

# A fluidized bed separator for biochar – PYSOLO project

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# The PYSOLO project

- *Project Overview*

# The PYSOLO project

- **PYSOLO** (PYrolysis of biomass by concentrated SOLar pOwer) offers a solution for both decarbonisation and defossilization by **combining concentrated solar power and biomass pyrolysis**.
- Thanks to the **use of solar heat in the pyrolysis process**, the **production of valuable products bio-oil, biochar and pyrogas can be maximized and the associated CO<sub>2</sub> emission minimized**.




# The PYSOLO project



**TYPE OF ACTION**  
Horizon Research & Innovation Action




**BUDGET**  
4,900,000



**PARTNERS**  
9



**COUNTRIES**  
4



**TERM**  
July 2023 – June 2027





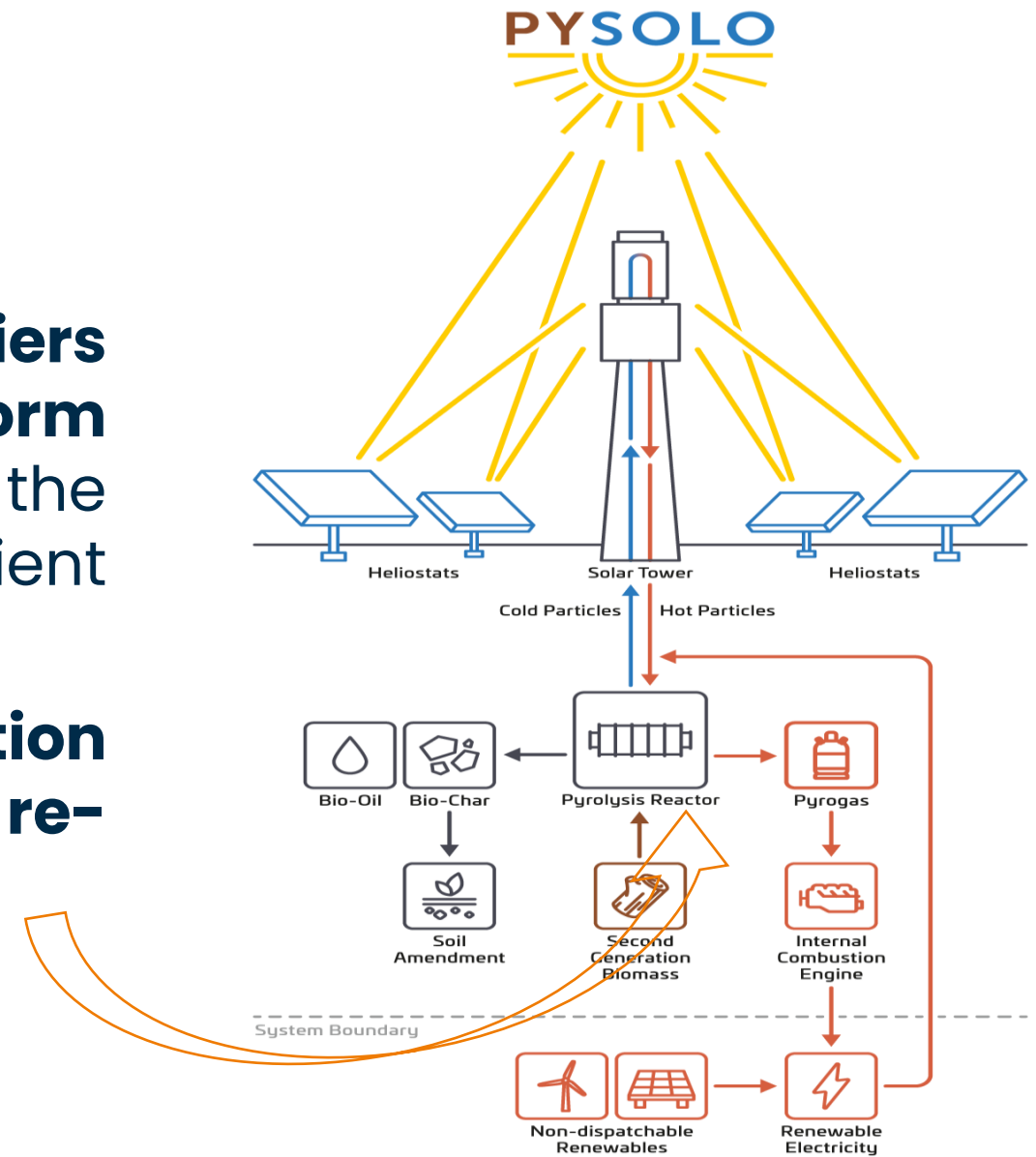
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# Biochar separator

- *Problem definition*
- *FB technologies*
- *Proposed approach*

# Problem definition

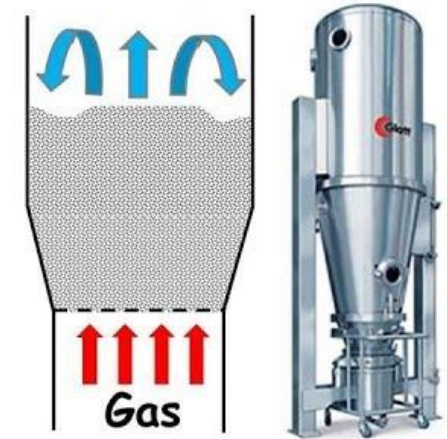
- **PYSOLO** reactor uses **Particle Heat Carriers** (PHC), such as sand, to **facilitate uniform heating** and **thermal stability** for the process, thereby enabling the efficient conversion of biomass.
- **PYSOLO** needs for an **effective separation device** to **recover valuable biochar** and **re-use** the Particle Heat Carrier (PHC).



