Another possibility is a precipitation of the mineral called Dawsonite ($NaAlCO_3(OH)_2$). Dawsonite,
385 however potassium containing, was found in the CAC cements when hardened CAC concrete is
386 exposed to an alkaline environment [49], [50]. Literature data [51], [52], [53], [54] suggest that
387 the optimal experimental conditions to synthesize dawsonite require moderately basic solutions.
388 TGA (Figure 15) data suggest the presence of dawsonite since they are similar to TGA curves of
389 synthetic $NaAlCO_3(OH)_2$ [55]; two characteristic effects are visible: mass loss at 300 °C and
390 575 °C.

391 Dawsonite, or other metastable Na-rich phase, present in the borax-retarded samples, is probably
392 amorphous since it was not detected by the XRD. Amorphous or weakly crystalline Dawsonite has been
393 reported [50] [54]. The TGA data at early times clearly suggest the presence one of this phase as shown
394 in Figure 15. The hypothesis of formation of this phase is supported by the low alumina concentration
395 and by the presence of limestone in the cement clinker (Table 2). Additional supporting argument is the
396 fact that the limestone can rapidly dissolve in the cement pore solution [56] to provide carbonate anions
397 to form Dawsonite.

398 It is widely recognized that sugars are one of the most effective hydration inhibitors of the hydraulic
399 cements. Based on several results of different studies, it has been hypothesized that saccharide
400 adsorption on hydrating cement particles contributes to their relative effectiveness in slowing the
401 hydration [24] [57] [58] [59] [60]. However, there is no clear explanation of the exact mechanism how
402 the sugars retard. The work of Smith et al. [61] shows that carboxylate-like glucose reacts with the –
403 Al(OH) groups of the calcium aluminium hydrates. This points out a strong adsorption of saccharine acids
404 onto the aluminium hydration products. The gluconate ion is a well-known inhibitor of gibbsite,
405 Al(OH)₃·3H₂O, precipitation and consequently it was proposed that gluconate might block the growth of
406 the gibbsite [62] [63].

407 Sugars are capable of complexing calcium and possibly aluminium since they contain numerous hydroxyl
408 groups that deprotonate to form multidentate, negatively charged molecules, which in turn tightly bind
409 positively charged solution ions [29]. Gluconate forms the complexes with the calcium, alumina and iron
410 with stability and composition depends on the pore solution pH [64] [65] [66]. This explains the higher
411 concentration of the calcium and iron in the cement pore solution measured. Additionally, the higher
412 concentration of Si can be associated with some complexes with gluconate.

413 The differences in the rate of ettringite formation and in the pore solution composition during the
414 hydration are probably responsible for the differences in the ettringite morphology observed by the SEM
415 investigations. Before the rapid dissolution of ye'elimite, the already formed ettringite crystals have
416 enough time to grow resulting in large, well-defined crystals. After the acceleration period, a significant
417 amount of ettringite forms over a short time explaining the smaller crystals filling the space between the
418 large crystals.

419 **7. Conclusions**

420 The effect of three different retarders – Na/K-tartrate, Na-gluconate and borax – on the early age
421 hydration of CSA cements was investigated using a multi-method approach. The evolution of solid
422 phases as well as of the pore solution composition was measured between 5 minutes and 7 days. The
423 early hydration of CSA cement is dominated by the ye'elimite hydration whose hydration is further
424 accelerated by the presence of the readily soluble alkalis and calcium bearing phases. The added
425 anhydrite seems to have little impact on the very early hydration. This is most probably related to its low
426 solubility. However, after about two hours of hydration, anhydrite participates in the reaction by
427 stabilizing the ettringite instead of AFm phases. Despite the strong effect of retarders on the CSA cement

428 hydration, the aforementioned hydration path is always kept e.g., ettringite is the main hydration
429 product in both C and CAH systems at early age.

430 The retarders have similar effects on the pore solution concentration. On the one hand, the calcium and
431 sulphate concentration is increased when compared to the neat samples. This is related to the complexing
432 action of the organic additives or lowering of the pH by borax. These high concentrations result in the
433 initial supersaturation of the pore solution with respect to gypsum. In the case of the neat samples, the
434 gypsum is undersaturated after 5 minutes. On the other hand, the alumina concentration is very low.
435 Further common point of all retarders is that the impact of a given retarder on the hydration mechanism
436 is similar for the two investigated cements, i.e. independent of the sulphate added.

437 Nevertheless, there are the differences among the investigated retarders:

- 438 • Tartrate and gluconate seems to delay the dissolution and / or precipitation and growth
- 439 • Borax destabilizes the hydrates because of the low pH

440 The main action of the both organic retarders is the slowing down of the hydration kinetics. However,
441 gluconate slows down the reaction much stronger suggesting much stronger interaction with the
442 hydrating cement. The retarders clearly act on the formation of ettringite as revealed by the
443 microstructure observation.

444 In the case of borax, a clearly different retarding effect is observed. Firstly, the addition of borax results
445 in a significant drop of the pH, whereas the additions of tartrate and gluconate resulted in its increase.
446 Borax stops completely the reaction of ye'elimite and other cement clinker phases but not the reaction
447 of anhydrite. As a result, gypsum is the only crystalline phase formed at early age. Some amorphous
448 phases may precipitate as revealed by the TG. The results indicate that a meta-stable sodium-bearing
449 phase precipitates. Borax is gradually consumed from the pore solution. Once its concentration is low
450 enough, the hydration reaction proceeds rapidly.

451 All investigated retarders may work efficiently as the set retarding agents since they suppress or slow
452 down the initial formation of ettringite. The correlation between the effect of retarders on the
453 microstructure development and on the evolution of the mechanical performance is a subject of our
454 further studies.

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458 **8. Literature**

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622 **Tables**

623

Table 1 Chemical composition of the investigated materials (wt.-%).

Component	Cement clinker	AH
SiO ₂	17.95	2.31
Al ₂ O ₃	15.30	0.73
TiO ₂	0.58	0.02
MnO	0.04	0.00
Fe ₂ O ₃	3.26	0.25
CaO	51.88	38.04
MgO	1.09	1.49
K ₂ O	0.74	0.17
Na ₂ O	0.13	0.00
SO ₃	6.68	51.93
P ₂ O ₅	0.20	0.02
Σ	98.77	98.62

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627 **Table 2 Mineral composition of the investigated materials determined by the Rietveld analysis (wt.-%).**

Phase	Cement clinker	AH
$C_4A_3S_2^-$	24.8	
$\beta-C_2S$	52.4	
C_4AF	6.6	
C_2F	2.1	
CA	1.2	
Cc (Calcite)	1.9	
KS_2^- (Ankarnite)	0.5	
$C_2KS_3^-$ (Langbainite)	1.5	
CS_2^- (Anhydrite)	2.2	88.0
Dolomite		7.4
Other	6.8	4.6
Σ	100.0	100.0

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Table 3 Experimental matrix in wt.-%.

