# Nature of the Magma Chamber Underlying the Mono Craters Area, Eastern California, as Determined From Teleseismic Travel Time Residuals

ULRICH ACHAUER,<sup>1</sup> LIZBETH GREENE, JOHN R. EVANS, AND H. M. IYER

U.S. Geological Survey, Menlo Park, California

A total of 94 teleseismic events of good quality were recorded by a dense mobile array of seismographs located in the Mono Craters volcanic area, eastern California, one of the youngest apparently active rhyolitic volcanic centers in North America. An inversion of travel time residuals from these events reveals a small anomalous volume,  $200-600 \text{ km}^3$ , directly beneath the Mono Craters with at least 7% low velocity and a top approximately 8–10 km deep. It reasonably may be interpreted as a magma chamber of molten or partially molten rock, although smaller, shallower, and differently placed than previously thought. The magma chamber probably is too small and young to produce a caldera-forming eruption within the foreseeable future.

#### INTRODUCTION

In recent years the analysis of teleseismic compressional waves has proven to be a useful tool for the detection of small anomalous velocity bodies in volcanic areas such as Long Valley, California [*Iyer and Stewart*, 1977; *Steeples and Iyer*, 1976], The Geysers-Clear Lake volcanic field [*Iyer et al.*, 1979; *Oppenheimer and Herkenhoff*, 1981], Mount Etna, Sicily [*Sharp et al.*, 1980], Coso geothermal area, California [*Reasenberg et al.*, 1980], Roosevelt Hot Springs, Utah [*Robinson and Iyer*, 1981], Newberry Volcano, Oregon (D. A. Stauber, unpublished manuscript, 1986) and other locations.

The Mono-Inyo Craters chain is a north trending silicic volcanic system extending from Long Valley caldera in the south to Mono Lake in the north (Figure 1). The chain is on the western margin of the Basin and Range province, just east of the Sierra Nevada range front. High heat flow, recent faulting, and strong seismic activity indicate that crustal extension still dominates the local tectonic regime, and that the region is volcanically and seismically active.

Kistler [1966] suggest that the Mono Craters erupted along the eastern part of a subcircular mylonitized Cretaceous pluton boundary. This mylonitized zone bounds the Grant Lake-June Lake embayment of the Sierra Nevada to the west and is inferred to underlie vents of the Mono Craters on the east (Figure 1). More recently, *Bailey and Koeppen* [1977] and *Bailey* [1982] mapped an additional series of concentric ring fractures east and south of the Mono Craters.

Bailey et al. [1976] and Bailey [1982] argue that together with these ring fracture systems, the youth, geochemistry, and frequency of eruptions suggest that the Mono Craters are fed by a ring dike from a moderately deep silicic magma chamber centered west of the craters beneath Pumice Valley. They infer that the chamber is largely molten and may still be rising toward the surface beneath an incipient caldera ring fracture zone (Figure 1). The teleseismic experiment described below is an attempt to test this model. While it tends to confirm the

Paper number 6B6023. 0148-0227/86/006B-6023\$05.00 existence of a magma chamber, it suggests that the chamber is smaller and shallower than Bailey inferred and is located beneath the Mono Craters themselves rather than being centered beneath Pumice Valley.

#### DESCRIPTION OF EXPERIMENT

To investigate the crustal compressional velocity structure of the Mono Craters area a network of portable analog seismic recorders was installed for a period of 2 months during the summer of 1982. The network consisted of 16 stations with an average station spacing of about 6 km (Figure 1). These stations formed a 20 by 30 km grid centered near the Mono Craters.

The recording instruments used were 11 U.S. Geological Survey (USGS) analog FM "5-day recorders" [Criley and Eaton, 1978]. Two of the recorders also received data from a total of five radio transmitter sites. The transmitter sites each had one 1-Hz vertical seismometer, while the remaining stations included one vertical and two horizontal 1-Hz seismometers. Arrival times of P and PKIKP were read from the vertical component in each case.

During the 2-month recording period, 94 teleseismic events of good quality were recorded (Table 1 and Figure 2). All events were digitized and timed using digital band-pass filters and correlative methods similar to those of *Steeples and Iyer* [1976]. Timing precision is approximately 0.05 s. Theoretical travel times were calculated from hypocenters given in the "Preliminary Determinations of Epicenters," a U.S. Geological Survey periodical, and the *Herrin et al.* [1968] travel time tables. Absolute residuals then were obtained by subtracting the theoretical travel time from the observed travel time:

$$R_{ij} = T_{\mathbf{o}_{ij}} - T_{\mathbf{th}_{ij}} \tag{1}$$

To isolate the effects of local structure from the extraneous, but often larger, effects of source and path errors and anomalies, relative residuals were calculated. This correction was made by subtracting the weighted mean residual for each event from the absolute residuals of every station for that event:

$$RR_{ij} = R_{ij} - \frac{1}{\sum_{i=1}^{N_j} W_{ij}} \sum_{i=1}^{N_j} W_{ij}R_{ij}$$
(2)

<sup>&</sup>lt;sup>1</sup> Now at Geophysikalisches Institut, Universität Fridericiana Karlsruhe, Karlsruhe, Federal Republic of Germany.

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Fig. 1. Map of the Mono-Inyo Craters area showing major volcanic, tectonic, and geographic features, and the stations used in the teleseismic imaging experiment. Open symbols are transmitter sites; solid symbols are recorder sites. Cross north of MC9 is model center (cf. Figures 6a-6c). Geology based on work by Kistler [1966], Bailey and Koeppen [1977], and Strand [1967].

where *i* is the station index, *j* is the event index,  $N_j$  stations report event *j*, and  $W_{ij}$  are weights derived from subjective pick qualities. Relative residuals are used for the remainder of this paper and simply may be called "residuals."

Figure 3a shows mean relative residuals for each station with teleseisms arriving from all azimuths averaged together:

$$AR_{i} = \frac{1}{M_{i}} \sum_{j=1}^{M_{i}} RR_{ij}$$
(3)

where  $M_i$  events were recorded at station *i* during the experiment. These average residuals are independent of azimuth and incidence angle and reflect velocity heterogeneities at shallow depth. They are called the "invariant" part of the residuals.

Equation (3) is subject to an azimuthal bias caused by the inhomogeneous distribution of events around the earth. For comparison, we calculated unbiased invariant residuals by weighting the residuals so that each way "bundle," discussed below, contributed equally to the invariant residual. The azimuthal bias revealed by this procedure is very small, generally less than 0.02 s. It has no significant effect on the following

discussion and no effect at all on the inversion results presented later.

To show the effects of deeper structures, the teleseismic compressional waves next were divided into five groups according to ray orientation beneath the array. All events in such a ray bundle are averaged together and the invariant part is removed according to

$$DR_{ib} = \left[\frac{1}{X_{ib}}\sum_{j=1}^{X_{ib}} RR_{ijb}\right] - AR_i$$
(4)

where  $X_{ib}$  is the number of events reported at station *i* for ray bundle *b*. *P* waves have incidence angles from about  $14^{\circ}-30^{\circ}$ near the surface and are divided into four groups according to azimuth (Figure 3b-3e). The azimuth groupings chosen follow the natural clustering of events to the northwest, southeast, and southwest, as seen from the western United States. The fifth ray group (Figure 3f) is *PKIKP* with all azimuths grouped together; incidence angles are less than 6° for *PKIKP*. The changes in residual patterns between these five ray directions are due to anomalous velocity regions at depth

| TABLE | 1. | Hypocenters of Teleseismic Events Used  |  |
|-------|----|---|--|
| TADLE | 1. | Typocements of Teleseistine Lycins Oscu |  |

