

The Discontinuous Galerkin method for coastal ocean modeling

Balthasar Reuter, Vadym Aizinger

Applied Mathematics I, Friedrich-Alexander-University Erlangen-Nürnberg

2016-12-09



Outline

Model

Application to the Lena delta

Model



3D shallow water equations

System of hydrostatic primitive equations with free surface

Free surface elevation
$$\partial_t \xi + \nabla_{xy} \cdot \int_z^\xi \mathbf{u}_{xy} d\tilde{z} = 0,$$

Continuity equation
$$\nabla \cdot \mathbf{u} = 0,$$

Momentum equations in conservative form

$$\partial_t \mathbf{u}_{xy} + \nabla \cdot (\mathbf{u}_{xy} \otimes \mathbf{u}) - \partial_z (\nu_t \partial_z \mathbf{u}_{xy}) + g \nabla_{xy} (\xi + \frac{1}{\rho_0} \int_z^\xi \rho d\tilde{z}) - f_c \mathbf{e}_z \times \mathbf{u}_{xy} = \mathbf{f}_u,$$

Transport equation(s) for temperature / salinity
$$\partial_t r + \nabla \cdot (\mathbf{u} r) - \partial_z (\nu_r \partial_z r) = f_r \quad \text{for } r \in \{s, \theta\},$$

Transport equation(s)¹ for turbulence variables
$$\partial_t m - \partial_z (\nu_m \partial_z m) = f_m \left(\|\partial_z \mathbf{u}_{xy}\|^2, \partial_z \rho \right) \quad \text{for } m \in \{k, \psi\}.$$

ξ – free surface elevation,	$\nabla_{xy} = (\partial_x, \partial_y)$	f – body forces,
$\mathbf{u} = (u, v, w)$ – velocity,	$\mathbf{u}_{xy} = (u, v),$	ν – eddy viscosity coefficients,
θ – temperature,	$\mathbf{e}_z = (0, 0, 1),$	$\rho = \rho(\theta, s)$ – density (equation of state),
s – salinity,	g – gravity constant,	f_c – Coriolis coefficient.

¹Umlauf, Burchard (2003), doi:10.1357/002224003322005087

3D shallow water equations

System of hydrostatic primitive equations with free surface

Free surface elevation

$$\partial_t \xi + \nabla_{xy} \cdot \int_z^\xi \mathbf{u}_{xy} d\tilde{z} = 0,$$

Continuity equation

$$\nabla \cdot \mathbf{u} = 0,$$

Barotropic model

Momentum equations in conservative form

$$\partial_t \mathbf{u}_{xy} + \nabla \cdot (\mathbf{u}_{xy} \otimes \mathbf{u}) - \partial_z (\nu_t \partial_z \mathbf{u}_{xy}) + g \nabla_{xy} (\xi + \cancel{\frac{1}{\rho_0} \int_z^\xi \rho d\tilde{z}}) - f_c \mathbf{e}_z \times \mathbf{u}_{xy} = \mathbf{f}_u,$$

Transport equation(s) for temperature / salinity

$$\partial_t r + \nabla \cdot (\mathbf{u} r) - \partial_z (\nu_r \partial_z r) = f_r \quad \text{for } r \in \{s, \theta\},$$

Transport equation(s)¹ for turbulence variables $\partial_t m - \partial_z (\nu_m \partial_z m) = f_m \left(\|\partial_z \mathbf{u}_{xy}\|^2, \partial_z \rho \right) \quad \text{for } m \in \{k, \psi\}.$

ξ – free surface elevation, $\nabla_{xy} = (\partial_x, \partial_y)$

$\mathbf{u} = (u, v, w)$ – velocity, $\mathbf{u}_{xy} = (u, v),$

θ – temperature, $\mathbf{e}_z = (0, 0, 1),$

s – salinity,

g – gravity constant, f_c – Coriolis coefficient.

$f.$ – body forces,

$\nu.$ – eddy viscosity coefficients,

$\rho = \rho(\theta, s)$ – density (equation of state),

¹Umlauf, Burchard (2003), doi:10.1357/002224003322005087

3D shallow water equations

System of hydrostatic primitive equations with free surface

Free surface elevation
$$\partial_t \xi + \nabla_{xy} \cdot \int_z^\xi \mathbf{u}_{xy} d\tilde{z} = 0,$$

Continuity equation
$$\nabla \cdot \mathbf{u} = 0,$$

Baroclinic model

Momentum equations in conservative form

$$\partial_t \mathbf{u}_{xy} + \nabla \cdot (\mathbf{u}_{xy} \otimes \mathbf{u}) - \partial_z (\nu_t \partial_z \mathbf{u}_{xy}) + g \nabla_{xy} (\xi + \frac{1}{\rho_0} \int_z^\xi \rho d\tilde{z}) - f_c \mathbf{e}_z \times \mathbf{u}_{xy} = \mathbf{f}_u,$$

Transport equation(s) for temperature / salinity
$$\partial_t r + \nabla \cdot (\mathbf{u} r) - \partial_z (\nu_r \partial_z r) = f_r \quad \text{for } r \in \{s, \theta\},$$

Transport equation(s)¹ for turbulence variables
$$\partial_t m - \partial_z (\nu_m \partial_z m) = f_m \left(\|\partial_z \mathbf{u}_{xy}\|^2, \partial_z \rho \right) \quad \text{for } m \in \{k, \psi\}.$$

ξ – free surface elevation,	$\nabla_{xy} = (\partial_x, \partial_y)$	f – body forces,
$\mathbf{u} = (u, v, w)$ – velocity,	$\mathbf{u}_{xy} = (u, v),$	ν – eddy viscosity coefficients,
θ – temperature,	$\mathbf{e}_z = (0, 0, 1),$	$\rho = \rho(\theta, s)$ – density (equation of state),
s – salinity,	g – gravity constant,	f_c – Coriolis coefficient.

¹Umlauf, Burchard (2003), doi:10.1357/002224003322005087

3D shallow water equations

System of hydrostatic primitive equations with free surface

Free surface elevation
$$\partial_t \xi + \nabla_{xy} \cdot \int_z^\xi \mathbf{u}_{xy} d\tilde{z} = 0,$$

Continuity equation
$$\nabla \cdot \mathbf{u} = 0,$$

Baroclinic model with turbulence

Momentum equations in conservative form

$$\partial_t \mathbf{u}_{xy} + \nabla \cdot (\mathbf{u}_{xy} \otimes \mathbf{u}) - \partial_z (\nu_t \partial_z \mathbf{u}_{xy}) + g \nabla_{xy} (\xi + \frac{1}{\rho_0} \int_z^\xi \rho d\tilde{z}) - f_c \mathbf{e}_z \times \mathbf{u}_{xy} = \mathbf{f}_u,$$

Transport equation(s) for temperature / salinity
$$\partial_t r + \nabla \cdot (\mathbf{u} r) - \partial_z (\nu_r \partial_z r) = f_r \quad \text{for } r \in \{s, \theta\},$$

Transport equation(s)¹ for turbulence variables
$$\partial_t m - \partial_z (\nu_m \partial_z m) = f_m \left(\|\partial_z \mathbf{u}_{xy}\|^2, \partial_z \rho \right) \quad \text{for } m \in \{k, \psi\}.$$

ξ – free surface elevation,	$\nabla_{xy} = (\partial_x, \partial_y)$	f – body forces,
$\mathbf{u} = (u, v, w)$ – velocity,	$\mathbf{u}_{xy} = (u, v),$	ν – eddy viscosity coefficients,
θ – temperature,	$\mathbf{e}_z = (0, 0, 1),$	$\rho = \rho(\theta, s)$ – density (equation of state),
s – salinity,	g – gravity constant,	f_c – Coriolis coefficient.

¹Umlauf, Burchard (2003), doi:10.1357/002224003322005087

UTBEST3D⁶

- ▶ Physics:
 - ▷ **Baroclinic** or **barotropic** system
 - ▷ **Wetting/drying**
 - ▷ **Vertical eddy viscosity**: algebraic, 1st, and 2nd order closures
- ▶ Numerics²:
 - ▷ up to 2nd order **discontinuous Galerkin** approx. in space and up to 3rd in time
 - ▷ Non-conforming **prismatic meshes**
 - ▷ Local mesh and space refinement (**hp-adaptivity**)
 - ▷ Individual choice of discretization for each unknown
 - ▷ **Riemann solvers**: Lax-Friedrichs, Roe's, HLL, HLLC
 - ▷ **Slope limiters**: Vertex-based³
- ▶ Written in C++, **parallelized** with MPI and OpenMP
- ▶ Domain partitioning with METIS⁴
- ▶ **Scalable** and **portable**⁵: runs on x86, Power, ARM

²Dawson, Aizinger (2005), doi:10.1007/s10915-004-4139-3 — Aizinger, Dawson (2007), doi:10.1016/j.cma.2006.04.010