Sample	C	CAH	T	B	G
			W/C=2.0		
C	100				
CAH		100			
C-T	100		2		
C-B	100			2	
C-G	100				2
CAH-T		100	2		
CAH-B		100		2	
CAH-G		100			2

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634 **Table 4 Contents of anhydrous clinker phases, ettringite (Et) and XRD amorphous relative to the dry content in**
 635 **wt.-% determined by the XRD-Rietveld analysis (cement C).**

	anhydrous	30 min	1 h	2 h	4 h	8 h	24 h	48 h	168 h
C									
C4A3S; ₂ ⁻	24.8	20.3	20.4	20.7	16.2	3.0	0.0	-	0.0
C2S	52.4	47.3	48.1	50.5	43.7	39.3	35.4	-	27.7
C4AF	6.6	6.1	6.2	6.1	5.2	3.4	2.3	-	0.0
C2F	2.1	1.6	1.7	1.9	1.7	1.4	1.5	-	0.0
CA	1.2	0.7	0.7	0.8	0.7	0.3	0.0	-	0.0
Cc	1.9	1.4	1.3	1.4	1.1	0.7	0.1	-	0.0
CS; ₂ ⁻	2.2	1.4	1.2	1.2	0.8	0.0	0.0	-	0.0
Et	0.0	5.0	5.6	7.7	8.4	15.0	15.6	-	14.8
XRD Amorphous	0.0	11.5	10.2	4.7	18.0	32.7	41.0	-	53.0
C-T									
C4A3S; ₂ ⁻	24.8	24.7	24.8	24.7	24.4	17.3	13.7	-	0.0
C2S	52.4	51.3	52.5	52.9	51.8	43.2	43.4	-	25.4
C4AF	6.6	6.8	6.8	6.9	6.8	5.5	4.9	-	0.0
C2F	2.1	2.1	2.0	2.1	2.2	1.7	1.8	-	0.9
CA	1.2	1.0	0.9	1.0	0.8	0.6	0.4	-	0.0
Cc	1.9	1.6	1.7	1.5	1.5	1.2	1.1	-	0.2
CS; ₂ ⁻	2.2	1.9	2.0	1.9	1.9	1.2	0.0	-	0.0
Et	0.0	0.0	0.0	0.0	0.0	5.7	11.1	-	19.9
XRD Amorphous	0.0	5.5	4.3	3.9	5.9	19.7	19.5	-	50.9
C-B									
C4A3S; ₂ ⁻	24.8	24.3	23.5	24.0	23.9	24.0	23.6	0.0	0.0
C2S	52.4	50.1	49.3	50.7	49.7	50.6	49.1	33.0	30.5
C4AF	6.6	6.4	6.7	6.6	6.6	6.7	6.6	2.2	0.0
C2F	2.1	2.1	2.1	2.3	2.0	2.2	2.2	0.7	0.0
CA	1.2	0.9	0.8	0.7	0.9	0.7	0.8	0.2	0.0
Cc	1.9	1.5	1.6	1.6	1.6	1.4	1.5	0.0	0.0
CS; ₂ ⁻	2.2	1.8	1.8	1.9	1.8	1.8	1.9	0.0	0.0
Et	0.0	0.0	0.0	0.0	0.0	0.0	0.0	17.4	14.8
XRD Amorphous	0.0	7.7	8.0	6.5	7.7	6.7	8.2	43.8	51.9
C-G									
C4A3S; ₂ ⁻	24.8	24.1	24.3	24.1	22.4	21.3	18.1	-	11.0
C2S	52.4	49.6	49.6	50.2	46.4	47.9	44.2	-	42.0
C4AF	6.6	6.5	6.5	6.7	5.7	6.1	5.2	-	4.5
C2F	2.1	1.8	2.1	2.1	2.0	1.6	1.6	-	1.5
CA	1.2	0.6	0.8	0.8	0.7	0.6	0.6	-	0.5
Cc	1.9	1.5	1.5	1.5	1.5	1.3	1.2	-	1.0
CS; ₂ ⁻	2.2	1.9	1.9	1.9	1.7	1.6	1.1	-	0.0
Et	0.0	0.0	0.0	0.0	1.8	4.6	6.8	-	11.6
XRD	0.0	9.0	8.5	7.9	13.2	10.6	17.1	-	23.5

Amorphous									
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638 **Table 5 Contents of anhydrous clinker phases, e ringite (Et) and XRD amorphous relative to the dry content in**
 639 **wt.-% determined by the XRD-Rietveld analysis (cement CAH).**

	anhydrous	30 min	1 h	2 h	4 h	8 h	24 h	48 h	168 h
CAH									
C4A3S; ⁻	22.3	18.4	20.1	16.4	3.7	0.0	0.0	-	0.0
C2S	47.2	41.0	47.8	40.9	36.3	35.6	35.0	-	28.5
C4AF	5.9	5.4	5.7	5.0	3.3	2.8	3.1	-	2.9
C2F	1.9	1.7	1.7	1.3	1.3	1.5	1.2	-	0.8
CA	1.1	0.7	0.6	0.5	0.3	0.3	0.1	-	0.0
Cc	11.1	1.2	1.2	1.1	0.8	0.8	0.8	-	0.9
CS; ⁻	2.0	10.2	10.0	9.6	10.0	9.7	6.4	-	0.0
Et	0.0	4.9	6.0	7.7	22.9	29.2	31.9	-	32.2
XRD Amorphous	0.0	11.9	1.0	13.8	23.8	24.5	24.8	-	32.0
CAH-T									
C4A3S; ⁻	22.3	21.3	21.4	21.3	22.1	18.1	11.4	-	0.0
C2S	47.2	45.1	45.4	44.4	45.9	44.2	39.6	-	31.7
C4AF	5.9	6.1	6.4	6.5	6.5	5.8	4.9	-	3.6
C2F	1.9	1.7	1.9	1.7	1.7	1.8	1.8	-	0.9
CA	1.1	0.8	0.8	0.8	0.5	0.4	0.3	-	0.0
Cc	1.7	1.4	1.5	1.5	1.4	1.3	1.2	-	0.7
CS; ⁻	11.1	9.8	10.0	10.0	9.9	9.5	9.7	-	0.0
Et	0.0	0.0	0.0	0.0	0.0	3.8	11.6	-	36.6
XRD Amorphous	0.0	7.8	7.1	8.4	6.6	10.2	19.0	-	23
CAH-B									
C4A3S; ⁻	22.3	21.8	22.3	21.9	21.2	21.4	20.8	0.0	0.0
C2S	47.2	45.7	46.6	45.2	45.1	43.9	43.4	32.4	31.8
C4AF	5.9	6.6	6.7	6.1	6.1	6.0	6.4	3.8	3.5
C2F	1.9	1.8	2.0	1.9	2.0	1.9	1.5	1.2	1.1
CA	1.1	0.7	0.6	0.6	0.6	0.5	0.6	0.3	0.1
Cc	1.7	1.5	1.6	1.5	1.4	1.5	1.4	0.8	1.1
CS; ⁻	11.1	9.8	10.0	10.0	9.9	9.5	9.7	0.0	0.0
Et	0.0	0.0	0.0	0.0	0.0	0.0	0.0	26.5	25.8
XRD Amorphous	0.0	6.9	4.3	6.9	7.1	8.7	9.7	33.0	34.0
CAH-G									
C4A3S; ⁻	22.3	21.8	21.2	21.2	20.1	19.0	17.1	-	8.5
C2S	47.2	44.9	43.9	44.5	42.6	42.0	41.6	-	36.8
C4AF	5.9	6.1	6.1	6.0	6.1	5.5	5.9	-	4.4
C2F	1.9	2.0	1.9	1.8	1.5	1.6	1.2	-	1.3
CA	1.1	0.5	0.8	0.5	0.6	0.4	0.6	-	0.3
Cc	1.7	1.5	1.4	1.5	1.4	1.3	1.4	-	1.0
CS; ⁻	11.1	9.9	9.4	9.8	9.9	9.7	9.2	-	5.0
Et	0.0	0.0	0.0	0.0	0.0	3.9	7.0	-	13.0
XRD	0.0	8.4	9.7	8.7	12.3	11.7	10.9	-	25.3