# Opportunities of the Fluidised Beds

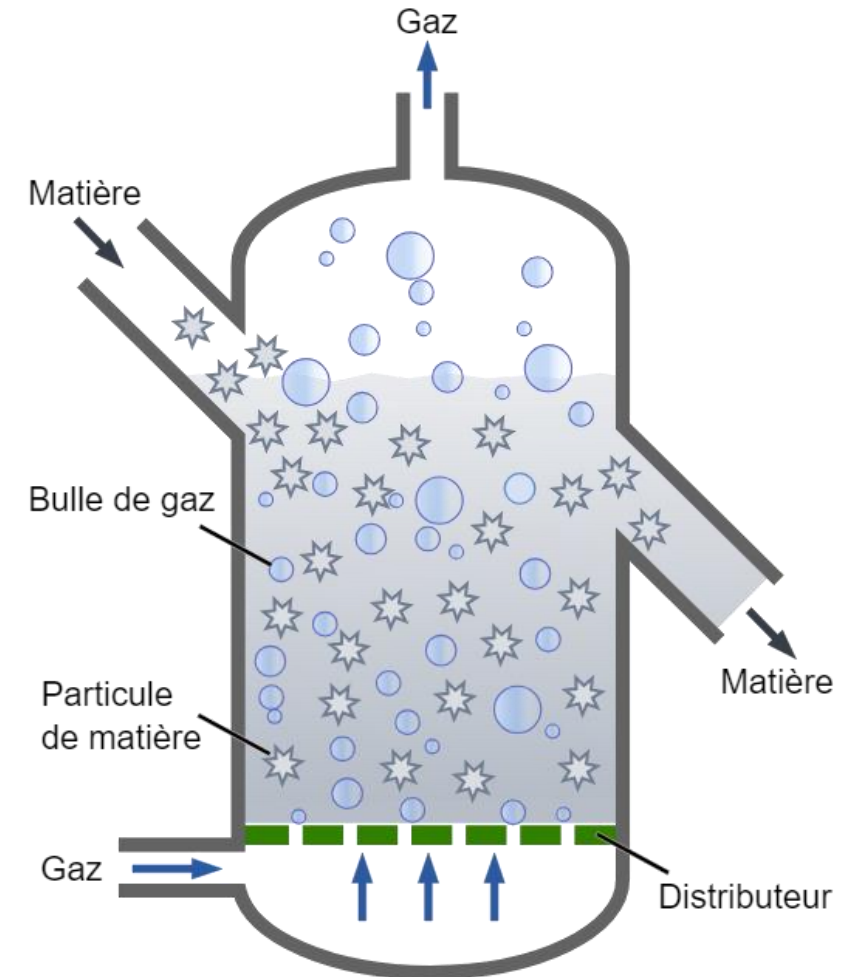
- **Particle separation technologies**, applied to fast pyrolysis, involve both **mechanical** and **non-mechanical** methods.
  - **Mechanical** methods like **centrifugation** and **vibrating screens**.
  - **Non-mechanical** approaches make use of well-proven technology like **fluidized beds**.

## Fluidization



# Opportunities of the Fluidised Beds

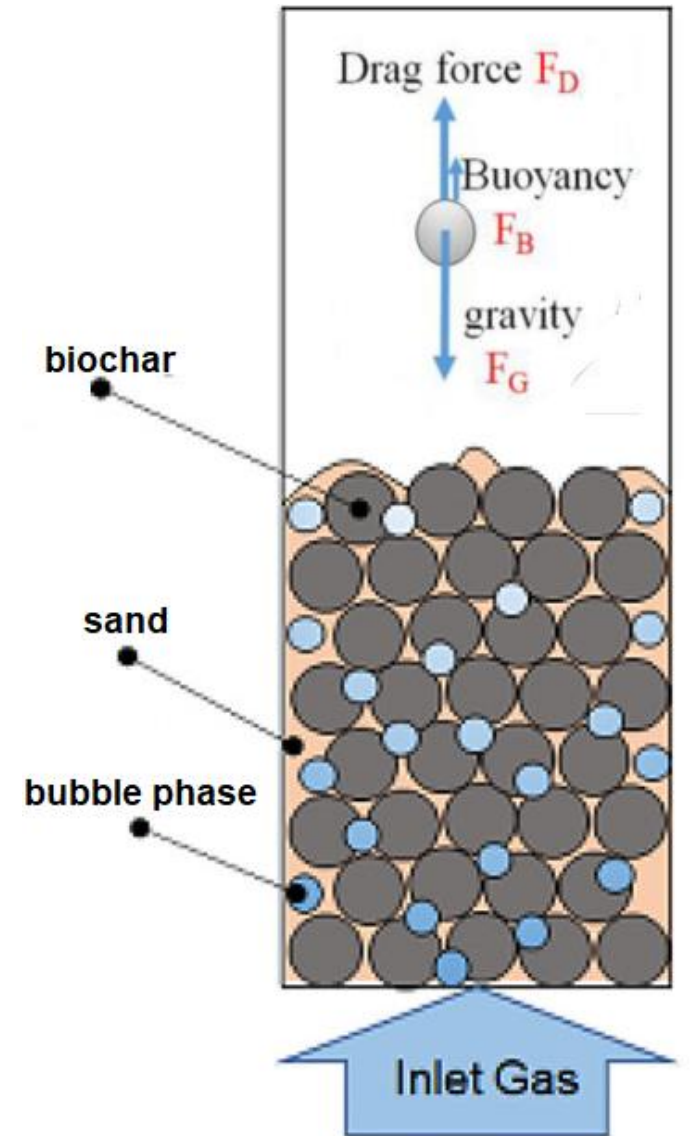
- **Fluidised beds** are a **proven technology**.
- It **can handle hot streams** of fluids and particle with **high reliability**.
- Scientific literature offers a **sound body of knowledge** for supporting the development of new concept and designs.





# Key Parameters

- **U<sub>mf</sub>**: determine the condition at which the particles are suspended in the fluid and are free to move. The **behavior** of the **mix** resembles the one of a **fluid**. The “minimum fluidization velocity” (U<sub>mf</sub>) is a function of the shape, size and density of the particles and the viscosity and density of the fluid.
- **U<sub>t</sub>**: The terminal velocity of single particle is a characteristic parameter in fluidized beds, which represents the **velocity** of a **particle whose weight is balanced** with the **drag** force from its surrounding viscous fluid.



## Experimental formula

$$U_{mf} = \frac{\mu}{D_p \cdot \rho_f} \left[ \sqrt{22.1^2 + 0.0354 \frac{D_p^3 \cdot \rho_f (\rho_p - \rho_f) g}{\mu^2}} - 22.1 \right]$$

$$U_{mf} = 1.78 \left( \frac{(1 - \varepsilon) \cdot \rho_f \cdot g \cdot D_p^3 (\rho_p - \rho_f)}{\mu^2} \right)^{0.14}$$

$$U_{mf} = \left( \frac{\rho_p - \rho_f}{\rho_f} \right)^{0.5} \cdot \left( \frac{18\mu}{\rho_f \cdot D_p} \right)^{0.5} \cdot D_p^{1.14}$$

$$U_{mf} = \left[ (27.3^2 + 0.0434 \frac{D_p^3 \cdot \rho_f \cdot (\rho_p - \rho_f) g}{\mu^2})^{0.5} \right] \frac{\mu f}{D_p \cdot \rho_f}$$