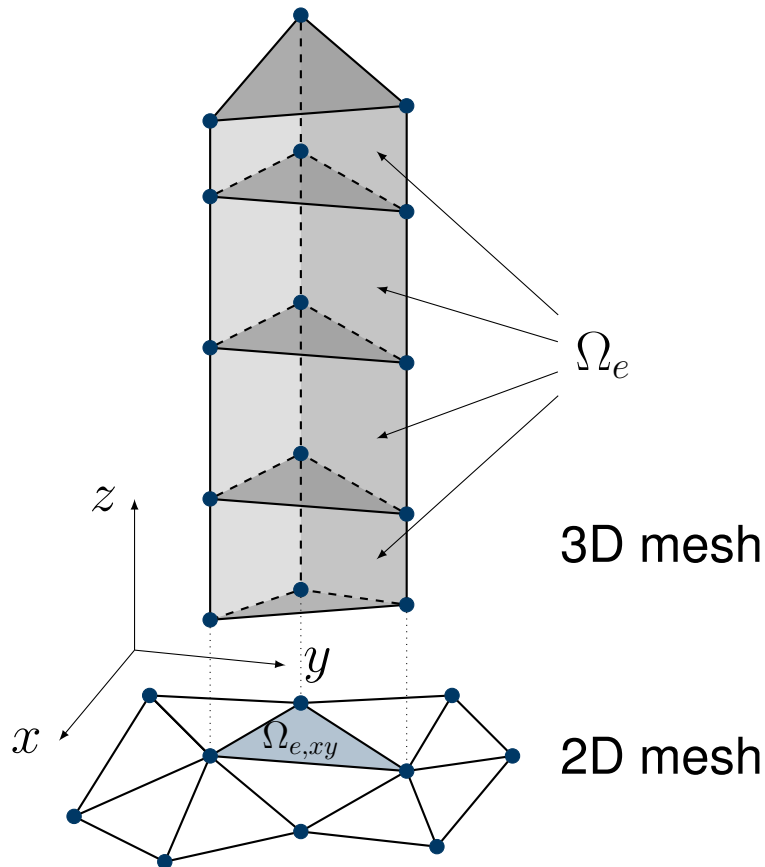
³Aizinger (2011), doi:10.1007/978-3-642-17770-5_16 — Kuzmin (2010), doi:10.1016/j.cam.2009.05.028

⁴Karypis, Kumar (1999), doi:10.1137/S1064827595287997

⁵Reuter, Aizinger, Köstler (2015), doi:10.1016/j.compfluid.2015.05.020

⁶<https://math.fau.de/utbest3d>

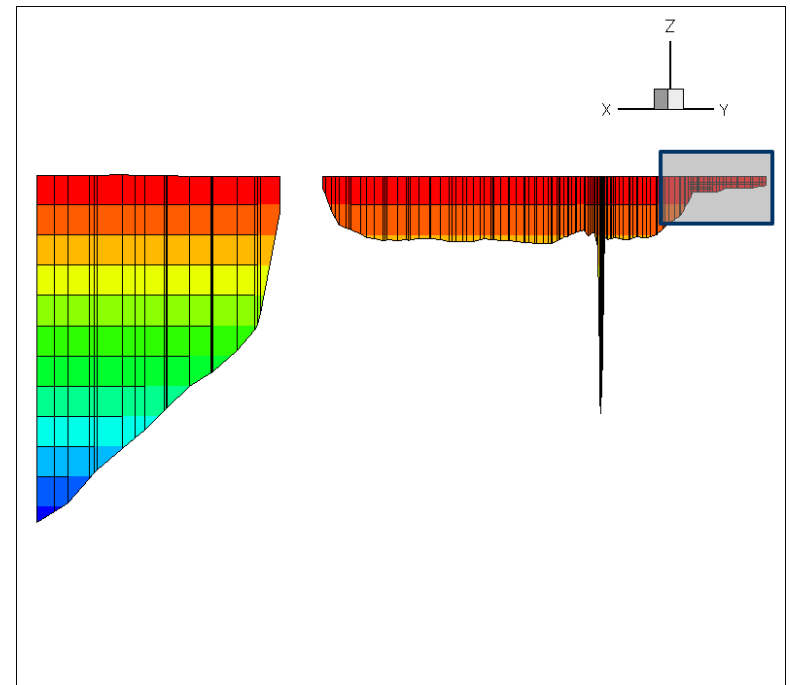
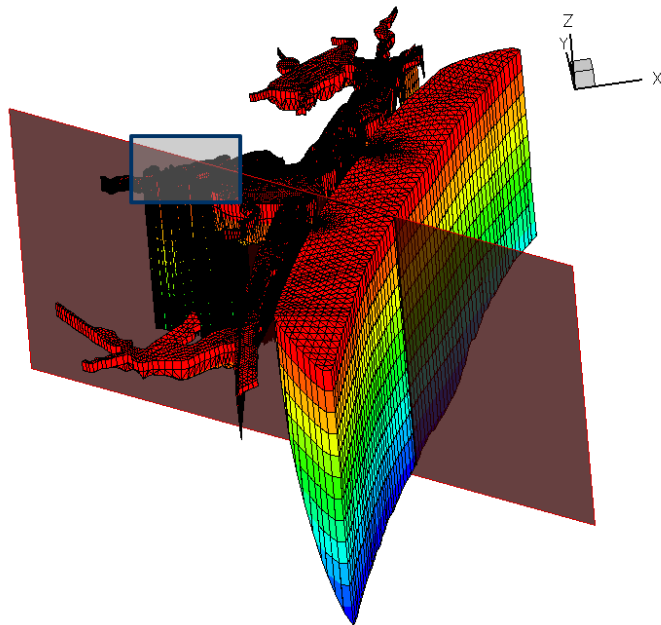
Mesh



- ▶ Input data: 2D **triangulation** with **bathymetry** at nodes
- ▶ 3D mesh: columns of **prismatic elements** aligned with 2D elements
- ▶ **Non-parallel** faces on top and bottom
- ▶ Dynamic **merging/unmerging** of thin elements
- ▶ Different layer structure in subdomains possible

Dynamic merging and subdomains: Corpus Christi Bay circulation I

- Area of interest: **Nueces Bay**, max. depth 2m
- 12 vertical layers. Layer thickness in Nueces Bay: 0.16m, outside: 2m

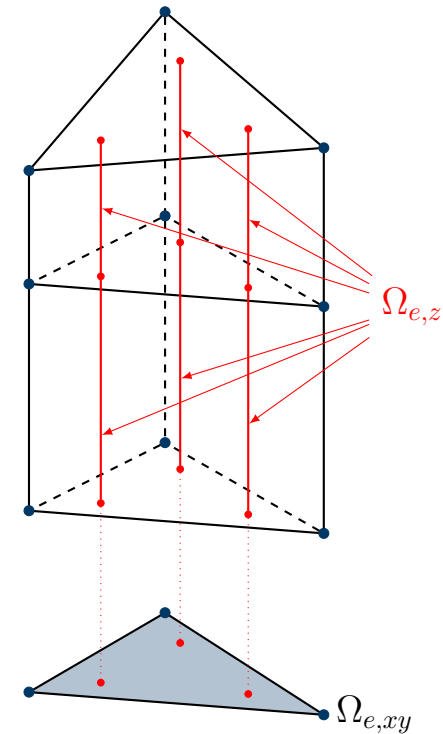


Dynamic merging and subdomains: Corpus Christi Bay circulation II

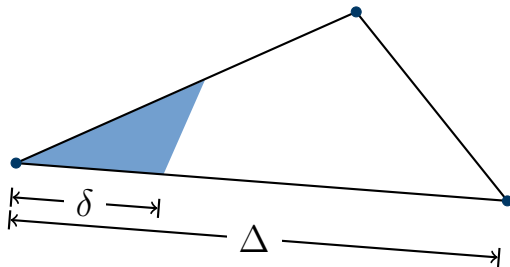
- ▶ Nueces bay mesh: 12 x 0.16m layers. Global mesh: 12 x 2m layers

Segments for turbulence variables

- ▶ Vertical **segments** aligned with 2D quadrature points.
- ▶ Turbulence quantities are **1D variables**



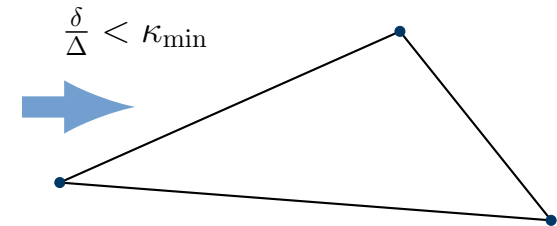
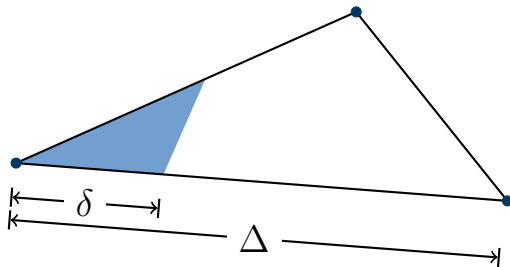
Wetting / Drying



Traditionally: two approaches

1. Partially wet elements
 - ▷ Dry elements contain **some water**
or
 - ▷ Wet elements with **dry areas**
2. Split cells: elements subdivided into wet and dry parts

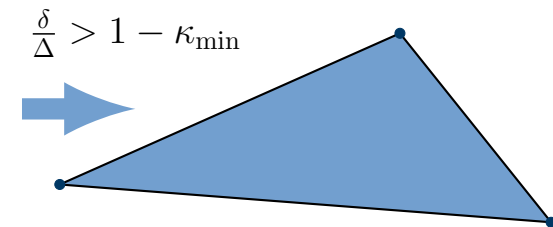
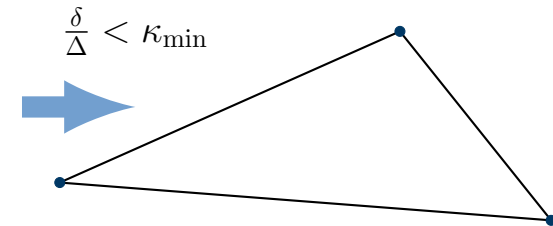
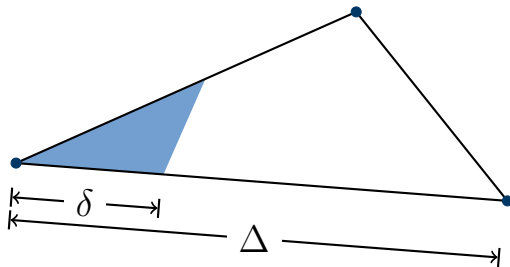
Wetting / Drying