| Location                        | Date                           | Origin<br>Time | Depth,<br>km | M <sub>b</sub> | Latitude<br>N                           | Longitude<br>W                            |
|---------------------------------|--------------------------------|----------------|--------------|----------------|---|---|
| El Salvador                     | June 19, 1982                  | 0621:58.0      | 82           | 6.2            | 13°18.8′                                | 89°20.3′                                  |
| Fiji Islands                    | June 19, 1982                  | 1849:02.5      | 611          | 4.9            | -21° <b>04.2′</b>                       | 178°46.6'                                 |
| Vanuatu Islands                 | June 19, 1982                  | 2246:08.8      | 33           | 5.6            | -14°43.1′                               | -167°52.6′                                |
| North Atlantic                  | June 20, 1982                  | 0829:15.3      | 10           | 5.1<br>1 Q     | 30°42.0'<br>13°03.6'                    | 41°44.0<br>80°10 7/                       |
| Santa Cruz Islands              | June 21, 1982                  | 1915:56.3      | 48           | 5.6            | $-10^{\circ}47.0^{\prime}$              | $-164^{\circ}10.4'$                       |
| Banda Sea                       | June 22, 1982                  | 0418:40.5      | 450          | 6.3            | -7°20.3′                                | -126°02.6′                                |
| Aleutian Islands                | June 22, 1982                  | 0705:27.1      | 90           | 4.8            | 53°55.7′                                | 166°38.6'                                 |
| Honshu, Japan                   | June 23, 1982                  | 0151:54 8      | 476          | 5.3            | 29°03.7′                                | -138°46.1′                                |
| Fiji Islands<br>South Atlantic* | June 23, 1982                  | 1324:09.3      | 623          | 4.8            | - 20°45.0°<br>- 44°00.5'                | 1/8°53.1'<br>15°58 7'                     |
| Sumatera                        | June 25, 1982                  | 1023:51.2      | 35           | 5.3            |   | $-103^{\circ}26.2'$                       |
| Kuril Islands*                  | June 30, 1982                  | 0157:34.1      | 33           | 6.6            | 44°40.7′                                | -151°08.6′                                |
| Chile                           | July 1, 1982                   | 0256:27.2      | 149          | 5.0            | 18°40.8′                                | 69°23.8′                                  |
| Aleutian Islands                | July 1, 1982                   | 0741:53.2      | 48           | 6.3            | 51°25.6′                                | 179°56.6′                                 |
| Chile-Bolivia                   | July 1, 1982                   | 0847:32.7      | 119          | 4.4            | $-21^{\circ}25.8'$                      | 68°48.0'                                  |
| Fl Salvador                     | July 1, 1982<br>July 2, 1982   | 1159.35.6      | 64           | 5.0            | -21 40.0<br>13°03.4'                    | 89°17.2′                                  |
| Volcano Islands                 | July 3, 1982                   | 1436:30.3      | 165          | 5.2            | 22°19.0'                                | -143°24.7'                                |
| Kazakh, SSR                     | July 4, 1982                   | 0117:14.4      | 1            | 6.1            | 49°59.7′                                | - 78°51.4′                                |
| Ryukyu Island                   | July 4, 1982                   | 0120:06.8      | 536          | 6.3            | 27°55.7′                                | -136°58.0′                                |
| Colombia                        | July 4, 1982                   | 0616:08.4      | 54           | 5.5            | 7°39.2′                                 | 72°11.8′                                  |
| Japan<br>Fiu Islande            | July 5, 1982                   | 2172-26.0      | 615          | 5.7            | 30 39.8<br>                             | -130 27.1<br>178°48 1'                    |
| Peru                            | July 11, 1982                  | 0213:37.7      | 39           | 5.3            | - 16°38.9'                              | 73°12.8′                                  |
| North Atlantic                  | July 11, 1982                  | 1040:12.4      | 10           | 5.1            | 23°43.6′                                | 44°53.9′                                  |
| Honshu, Japan                   | July 13, 1982                  | 0845:55.7      | 341          | 4.9            | 32°56.3′                                | $-137^{\circ}39.2'$                       |
| Gilbert Islands                 | July 13, 1982                  | 1349:48.3      | 30           | 5.5            | - 3°18.3'                               | -177°35.5′                                |
| Japan                           | July 14, 1982                  | 1042:13.5      | 325          | 5.3            | 45°38.5'                                | - 143°21.8'                               |
| Alaska<br>Gilbert Islands       | July 14, 1982<br>July 15, 1982 | 0213:47.0      | 33           | 5.0            | - 3°20.5′                               | $-177^{\circ}34.9'$                       |
| Fiji Islands                    | July 16, 1982                  | 1433:40.7      | 547          | 5.4            | -21°24.7'                               | 178°50.2′                                 |
| Gilbert Islands                 | July 17, 1982                  | 1832:09.7      | 33           | 5.4            | - 3°15.0′                               | -177°37.1′                                |
| Vanuatu Islands                 | July 17, 1982                  | 2202:07.9      | 37           | 5.6            | -21°44.1′                               | -173°07.9′                                |
| Colombia                        | July 17, 1982                  | 2224:14.2      | 163          | 4.9            | 6°47.5′                                 | 73°02.5′                                  |
| Argentina                       | July 19, 1982                  | 2352:55.2      | 207          | 5.2<br>5.5     | -23°30.9<br>54°33.0'                    | 00 44.3                                   |
| Peru                            | July 20, 1982                  | 2211:03.5      | 99           | 5.1            | -13°12.9'                               | - 101 28.5<br>75°05.6′                    |
| Honshu, Japan                   | July 23, 1982                  | 1125:01.3      | 32           | 5.1            | 36°07.3′                                | -141°45.5′                                |
| Java                            | July 23, 1982                  | 1351:42 3      | 34           | 5.2            | $-10^{\circ}47.8'$                      | -111° <b>42.9</b> ′                       |
| Honshu, Japan                   | July 23, 1982                  | 1423:53 5      | 37           | 6.2            | 36°11.6′                                | -141°42.1′                                |
| Honshu, Japan <sup>+</sup>      | July 23, 1982                  | 1505.07.8      | 50<br>31     | 5.1<br>5.7     | 30°09.4<br>36°04.0'                     | $-141^{\circ}43.0^{\circ}$<br>-141°43.5'  |
| Africa                          | July 24, 1982                  | 0917:27.5      | 10           | 5.2            | - 52°52.8′                              | $-20^{\circ}51.7'$                        |
| New Britain                     | July 24, 1982                  | 1233:56.2      | 76           | 4.6            | -5°51.7′                                | -151°17.0′                                |
| Aleutian Islands*               | July 25, 1982                  | 0539:01.8      | 106          | 4.5            | 52°02.4′                                | -178°26.6′                                |
| Honshu, Japan                   | July 25, 1982                  | 0801:28.6      | 45           | 5.5            | 36°18.8'                                | - 141°38.6′                               |
| Africa                          | July 25, 1982<br>July 26, 1982 | 0343.24.0      | 10           | 5.0            | $-21^{\circ}31.8$<br>$-52^{\circ}48.2'$ | - 20°56 6'                                |
| El Salvador                     | July 26, 1982                  | 1034:58.6      | 67           | 5.1            | 13°21.9′                                | 89°03.8′                                  |
| Galapagos Islands               | July 27, 1982                  | 1127:17.9      | 10           | 5.2            | 1°15.2′                                 | 90°41.8′                                  |
| Aleutian Islands                | July 27, 1982                  | 1234.51 8      | 228          | 4.6            | 52°50.4′                                | 176°24.6′                                 |
| Longa Islands                   | July 30, 1982                  | 0340:51.4      | 33           | 5.7            | - [8°39.1'<br>51°45 3'                  | $1/3^{\circ}38.1^{\circ}$<br>= 176°08 2'  |
| Tonga Islands                   | Aug. 2. 1982                   | 1100:07.0      | 33           | 0.2<br>4.9     | 20°21.1′                                | -170 08.2<br>174°27.2'                    |
| Mariana Islands*                | Aug. 3, 1982                   | 0604:39.6      | 47           | 5.8            | 13°44.5'                                | -146°20.4′                                |
| New Guinea                      | Aug. 5, 1982                   | 0728:08.8      | 113          | 5.6            | - 5°46.0′                               | $-146^{\circ}34.0'$                       |
| Chile                           | Aug. 5, 1982                   | 0815:01.7      | 33           | 5.0            | -37°37.7′                               | 73°00.7′                                  |
| Chile                           | <sup>-</sup> Aug. 5, 1982      | 0916:41.3      | 40           | 5.4            | - 26°40.7′                              | 70°39.4′                                  |
| Santa Cruz Islands              | Aug. 5, 1982                   | 2032-52.9      | 33           | 5.2<br>62      | - 5 22.8<br>- 12°35.8'                  | -17739.7<br>-165°559'                     |
| Aleutian Islands                | Aug. 6, 1982                   | 0453:58.6      | 64           | 5.4            | 51°56.8′                                | 176°05.1′                                 |
| Indian Rise                     | Aug. 6, 1982                   | 1345:26.8      | 10           | 5.1            | -10°22.7′                               | -66°14.9′                                 |
| Fıjı Islands                    | Aug. 7, 1982                   | 0120:29.5      | 33           | 5.1            | -16°14.0′                               | -178°17.0′                                |
| Tonga Islands*                  | Aug. 7, 1982                   | 1309:21.5      | 33           | 5.0            | -24°26.7′                               | 175°12.7′                                 |
| Samoa<br>Alaska                 | Aug. 7, 1982                   | 1820:22.1      | 35<br>15     | 5.5<br>1 8     | - 10°32.9'<br>65°50 0'                  | 1/2-38.2'<br>166°46 0'                    |
| Bali                            | Aug. 7, 1982                   | 2056:22.7      | 33           | <br>6.1        | $-11^{\circ}08.6'$                      | $-115^{\circ}25.1'$                       |
| Kamchatka                       | Aug. 8, 1982                   | 0614:09.5      | 140          | 5.3            | 51°03.1′                                | -156°26.4′                                |
| Peru                            | Aug. 9, 1982                   | 0450:38.6      | 164          | 4.8            | -15°13.8′                               | 71°02.5′                                  |
| New Britain                     | Aug. 9, 1982                   | 0502:34.4      | 163          | 5.4            | -4°38.5'                                | - 151°45.8'                               |
| New Britain                     | Aug. 9, 1982                   | 1847:03.8      | 143          | 5.3            | -4°58.9′                                | $-151^{\circ}04.9$<br>$-151^{\circ}22.3'$ |
|                                 |                                |                |              |                |   |   |

| Location         | Dațe          | Origin<br>Time | Depth,<br>km | $M_{b}$ | Latitude<br>N | Longitude<br>W |
|------------------|---------------|----------------|--------------|---------|---------------|----------------|
| Vanuatu Islands  | Aug. 9, 1982  | 2327:31.9      | 229          | 5.0     | - 18°47.1′    | - 169°10.3′    |
| Peru             | Aug. 10, 1982 | 0451:48.5      | 33           | 5.5     | -5°21.1'      | 77°22.0′       |
| Tonga Islands    | Aug. 11, 1982 | 0808:50.1      | 33           | 5.1     | -19°28.9'     | 173°02.0'      |
| Samoa            | Aug. 11, 1982 | 1202:02.8      | 33           | 5.3     | -16°25.4′     | 172°42.2'      |
| Honshu, Japan    | Aug. 12, 1982 | 0433:00.1      | 34           | 5.3     | 34°53.9′      | -139°29.0'     |
| Gilbert Islands  | Aug. 12, 1982 | 1003:15.5      | 33           | 5.5     | - 3°23.2′     | -177°34.1′     |
| Honshu, Japan    | Aug. 12, 1982 | 1146:50.8      | 33           | 5.3     | 39°24.4′      | -143°16.6'     |
| Gilbert Islands  | Aug. 13, 1982 | 0605:45.1      | 33           | 5.3     | -3°18.1′      | -177°35.8'     |
| Mariana Islands  | Aug. 14, 1982 | 0058:54.0      | 156          | 5.3     | 18°29.2'      | -145°52.0'     |
| New Guinea       | Aug. 14, 1982 | 1427:40.2      | 106          | 5.9     | - 5°03.3'     | -143°57.8'     |
| Peru             | Aug. 15, 1982 | 0611:15.9      | 106          | 5.5     | -10°03.8'     | 76°21.1′       |
| Honshu, Japan    | Aug. 15, 1982 | 1658:15.8      | 50           | 5.4     | 36°29.8'      | -141°02.0′     |
| Guatemala        | Aug. 16, 1982 | 0632:58.8      | 76           | 5.0     | 14°22.5'      | 91°36.2′       |
| Fiji Islands     | Aug. 16, 1982 | 0721:26.9      | 596          | 5.1     | -19°42.5'     | 178°08.6'      |
| Aleutian Islands | Aug. 16, 1982 | 2058:20.7      | 49           | 5.4     | 51°47.0′      | 174°03.4′      |
| Kuril Islands    | Aug. 17, 1982 | 0528:59.2      | 48           | 5.0     | 45°41.3'      | -151°21.2'     |
| Solomon Islands  | Aug. 17, 1982 | 2255:46.9      | 33           | 5.4     | -9°15.0'      | -157°39.7′     |
| Mexico†          | Aug. 18, 1982 | 0358:20.8      | 38           | 5.0     | 18°04.2′      | 105°34.6'      |
| Vanuatu Islands  | Aug. 19, 1982 | 0440:48.2      | 39           | 5.6     | -19°04.0'     | - 169°34.7'    |
| Panama           | Aug. 19, 1982 | 1559:01.5      | 10           | 6.2     | 6°43.1'       | 82°40 8'       |
| Gilbert Islands  | Aug. 19, 1982 | 1633:25.6      | 33           | 5.1     | - 3°25.1′     | - 177°40.3′    |
|                  |               |                |              | 2       |               |                |

TABLE 1. (continued)

\*Too few readings; not used in ACH inversion.

†Not used in Figure 3.

beneath the array. These patterns usefully can be thought of as the "shadows" of deep objects projected to the surface along five different illuminating "beams."

# **Observations**

The invariant part of the delay pattern (Figure 3a) shows that the stations near Mono Lake (MCC, MD1, MD2, and MCG) are 0.1-0.2 s late. These delays probably are caused by low-velocity sediment filling Mono basin, *Pakiser*'s [1976]

time terms form a very similar delay pattern which he related to a thin layer of very low-velocity sediments filling the basin.

This invariant part has been subtracted from Figures 3b-3f, so that the Mono basin sediment effect is removed in these maps. The remaining part reveals a deeper low-velocity anomaly. A delayed region migrates with event azimuth and appears at stations MCA and MCB for northwest *P* wave events (Figure 3*e*); MC2, MC3, and MC9 for northeast events (Figure 3*b*); MC7, MC8, and MD1 for southeast events



Fig. 2. Azimuthal equidistant maps of epicenters (crosses) of teleseismic events used in this study. The Mono Craters area is indicated by the square (P events); the antipode of the area is indicated by the diamond (PKIKP events). Hypocenter data are listed in Table 1



AZIMUTH 0°- 360° N=93 DISTANCE 25°-180°



AZIMUTH 180°-270° N=33 DISTANCE 25°-100°



AZIMUTH 0°- 90° N=2 DISTANCE 25° - 100°





AZIMUTH 90°-180° N= 19 DISTANCE 25°-100°





AZIMUTH 0°- 360° N=8 DI STANCE 110°- 180°

Fig. 3. Mean relative residuals for six distance-azimuth groups (seconds; positive indicates delays). (a) All events together (i.e., "invariant part"); (b) northeast P wave events; (c) southeast events; (d) southwest events; (e) northwest events; and (f) PKIKP. Dotted line in Figure 3f shows approximate maximum size of the low-velocity feature. Invariant part has been removed from Figures 3b-3f. "N" is the number of events per group (not all stations report for each event).