$$U_{mf} = \frac{D_p^2 \cdot (\rho_p - \rho_f) g}{1659 \mu f}$$

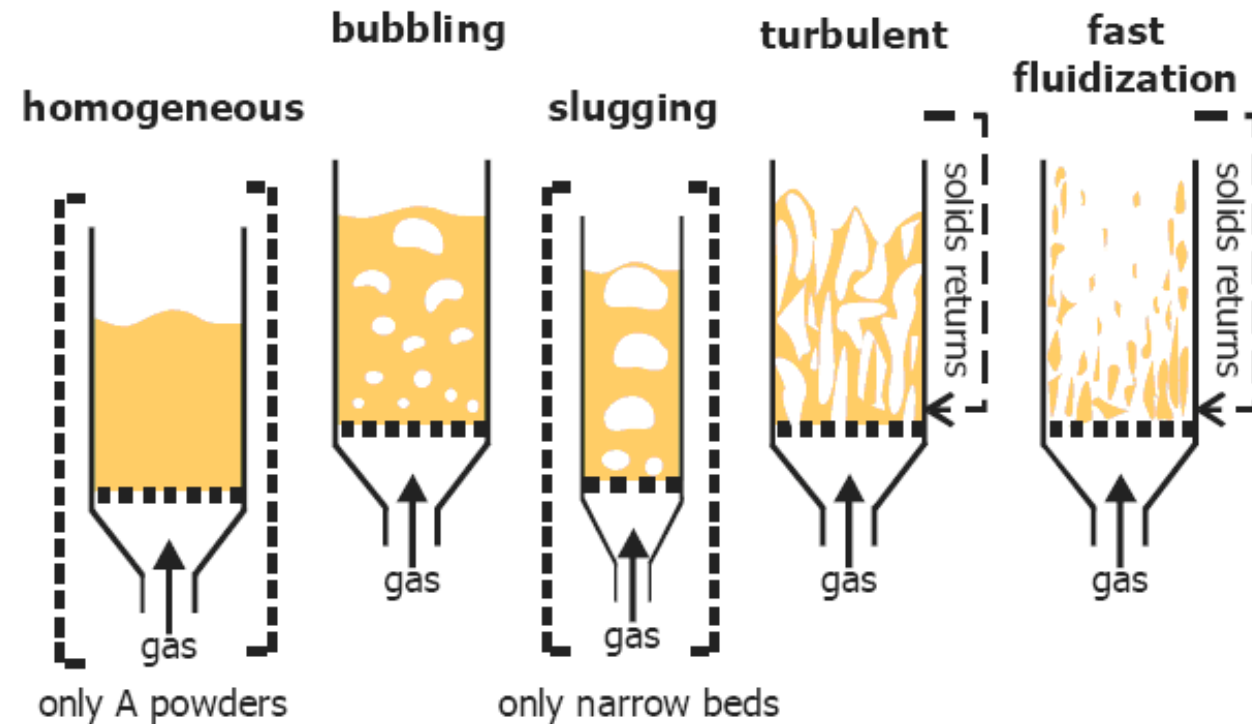
## Theoretical formula

$$U_{mf} = \frac{\varepsilon \cdot (\rho_p - \rho_f) \cdot g \cdot D_p^2}{180 \cdot (1 - \varepsilon) \cdot \mu f}$$

$$U_{mf} = \frac{\varepsilon^3 (\rho_p - \rho_f) \cdot g \cdot D_p^2 \cdot \phi_s^2}{150 \cdot (1 - \varepsilon) \cdot \mu f}$$

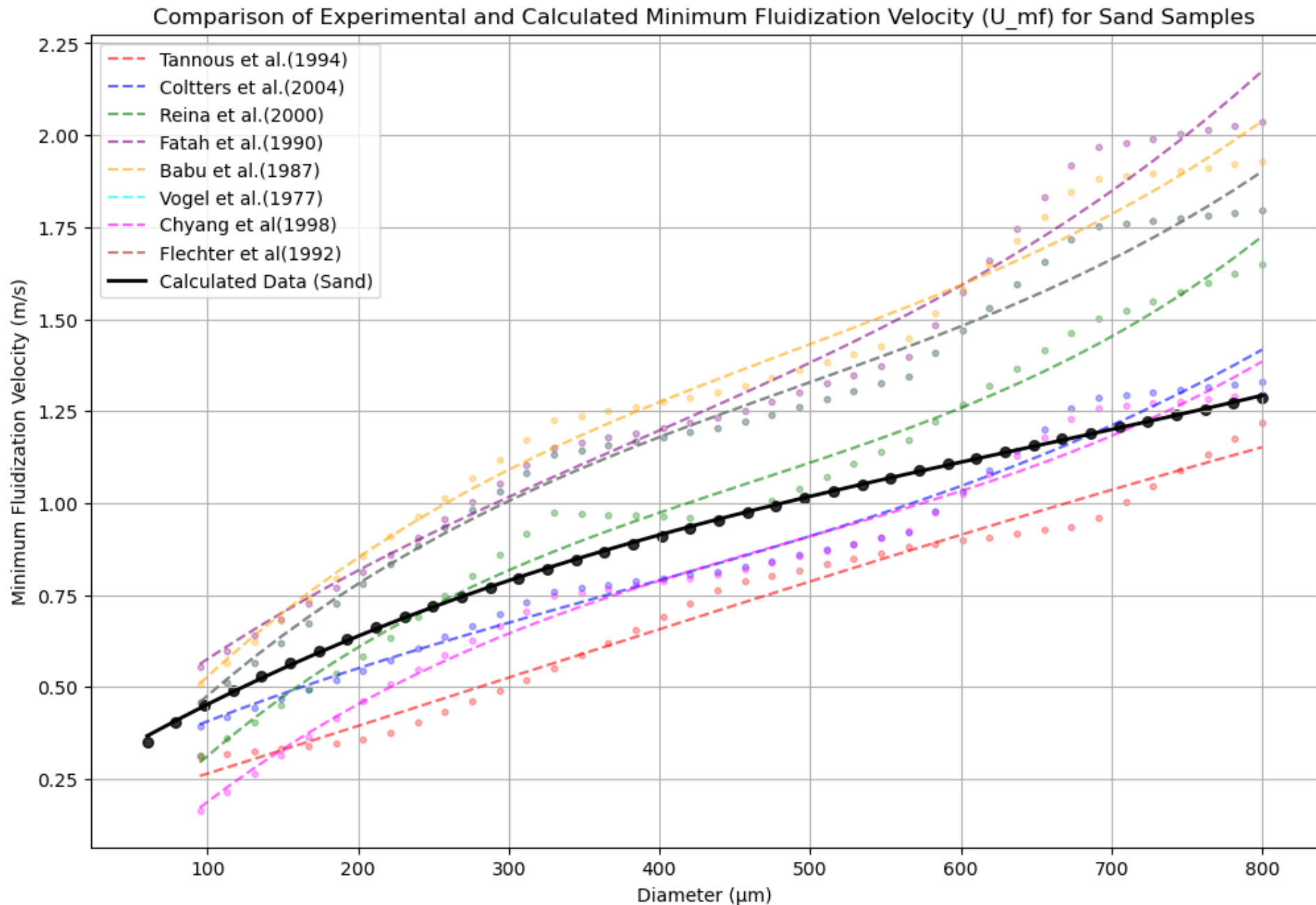
$$U_{mf} = \sqrt{\frac{\phi_s \cdot D_p \cdot (\rho_p - \rho_f) \cdot g \cdot \varepsilon^3}{1.75 \cdot \rho_p}}$$