Amorphous									
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Table 1 Pore solution chemistry of cements C measured by ICP (mmol/l) and pH electrode (-)

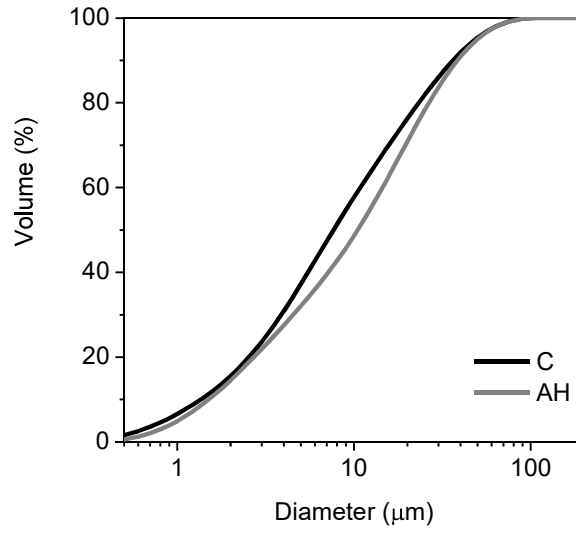
	5 min	30 min	1 h	2 h	4 h	8 h	24 h	48 h	168 h
C									
Ca	16.5	7.6	3.8	2.8	2.0	1.1	0.3	-	0.45
Si	0.01	0.01	0.01	0.01	0.01	0.01	0.01	-	0.01
Al	11.38	20.98	34.43	47.85	67.31	66.79	20.57	-	0.05
Na	11.9	12.7	12.5	11.6	12.0	15.1	15.5	-	17.8
K	80.3	78.3	78.8	78.3	78.8	56.8	54.2	-	62.1
Fe	0.01	0.01	0.01	0.01	0.01	0.01	0.01	-	0.01
S (sulphur)	49.2	35.9	26.4	18.1	7.3	1.6	1.3	-	0.1
pH	11.17	11.15	11.42	11.52	11.73	12.58	13.1	-	13.49
C-T									
Ca	28.8	28.4	27.1	25.5	22.7	4.3	1.6	-	0.50
Si	0.01	0.01	0.01	0.01	0.01	0.01	0.01	-	0.01
Al	0.03	0.01	0.01	0.04	0.04	39.81	77.09	-	1.06
Na	66.3	43.6	43.1	43.1	44.4	45.7	47.2	-	45.2
K	121.7	100.0	100.3	100.3	102.8	95.42	97.42	-	97.21
Fe	0.01	0.01	0.01	0.01	0.01	0.01	0.01	-	0.01
S (sulphur)	104.1	84.2	84.8	85.4	85.4	65.8	41.4	-	0.34
pH	11.7	11.9	12.0	12.1	12.2	11.5	12.1	-	13.5
C-B									
Ca	57.6	37.3	29.2	47.9	42.4	35.0	33.4	0.0	2.4
Si	0.74	0.01	0.01	1.03	0.99	0.34	0.01	0.01	0.01
Al	0.01	0.01	0.01	0.01	0.01	0.01	0.01	25.57	0.05
Na	15.0	13.4	13.1	15.4	15.4	16.6	16.5	73.5	25.0
K	58.8	71.4	68.3	58.6	58.8	53.2	52.4	65.5	63.2
Fe	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
S (sulphur)	81.1	65.8	43.0	65.8	60.8	60.8	55.0	1.7	0.1
B	122.2	111.1	94.4	75.9	85.2	72.2	59.3	<0.1	0.60
pH	8.5	8.6	8.9	8.9	9.1	9.6	11.0	13.3	13.3
C-G									
Ca	48.1	28.1	24.1	22.5	23.9	11.6	7.5	-	2.02
Si	0.01	0.59	0.01	0.01	1.31	0.01	0.01	-	0.01
Al	2.98	1.88	1.78	1.52	13.45	32.65	43.51	-	88.95
Na	80.6	56.9	56.7	57.0	62.7	69.5	65.1	-	54.5
K	80.8	70.3	70.6	70.6	71.9	63.9	61.9	-	61.9
Fe	0.10	0.07	0.06	0.06	0.37	0.52	0.67	-	0.65
S (sulphur)	111.6	75.5	75.1	75.5	73.9	68.0	55.8	-	18.8
pH	11.8	11.9	12.0	12.1	11.7	11.7	11.8	-	12.0

Table 2 Pore solution chemistry of cements CAH measured by ICP (mmol/l) and pH electrode (-)