(Figure 3c); and MCE for southwest events (Figure 3d). In each case a small region of delayed arrivals is seen near the Mono Craters and is always on the opposite side of the craters from the events.

These delays (comparing opposite sides of the craters along single ray corridors) average about 0.2 s for the four main ray bundles (Figures 3b-3e). The northeast quadrant (Figure 3b) contributes strongly to this average but contains only two

TABLE 2a. Inversion Models

|       |                                       | Model A   |   |                                 | Model B                              |  | Model C               |  |                              |
|-------|---------------------------------------|---|---|---------------------------------|--------------------------------------|--|-----------------------|--|------------------------------|
| Layer | Thick-<br>ness,<br>km                 | Horizontal<br>Block Size,<br>km × km  | Initial<br>Velocity,<br>km/s              | Thick-<br>ness,<br>km           | Horizontal<br>Block Size,<br>km × km | Initial<br>Velocity,<br>km/s   | Thick-<br>ness,<br>km | Horizontal<br>Block Size,<br>km × km           | Initial<br>Velocity,<br>km/s |
| 1     | *                                     | special   | 4.5                                       | *                               | special                              | †  |                       | special  | †                            |
| 2     | 7.5                                   | 5 × 5   | 6.0                                       | 7.5                             | 5 × 5                                | 6.0  | 9.0                   | 6 × 6  | 6.0                          |
| 3     | 7.5                                   | 5 × 5   | 6.25                                      | 7.5                             | 5 × 5                                | 6.25   | 9.0                   | 6 × 6  | 6.25                         |
| 4     | 7.5                                   | 5 × 5   | 6.5                                       | 7.5                             | 5 × 5                                | 6.5  | 9.0                   | 6 × 6  | 6.5                          |
| 5     | 7.5                                   | 5 × 5   | 6.9                                       | 7.5                             | 5 × 5                                | 6.9  | 9.0                   | 6 × 6  | 6.9                          |
|       |                                       | Description   |   | Mod                             | lel A                                | Model B  |                       | Model C  |                              |
|       | Blocl<br>Dam<br>Data<br>Rema<br>Varia | k orientation;<br>ping, s <sup>2</sup> /% <sup>2</sup><br>variance, s <sup>2</sup><br>aining variance<br>ance reduction | ;<br>;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;; | 45° ×<br>0.0<br>0.0<br>0.0<br>7 | 135°<br>010<br>170<br>045<br>3       | $\begin{array}{c} 45^{\circ} \times 135 \\ 0.0010 \\ 0.0088 \\ 0.0036 \\ 60 \end{array}$ | <b>.</b>              | 45° × 135°<br>0.0005<br>0.0088<br>0.0033<br>62 |                              |

\*Layer thickness equals the station elevation; bottom of first layer is at sea level. †See Table 2b for velocities. ‡Azimuth of block edges

TABLE 2b. Station Coordinates and Sediment-Corrected Velocities for Layer 1

| Station | Latitude<br>N | Longitude<br>W | Elevation,<br>m | Velocity,<br>km/s |
|---------|---------------|----------------|-----------------|-------------------|
| MC1     | 37°53.13′     | 119°10.18′     | 2640            | 5.40              |
| MC2     | 37°51.28′     | 119°07.06′     | 2323            | 4.50              |
| MC3     | 37°48.86'     | 119°04.44'     | 2354            | 4.50              |
| MC4     | 37°46.01′     | 119°02.48′     | 2692            | 4.95              |
| M5A*    | 37°43.64'     | 119°01.21'     | 2561            | 4.50              |
| M5B*    | 37°43.56'     | 119°00.95'     | 2442            | 4.50              |
| MC6     | 37°57.96'     | 119°09.24'     | 2847            | 4.72              |
| MC7     | 37°55.40′     | 119°08.03'     | 2296            | 4.95              |
| MC8     | 37°53.26'     | 119°04.25'     | 2091            | 4.50              |
| MC9     | 37°51.04′     | 119°02.19′     | 2244            | 4.50              |
| MCA     | 37°48.25'     | 118°58.58'     | 2497            | 4.95              |
| MCB     | 37°46.59'     | 118°55.55'     | 2341            | 4.50              |
| MCC     | 37°57.66′     | 119°05.36'     | 1963            | 3.38              |
| MD1†    | 37°55.49′     | 119°03.03′     | 2073            | 3.83              |
| MD2†    | 37°55.08'     | 119°00.91′     | 2064            | 3.38              |
| MCE     | 37°52.81′     | 118°58.31'     | 2262            | 4.95              |
| MCF     | 37°51.11'     | 118°55.02'     | 2540            | 4.72              |
| MCG     | 37°56.37'     | 118°56.85'     | 2037            | 3.60              |
|         |               |                |                 |                   |

\*M5A moved to M5B; July 4, 1982.

†MD1 moved to MD2; June 27-29, 1982.

events and may be less accurate than the other three; the mean contrast in the three remaining quadrants is 0.13 s.

Though small, this contrast is significant. The standard deviations of the means plotted in Figure 3 are about 0.01 s, and the several means used together to make such comparisons give a combined accuracy of about  $\pm 0.05$  s. The observed 0.13-s contrast is about 3 times larger than this error estimate.

This moving pattern of delays can be explained most easily by a small midcrustal low-velocity region beneath the Mono Craters. The horizontal dimension of the delaying volume is about 1 or 2 times the distance between stations (since the delays cover one to three stations) or about 6-12 km. Assuming, for example, a 10-km-diameter sphere causing a maximum of 0.2-s delay, as discussed above, one can estimate that it would have about 11% low velocity if embedded in a 6 km/s layer. The Mono Craters low-velocity feature is of this order. The depth of the feature can be estimated from the ray incidence angles and the distance the delay shadow moves between opposite azimuths. In this case the low-velocity region must be centered at roughly 12–20 km deep. Based on the positions of the residual maxima and the ray azimuths used, it is probably beneath the southern half of the Mono Craters.

The fifth (near-vertical) ray bundle (Figure 3f) unfortunately lacks any data above this suspect region. In fact, the near-zero residuals at MC2, MC3, MC8, MCA, MD2, MCE, and MCF constrain the horizontal size and position of the anomalous volume to be within the dashed line in Figure 3f, consistent with the data for the other ray bundles.

# INVERSION OF THE MONO CRATERS DATA: METHOD

To investigate the low-velocity anomaly in more detail, we inverted the relative residuals using a modified version of the "ACH" inversion technique first described by *Aki et al.* [1977]. In this section we briefly outline the method, which is described in great detail by *Ellsworth* [1977], *Aki et al.* [1977] *Iyer et al.* [1981*a*, *b*], and many other authors. Results of this modeling are given in the following section.

In this method the volume of interest below the seismic array is parameterized by dividing it into plane layers and dividing each layer into a grid of rectangular blocks. An initial average compressional wave velocity is assigned to each layer for purposes of ray tracing, but the results are not very sensitive to these initial velocities [Aki et al., 1977]. The block sizes are governed by the station spacing of the network and the wavelength of the recorded compressional waves (both about 6 km).

This version of the ACH method uses plane waves incident on the bottom of the layered model. To linearize the equations, each segment of ray is assigned to the block in which it travels and refraction by the anomalous structure is disregarded. The linear equations can be expressed in matrix form as

$$\mathbf{A}m = d \tag{5}$$



Fig. 4. Residual variance (i.e., model misfit) versus the length (i.e., complexity) of the solution vector  $(||\hat{m}||)$  showing the trade-off between these factors for a range of damping parameters  $\theta^2$ .



MODEL A LAYER 1 0.0 - 2.0 KM VELOCITY 4.50 KM/S





MODEL B LAYER 1 0 0 - 2.0 KM VELOCITY 3 38 - 5.40 KM/S

MODEL C LAYER 1 0.0 - 2.0 KM VELOCITY 3.38 - 5.40 KM/S

where *m* is a vector containing the unknown fractional slowness perturbations, **A** is a semidefinite matrix with the calculated unperturbed travel times of ray segments, and *d* is a vector containing the travel time residuals.  $\mathbf{A}^{T}\mathbf{A}$  is singular because, for example, a uniform velocity perturbation in one layer is indistinguishable from origin time changes [*Aki and Lee*, 1976]. Thus to solve these equations we use the method of damped least squares [*Levenberg*, 1944; *Franklin*, 1970]:

$$\hat{m} = (\mathbf{A}^T \mathbf{A} + \theta^2 \mathbf{I})^{-1} \mathbf{A}^T d \tag{6}$$

where  $\hat{m}$  is the model estimate,  $\theta^2 \approx \sigma d^2/\sigma m^2$  is the damping parameter [Aki et al., 1977], and  $\sigma d^2$  and  $\sigma m^2$  are the estimated variances of the data and the true model *m*. The solution of the linearized problem gives the velocity perturbation of each block (approximated as the negative of the slowness perturbation) relative to an unknown mean layer velocity. Absolute velocities are indeterminate because relative, rather than absolute, residuals must be used and by reason of the singularity argument given above.

To examine the problems of velocity anomalies arising from near-surface sediments and of the trade-off between resolution and block size, we present three slightly different models. All three models have five layers; in the first layer the block structure is replaced by a separate first-layer "block" for each station. The reason for this special treatment is that in the first layer the rays arriving at a given station generally sample a volume through which rays to no other station pass.

Tables 2a and 2b show layer thicknesses, initial velocities, and block sizes for each model. The initial velocities and the thickness of the first layer were obtained from refraction profiles in the Mono basin area [Pakiser, 1976], and the Long Valley caldera area [Hill, 1976; Kissling et al., 1984]. Model A has a uniform initial velocity assigned to all stations in layer 1, that is, no sediment corrections. The calculated velocity perturbations in layer 1 of model A were used to estimate the first-layer velocity corrections subsequently used in models B and C (Table 2b). These corrections produce travel time variations that are in the same sense but smaller than Pakiser's [1976] refraction time terms for Mono basin (presumably because teleseismic rays have steeper angles of incidence, i.e., are shorter than refraction rays). The sediment corrections reduce the starting data variance, of course, but they also improve the fit of the calculated model to the data. That is, they reduce the unmodeled-data variance, the part of the data left unexplained by the model ("remaining varience" in Table 2a; see the appendix).

For layers 2-5 the blocks have horizontal dimensions of 5 km in models A and B and 6 km in model C. These dimensions are appropriate for the station spacing and give the good resolution characteristics discussed later. The height of the blocks was chosen to be 1.5 times the horizontal block size in a compromise between steep ray angles and block equidimensionality [cf. *Ellsworth and Koyanagi*, 1977]. To improve the resolution, only blocks sampled by at least 10 rays were used in the inversion.