# Correlative approach



# Validation against the literature of $U_{mf}$ for sand

**Data:**  
Sand:  $95\mu\text{m} < d < 800\mu\text{m}$   
Density: 2000–2650  $\text{kg}/\text{m}^3$

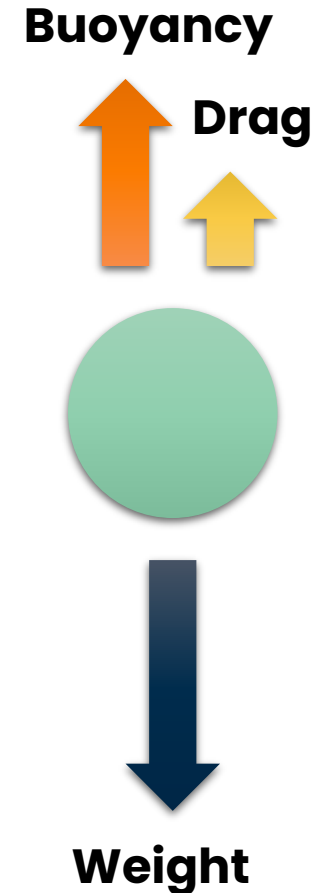


# Proposed approach

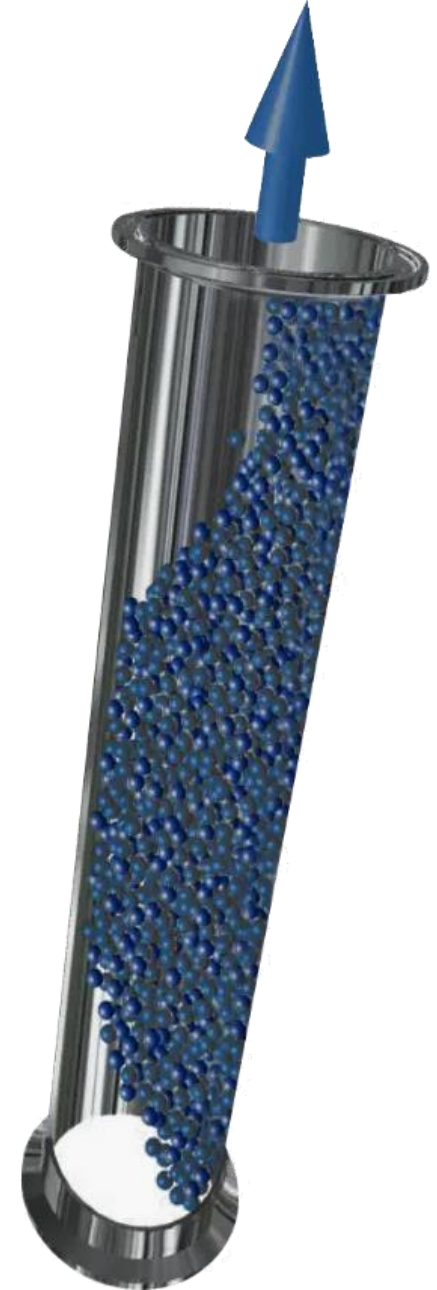
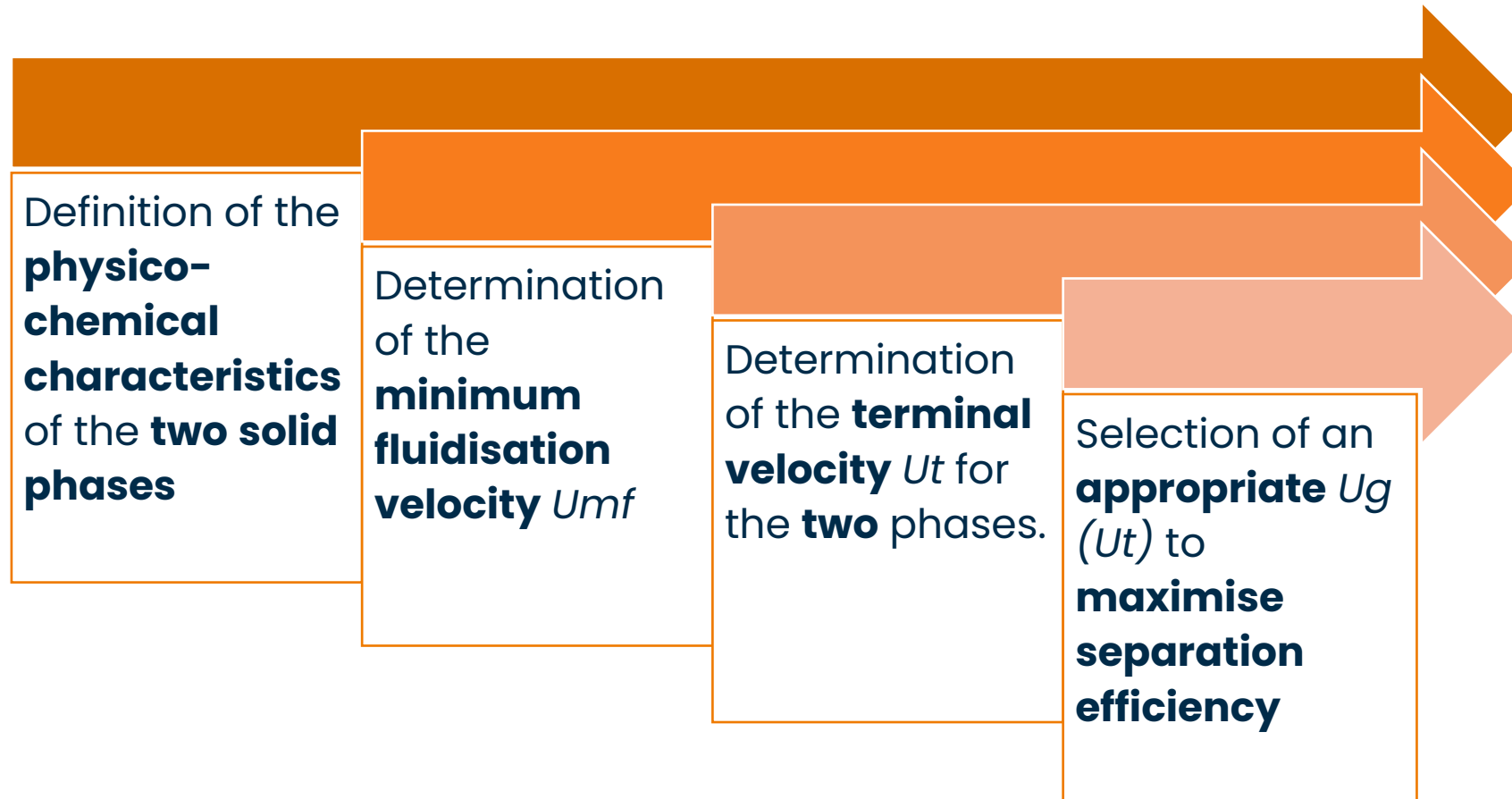
- **Ut** it represents the **flow speed** at which the **three main forces balance** and a **steady state** can be considered for a **particle**.
- The core **idea** of this study is to determine the **Ut above which Biochar is transported** to the **top** of the separator, **while** the **second phase** (e.g. sand) **not** as its  $U_{t\_ph2}$  is higher.