Traditionally: two approaches

1. Partially wet elements
 - ▷ Dry elements contain **some water**
or
 - ▷ Wet elements with **dry areas**
2. Split cells: elements subdivided into wet and dry parts

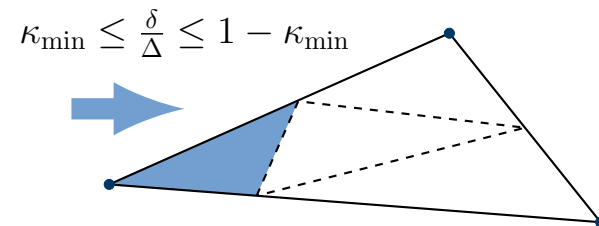
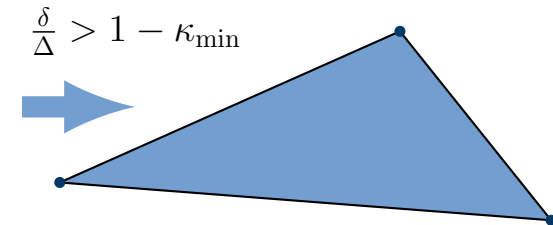
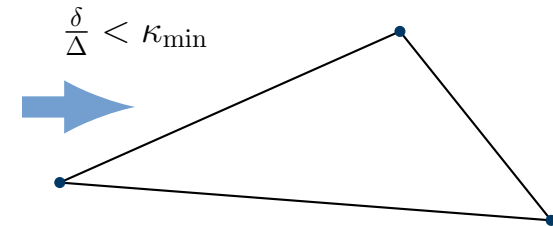
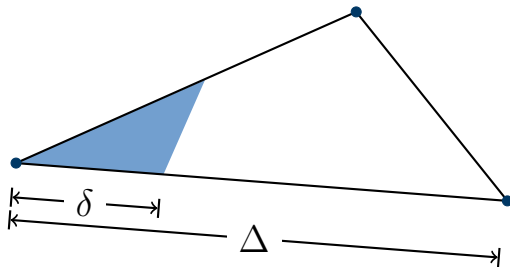
Wetting / Drying



Traditionally: two approaches

1. Partially wet elements
 - ▷ Dry elements contain **some water**
or
 - ▷ Wet elements with **dry areas**
2. Split cells: elements subdivided into wet and dry parts

Wetting / Drying



Traditionally: two approaches

1. Partially wet elements
 - ▷ Dry elements contain **some water** or
 - ▷ Wet elements with **dry areas**
2. Split cells: elements subdivided into wet and dry parts

Dam Break

Piecewise constant approximation

Dam Break

Piecewise linear approximation

Application to the Lena delta



Lena delta - problem setting (1)

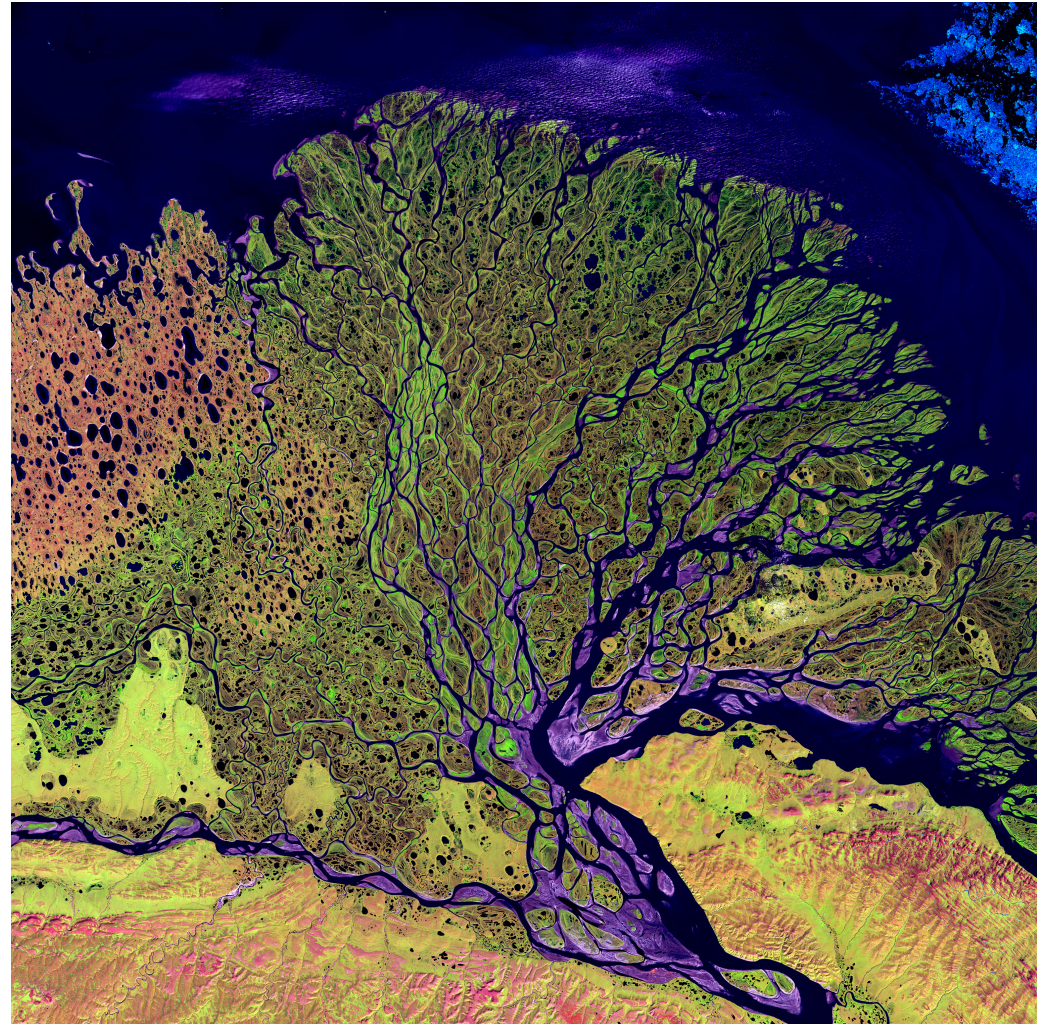
- ▶ Joint work with **Vera Fofonova (Alfred Wegener Institute, Bremerhaven)** and **Tony Ying**
- ▶ Second largest river discharging in the Arctic Ocean
- ▶ Substantial impact in the context of climate change



Lena delta - problem setting (2)

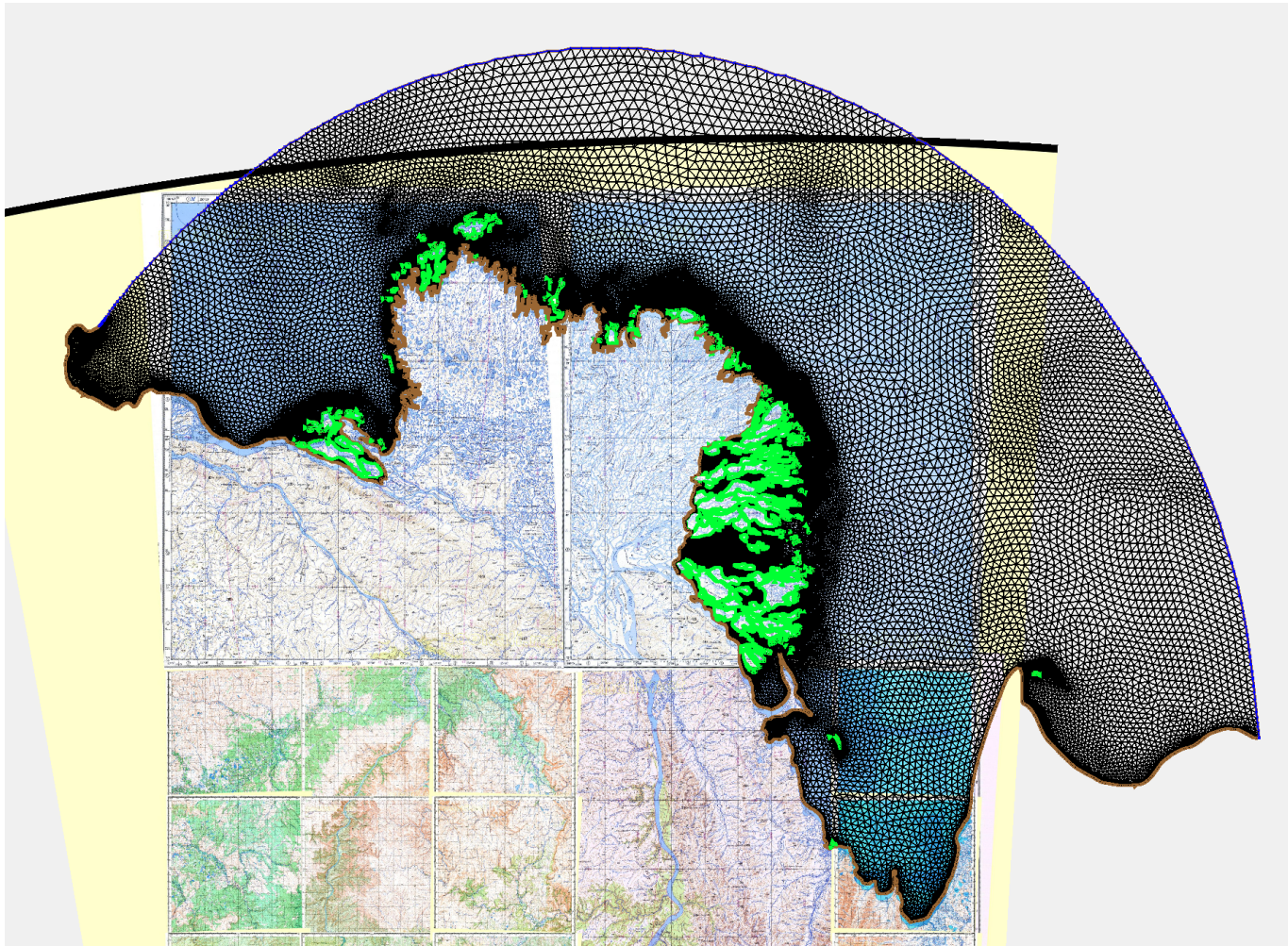
- ▶ Highly complex delta geometry
- ▶ A number of unique physical processes and characteristics
- ▶ Sensitive environmental system
- ▶ New study object for 3D numerical modeling