	5 min	30 min	1 h	2 h	4 h	8 h	24 h	48 h	168 h
CAH									
Ca	17.5	9.7	6.9	4.3	0.8	0.3	0.2	-	0.3
Si	0.01	0.01	0.01	0.01	0.01	0.01	0.01	-	0.01
Al	11.01	21.09	22.31	31.13	53.45	24.83	22.57	-	8.23
Na	13.1	14.9	14.8	13.5	15.4	15.4	14.7	-	14.7
K	56.5	2.9	65.9	55.2	58.8	50.4	52.2	-	48.8
Fe	0.01	0.01	0.01	0.01	0.01	0.01	0.01	-	0.01
S (sulphur)	52.8	44.3	29.7	22.5	9.4	18.3	6.8	-	1.6
pH	11.1	11.0	11.1	11.4	11.9	12.3	12.8	-	13.0
CAH-T									
Ca	27.1	23.3	22.4	22.6	21.3	5.7	2.6	-	0.2
Si	0.60	0.79	0.73	0.83	0.56	0.01	0.01	-	0.01
Al	0.01	0.01	0.01	0.01	0.01	36.84	36.06	-	64.60
Na	39.8	41.5	42.4	42.5	42.4	56.1	46.5	-	45.2
K	82.4	102.0	101.8	78.3	76.7	87.0	85.9	-	77.5
Fe	0.01	0.01	0.01	0.01	0.01	0.01	0.01	-	0.01
S (sulphur)	79.5	79.2	84.5	80.4	83.3	74.2	68.6	-	19.6
pH	11.8	11.9	12.0	12.1	12.2	11.4	11.5	-	12.9
CAH-B									
Ca	61.9	57.1	52.6	49.2	43.8	37.5	35.1	0.1	0.1
Si	0.01	0.60	0.44	0.42	0.27	0.41	0.54	0.01	0.01
Al	0.01	0.01	0.01	0.01	0.01	0.01	0.01	20.00	9.64
Na	14.1	13.4	13.4	13.4	13.7	18.7	16.2	70.9	27.6
K	48.5	63.9	63.7	63.7	63.7	53.2	50.7	53.7	46.0
Fe	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
S (sulphur)	83.6	64.9	61.5	58.4	52.9	67.0	55.5	43.0	12.4
B	131.5	118.5	114.8	100	88.9	74.1	63	<0.1	0.9
pH	8.5	8.6	8.7	8.9	9.1	9.5	10.5	12.9	12.9
CAH-G									
Ca	52.1	40.8	36.9	32.5	32.4	11.8	8.8	-	4.1
Si	0.27	1.11	1.67	0.96	0.15	0.01	0.01	-	0.01
Al	2.87	1.71	1.59	1.54	2.49	29.17	35.03	-	32.39
Na	50.4	56.9	50.1	50.4	50.3	80.3	66.7	-	54.2
K	48.8	64.7	52.7	49.3	53.5	60.4	60.4	-	54.7
Fe	0.10	0.06	0.07	0.06	0.08	0.44	0.59	-	0.90
S (sulphur)	98.8	72.7	87.9	82.3	82.0	71.7	62.7	-	52.4
pH	11.8	12.0	12.0	12.1	12.2	11.7	11.6	-	11.4

672 **Figures**

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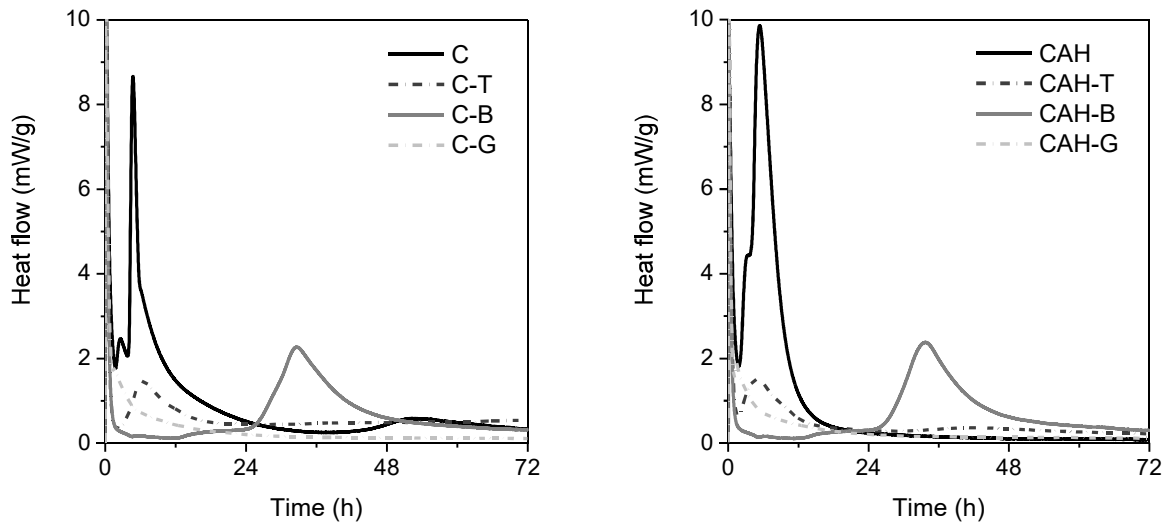


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Figure 1. Particle size distribution of C and AH determined by laser diffraction.

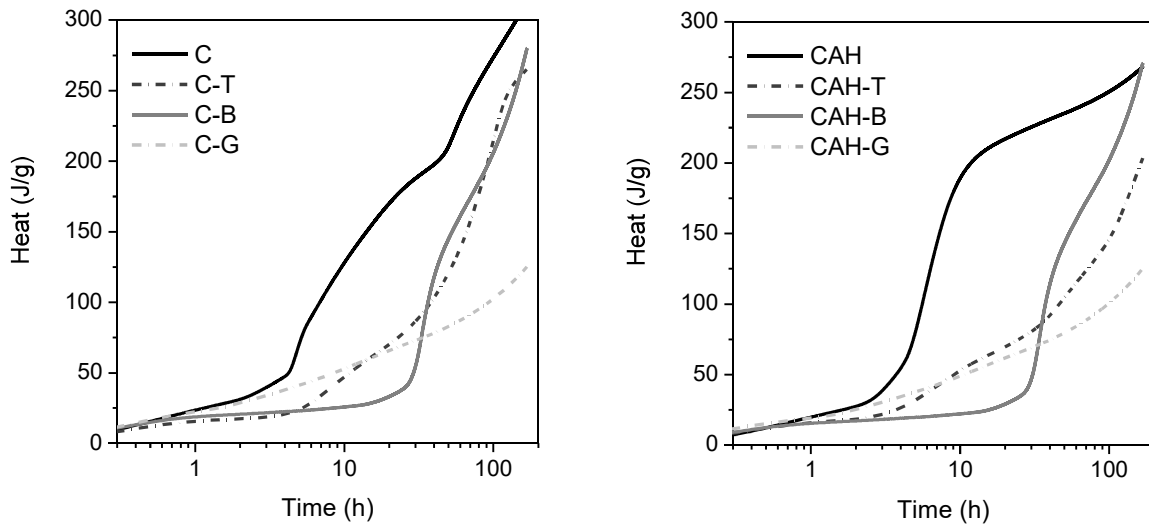
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Figure 2. Heat flow of the investigated samples within the first 72 hours.

