

# DISRUPTION AND DAMAGE OF AN ELECTROOPTIC MODULATOR BY PULSED MICROWAVES

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## Introduction

High-power microwave (HPM) sources pose a growing threat to avionic systems [1-3]. In particular, microwave receivers that employ sensitive low-noise amplifiers (LNAs) are susceptible to damage by a high-power input. Although electronic limiters may be used to protect the LNA and subsequent receiver electronics, conventional high-power limiters can suffer from non-instantaneous turn-on, relatively slow recovery, and limited power protection. An attractive alternative is to replace the electronic LNA and RF limiter with a low-noise photonic link, which eliminates all electrical connections between antenna and receiver. Key to this approach, however, is the electro-optic (EO) modulator's ability to withstand a high-power input, both in terms of permanent damage and short-term disruption. In this paper, we investigate the susceptibility of a commercial EO modulator to disruption and damage by microwave pulses. We report a 200 W modulator damage threshold that is on par with many high-power RF limiters. Significant disruption at peak powers as low as a few Watts, however, indicates a need for improved modulator power tolerance.

## Experiment and Results

The experimental setup is shown in Fig. 1(a). Microwave pulses with 2.0 GHz center frequency were amplified by a traveling-wave tube amplifier, and then launched directly into the coaxial RF input port of an X-cut LiNbO<sub>3</sub> Mach-Zehnder intensity modulator. The optical transmission of the modulator was concurrently measured by transmitting light from a 1550 nm wavelength laser through the modulator and onto a high-frequency (18 GHz) photodiode (PD). Link transient response was recorded using a 20 MHz bandwidth oscilloscope, which functioned as a pulse envelope detector and also responded to lower frequency variations in the modulator transmission.

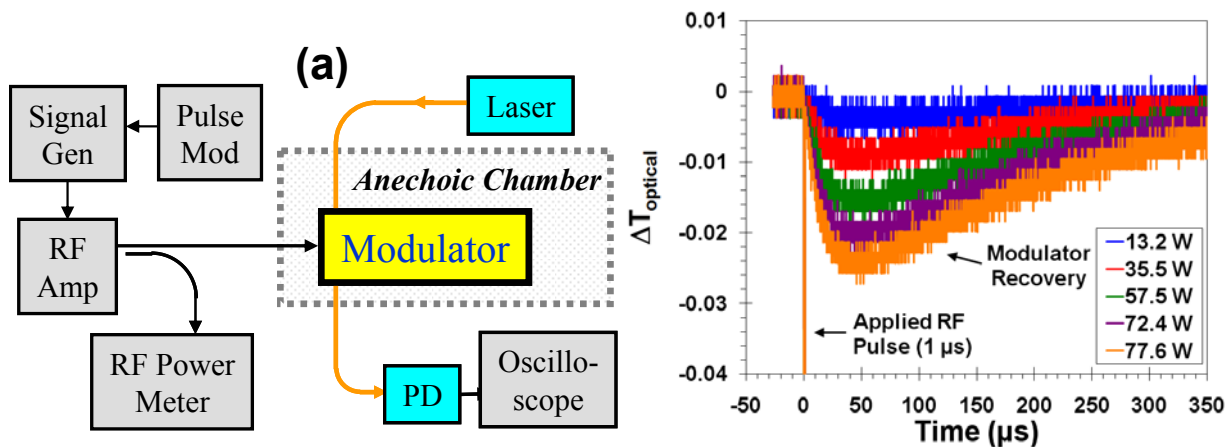
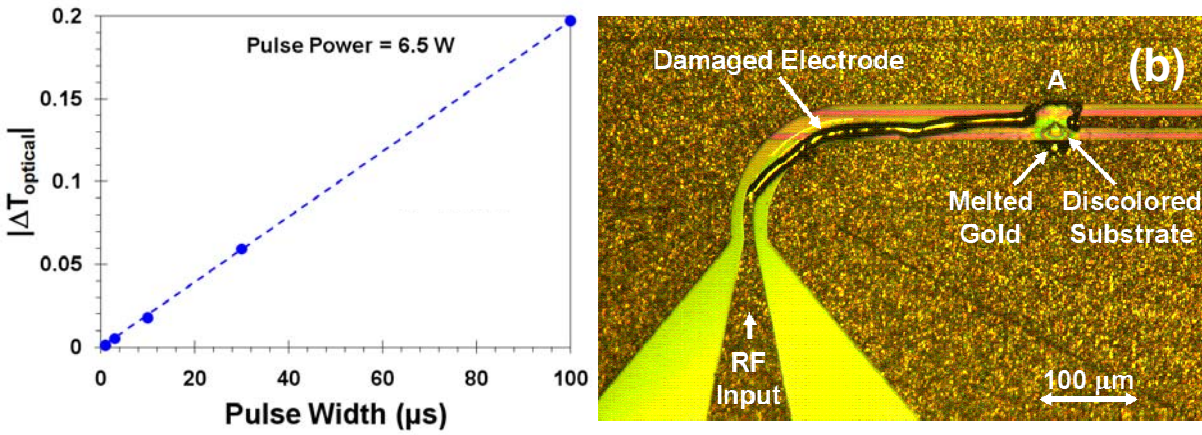


Fig. 1. Photonic link test setup (a), and modulator disruption resulting from a single RF pulse (b).

The single-pulse response for a 1  $\mu s$  pulse width and various pulse peak powers is shown in Fig. 1(b), where  $T_{optical}$  is the normalized optical transmission of the modulator ( $0 \leq T_{optical} \leq 1$ ). Following the initial pulse, the modulator response exhibited a clear “after-pulse” that recovered with a 1/e time constant of approximately 300  $\mu s$ . At powers greater than a few Watts, this observed change in modulator

transmission  $\Delta T_{optical}$  was sufficient to substantially disrupt an analog photonic link. The peak change in transmission during the after-pulse was observed to increase linearly with peak pulse power and with pulse width, as shown in Fig. 2(a). This implies that the modulator disruption depended primarily on the RF pulse energy, and along with the 300  $\mu$ s time scale suggests RF heating as a probable cause.



**Fig. 2. Link disruption as a function of RF pulse width (a), and damaged modulator electrodes after repetitive RF pulsing at 200 W peak power, 40  $\mu$ s pulse width (b).**

The modulator continued to function without noticeable damage after a 10000-pulse burst at 200 W peak power, 20  $\mu$ s width, 2.5 GHz center frequency, and 1 kHz repetition frequency. When the pulse width was increased to 40  $\mu$ s, however, the coplanar RF electrode of the modulator was permanently destroyed, as shown in Fig. 2(b). A small portion of the central gold strip was destroyed by electrical breakdown at point “A,” which left some gold re-distributed as an electrical bridge to the upper electrode. The portion of central electrode closest the RF input was then partially-melted and separated from the substrate surface due to enhanced Joule heating from the electrical short. That dielectric breakdown at 200 W is not unreasonable, due to the roughly 11 MV/m peak electric field across the 13  $\mu$ m electrode gap. Increasing the electrode gap may help to alleviate this problem.

## Conclusion

These results demonstrate the ability of a commercial LiNbO<sub>3</sub> EO modulator to withstand damage from direct pulsed RF input up to 200 W. However, short-term disruption occurred at a few Watts, which suggests a need for improved modulator thermal design.

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## References

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