Image: NASA Landsat



Lena delta - data challenge (1)

Main bathymetry data source for the delta: **soviet military topographic maps.**



Lena delta - first results (1)

Lena delta - first results (2)

Take home messages

- ▶ **UTBEST3D**, a numerical solver for the primitive hydrostatic equations
- ▶ Hierarchical physical model
- ▶ **Lena delta** as challenging study object for numerical modeling

Take home messages

- ▶ **UTBEST3D**, a numerical solver for the primitive hydrostatic equations
- ▶ Hierarchical physical model
- ▶ **Lena delta** as challenging study object for numerical modeling

Thank you for your attention!

`https://math.fau.de/utbest3d
{reuter, aizinger}@math.fau.de`

Appendix



LDG-Discretization

Exemplary for transport equations

Mixed formulation⁷

$$\begin{aligned}\partial_t r + \nabla \cdot (\mathbf{u}r) - \partial_z(\nu_r q_r) &= f_r \\ q_r &= \partial_z r.\end{aligned}$$

Weak formulation

$$\begin{aligned}\int_{\Omega_e} \partial_t r \varphi_r \, d\mathbf{x} + \int_{\partial\Omega_e} \left(\widehat{(\mathbf{u}r)} \cdot \mathbf{n} + \widehat{\nu_r q_r n_z} \right) \varphi_r \, d\mathbf{s} - \\ \int_{\Omega_e} \left((\mathbf{u}r) \cdot \nabla + \nu_r q_r \partial_z \right) \varphi_r \, d\mathbf{x} &= \int_{\Omega_e} f_r \varphi_r \, d\mathbf{x} \\ \int_{\Omega_e} q_r \lambda_r \, d\mathbf{x} &= \int_{\partial\Omega_e} \widehat{r n_z} \lambda_r \, d\mathbf{s} - \int_{\Omega_e} r \partial_z \lambda_r \, d\mathbf{x},\end{aligned}$$

with $\mathbf{n} = (n_x, n_y, n_z)$ exterior unit normal to $\partial\Omega_e$, and test functions $\varphi_r, \lambda_r \in H^1(\Omega_e)$.

Choose fluxes and approximate Riemann solvers⁸

Local basis representation

$$r_h(t, \mathbf{x}) = \sum_i R_i(t) \phi_{r,i}(\mathbf{x}), \quad q_{r,h}(t, \mathbf{x}) = \sum_i Q_{r,i}(t) \phi_{q_r,i}(\mathbf{x}).$$

Test with $\phi_{r,i}, \phi_{q_r,i}$ and build linear system of equations

⁷Cockburn, Shu (1998), doi:10.1137/S0036142997316712

⁸Dawson, Aizinger (2005), doi:10.1007/s10915-004-4139-3

Discretization of the primitive continuity equation⁹

$$\partial_t h + \nabla_{xy} \cdot \int_{z_b}^{\xi} \mathbf{u}_{xy} d\tilde{z} = 0$$

2D form of weak formulation

$$\int_{\Omega_{e,xy}} \partial_t h \varphi_h dx dy + \int_{\partial\Omega_{e,xy}} \int_{z_b}^{\xi} \mathbf{u}_{xy} dz \cdot \mathbf{n} \varphi_h d\mathbf{s} - \int_{\Omega_{e,xy}} \int_{z_b}^{\xi} \mathbf{u}_{xy} dz \cdot \nabla_{xy} \varphi_h dx dy = 0$$

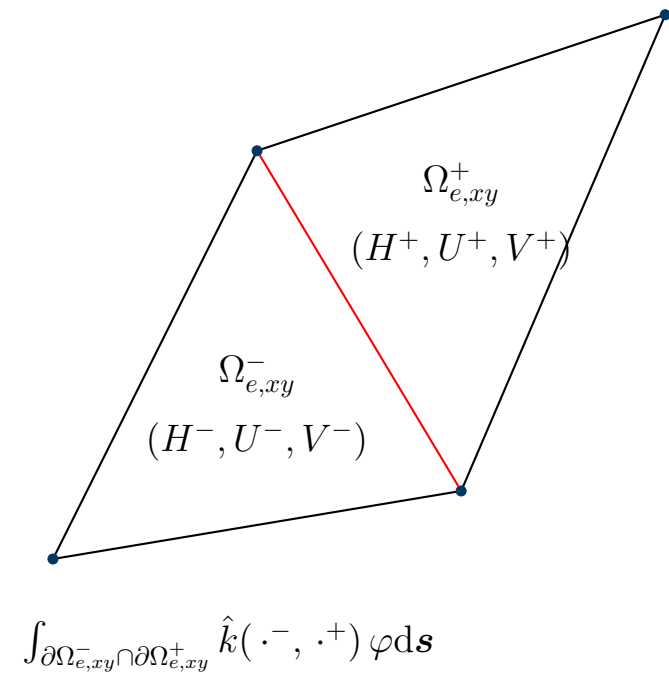
3D form of weak formulation

$$\int_{\Omega_{e,xy}} \partial_t h \varphi_h dx dy + \sum_{\Pi_{xy}\Omega_e = \Omega_{e,xy}} \int_{\partial\Omega_{e,lat}} \mathbf{u}_{xy} \cdot \mathbf{n} \varphi_h d\mathbf{s} - \sum_{\Pi_{xy}\Omega_e = \Omega_{e,xy}} \int_{\Omega_e} \mathbf{u}_{xy} \cdot \nabla_{xy} \varphi_h d\mathbf{x} = 0$$

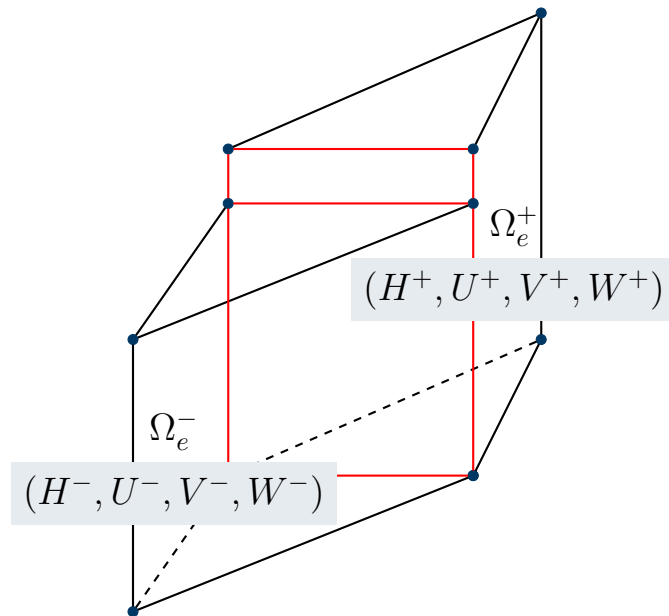
with $\Omega_{e,lat}$ lateral boundary of Ω_e .

⁹Aizinger (2004), PhD Dissertation, UT Austin

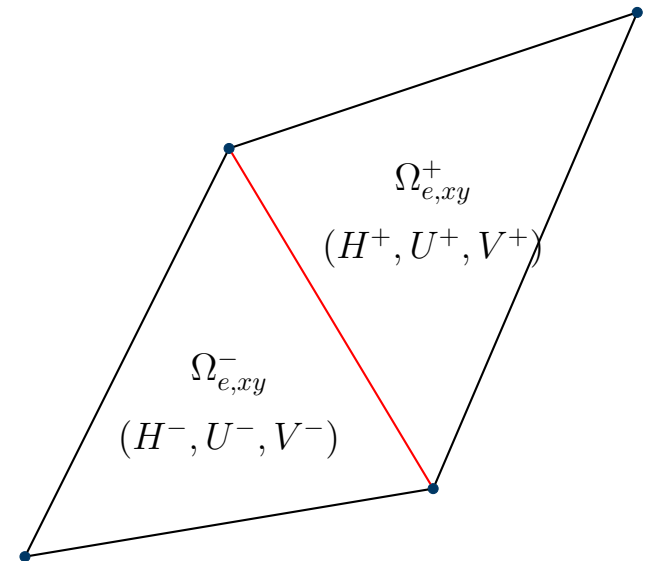
Riemann problem in 3D



Riemann problem in 3D

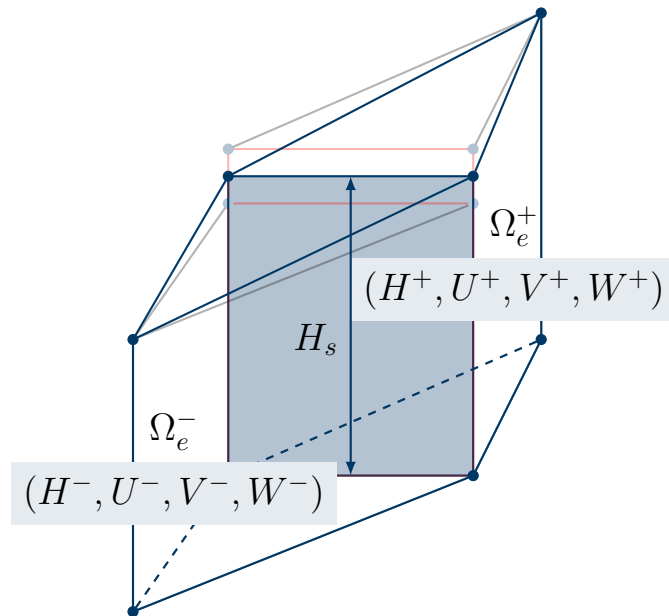


$$\int_{\partial\Omega_e^- \cap \partial\Omega_e^+} \hat{k}(\cdot^-, \cdot^+) \varphi d\mathbf{s}$$