Different damping factors (between  $\theta^2 = 0.0200$  and 0.0002

Fig. 5. (opposite) Velocity models produced by ACH inversion method. The same layer of three models (A, B, and C) are shown in each figure; the depth range of model C is slightly different from the others (Table 2a). Contour intervals vary from model to model and layer to layer. They are labeled in percent (negative indicates slow). (a) Layer one (small crosses show station locations); (b)-(e) layers 2-5 (small crosses show block centers). Cross section in Plate 1 taken along line shown in Figure 5c for model B.



MODEL A LAYER 2 2.0 - 9.5 KM VELOCITY 6 00 KM/S



MODEL B LAYER 2 2.0 - 9.5 KM VELOCITY 6.00 KM/S







MODEL A LAYER 3 9.5 - 17.0 KM VELOCITY 6.25 KM/S



MODEL B LAYER 3 9.5 - 17.0 KM VELOCITY 6.25 KM/S



MODEL C LAYER 3 11.0 - 20 0 KM VELOCITY 6.25 KM/S

Fig. 5. (continued)



MODEL A LAYER 4 17.0 - 24.5 KM VELOCITY 6.50 KM/S



MODEL B LAYER 4 17.0 - 24.5 KM VELOCITY 6.50 KM/S





Fig. 5d



MODEL A LAYER 5 24.5 -32.0 KM VELOCITY 6.90 KM/S



MODEL B LAYER 5 24.5 - 32.0 KM VELOCITY 6.90 KM/S





Fig. 5. (continued)

| 67           | • | 74   | 0<br>19                             | 88<br>2                             | 95<br>2                              | 102<br>2                             | 109                                  | 0<br>911                             | 621<br>0                            | 0                                   |
|--------------|---|--|-------------------------------------|-------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|-------------------------------------|-------------------------------------|
| <b>9</b> 9 0 |   | 57<br>0  | 80<br>0                             | 3                                   | 94<br>-4,09<br>20<br>0.4029<br>0.79  | 101<br>-1.29<br>12<br>0.1793<br>0.75 | 108<br>-0.69<br>11<br>0.4417<br>0.94 | 211<br>5                             | 122<br>2                            | 129<br>0                            |
| 65           |   | 5  | 79<br>-4.69<br>20<br>0.4062<br>0.86 | 86<br>-2.68<br>20<br>0.4717<br>0.88 | 88"0<br>07<br>80"T-<br>80"T-         | 100<br>-5.11<br>52<br>0.6254<br>0.82 | 107<br>0.80<br>65<br>0.5200          | 114<br>-0.44<br>27<br>0.4136<br>0.86 | 121<br>3.24<br>9.738<br>9.0.94      | 128<br>1                            |
| 64           |   | 17<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,00<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,00000000 | 78<br>-4.65<br>43<br>0.4936<br>0.82 | 85<br>-0.75<br>53<br>0.6296<br>0.79 | 92<br>0.00<br>39<br>0.876<br>0.86    | 99<br>-6.87<br>61<br>0.6940<br>0.77  | 106<br>-3.90<br>0.6602<br>0.82       | 113<br>1.99<br>0.5029<br>0.86        | 120<br>2,46<br>25<br>0,3659<br>0,84 | 127<br>16.0<br>11<br>0.3127<br>0.82 |
| 63           | , | 70<br>1.44<br>20<br>0.4531<br>0.93   | 77<br>-2.17<br>42<br>0.6125<br>0.78 | 84<br>1.53<br>45<br>0.5651<br>0.88  | 16<br>3.44<br>62<br>0.6923           | 98<br>1.07<br>44<br>0.6026<br>0.81   | 105<br>-0.06<br>50<br>0.5740<br>0.75 | 112<br>1.41<br>31<br>0.5428<br>0.80  | 8                                   | 126<br>1                            |
| 62           | • | 69   | 76<br>3.97<br>28<br>0.5296<br>0.76  | 83<br>1.34<br>29<br>0.4537<br>0.83  | 90<br>1.17<br>39<br>0.5101<br>0.5101 | 97<br>3.40<br>12<br>0.5909           | 104<br>0.82<br>54<br>0.5535<br>0.79  | 111<br>1.52<br>32<br>0.4461<br>0.81  | 811<br>64,0<br>11<br>7266.0         | 125<br>3                            |
| 61           | , | 89 O   | 75<br>0                             | <b>6</b> 2                          | 68 0                                 | 96 O                                 | 103<br>-0.14<br>15<br>0.1674<br>0.65 | 0.77<br>0.77<br>16<br>0.3675<br>0.69 | 117                                 | 124                                 |

Layer 3:

|         | 25<br>0                      | 30<br>0                                    | 0<br>SE                              | 40<br>-4.83<br>18<br>0.4664<br>0.86  | 45<br>-6.72<br>29<br>0.5508<br>0.84 | 50<br>5                            | 55<br>2                             | 0                                   |
|---------|------------------------------|--|--------------------------------------|--------------------------------------|-------------------------------------|------------------------------------|-------------------------------------|-------------------------------------|
|         | 24                           | 29<br>-7.94<br>25<br>0.5185<br>0.78        | 34<br>-6.74<br>24<br>0.3675<br>0.90  | 39<br>-10.38<br>46<br>0.6127<br>0.80 | 44<br>0.34<br>0.6617<br>0.70        | 49<br>2.18<br>72<br>0.7005<br>0.65 | 54<br>1.81<br>21<br>0.5139<br>0.75  | 59                                  |
| Layer 2 | 23<br>3.26<br>0.4709<br>0.74 | 28<br>2.82<br>77<br>0.6783<br>0.69         | 33<br>-0.37<br>50<br>0.5698<br>0.85  | 38<br>-1.86<br>69<br>0.6577<br>0.778 | 43<br>1.39<br>63<br>0.4784<br>0.86  | 48<br>4.22<br>53<br>0.6261<br>0.79 | 53<br>2.05<br>55<br>0.6970<br>0.69  | 58<br>2.01<br>17<br>0.5035<br>0.71  |
|         | 22                           | 27<br>4.92<br>33<br>0.4826<br>0.92         | 32<br>47,4<br>74<br>1,6471<br>0,6471 | 37<br>-2.38<br>99<br>0.5888          | 42<br>0.76<br>0.6369<br>0.73        | 47<br>1.30<br>42<br>0.3515<br>0.74 | 52<br>-0.39<br>15<br>0.1607<br>0.64 | 57<br>2                             |
|         | 0                            | 26<br>2.17<br>2.17<br>22<br>0.1775<br>0.65 | 31<br>3.31<br>2.4335<br>0.4335       | 36<br>-0.27<br>118<br>0.291          | 41<br>-0-49<br>35<br>0.4370<br>47.0 | 46<br>3.64<br>0.6126<br>0.60       | 51<br>2.77<br>58<br>0.6310<br>0.68  | 56<br>-2.33<br>10<br>0.2652<br>0.76 |

| nd:  | Block number                      | rays)<br>resolution matrix   |
|------|-----------------------------------|--|
| Lege | Station name<br>Volooit: souturbo | verocity perturve<br>Number of hits (i<br>Diagonal of the r<br>Standard errors |

| ÷     |  |
|-------|--|
| Layer |  |

| mc4 4                                  | nac7 8                                | mca 12                                  | md2 16                                  | 20                                |
|--|---------------------------------------|---|---|-----------------------------------|
| 2.31                                   | 2.53                                  | 4.07                                    | -5.78                                   |                                   |
| 71                                     | 56                                    | 68                                      | 41                                      |                                   |
| 0.2727                                 | 0.2947                                | 0.3116                                  | 0.1554                                  |                                   |
| 0.58                                   | 0.74                                  | 0.70                                    | 0.158                                   |                                   |
| mc3 3<br>0.48<br>81<br>0.2874<br>0.64  | mc6 7<br>1.49<br>63<br>0.3344<br>0.69 | mc9 II<br>1.58<br>37<br>0.2237<br>0.67  | Edl 15<br>-1.94<br>15<br>0.0946         | mcg 19<br>-4.19<br>0.1316<br>0.41 |
| mc2 2<br>-0.11<br>70<br>0.2505<br>0.60 | m5b 6<br>0.08<br>40<br>0.2523<br>0.73 | m8b 10<br>-0.24<br>53<br>0.2377<br>0.73 | mcc 14<br>−6.53<br>43<br>0.1380<br>0.48 | mcf 18<br>1.57<br>0.2990<br>0.63  |
| ac1 1                                  | n5a 5                                 | Ba 9                                    | acb 13                                  | mce 17                            |
| 6.38                                   | -0.29                                 | -0.19                                   | -0.31                                   | 3.31                              |
| 6.3                                    | 21                                    | 19                                      | 67                                      | 79                                |
| 0.3211                                 | 0.2171                                | 0.1405                                  | 0.2599                                  | 0.2393                            |
| 0.66                                   | 0.79                                  | 0.68                                    | 0.62                                    | 0.59                              |