$$U_{mf} < U_{tph1} < U_g < U_{tph2}$$

- **Important to notice** that **particle size distribution** **complicate** the **identification** of the **Ut**.



# Proposed approach





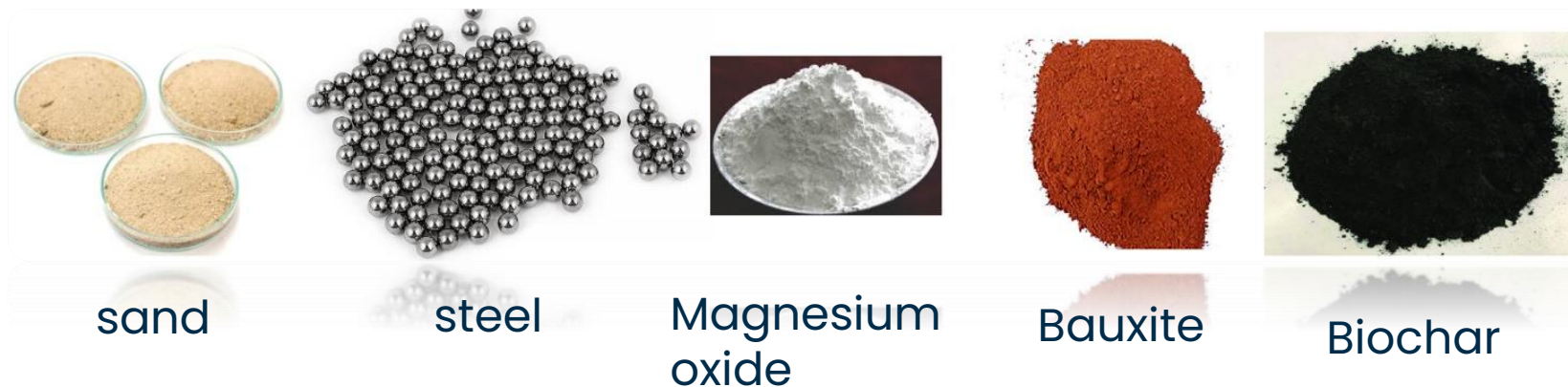
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# Particle Heat Carriers