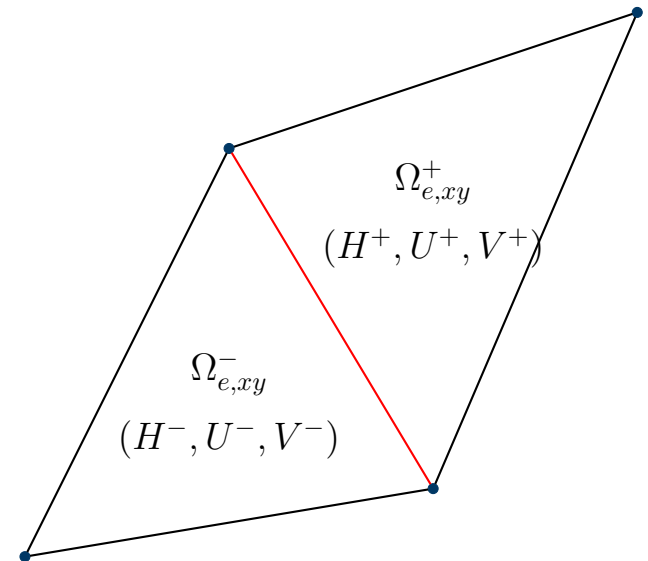


$$\int_{\partial\Omega_{e,xy}^- \cap \partial\Omega_{e,xy}^+} \hat{k}(\cdot^-, \cdot^+) \varphi d\mathbf{s}$$

Riemann problem in 3D



$$\int_{\partial\Omega_e^- \cap \partial\Omega_e^+} \hat{k}(\cdot^-, \cdot^+) \varphi ds$$



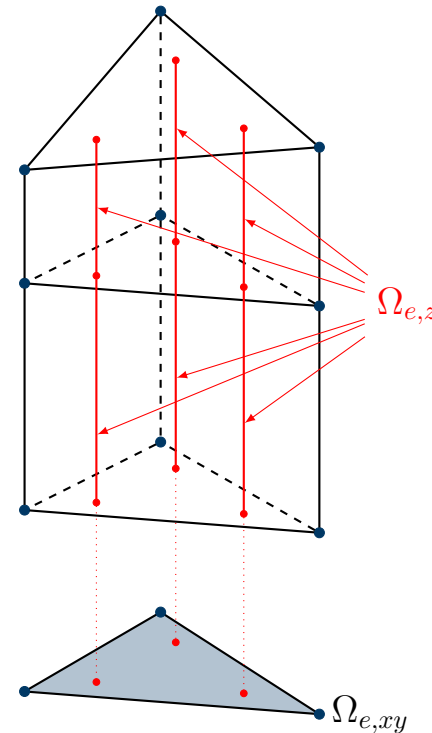
$$\int_{\partial\Omega_{e,xy}^- \cap \partial\Omega_{e,xy}^+} \hat{k}(\cdot^-, \cdot^+) \varphi ds$$

Discretization of turbulence transport equations

Vertical **segments** aligned with 2D quadrature points.

Mixed formulation

$$\begin{aligned}\partial_t m - \partial_z(\nu_m q_m) &= f_m \\ f_m &= \partial_z m.\end{aligned}$$

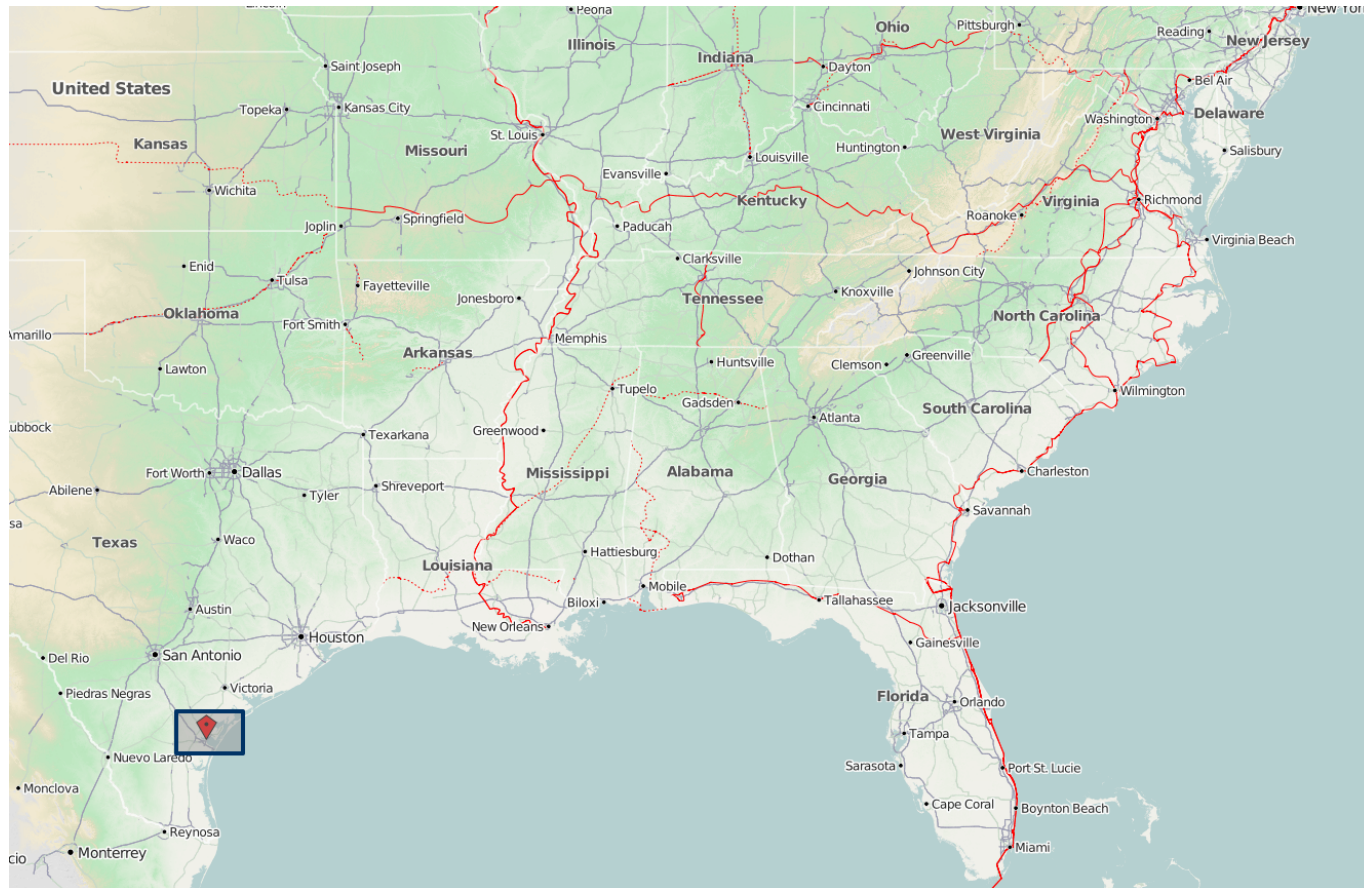


Weak formulation

$$\begin{aligned}\int_{\Omega_{e,z}} \partial_t m \varphi_m \, dz + (\nu_m q_m n_z \varphi_m) \Big|_{\partial\Omega_{e,z}} - \int_{\Omega_{e,z}} \nu_m q_m \partial_z \varphi_m \, dz &= \int_{\Omega_{e,z}} f_m \varphi_m \, dz \\ \int_{\Omega_{e,z}} q_m \lambda_m \, dz &= (m n_z \lambda_m) \Big|_{\partial\Omega_{e,z}} - \int_{\Omega_{e,z}} m \partial_z \lambda_m \, dz,\end{aligned}$$

with $\mathbf{n} = (0, 0, n_z)$ exterior unit normal to $\partial\Omega_{e,z}$, and test functions $\varphi_m, \lambda_m \in H^1(\Omega_{e,z})$.