13,882

| 218<br>0                            | 226<br>0                             | 4C2<br>L  | 242   | 250<br>1  | 258<br>0   | 266  | 274  | 282   | 290  | 298<br>0   | 306   |
|-------------------------------------|--------------------------------------|---|---|---|--|--|--|---|--|--|---|
| 217<br>0                            | 225<br>0                             | 233<br>1  | 241<br>2  | 349   | 357  | 33   | 273<br>6   | 281<br>-1.37<br>11<br>0.1970<br>0.71  | 289<br>5   | 297<br>3   | 305   |
| 216<br>1                            | 224                                  | 232<br>5  | 240<br>5  | 248<br>-0.29<br>0.3793<br>0.90  | 256<br>0.81<br>13<br>0.3514<br>0.89  | 264<br>8   | 272<br>-3.96<br>01<br>247<br>0,816<br>0,816  | 280<br>-0.03<br>14<br>0.3183<br>0.86  | 288<br>-1.19<br>23<br>0.3361<br>0.79   | 296<br>0.80<br>20<br>0.2245<br>0.78  | 30E 2   |
| 215<br>7                            | 223<br>1.19<br>12<br>0.2939<br>0.82  | 1<br>-2.53<br>1<br>0.4049<br>0.87   | -1.52<br>-1.52<br>0.4162<br>0.90  | 247<br>0.88<br>38<br>0.4305<br>0.93   | 255<br>-2,80<br>45<br>0,6060<br>0,89   | 263<br>-1.76<br>30<br>0.5318<br>0.91   | 271<br>-2.23<br>23<br>0.5067<br>0.987  | 279<br>-1.90<br>17<br>0.4745<br>0.94  | 287<br>6   | 295<br>1.45<br>0.3166<br>0.3166  | 303<br>0.90<br>14<br>0.2566<br>n.70   |
| 214<br>3.53<br>13<br>0.2756<br>0.81 | 222<br>-0.93<br>18<br>0.3912<br>0.88 | 230<br>1.02<br>23<br>0.4505<br>0.89   | 238<br>-2.01<br>34<br>0.5352<br>0.68  | 246<br>-1.19<br>32<br>0.5166<br>0.94  | 254<br>-2.52<br>43<br>0.5733   | 262<br>-0.53<br>73<br>0.6197<br>0.88   | 270<br>0.23<br>58<br>0.6762<br>0.85  | 278<br>-1.10<br>1.6<br>0.4957<br>0.93   | 286<br>-0.20<br>21<br>0.4541<br>0.91   | 294<br>1.28<br>17<br>0.3121<br>0.89  | 302<br>5  |
| 213<br>3                            | 221<br>B                             | 229<br>-0.53<br>41<br>0.6204<br>0.86  | 237<br>-1.20<br>44<br>0.5880  | 245<br>-0.37<br>0.6097<br>0.90  | -0.63<br>-0.63<br>-0.63<br>-0.63<br>-0.96  | 261<br>97,0<br>20,5302<br>0,999  | 269<br>-0.85<br>46<br>0.5793<br>0.92   | 277<br>-0.41<br>34<br>0.88  | 285<br>2.49<br>15<br>0.3326<br>0.84  | 293<br>1.41<br>17<br>0.3230<br>0.80  | 301<br>-1.38<br>11<br>0.1723<br>17.0  |
| 0<br>217                            | 220                                  | 228<br>-0.62<br>10<br>0.2111<br>0.82  | 236<br>0.59<br>23<br>0.4454<br>0.93   | 244<br>0.09<br>0.4082<br>0.95   | 252<br>1.41<br>0.6074<br>0.92  | 260<br>1.82<br>1.5056<br>0.93  | 268<br>0.97<br>11<br>0.3796<br>0.94  | 276<br>-0.01<br>10<br>0.2490<br>0.79  | 284<br>3   | 292<br>1   | 300<br>1  |
| 0                                   | 219<br>0                             | 227<br>D  | 235<br>17.0<br>15<br>0.2981<br>0.2985   | 243<br>B  | 251<br>0.00<br>15<br>0.3879<br>0.95  | 259<br>n.15<br>18<br>0.4555<br>0.94  | 267<br>-0.35<br>17<br>0.5167<br>0.68   | 275<br>-0.04<br>10<br>0.2403<br>0.67  | 283<br>1   | 291<br>0   | 995<br>0  |
|                                     |                                      |   |   |   |  |  |  |   |  |  |   |
| er 5:                               |                                      |   |   |   |  |  |  |   |  |  |   |
| Layer 5:                            | L                                    | 13e   | 146<br>D  | 154<br>D  | 162<br>0   | 170<br>0   | 178<br>1   | 186<br>1  | 194<br>0   | 202<br>0   | 210<br>0  |
| Layer 5:                            |                                      | 137 138<br>0 0  | 145 146<br>0 0  | 153 154<br>2 0  | 161 162<br>2 0   | 169 170<br>2 D   | 177 178<br>0 1   | 185 186<br>0.68 1.68 1.6<br>11 1<br>0.3592 0.68   | 193 194<br>8 0   | 201 202<br>1 0   | 209 210<br>0 0  |
| Layer 5:                            |                                      | 136 137 136<br>1 0 1  | 144 145 146<br>2 0 0  | 152 153 154<br>6 2 0  | -0.460 161 162<br>-0.469 2<br>0.3692 2 0   | 168 169 170<br>-161 26 20<br>262 2 0<br>0.4458 2 0   | 176 117 178<br>-1.76 0 1<br>0.419 0 1  | 184 185 186<br>-4.39 0.66<br>15 11 1<br>0.3772 0.3992 0.88  | 0.192 193 194 0.194 0.194 0.194 0.194 0.195 0.041400 0.04140000000000   | 0.240 201 202<br>0.56 1 20<br>0.945 1 0<br>0.945 0.69  | 288 209 210<br>5 0 0  |
| Layer 5:                            | r 4:                                 | 135 126 121 136<br>0 1 0 0  | -2.43 144 145 146<br>-2.43 2 0 0<br>0.363 2 0 0   | -1.55 153 154<br>-1.55 153 154<br>0.4260 6 2 0<br>0.4260 0.90   | -2.04 161 162<br>-2.04 -0.99 161 162<br>0.501 0.562 2 0<br>0.503 0.692 2   | 0.267 -1.648 169 170<br>228 -1.64<br>0.5631 0.4438 2<br>0.286 0.677  | -2.05 -1.76 1.77 1.76<br>-2.05 -1.76 1.7<br>0.5719 0.4129 0.412<br>0.687 0.412   | -4.18 184 0.68 166<br>-4.18 -4.38 0.69 16<br>0.9918 0.177 0.1322 0.1322 0.902 0.64  | 0.02 191 192 193 194 0.02 0.16 192 0.16 193 0.16 193 0.16 194 0.02 194 0.02 195 0.16 195 0.02 195 0.00 | 199 200 201 202<br>7 0.56 1 0<br>0.949 1 0<br>0.43   | 207 288 209 210<br>0.43 5 0 0<br>1.23 5 0 0<br>0.75 5 0   |
| Layer 5:                            | Layer 4:                             | 134 135 136 137 136<br>1.36 13 136 137 136<br>0.301 8 1 0 0<br>0.202 0.72       | 0.142 14.3 14.4 14.5 14.6<br>0.17 -2.13 24.0 14.5 14.6<br>0.1702 0.588 2 0 0<br>0.87 0.788 2.78       | -150 151 152 154<br>-1.90 -1.55 153 154<br>0.5043 0.4260 6 2 0<br>0.5043 0.4200 6 2   | 158 -2.04 160 161 162<br>0.78 -2.04 -0.49 161 162<br>0.552 0.501 0.562 2<br>0.65 0.490 0.69                        | -0.16 1.67 1.68 1.69 1.70<br>-0.10 1.22 -1.61 1.69 1.70<br>0.5540 0.5631 0.4436 2 0<br>0.574 0.764               | -174 -2.05 -175 177 178<br>-1.60 -2.05 -1.76 177 178<br>0.6380 0.7719 0.4113 0 1<br>0.64 0.877 0.4113                            | -2.14 183 184 184 184 185 186<br>-2.14 -4.18 -4.28 0.68 186<br>0.452 0.9918 0.172 0.392 1<br>0.433 0.64 0.452 0.392                                     | 0.22 0.191 0.192 193 194 1.22 0.269 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16  | 19e         199         200         201         202           1.37         0.56         0.56         1         0           0.4290         0.599         1         0         0           0.6130         0.619         0.799         1         0 | 206         207         288         209         210           6         0.43         5         0         0           6         0.1871         5         0         0           0.755         5         0         0         0   |
| Layer 5:                            | Layer 4:                             | 134 135 136 137 136 137 136 137 136 137 136 136 136 136 136 136 136 136 136 136 | 141 0.12 - 143 144 145 146<br>0.17 - 2.13 144 145 146<br>0.1984 0.170 0.588 2 0 0<br>0.186 0.87 0.588 | -0.50 -3.150 -1.51 1.52 1.53 1.54 -0.50 -1.59 -1.55 1.53 1.54 -1.55 1.57 1.53 1.54 -1.55 1.57 1.57 1.57 1.57 1.57 1.57 1.57 | 0.55 0.58 1.59 1.60 161 162<br>0.53 0.88 2.04 0.69 161 162<br>0.537 0.552 0.590 0.562 2<br>0.536 0.555 0.690 0.569 | 165 166 157 168 167 170<br>-0.13 -0.10 0.12 1-61 20<br>253 0.554 0.554 0.561 0.648 2 0<br>0.564 0.580 0.563 0.67 | 1/2 1/2 1/2 1/2 1/2 1/2 1/6 1/7 1/6<br>2.25 -1.60 -2.05 -1.76 1/7 1/6<br>0.6639 0.5380 0.5779 0.412 0<br>0.682 0.644 0.677 0.412 | 0.161 1.182 1.83 1.843 1.844 0.648 1.65<br>0.70 -2.14 4.18 -4.28 0.648 1.6<br>0.4605 0.4425 0.9918 0.772 0.392 0.485<br>0.693 0.4423 0.9918 0.772 0.492 | 0.00 0.72 0.191 0.192 193 194 194 0.00 0.00 0.102 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16  | 0.00 1.7 199 0.500 201 202<br>0.00 1.7 0.56 201 202<br>0.384 0.220 7 0.5949 1 0<br>0.884 0.650 7 0.2949 1 0  | 205         206         207         208         209         210           -0.61         0.43         5         0.43         5         0         0           13         6         0.2872         5         0         0         0         0           20.66         0.7872         5         0         0         0         0         0           20.66         0.7872         5         0 |

131 0

D

1

-0.74 -0.74 0.1379 0.61

0.06 0.2930 0.65

1

Fig. 6a. Model A. Note that layers 2–5 are shown in approximately correct geographic arrangement, though the blocks should be square. The plus corresponds to the "model center" in Figure 1; the top of the figure is "northwest." For layer 1, compare station names with Figure 1.

Legend:

Station name Block number Velocity perturbation Number of hits (rays) Diagonal of the resolution matrix Row 99 of the resolution matrix Standard errors Row 99 of the covarience matrix

Layer 1:

| mc4 4<br>0.12<br>0.2427<br>0.49<br>-0.0016                | mc7 8<br>0.52<br>0.2605<br>-0.0029<br>0.63<br>0.085         | mca 12<br>1.42<br>68<br>0.2765<br>0.0196<br>0.60<br>-0.60            | md2 16<br>-1.57<br>41<br>0.2345<br>0.230<br>0.59<br>0.030  | 20   |
|---|---|--|--|--|
| mc3 3<br>0.91<br>81<br>0.2882<br>0.0126<br>0.57<br>0.57   | mc6 7<br>63<br>63<br>0.3203<br>-0.0014<br>0.61              | mc9 11<br>1.78<br>37<br>0.2237<br>-0.0241<br>0.59<br>-0.218          | mdi 15<br>-1.92<br>15<br>0.1229<br>0.015<br>0.57<br>0.57   | mcg 19<br>-0.76<br>42<br>0.1816<br>0.0005<br>0.41<br>0.023   |
| mc 2 2<br>0.75<br>70<br>0.2504<br>0.0060<br>0.53<br>0.085 | m5b 6<br>0.38<br>40<br>0.2533<br>-0.0005<br>0.65<br>-0.002  | 10 10<br>-0.41<br>53<br>0.2372<br>0.2372<br>0.0491<br>0.64<br>-0.273 | mcc 14<br>-2.45<br>43<br>0.2111<br>0.0078<br>0.50<br>0.122 | BLCE 18<br>0.86<br>0.2881<br>0.2881<br>0.57<br>0.57<br>0.252 |
| acl 1<br>2.01<br>69<br>0.2564<br>-0.0019<br>0.54<br>0.54  | m5a 5<br>0.25<br>0.2175<br>0.2175<br>0.2175<br>0.70<br>0.70 | mBa 9<br>-0.10<br>19<br>0.1406<br>0.0003<br>0.60<br>-0.034           | meb 13<br>0.52<br>67<br>0.2613<br>-0.0062<br>0.56          | mce 17<br>0.53<br>0.53<br>0.2101<br>0.0371<br>0.50<br>-0.279 |