- *PHC in PYSOLO*
- *Phase characteristics*

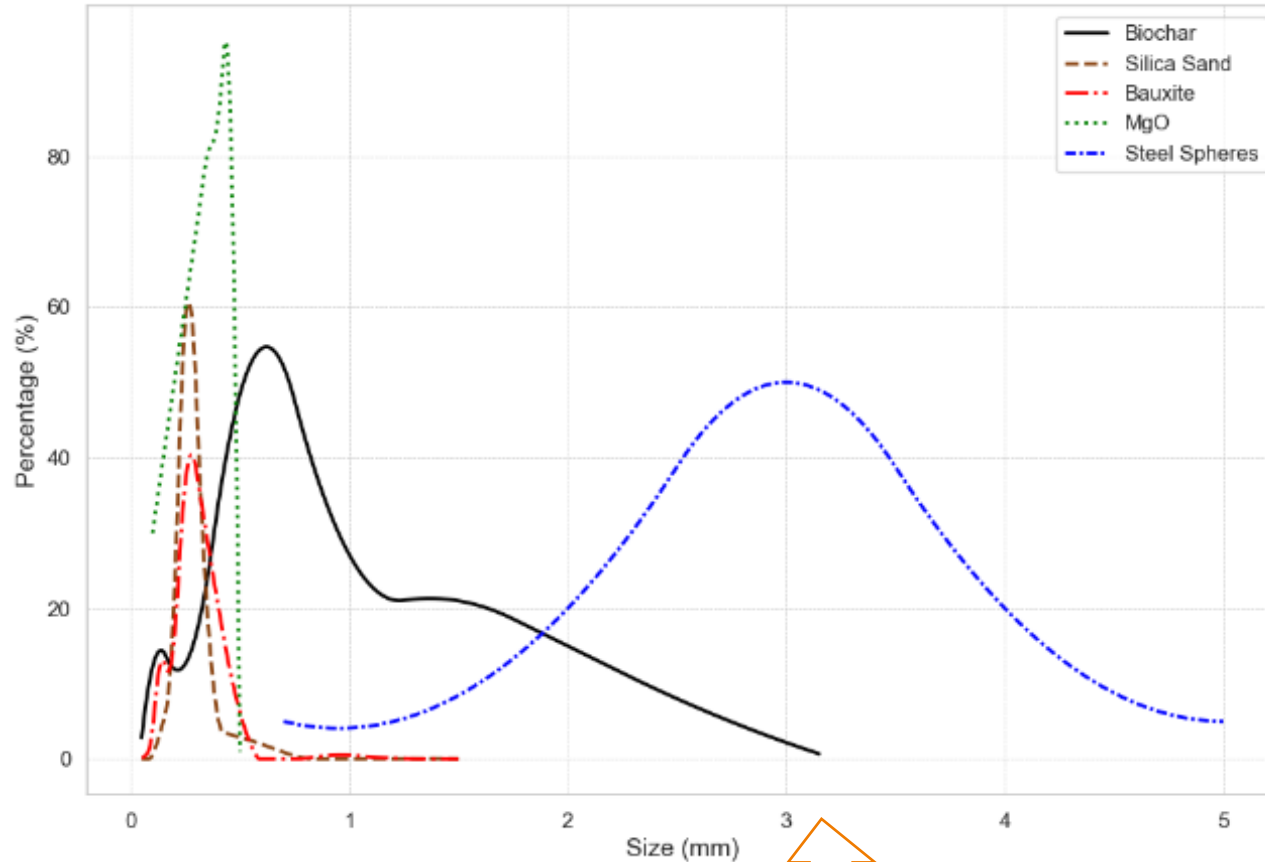
# PYSOLO Particle Heat Carrier

- **PYSOLO** project partner DLR **just started** the **characterization campaign** to **identify** the best **particle heat carrier** for biomass pyrolysis.
- **Four materials** will be selected among several; for the present study the following materials have been considered:



# Particle distribution in real PHC

Particle Size Distribution for Different Materials



## Info received from RE-CORD

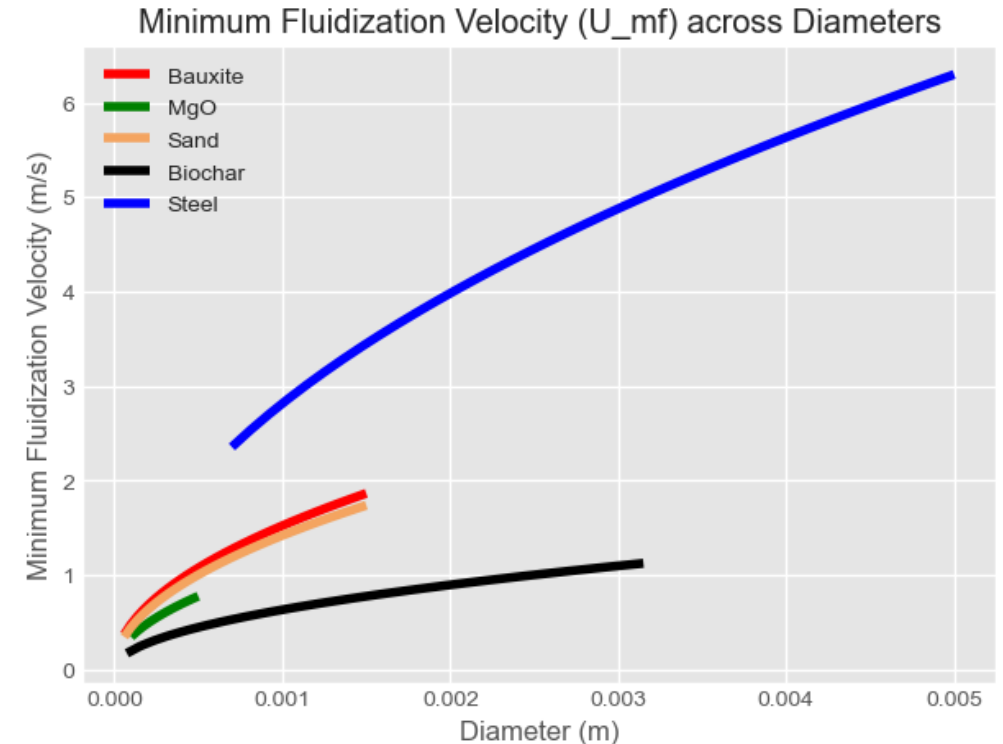
Material	Diameter (mm)	Particle density (Kg/m <sup>3</sup> )	Absorptance	Thermal conductivity (W/m-K)	Specific heat capacity (J/Kg-K)
Biochar	0.075-3.15	400	n/a	0.2-0.3	600-1500
Sintered Bauxite	0.06-1.5	2300	0.89-0.93	2	1175-1275
MgO	0.1-0.5	1200	0.90	48.4	955
Sand	0.06-1.5	2000	0.44-0.66	1.4	740-1175
Steel spheres	0.7-5	7860	Depends on polishing and heat treatment	16	540



# Fluidization minimum velocity

The **U<sub>mf</sub>** has been **calculated** for all the **selected materials**.

This is an **important** parameter to **verify** the **preposed** results **against** the existing **literature**.



The calculation of the terminal velocity considering the **steady state** equilibrium among the drag force, buoyancy and gravity, as represented.

$$F_d = \frac{C_d U^2 \rho A_p}{2}, \quad F_b = V \rho g, \quad F_g = mg$$

$$V = \frac{m}{\rho_p}$$

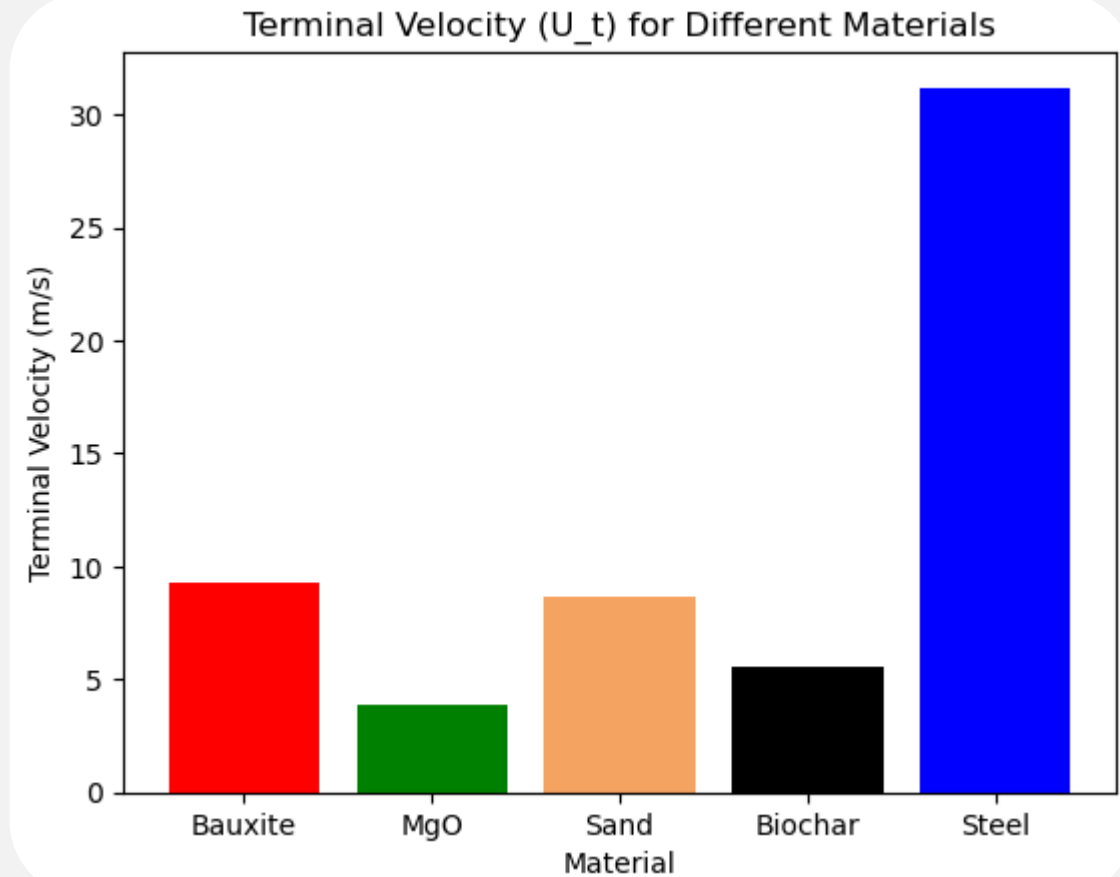
$$\Sigma F = F_g - F_b - F_d \quad (1)$$