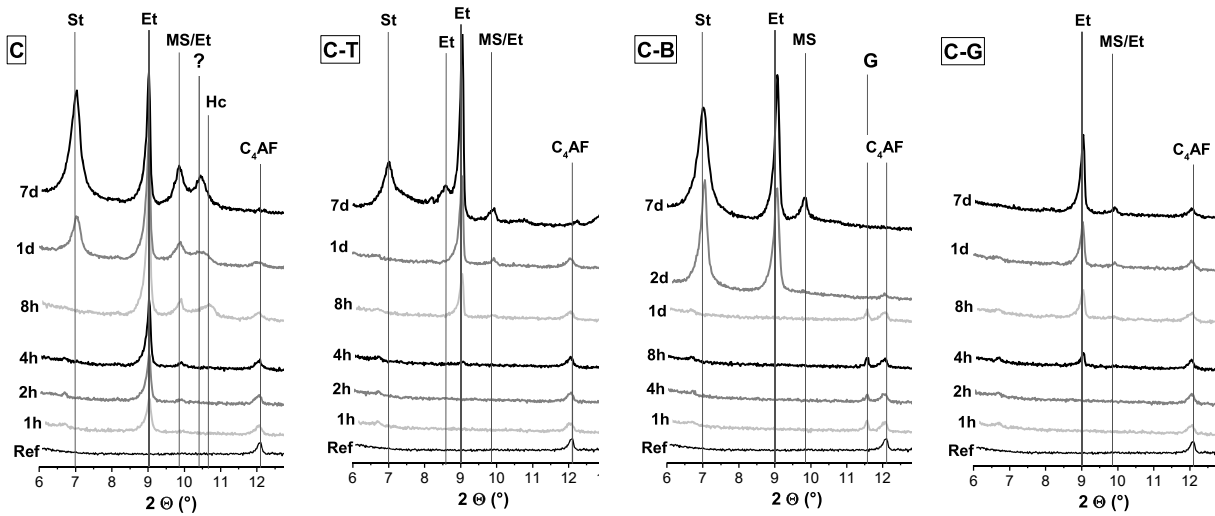
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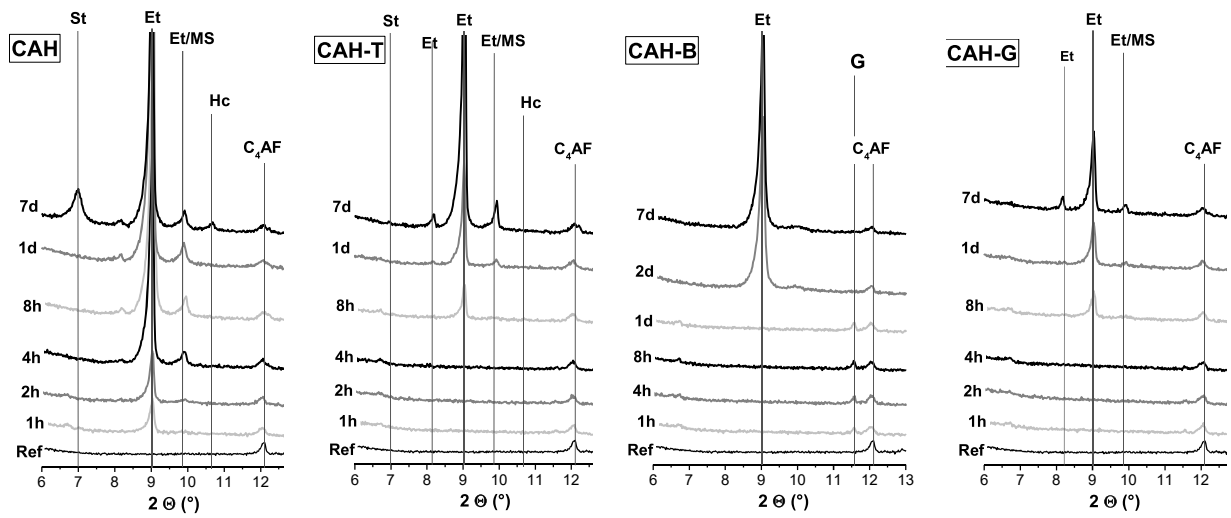
679 **Figure 3. Cumulative heat of the investigated samples during the first 7 days of hydration.**

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682 **Figure 4. Comparison of XRD plots for investigated C cements**

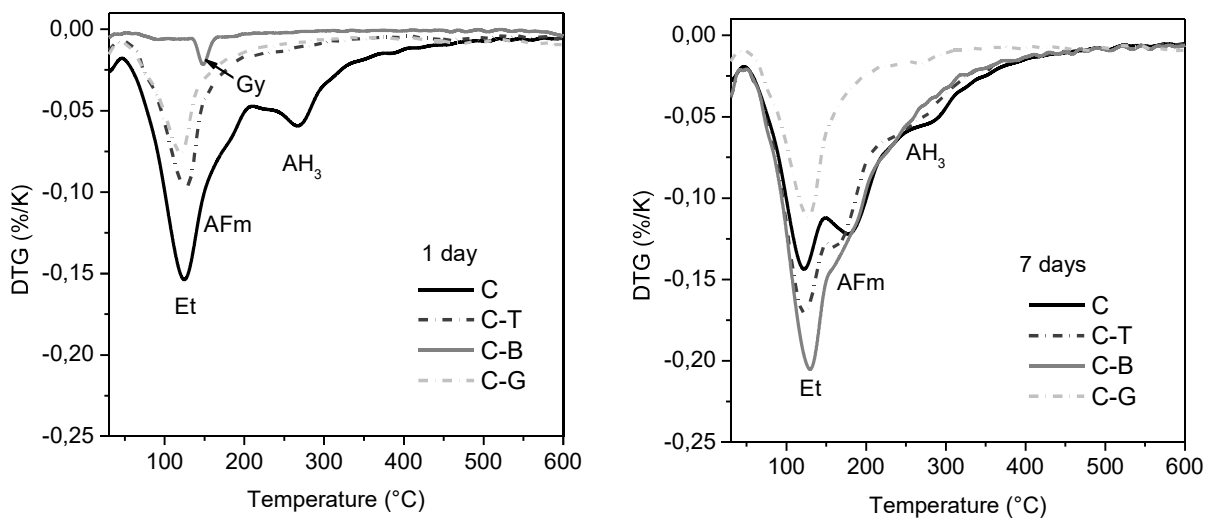


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Figure 5. Comparison of XRD plots for inves gated CAH cements