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| ayer 2: | 23<br>7 58 |
| -       | ~          |

| 25<br>0   | 9<br>0  | 0<br>50  | 0,<br>10,<br>11,<br>10,<br>11,<br>10,<br>10,<br>10,<br>10,<br>10,<br>1 | 45<br>-1.64<br>33<br>0.5324<br>0.0020<br>0.71<br>0.085         | 50<br>S  | 55<br>2  | 0   |
|---|---|--|--|--|--|--|---|
| 24  | 22<br>24<br>25<br>0.4839<br>0.67<br>0.67<br>0.67      | 4<br>2,27<br>25<br>0,08<br>25<br>0,08<br>26<br>0,08<br>0,77<br>0,107 | 210<br>210<br>210<br>210<br>210<br>210<br>210<br>210<br>210<br>210     | 44<br>-1.13<br>75<br>0.6663<br>0.0603<br>0.603<br>0.723        | 64<br>11.0<br>72<br>0.0009<br>0.338<br>0.376       | 54<br>1.27<br>21<br>0.5173<br>-0.0013<br>0.67<br>-0.026          | 2   |
| 23<br>2.58<br>2.5<br>0.4791<br>0.0003<br>0.613<br>0.013 | 28<br>1.78<br>7.5<br>0.6850<br>0.0017<br>0.62<br>0.62 | 33<br>-1.17<br>48<br>0.5646<br>0.76<br>0.76<br>0.359                 | 38<br>-1.59<br>72<br>0.6563<br>0.0713<br>0.69<br>-0.270                | 43<br>1.03<br>64<br>0.4780<br>0.4780<br>0.76<br>0.76<br>-0.174 | 48<br>2.33<br>0.6364<br>0.0401<br>0.70<br>-0.274   | 53<br>1.49<br>56<br>0.6974<br>0.61<br>0.61                       | 58<br>2,53<br>17<br>0,5037<br>0,637<br>0,63<br>0,63 |
| 22<br>4   | 27<br>2.90<br>34<br>0.5066<br>0.0003<br>0.82<br>0.82  | 32<br>1.83<br>0.6531<br>-0.0023<br>0.69<br>0.69                      | 37<br>-1,44<br>102<br>0.5868<br>0.0039<br>0.186                        | 42<br>1.61<br>95<br>0.6353<br>0.0082<br>0.082<br>0.64          | 47<br>0.54<br>42<br>42<br>0.3586<br>0.566<br>0.190 | 52<br>-0.79<br>15<br>0.1642<br>-0.0009<br>-0.016                 | 2   |
| 5 0   | 26<br>1.35<br>23<br>0.2076<br>0.0007<br>0.60<br>0.60  | 31.45<br>1.45<br>0.0006<br>0.0006<br>0.63<br>0.035                   | 36<br>0.19<br>18<br>0.2976<br>0.64<br>0.64                             | 41<br>-0.17<br>36<br>0.6344<br>-0.0035<br>0.66<br>-0.062       | 46<br>1.37<br>0.6255<br>0.0004<br>0.0011           | 51<br>2.97<br>5.97<br>0.6343<br>0.6343<br>0.001<br>0.61<br>0.006 | -2.02<br>-2.02<br>10<br>0.2658<br>0.0000<br>0.000   |

| P  | -1.<br>0.48<br>0.00<br>0.0                                   | -0.<br>-0.62<br>-0.02   | 0.59<br>-0.25<br>-0.2                                    | -6.<br>0.69                |
|--|--|---|--|----------------------------|
| 70<br>1.50<br>20<br>0.4605<br>-0.0014<br>-0.0014 | 77<br>-2.38<br>42<br>42<br>0.6116<br>0.012<br>0.69<br>-0.002 | 84<br>1.91<br>4.2<br>0.5646<br>0.78<br>0.78<br>0.78   | 91<br>2.59<br>0.6910<br>0.6910<br>0.68<br>0.6910<br>0.68 | 96<br>1.08<br>48           |
| 69   | 76<br>1.57<br>0.5327<br>0.0010<br>0.68<br>-0.024             | 69<br>86.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1924.0<br>1 | 90<br>0.98<br>39<br>0.5104<br>-0.0024<br>0.72<br>-0.226  | 79<br>2.92<br>51<br>0.5117 |
| 89 0   | 27<br>5  | 82<br>5   | 69   | 0<br>96                    |
|  |  |   |  |                            |

| 67<br>0        | 74   | 61   | 86<br>2  | 95<br>2  | 2<br>2  | 109<br>2  | 0<br>911  | 123<br>0  | 130<br>0  |
|----------------|--|--|--|--|---|---|---|---|---|
| 990            | £7<br>0  | 0  | 87<br>E  | 94<br>-1.91<br>20<br>0.3963<br>-0.0030<br>0.68           | 101<br>-1.00<br>13<br>0.1768<br>0.0009<br>0.66<br>0.046                           | 108<br>0.32<br>11<br>0.4384<br>-0.0059<br>0.84<br>0.114                 | 5<br>5  | 122<br>2  | 129<br>D  |
| 65             | 9  | 79<br>-2.47<br>20<br>0.3962<br>-0.0001<br>0.75<br>-0.020 | 86<br>-0.44<br>20<br>0.4622<br>0.0011<br>0.79<br>-0.272  | 93<br>-0.93<br>41<br>0.5869<br>-0.0537<br>0.78<br>-0.147 | 100<br>-3.31<br>53<br>53<br>53<br>53<br>53<br>0.6285<br>-0.0518<br>0.73<br>-0.528 | 107<br>1.00<br>65<br>0.5204<br>-0.0395<br>0.74<br>-0.492                | 114<br>-0.82<br>27<br>0.4127<br>-0.0018<br>0.76<br>-0.104 | 1,21<br>3,22<br>1,4<br>0,3722<br>0,0000<br>0,83<br>-0,004 | 126<br>1  |
| 64<br>9        | 71<br>-0.14<br>- 27<br>0.3846<br>0.0003<br>0.72<br>0.72<br>0.003 | 78<br>41.74<br>41<br>0.4849<br>0.0033<br>0.73<br>0.73    | 85<br>-0.90<br>53<br>0.6294<br>-0.0248<br>0.70<br>-0.70  | 92<br>0.26<br>39<br>0.5918<br>-0.0516<br>0.77<br>-0.250  | 99<br>-6.93<br>-6.93<br>0.6957<br>0.6857<br>0.68                                  | 106<br>-3.58<br>-3.58<br>-3.58<br>-3.58<br>-0.6604<br>-0.0771<br>-0.771 | 113<br>1.91<br>44<br>0.4994<br>0.074<br>0.77              | 120<br>2.2<br>25<br>0.3644<br>0.0009<br>0.75<br>0.75      | 127<br>0.57<br>13<br>0.3128<br>0.0009<br>0.72<br>0.72 |
| <b>63</b><br>0 | 70<br>1.50<br>20<br>0.4605<br>-0.0014<br>0.82<br>-0.004          | 77<br>-2.38<br>42<br>0.6116<br>0.0012<br>0.69<br>-0.002  | 84<br>1.91<br>4.2<br>0.5646<br>-0.0073<br>0.78<br>-0.195   | 91<br>2.59<br>0.6910<br>-0.0387<br>0.68<br>0.114         | 98<br>1.08<br>0.5947<br>-0.0250<br>0.72   | 105<br>-0.22<br>51<br>0.5721<br>-0.0309<br>0.66<br>-0.302               | 112<br>1.19<br>31<br>0.5437<br>-0.0037<br>0.72<br>-0.199  | 611<br>8  | 126<br>1  |
| 62             | 69   | 76<br>1.57<br>28<br>0.5327<br>0.0010<br>0.0010           | 63<br>86.0<br>162<br>162<br>162<br>162<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10 | 90<br>0.98<br>39<br>0.5104<br>-0.0024<br>0.72            | 97<br>2.92<br>51<br>0.5917<br>-0.0029<br>-0.144                                   | 104<br>0.83<br>53<br>0.5549<br>-0.0040<br>0.70                          | 111<br>1.31<br>0.4502<br>0.72<br>0.72<br>0.72             | 118<br>0.83<br>11<br>0.3343<br>0.0001<br>0.65<br>0.001    | 221<br>E  |
| 61             | 68<br>0  | 3  | 93 S   | 58 0   | 96<br>0   | 103<br>-0.12<br>1.1679<br>0.0004<br>0.58<br>0.58                        | 110<br>1.000<br>1.3680<br>-0.0004<br>-0.003               | 11  | 124<br>0  |

| caption.   |
|------------|
| igure 6a ( |
| B. See F   |
| Model      |
| 6b.        |
| Fig.       |

| 218<br>0   | 226<br>0   | 234<br>1  | 242<br>1  | 250<br>1  | 258<br>0  | 266  | 274<br>2   | 282  | 290<br>2   | 298<br>0   | 306  |
|--|--|---|---|---|---|--|--|--|--|--|--|
| 217<br>0   | 0<br>0   | EE2   | 241   | 33  | 722<br>3  | 265<br>3   | 273<br>6   | 281<br>-0.53<br>11<br>11<br>110.0<br>2012<br>0.083       | 5  | 3  | 305<br>D   |
| 216<br>1   | 224  | 252<br>5  | 240<br>6  | 248<br>-0.36<br>13<br>0.3793<br>0.0043<br>0.79<br>0.123 | 256<br>0.06<br>1.3<br>0.0051<br>0.0051<br>0.79<br>0.115 | 264<br>8   | 272<br>-2.18<br>10<br>0.3155<br>0.0096<br>0.75<br>0.75       | 280<br>0.45<br>13<br>0.3011<br>0.0037<br>0.76<br>0.277   | 288<br>-0.62<br>23<br>0.1335<br>0.0006<br>0.70<br>0.70 | 296<br>1.02<br>20<br>0.2161<br>-0.0009<br>0.68             | 304  |
| 215  | 223<br>2.15<br>12<br>0.2972<br>-0.0014<br>0.73         | 231<br>-2.21<br>17<br>0.4019<br>-0.0019<br>0.78         | 239<br>-1.22<br>-1.22<br>23<br>-0.44<br>0.44<br>0.80<br>0.00<br>0.070 | 247<br>-1.68<br>37<br>0.4322<br>0.0040<br>0.82<br>0.086 | 255<br>-3.02<br>45<br>0.6027<br>0.0153<br>0.086         | 263<br>-1.97<br>30<br>0.5309<br>-0.0086<br>0.81<br>0.81        | 271<br>-1.90<br>23<br>23<br>0.5102<br>0.0275<br>0.87<br>0.87 | 279<br>-1.18<br>17<br>0.4724<br>0.083<br>0.83            | 287<br>6   | 295<br>0.91<br>0.91<br>0.10<br>0.0004<br>0.80<br>0.80      | 303<br>0.74<br>1.74<br>0.2567<br>0.0001<br>0.021 |
| 214<br>2.97<br>13<br>0.2752<br>-0.0003<br>0.72<br>-0.010 | 222<br>-1.15<br>19<br>0.3843<br>0.0000<br>0.78<br>0.78 | 052<br>15.0-<br>55<br>64244.0<br>64.0<br>020.0          | 238<br>54.1-<br>54<br>0,5583<br>6010-0-<br>97.0<br>0.78               | 246<br>-0.14<br>32<br>0.5200<br>0.0202<br>0.83<br>0.125 | 254<br>-2.65<br>43<br>0.5786<br>0.0672<br>0.82          | 262<br>-0.96<br>73<br>873<br>0.6206<br>0.148<br>0.0148<br>0.78 | 270<br>0.29<br>58<br>58<br>0.6832<br>0.0263<br>0.74<br>0.74  | 278<br>-1.17<br>18<br>0.4951<br>0.0087<br>0.82<br>-0.074 | 286<br>036<br>0.4512<br>0.0653<br>0.063                | 294<br>2.8.0<br>8.1<br>8.0<br>1.10<br>0.0<br>0.70<br>0.040 | 302<br>5   |
| 213<br>4   | 221<br>8   | 229<br>-0.20<br>40<br>0.6177<br>0.0003<br>0.76<br>0.010 | 2.17<br>-0.53<br>0.54<br>0.5879<br>0.038<br>0.79<br>-0.044            | 245<br>0.02<br>40<br>0.6128<br>0.0000<br>0.80<br>0.96   | 253<br>0.17<br>38<br>0.5176<br>0.0031<br>0.83<br>0.128  | 261<br>0.43<br>0.5357<br>0.0184<br>0.0184<br>0.87<br>-0.008    | 269<br>2.5788<br>0.05788<br>0.05788<br>0.05788<br>0.110      | 772<br>0.20<br>34<br>0.5277<br>0.0066<br>87<br>0.029     | 285<br>1.95<br>1.5<br>0.3237<br>0.0014<br>0.74<br>0.74 | 293<br>1.50<br>1.7<br>0.3233<br>-0.0024<br>-0.016          | 301<br>-1.38<br>11<br>0.1772<br>0.0003<br>0.64   |
| 0  | 220  | 228<br>-0.48<br>0.2115<br>-0.0002<br>0.73<br>0.73       | 2.76<br>0.84<br>23<br>0.4566<br>-0.0001<br>0.82<br>-0.031             | 244<br>0.40<br>18<br>0.4047<br>-0.0023<br>-0.84         | 252<br>1.73<br>51<br>0.6098<br>-0.0020<br>0.82<br>0.036 | 260<br>1.82<br>42<br>0.5069<br>0.0032<br>0.82<br>0.140         | 268<br>0.87<br>30<br>0.3771<br>0.0055<br>0.84<br>0.162       | 276<br>-0.07<br>10<br>0.2490<br>0.70<br>0.70             | 3  | 292<br>1   | 1<br>1   |
| 112  | 0  | 227<br>0  | 212<br>20.00-<br>21<br>2090 0.0000<br>27.0<br>27.0                    | 243<br>8  | 251<br>0.28<br>15<br>0.3878<br>0.3878<br>0.84<br>0.84   | 259<br>0.50<br>0.4562<br>0.4562<br>0.84<br>0.018               | 267<br>-0.16<br>17<br>0.5174<br>0.0002<br>0.78<br>0.036      | 275<br>-0.03<br>10<br>0.2404<br>0.60<br>0.009            | 283<br>1   | 291<br>10  | 0  |