$$m \frac{dy}{dt} = mg - \frac{m \rho g}{\rho_p} - \frac{C_d U^2 \rho A_p}{2} \quad (2)$$

$$U = \sqrt{\frac{2mg(1 - \frac{\rho}{\rho_p})}{C_d \rho A_p}} \quad (3), \quad A_p = \frac{\pi D_p^2}{4}, \quad V = \frac{\pi D_p^3}{6}$$

$$U_t = \sqrt{\frac{4gD_p(\rho_p - \rho)}{3C_d\rho}} \quad (4) \quad \text{Archie-Kenney equation}$$

# Terminal Velocity





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# Results and discussion

- *Main results*
- *Next steps*

# Main results

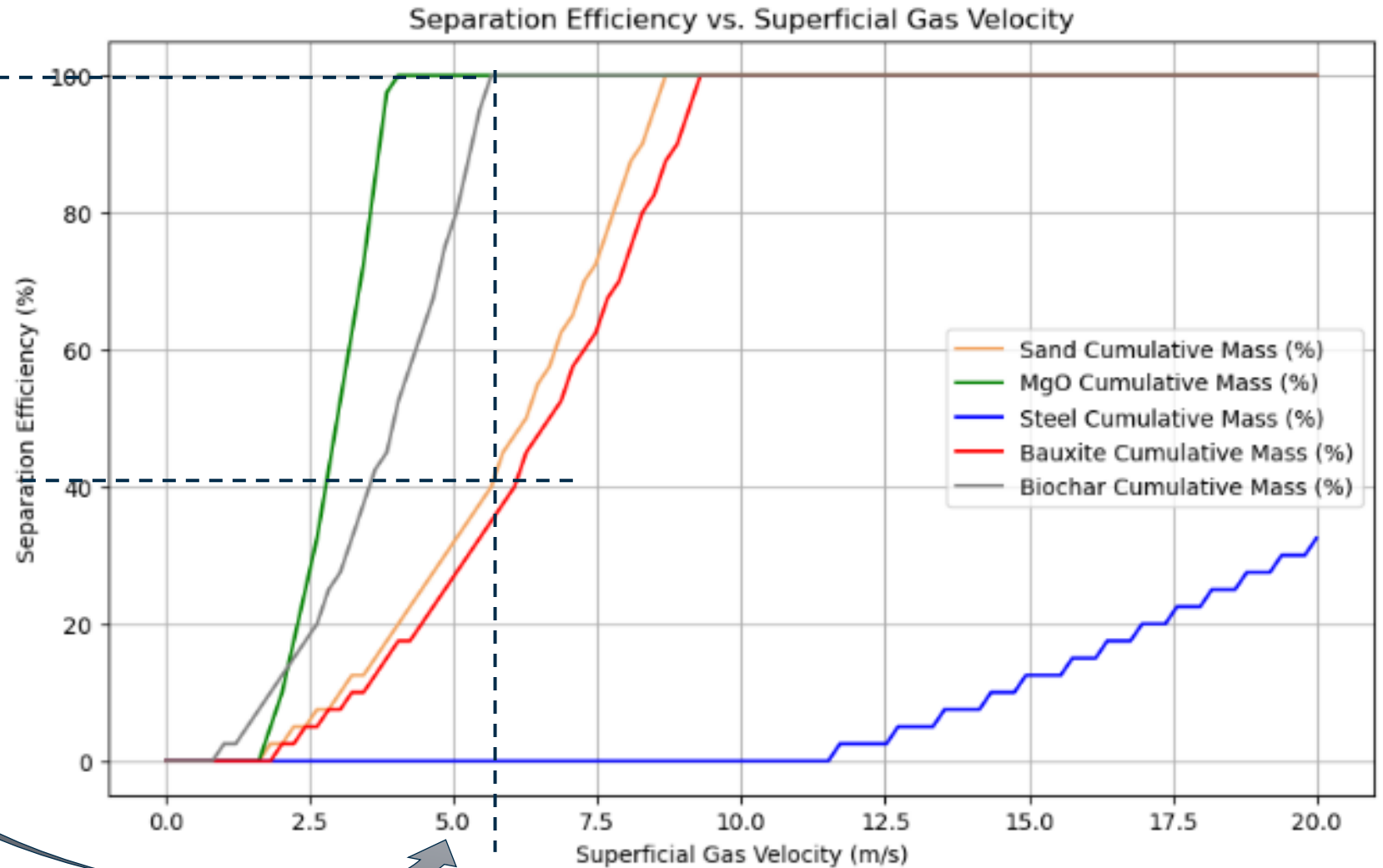
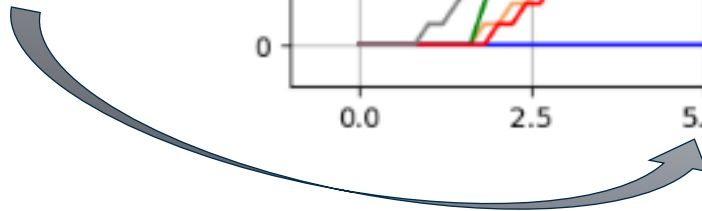
**100%  
Biochar  
collected**