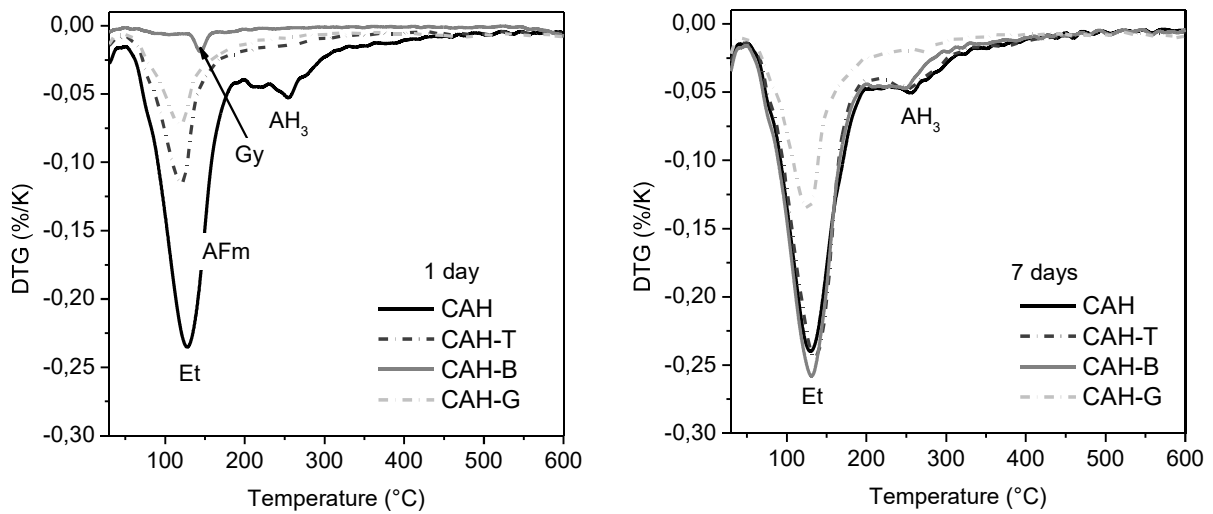
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686 Figure 6. Comparison of the DTG plots at 1 and 7 days for the C samples (Et – e ringite, AFm – monophases and
687 strätlingite, AH₃ – aluminium hydroxide, Gy - gypsum

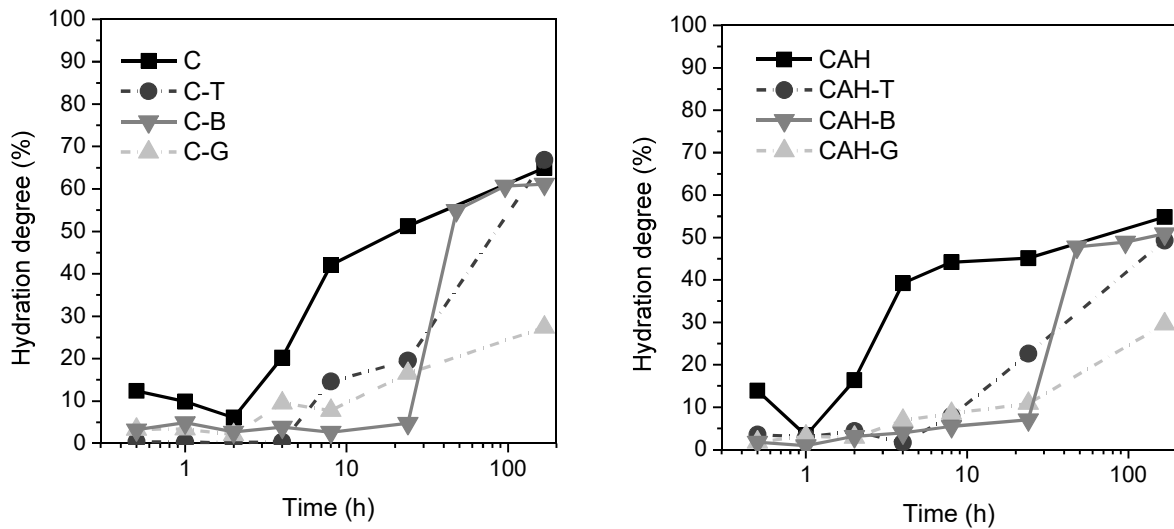
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689 **Figure 7. Comparison of the DTG plots at 1 and 7 days for the CAH samples (Et – e**
 690 **ringite, AFm – monophases and strätlingite, AH₃ – aluminium hydroxide, Gy - gypsum).**

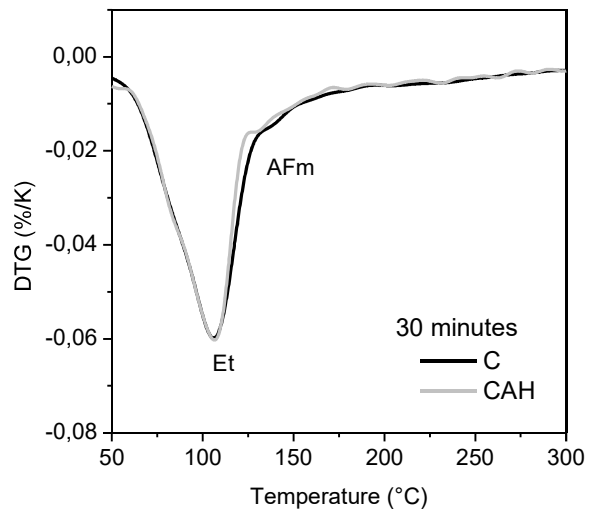
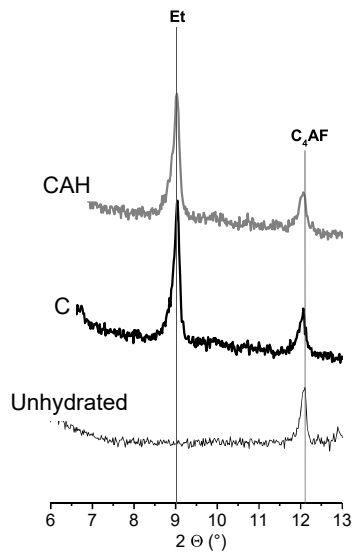
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693 **Figure 8. Hydration degree of cement clinker calculated as a sum of dissolution degrees of clinker minerals**
 694 **(C₄A₃S₃+C₂S+C₄AF+C₂F+CA). Calculations are based on the Rietveld analysis of the XRD measurements (Error!**
 695 **Reference source not found. and Error! Reference source not found.).**