# Layer 5:

Layer 4:

| 138<br>0                                     | 146   | 154<br>0  | 162<br>0   | 170<br>0  | 178<br>1  | 186<br>1   | 0<br>9  | 202<br>0   | 0  |
|--|---|---|--|---|---|--|---|--|--|
| 761<br>0                                     | 0<br>59T  | 153<br>2  | 161 2  | 2   | 0<br>771  | 185<br>1.466<br>1.1<br>0.3568<br>-0.0066<br>0.77<br>-0.071 | 601<br>B  | 201<br>2   | 209<br>D   |
| 136<br>L                                     | т<br>194  | 152<br>6  | 160<br>14.0-<br>13<br>13<br>13<br>13<br>13<br>14<br>14<br>14<br>13<br>13<br>13<br>13<br>13<br>13<br>13<br>13<br>13<br>13<br>13<br>13<br>13 | 168<br>-0.83<br>26<br>0.4440<br>0.0042<br>0.077<br>0.77                       | 176<br>-1.02<br>20<br>0.4132<br>0.0037<br>0.87<br>0.87<br>0.321 | 184<br>-2.47<br>1.5<br>0.3769<br>0.0078<br>0.076<br>0.213  | 192<br>0.49<br>16<br>0.4185<br>0.0034<br>0.74<br>0.154  | 200<br>0.28<br>23<br>0.4037<br>-0.0008<br>0.74           | 208  |
| 261<br>8                                     | 143<br>-1.10<br>17<br>0.3627<br>-0.0006<br>0.69<br>0.005      | - 151<br>-1.36<br>1.4179<br>-0.0023<br>0.80<br>-0.077     | 159<br>-2.30<br>36<br>0.5747<br>-0.0037<br>0.74<br>0.74  | 167<br>-0.20<br>50<br>0.5741<br>0.0184<br>0.76<br>0.76                        | 175<br>-2.20<br>44<br>0.5702<br>0.0466<br>0.77<br>0.071         | 183<br>-3.59<br>0.5916<br>0.0516<br>0.0575<br>-0.417       | 191<br>12<br>12<br>0.3623<br>0.0900<br>484<br>0.134     | 199  | 207<br>0.13<br>0.2872<br>0.0003<br>0.67          |
| 134<br>0.93<br>18<br>0.0000<br>0.640<br>0.64 | 142<br>-0.48<br>33<br>33<br>0.4712<br>0.0009<br>0.77<br>0.000 | 150<br>-1.20<br>32<br>0.4982<br>-0.0069<br>0.72<br>-0.090 | 158<br>1.13<br>38<br>0.5492<br>-0.0248<br>0.75<br>0.75   | 166<br>-0.32<br>33<br>0.5547<br>0.0089<br>0.78<br>-0.060                      | 174<br>-1.90<br>68<br>0.6402<br>0.1294<br>0.74<br>-1.600        | 182<br>-1.83<br>-1.83<br>0.5449<br>0.0198<br>0.73<br>0.73  | 190<br>1.11<br>32<br>0.0046<br>0.0046<br>0.027          | 198<br>1.18<br>20<br>0.4308<br>-0.0008<br>0.74<br>-0.033 | 206<br>6   |
| 5  | 141<br>2.02<br>35<br>0.4933<br>-0.0009<br>0.76<br>0.72        | 149<br>-0.16<br>47<br>0.5692<br>0.0001<br>0.74<br>-0.041  | 157<br>0.44<br>43<br>0.0314<br>0.0027<br>0.76<br>0.78  | 165<br>-0.32<br>53<br>53<br>53<br>53<br>53<br>0.6556<br>0.030<br>0.72<br>0.72 | 173<br>2.45<br>47<br>0.6558<br>0.0012<br>0.73<br>0.73           | 181<br>0.31<br>45<br>0.5618<br>0.0043<br>0.74<br>0.148     | 189<br>0.71<br>43<br>43<br>0.0065<br>0.73<br>0.060      | 197<br>-0.91<br>21<br>0.3893<br>0.0006<br>0.74<br>0.062  | 202<br>ET.0-<br>E1<br>2000.0<br>2000.0<br>2000.0 |
| 2£1<br>0                                     | 7<br>7  | 148<br>1.88<br>15<br>0.3557<br>-0.0005<br>0.71<br>-0.002  | 156<br>0.90<br>0.4309<br>0.0002<br>0.74<br>0.035   | 164<br>0.16<br>25<br>0.4852<br>-0.0002<br>0.73<br>0.73                        | 172<br>-0.18<br>34<br>0.5517<br>0.006<br>0.77<br>0.068          | 180<br>1.70<br>33<br>0.4827<br>0.0013<br>0.048             | 188<br>0.73<br>12<br>0.2447<br>0.0004<br>0.70<br>0.018  | 196<br>0   | 204<br>1   |
| 161  | 139   | 4   | 155  | 163   | 171   | 179<br>-0.59<br>0.1497<br>0.0001<br>0.019                  | 187<br>0.00<br>111<br>0.2931<br>0.2003<br>0.58<br>0.010 | 195  | 203  |

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| 67<br>0      | 74                                 | 81<br>0                      | 88<br>0                                  | 0<br>56   | 1<br>201                             | 0<br>60T                               | 0<br>9TT                                | 12 <b>3</b><br>0                    | 0<br>0E1             |
|--------------|------------------------------------|------------------------------|--|---|--------------------------------------|--|---|-------------------------------------|----------------------|
| 99 D         | 73<br>0                            | 80<br>0                      | 87<br>4                                  | 94<br>-1.57<br>15<br>0.5516<br>1.10                               | 101<br>1                             | 108<br>2.03<br>13<br>0.5995<br>1.13    | E                                       | 122<br>0                            | 129<br>0             |
| <b>6</b> 0   | 72<br>3                            | 79<br>-0,40<br>15<br>10,5361 | 86<br>2.11<br>21<br>21<br>0.6607<br>1.07 | 54<br>1,43<br>1,43<br>1,43<br>1,43<br>1,43<br>1,43<br>1,43<br>1,4 | 100<br>-2.60<br>48<br>0.8145<br>0.81 | 107<br>0.16<br>45<br>0.7182<br>0.95    | 114<br>-1.33<br>-1.33<br>0.5433<br>0.92 | 121                                 | 128<br>0             |
| 7 <b>6</b> 7 | 71<br>2,99<br>26<br>0,7279<br>1,00 | 78<br>1.19<br>49<br>0.7000   | 85<br>-0.11<br>62<br>0.7785<br>0.83      | 92<br>1,44<br>0,8096<br>0,80                                      | 99<br>-6.53<br>78<br>0.8260          | 106<br>-4,47<br>75<br>0.8194<br>0.8194 | E6*0<br>B669*0<br>IE<br>E11             | 120<br>0.87<br>15<br>0.5646<br>0.92 | 9<br>121             |
| • •          | 70<br>7                            | 77<br>-0.37<br>57<br>0.7000  | 84<br>1.82<br>56<br>0.7476<br>0.89       | 91<br>3,73<br>67<br>0.8257<br>0.74                                | 98<br>0.99<br>0.8084<br>0.8084       | 105<br>-0.74<br>62<br>0.8034<br>0.79   | 112<br>-1.48<br>42<br>0.7577<br>0.85    | 6                                   | 12 <del>6</del><br>0 |
| 62           | 69 0                               | 76                           | 83<br>1.45<br>25<br>0.5943<br>0.61       | 90<br>1,66<br>34<br>0,5804  | 97<br>1.91<br>55<br>0.7730           | 104<br>3.38<br>6.<br>0.7034<br>0.93    | 111<br>2.32<br>18<br>0.4879<br>1.17     | 6<br>BTT                            | 125<br>1             |
| ē 0          | 68                                 | 75<br>0                      | 62<br>0                                  | 0   | 96                                   | 103                                    | 9                                       | 117<br>0                            | 124                  |
|              |                                    |                              |  |   |                                      |  |   |                                     |                      |

|          | 25 | o  | 90         | 0                    | <b>SE</b> | 0                    | 40<br>-0.61 | 0.6300                | 45<br>-1.28 | 32<br>0.6736<br>0.85  | 20       | e.                            | 55 | 0                          | 09          | 0    |
|----------|----|----|------------|----------------------|-----------|----------------------|-------------|-----------------------|-------------|-----------------------|----------|-------------------------------|----|----------------------------|-------------|------|
| Layer 2: | 24 | o  | 29<br>1.00 | 14<br>0.2938<br>0.97 | 1E 59     | 40<br>0.6265<br>0.98 | 90<br>-2.87 | 50<br>0.7,300<br>0.83 | 44<br>-0.14 | 92<br>0.7777<br>0.74  | 46       | 0.2.2<br>90<br>0.7905<br>0.67 | 54 | 00°1<br>1665-0<br>1.00     | 65          | o    |
|          | 23 | 80 | 28<br>1.28 | 69<br>0.7189<br>0.77 | 33        | 87<br>0.7812<br>0.78 | 38<br>-1,79 | 63<br>0.8208<br>0.71  | 43<br>0.55  | 0.7174                | 64<br>67 | 46<br>46<br>0.7490<br>0.78    | 53 | 0.73<br>0.7651<br>0.73     | 85<br>-1 15 | 0.93 |
|          | 22 | 0  | 27<br>1.68 | 23<br>0.1875<br>0.71 | 32        | 0.7664               | 37<br>-0.48 | 0.7780                | 42<br>1.24  | 116<br>0.7879<br>0.70 | 47       | 0.7439                        | 52 | 0,2273<br>0,2273<br>0,84   | 57          | 0    |
|          | 12 | 0  | 26         | 0                    | и<br>ц    | 0.2692               | 36<br>-0.23 | 0.1054                | 41<br>0.18  | 32<br>0.2606<br>0.96  | 97<br>97 | -0.7446<br>0.7446<br>0.88     | я, | 42<br>42<br>0.7608<br>0.80 | 56          | m    |

| Legend: |  |
|---------|--|

| - | number         | matrix                               |
|---|----------------|--------------------------------------|
|   | Block          | ()<br>olution                        |
|   | e<br>rturbatic | lts (raye<br>the reac<br>rors        |
|   | ation name     | umber of h<br>agonal of<br>andard er |