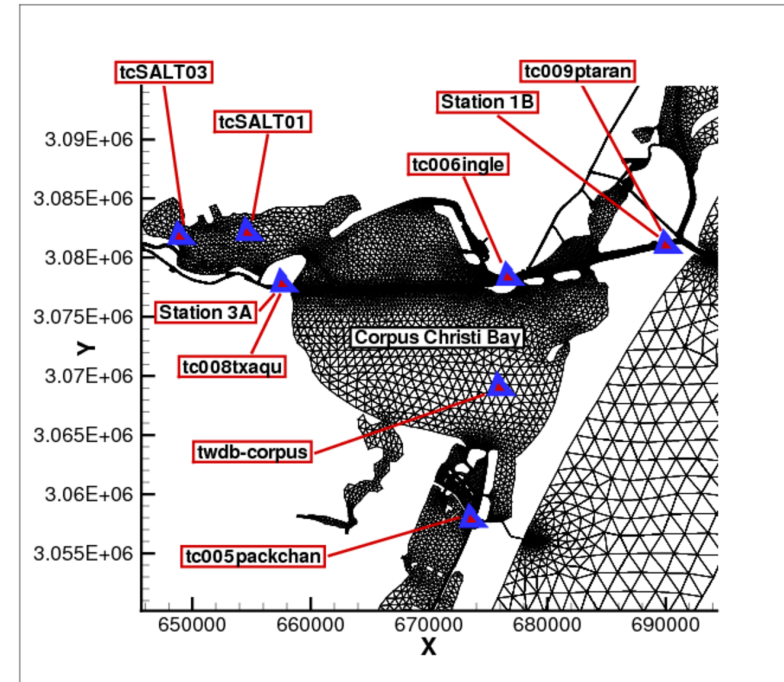
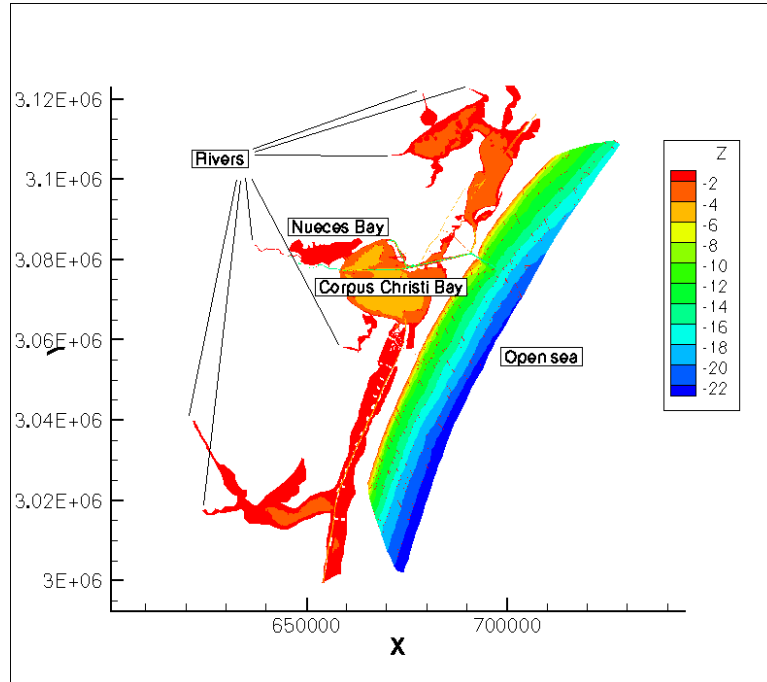
Corpus Christi Bay circulation I



<http://openstreetmap.de/karte.html?zoom=6&lat=33.97063&lon=-90.05908&layers=0B00TT>

Corpus Christi Bay circulation¹⁰ II

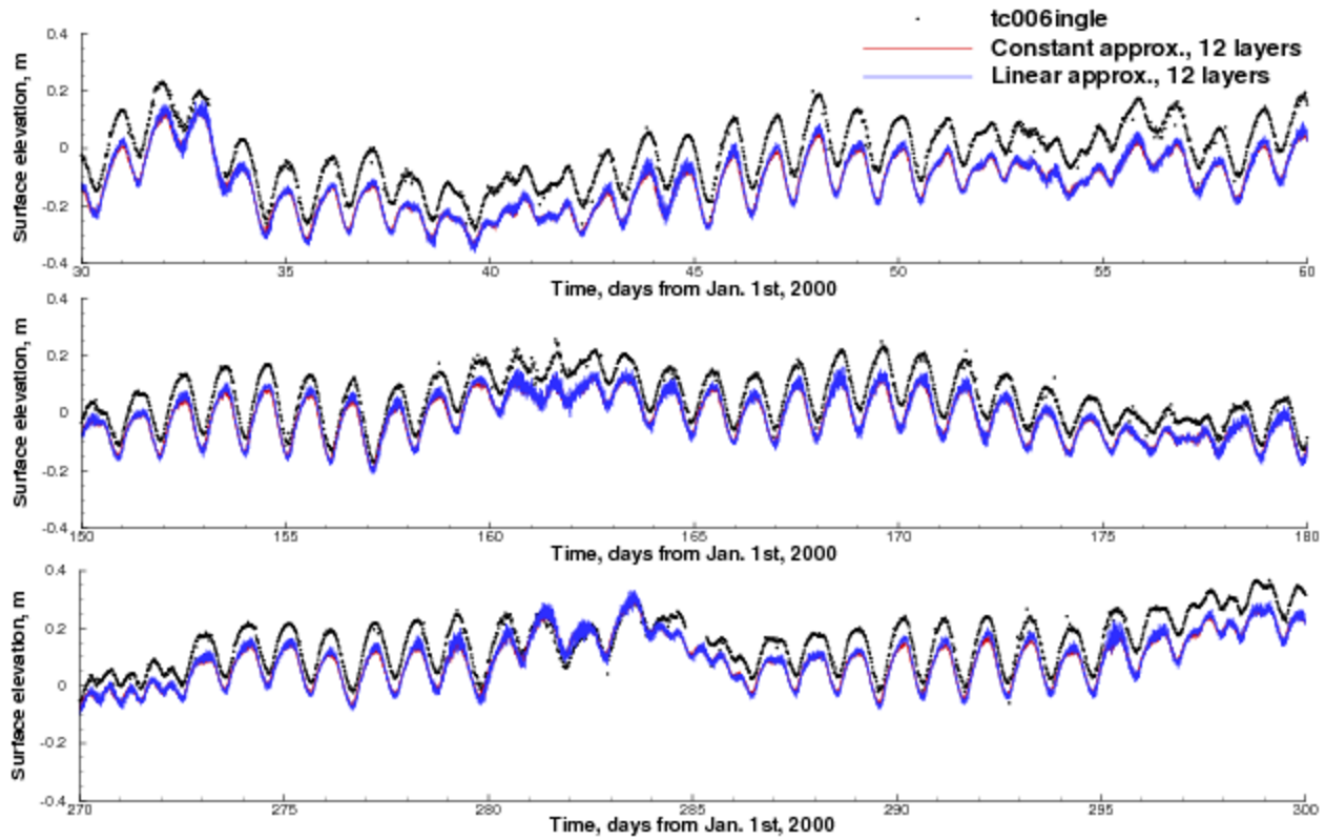
- ▶ Texas Water Development Board (TWDB) initiated **environmental study**.
- ▶ Specified river inflows, wind, precipitation, evaporation, open sea elevation and salinity for 2000-2001.
- ▶ Total of 18 **monitoring stations** for water elevation, velocity, salinity.



¹⁰Aizinger, Proft, Dawson, Pothina, Negusse (2013), doi:10.1007/s10236-012-0579-8