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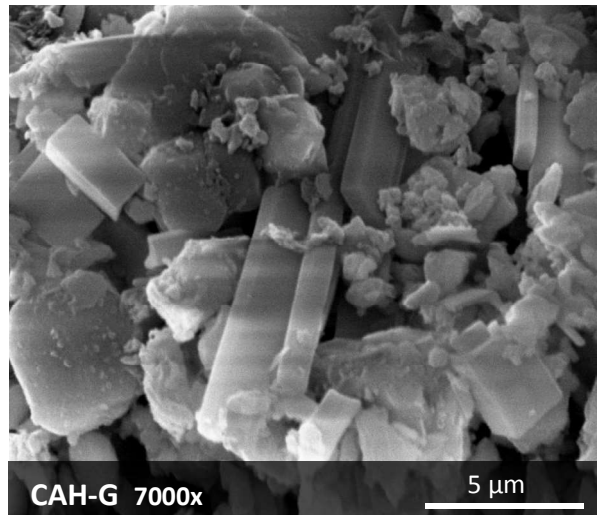
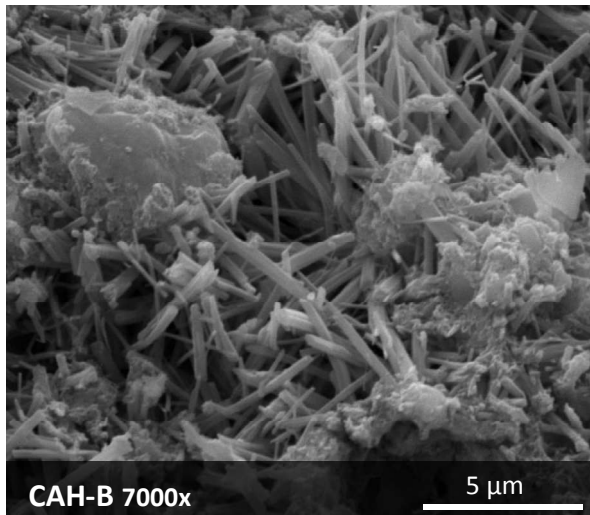
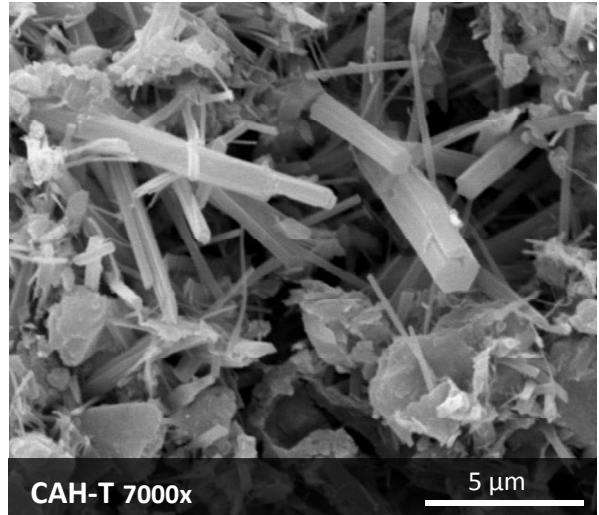
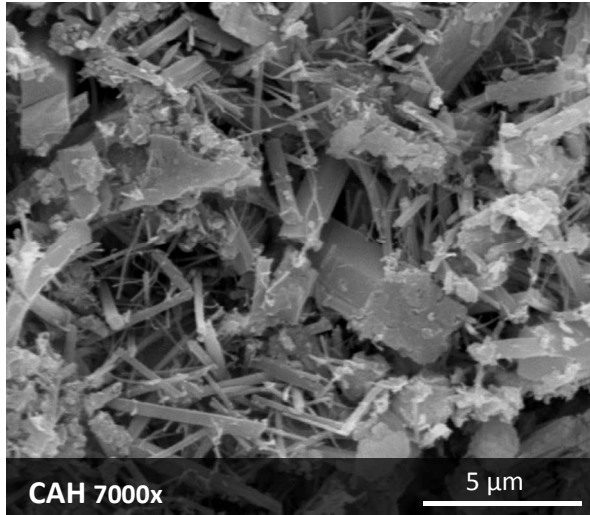
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Figure 9. DTG and XRD data for C and CAH samples after 30 minutes of hydration.

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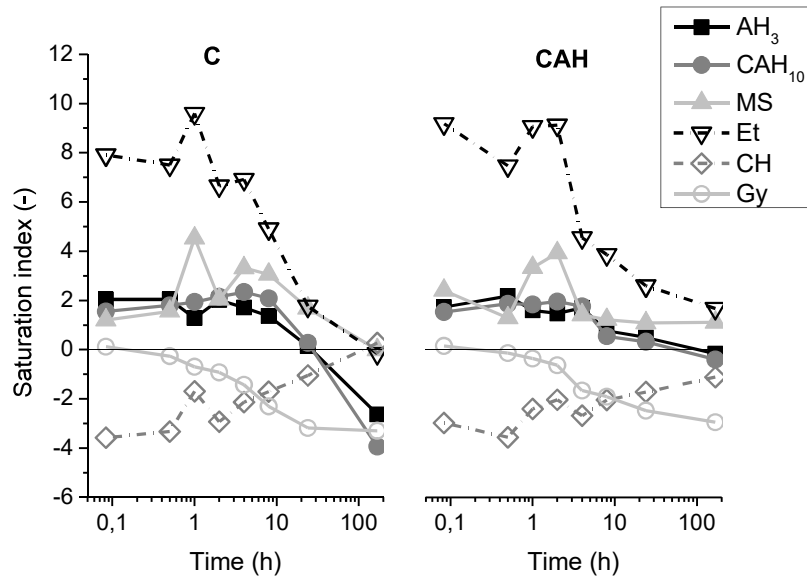
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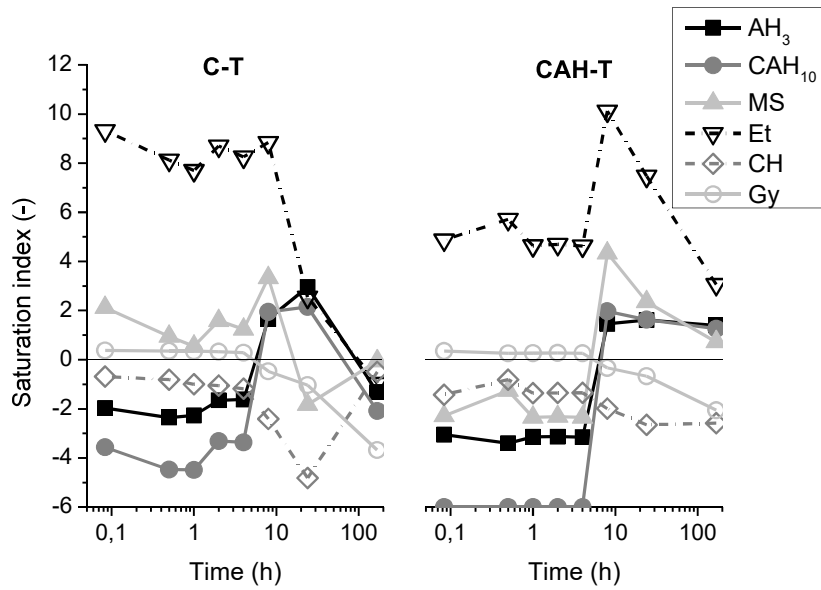
Figure 10. SEM images of fractured surfaces after 1 day of hydration (W/C of 0.5).