**Still 40% sand in  
the collected  
phase**

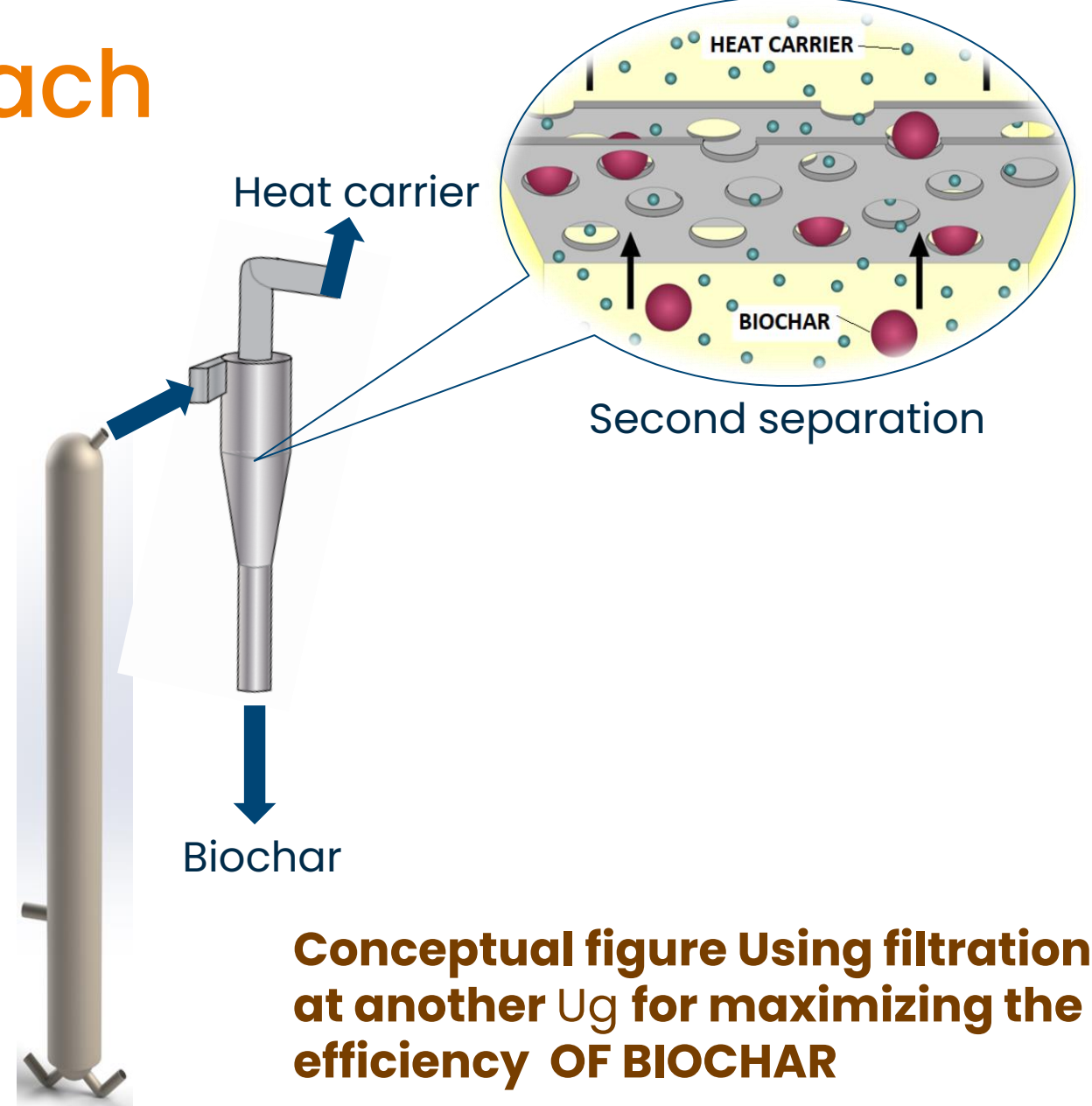


**Target Ug  
velocity**



# Multiple-steps approach

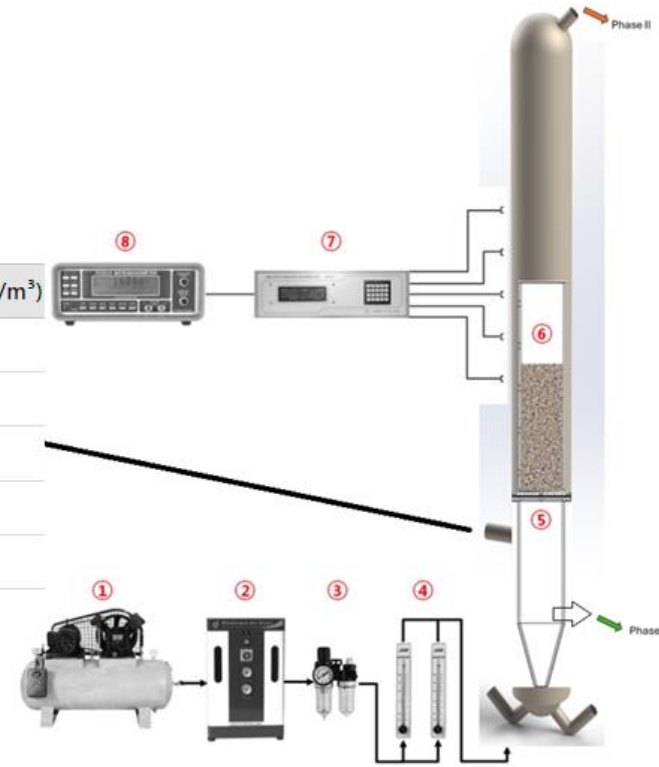
- A **second** separation **step** may be used to **collect** the **residual part** of the **sand**, transported together with the biochar.
- This stage may be operated at different  $U_g$ , to increase the biochar separation rate.



# Experimental validation and further optimisations

- An **experimental test bench** is under **consideration**.
- **Goal** of experimental testing would be to provide **validation** to the proposed approach.
- **Optimise operative parameters** as function of the **real particle size distribution**.
- Provide **optimization options** for design a full-scale equipment for the **PYSOLO** project.

Material	Diameter (mm)	Particle Density (Kg/m <sup>3</sup> )
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Steel spheres	0.7–5	7860





[pysolo.eu](https://pysolo.eu)

# PYrolysis of biomass by concentrated SOLar pOWER



Funded by  
the European Union

**Thanks for your attention!**

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