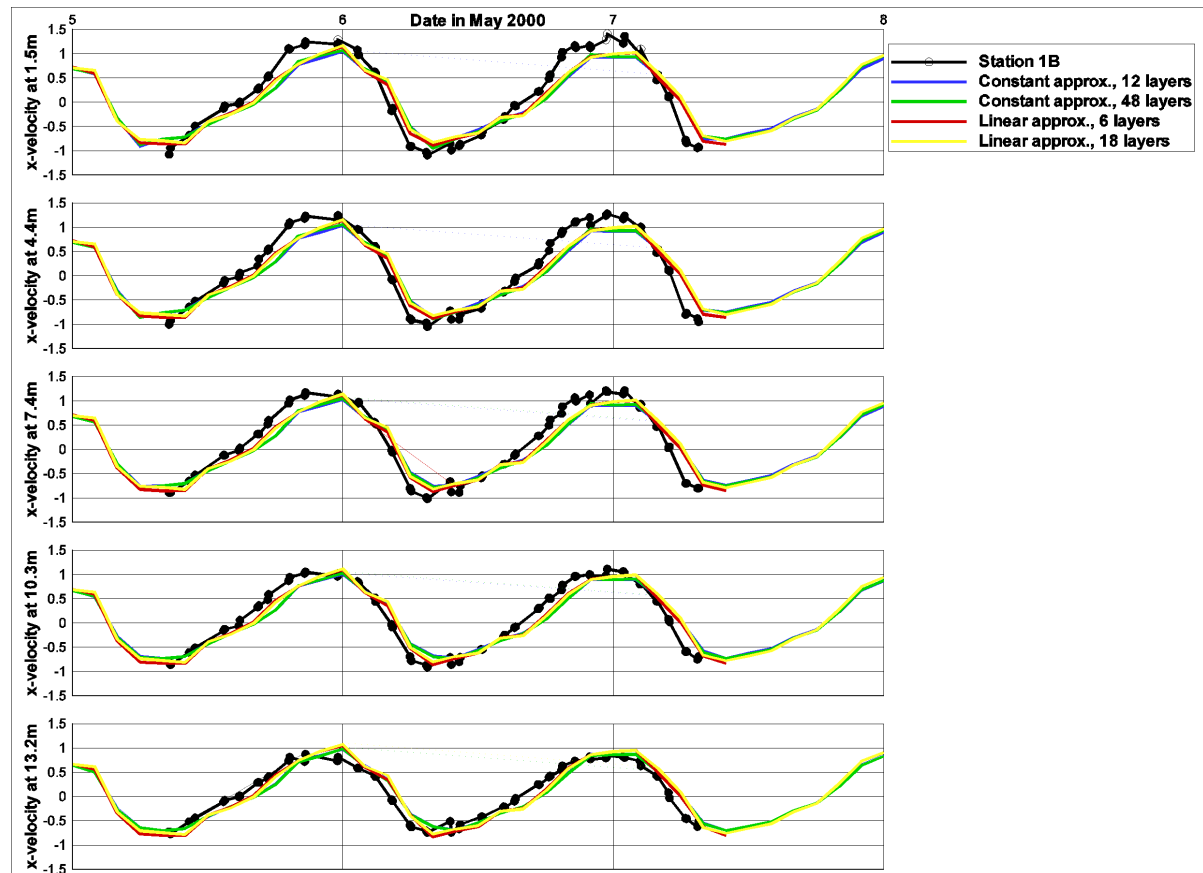
Corpus Christi Bay circulation V

- Elevation station tc006 Ingleside



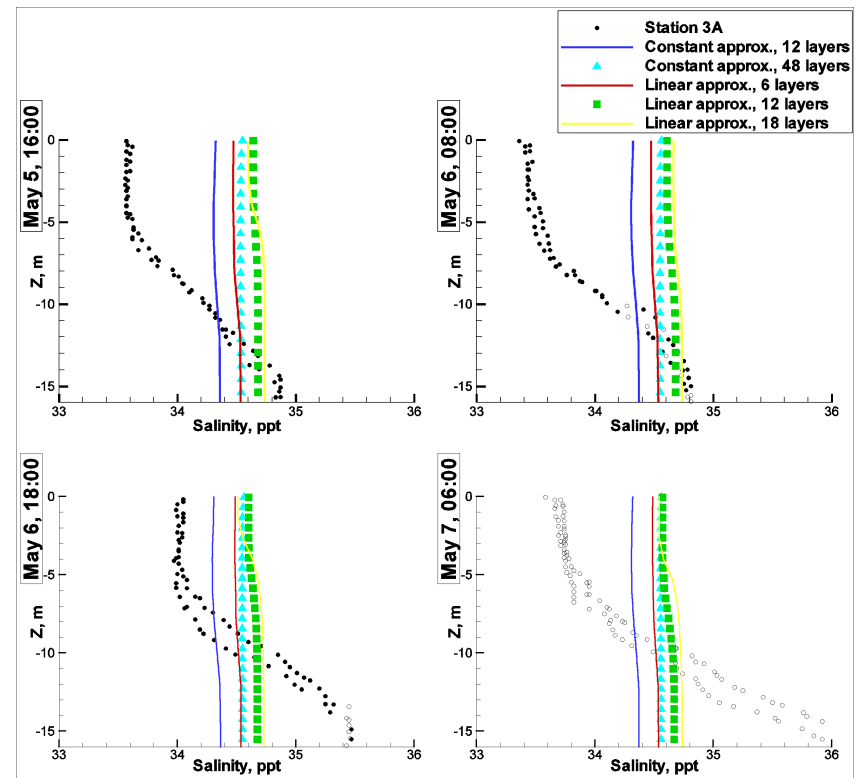
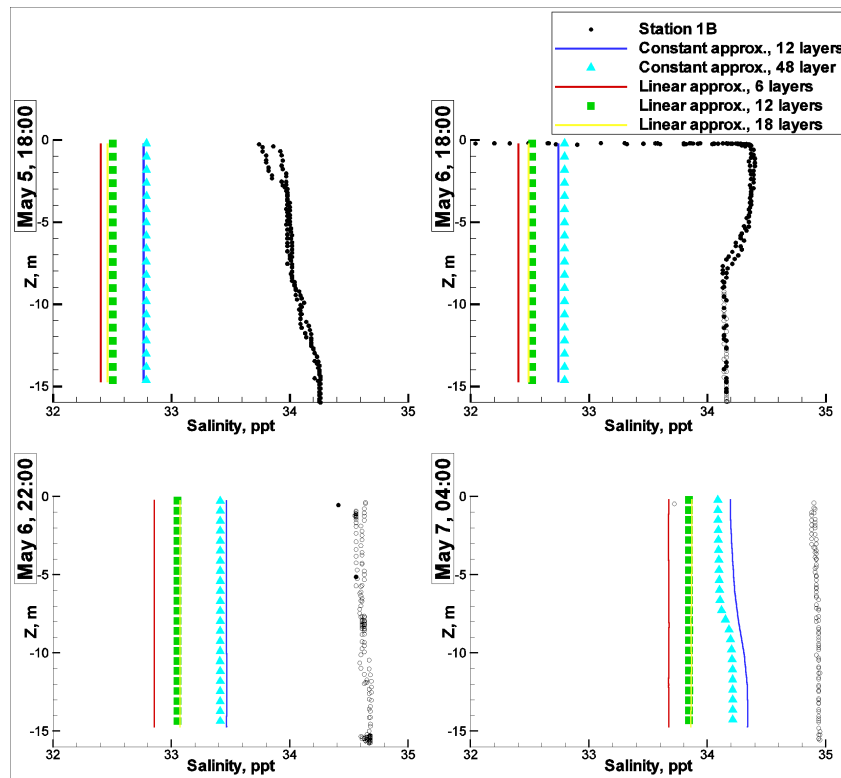
Corpus Christi Bay circulation VI