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Figure 11. Saturation indices calculated from the pore solution concentrations of C and CAH sample.



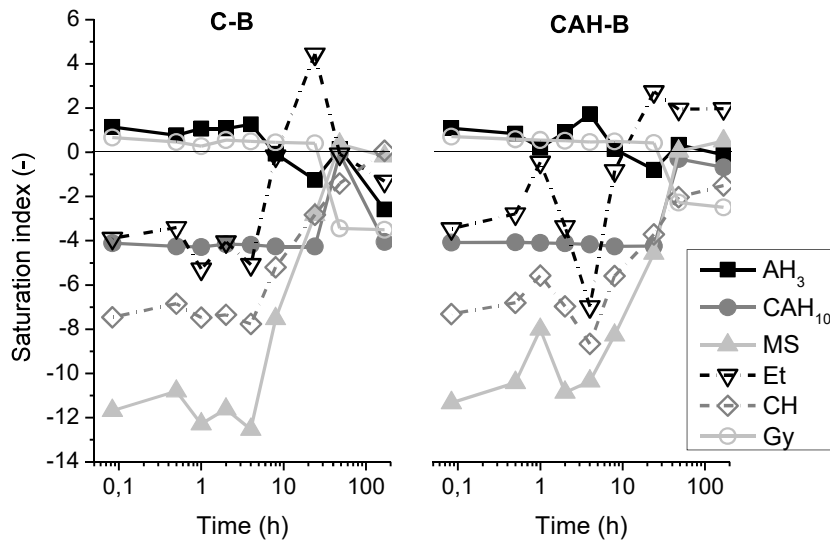
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Figure 12. Saturation indices calculated from the pore solution chemistry of C-T and CAH-T samples. If the concentration of Al was not measurable, the detection limit of 0.01 mmol/l was used for the calculations. The effect of tartrate was neglected.

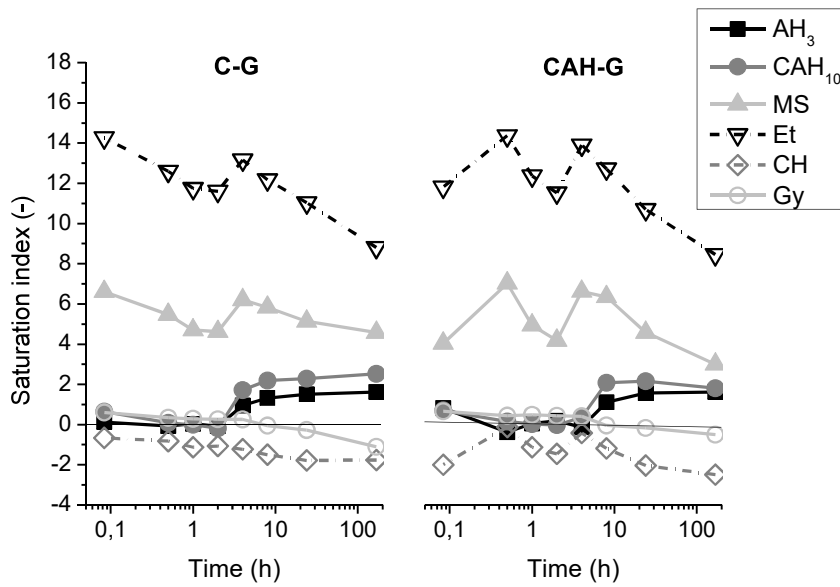


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Figure 13. Saturation indices calculated from the pore solution chemistry of C-B and CAH-B sample. If the concentration of Al was not measurable, the detection limit of 0.01 mmol/l was used for calculations.

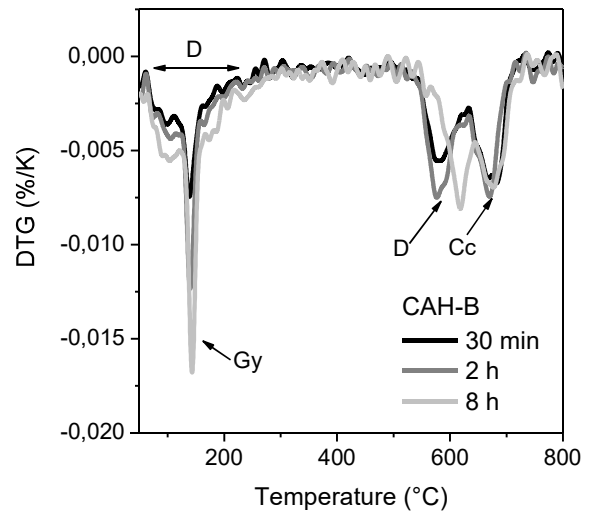
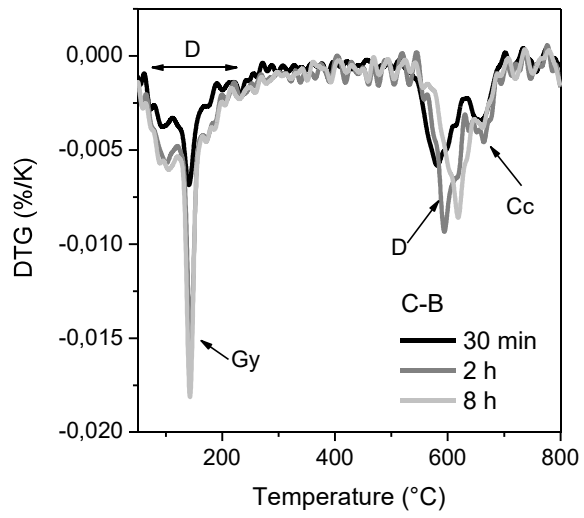


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Figure 14. Saturation indices calculated from the pore solution chemistry of C-G and CAH-G sample. If the concentration of Al was not measurable, the detection limit of 0.01 mmol/l was used for calculations.



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Figure 15. DTG curves of C-B and CAH-B at early mes, D – Dawsonite.

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