► Station 1B *x*-velocity depth profile



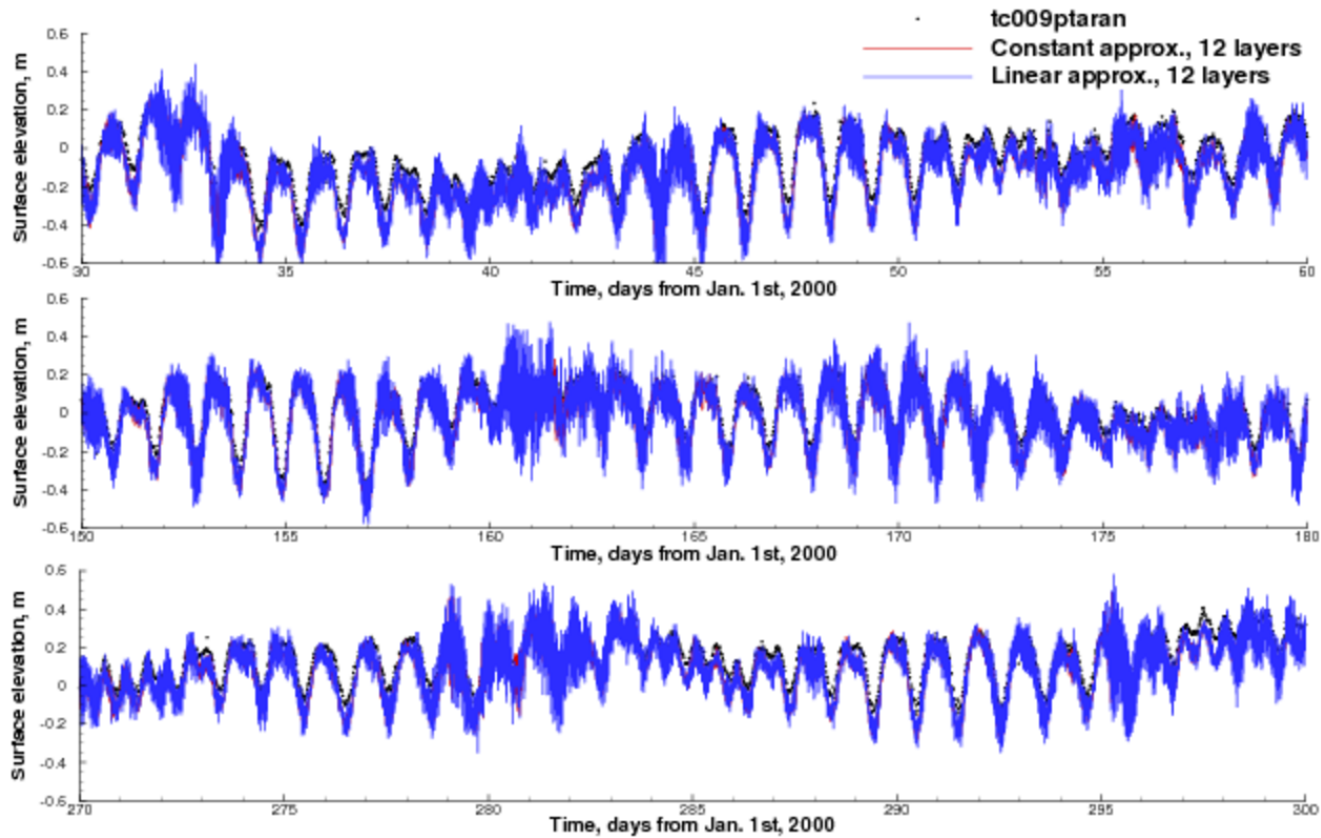
Corpus Christi Bay circulation VII

► Salinity depth profile: Station 1B vs. Station 3A



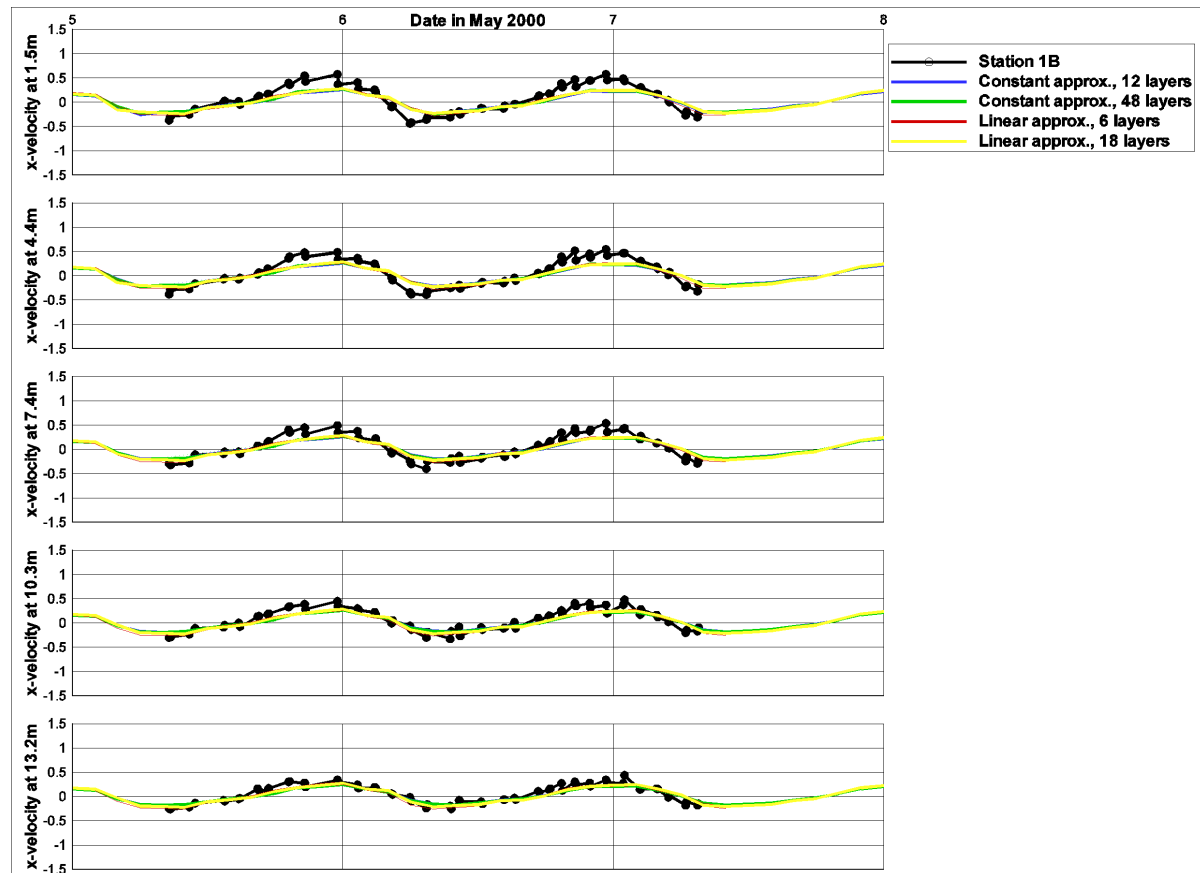
Corpus Christi Bay circulation

► Elevation station tc009 Port Aransas



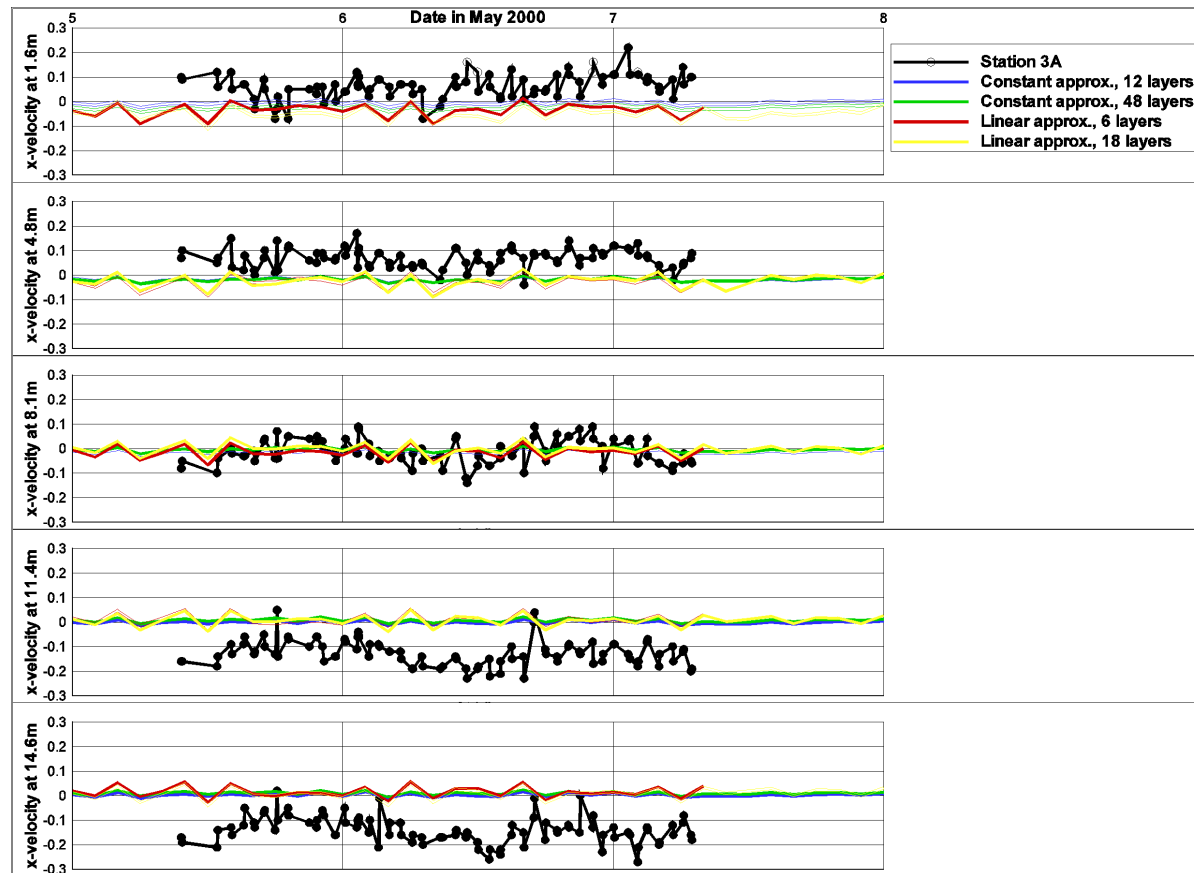
Corpus Christi Bay circulation

► Station 1B y -velocity depth profile



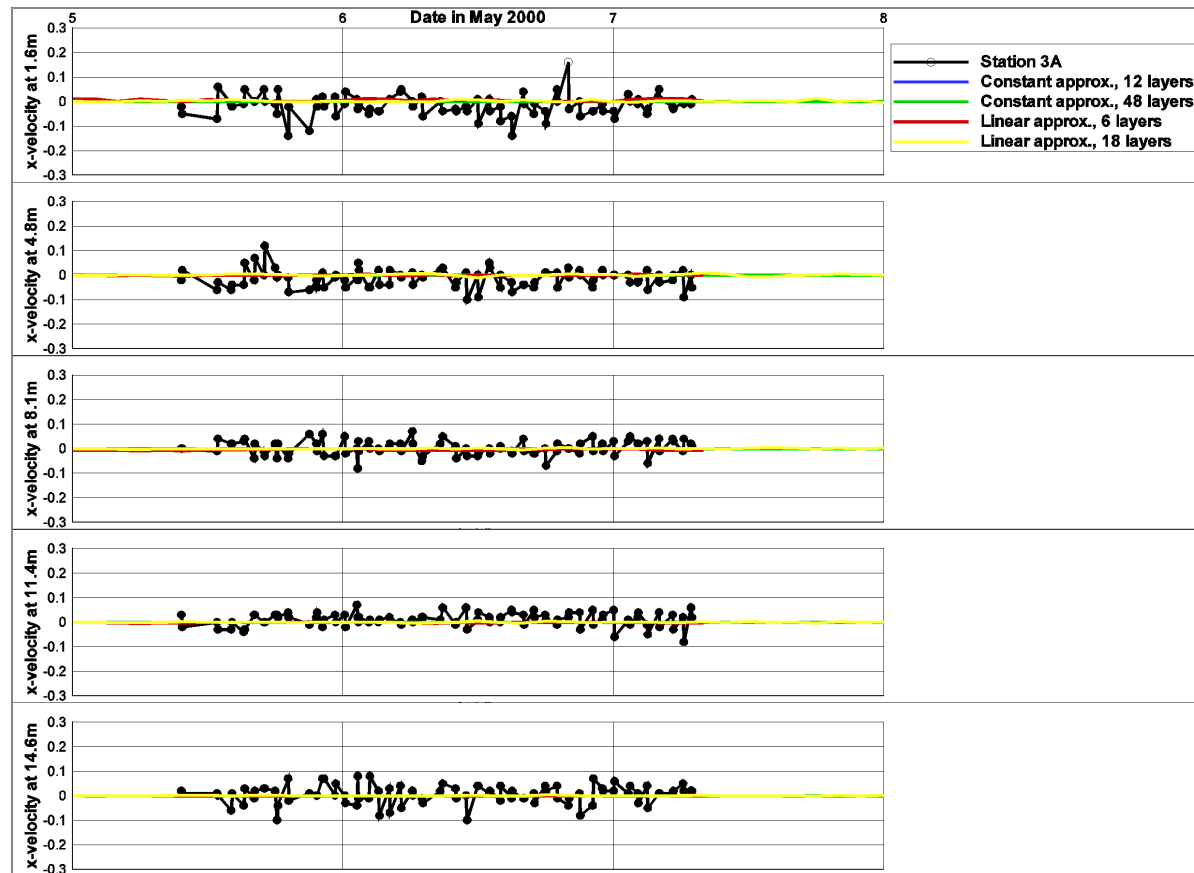
Corpus Christi Bay circulation

► Station 3A *x*-velocity depth profile



Corpus Christi Bay circulation

► Station 3A y -velocity depth profile



Corpus Christi Bay circulation

► Salinity station tcSALT01