Layer 1:

Г

| 0.3271<br>1.05                          | #8b 10<br>-0.31<br>53<br>0.3424<br>1.05 | adi 15<br>-2.81<br>-2.81<br>15<br>0.2144<br>0.99 | 20                                      |
|---|---|--|---|
| mc4 4<br>0.97<br>71<br>0.4308<br>1.00   | n8a 9<br>-0.10<br>19<br>0.2292<br>0.98  | mcc 14<br>-3.93<br>43<br>0.2981<br>0.86          | ncg 19<br>-0.70<br>42<br>0.2025<br>0.58 |
| at c3 3<br>0.87<br>81<br>0.3226<br>Λ.91 | mc7 8<br>0,53<br>56<br>0,3487<br>0,98   | mcb 13<br>-1.25<br>67<br>0.2366                  | mcf 18<br>0.40<br>0.2855<br>0.2855      |
| nc2 2<br>0.34<br>70<br>0.2710<br>0.86   | mc6 7<br>1.64<br>0.3188<br>0.8188       | BCA 12<br>0,56<br>68<br>0,3027<br>0.87           | mce 17<br>0.41<br>79<br>0.2612<br>0.81  |
| c1 1<br>1.83<br>69<br>0.2985<br>0.86    | 5b 6<br>0.73<br>40<br>0.3468<br>0.99    | e9 11<br>3.67<br>37<br>0.3077<br>0.98            | 12 16<br>-2.28<br>41<br>0.3226<br>0.97  |

| 218<br>0 | 226<br>0                            | 234<br>0                             | 242<br>0                             | 250<br>0                             | 258<br>0                             | 266<br>D                             | 2<br>7/2                             | 282<br>1                             | 290<br>1                             | 298<br>0                            | 0<br>90£  |
|----------|-------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|-------------------------------------|-----------|
| 217<br>0 | 225<br>0                            | 233<br>2                             | 241<br>2                             | 249                                  | 257<br>2                             | 265<br>2                             | 273<br>ع                             | 281<br>9                             | 289                                  | 297<br>2                            | 0<br>\$0£ |
| 216<br>1 | 224<br>1                            | 262<br>4                             | 240                                  | 248<br>-1.13<br>12<br>0.5890<br>1.12 | 256                                  | 264                                  | 272<br>-1.48<br>11<br>0.4468<br>1.17 | 280<br>-0.63<br>12<br>0.4882<br>1.12 | 288<br>-1.55<br>21<br>0.4978<br>0.84 | 296<br>2.35<br>14<br>0.4704<br>1.08 | 304<br>5  |
| 215      | 223<br>B                            | 162<br>                              | 239<br>-0.99<br>28<br>0.5903<br>1.05 | 247<br>-2.43<br>34<br>0.7120<br>0.98 | 255<br>-1.90<br>44<br>0.7807<br>0.90 | 263<br>-0.54<br>29<br>0.6532<br>1.11 | 271<br>-1.46<br>0.7392<br>0.99       | 279<br>8107-0<br>26<br>279<br>279    | 287<br>-0,85<br>0,4669<br>0,4669     | 295<br>0.66<br>15<br>0.4856<br>0.98 | 505<br>6  |
| 214<br>6 | 222<br>1.66<br>18<br>0.5332<br>1.06 | 230<br>-1.46<br>27<br>0.6594<br>1.03 | 238<br>10.2-<br>14<br>0.7205<br>0.97 | 246<br>-0.16<br>38<br>0.7383<br>0.98 | 254<br>-0.93<br>54<br>0.7839<br>0.90 | 262<br>-0.68<br>66<br>0.8207<br>0.82 | 270<br>1.33<br>53<br>0.8225<br>0.61  | 278<br>-2,45<br>31<br>0.7005<br>1.03 | 286<br>1.50<br>25<br>0.6619<br>1.01  | 294<br>0.97<br>14<br>0,5542<br>1.09 | £<br>20£  |
| 213<br>1 | 221<br>6                            | 229<br>2.99<br>34<br>0.7243<br>0.96  | 237<br>0.04<br>56<br>0.7543<br>0.90  | 245<br>-0.67<br>63<br>0.8043<br>0.86 | 253<br>0.50<br>54<br>0.8063<br>0.86  | 261<br>-2.59<br>57<br>0.7857<br>0.91 | 269<br>-1.22<br>39<br>0.7538<br>0.96 | 277<br>0.80<br>1.9<br>0.6811<br>1.04 | 285<br>3.12<br>1.5<br>0.6013         | 293<br>0.16<br>11<br>0.4173<br>1.07 | E<br>10E  |
| 212<br>0 | 220<br>0                            | 228<br>5                             | 236<br>2.46<br>17<br>0.6135<br>1.10  | 244<br>-0.93<br>28<br>0.6368<br>1.05 | 252<br>0.43<br>37<br>0.7323<br>0.96  | 260<br>1.04<br>34<br>0.7403<br>0.95  | 268<br>0.90<br>28<br>0.6151<br>1.11  | 276<br>3                             | 284<br>1                             | 292<br>0                            | 1<br>00£  |
| 112      | 219<br>0                            | 227<br>0                             | 235<br>3                             | 243<br>0.00<br>12<br>0.2893<br>1.05  | 251<br>0.29<br>0.3163<br>1.06        | 259<br>-0.14<br>15<br>0.4900<br>1.16 | 267<br>-0.51<br>19<br>0.6654         | 275<br>4                             | 283<br>1                             | 291<br>0                            | 0         |

Layer 5:

|       | 138<br>0 | 146<br>0                             | 154<br>0                             | 162<br>0                             | 0                                    | 1<br>1                               | 186<br>1                             | 194<br>0                                | 202<br>0                             | 210<br>D                            |
|-------|----------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---|--------------------------------------|-------------------------------------|
|       | 0<br>0   | 145<br>0                             | 153                                  | 161<br>2                             | 169<br>2                             | 2                                    | 185<br>7                             | 193<br>7                                | 201<br>D                             | 209<br>0                            |
|       | 136<br>1 | 144<br>1                             | 152                                  | 160<br>-0.52<br>13<br>0.6027<br>1.14 | 168<br>-0.99<br>19<br>0.6424<br>1.12 | 9                                    | 104<br>-1.76<br>11<br>0.6030<br>1.02 | 192<br>-1.58<br>17<br>0.4960<br>0.97    | 200<br>3.20<br>21<br>0.4669<br>0.97  | 208<br>4                            |
| er 4: | 135<br>B | 143<br>2.02<br>14<br>0.6140<br>1.06  | 151<br>-2.32<br>21<br>0.5847<br>1.03 | 159<br>-2.86<br>37<br>0.6737<br>0.94 | 167<br>-1.97<br>61<br>0.7877<br>0.83 | 175<br>-2.63<br>52<br>0.7953<br>0.85 | 183<br>-3.12<br>47<br>0.7351<br>0.93 | 191<br>2.06<br>23<br>0.5767<br>0.96     | 199<br>-0.49<br>13<br>0.4753<br>1.00 | 207<br>2.08<br>11<br>0.5684<br>1.13 |
| Lay   | 6<br>7EI | 142<br>-2.15<br>25<br>0.6337<br>1.00 | 150<br>-0.85<br>44<br>0.7002<br>0.94 | 158<br>0.98<br>42<br>0.7445<br>0.90  | 166<br>-2.35<br>58<br>0.7766<br>0.89 | 174<br>-1.49<br>0.8307<br>0.77       | 182<br>-0.15<br>0.7870<br>0.64       | 190<br>0.28<br>38<br>0.6923<br>0.95     | 198<br>0.66<br>0.5855<br>1.05        | 206<br>5                            |
|       | EET      | 141<br>4.80<br>17<br>0.5485<br>1.03  | 149<br>-1.47<br>53<br>0.7234<br>0.91 | 157<br>-1.80<br>56<br>0.7378<br>0.92 | 165<br>-0.49<br>76<br>0.7840<br>0.86 | 173<br>3,39<br>64<br>0,7900          | 181<br>0.21<br>55<br>0.7797<br>0.87  | 189<br>2.21<br>2.6406<br>0.6406<br>1.02 | 197<br>-0.27<br>19<br>0.6147<br>0.97 | 205<br>5                            |
|       | 132      | 140                                  | 148<br>8                             | 156<br>0.98<br>22<br>0.6274<br>1.01  | 164<br>0.33<br>27<br>0.6424<br>C.97  | 172<br>0.18<br>0.6591<br>0.633       | 180<br>n.07<br>28<br>0.58<br>0.58    | 186<br>B                                | 196<br>0                             | 204<br>1                            |
|       | 0        | 0<br>6E1                             | 0                                    | 155<br>0                             | 163                                  | 0<br>1/1                             | 8<br>8                               | 187<br>5                                | 0                                    | 203                                 |

Fig. 6c. Model C. See Figure 6a caption.

 $s^2/\%^2$  were tested to investigate the trade-offs between resolution, standard errors, the fit to the observations, and smoothing of the result. For the final models,  $\theta^2 = 0.0010 \ s^2/\%^2$  (models A and B) and 0.0005  $s^2/\%^2$  (model C) were adopted. In our opinion these values give the optimal trade-off, though the value chosen for this ad hoc parameter is essentially arbitrary. For damping parameters smaller than  $\theta^2 = 0.0005 \ s^2/\%^2$  the increase of the standard errors and of model length (i.e., model complexity) did not compare favorably with the small improvement grained in the fit (Figure 4). For damping factors larger than  $\theta^2 = 0.0010 \ s^2/\%^2$  the decrease in the fit is large compared to a small improvement in smoothing.

With another series of models (not presented here) we investigated the influence of block size, layer thickness, and block position on the pattern of highs and lows seen in the calculated models. Even though the magnitudes of the perturbations change (because the block boundaries are nonphysical and artifically influence the result), all models tested showed the same major features. Therefore we believe that the ensemble of models presented here fairly represents the set of possible solutions.

All the models explain the observed travel time residuals to within about the measurement error. For example, model B diminishes the variance of the residuals by 60% leaving an unmodeled variance of 0.0036  $s^2/\%^2$ , which compares favorably with the timing accuracy of about 0.05 s.

# DISCUSSION

#### Inversion Model

The three-dimensional velocity structure obtained from the inversion reveals several significant features (Figure 5 and Plate 1a). (Plate 1 can be found in the separate color section in this issue.) The most important of these is the low-velocity anomaly in the middle crust under the southern part of the Mono Craters. Its top is about 8-10 km deep (depending on the inversion model). The feature is visible clearly in layers 3 and 4 of all models and may reach to the bottom of the crust in layer 5 ( $\approx$  32 km). Its slowest velocity is about 7% below the mean and occupies a single block in layer 3. Since damping in the inversion tends to reduce the magnitude of these velocity estimates, the velocity of the feature may be even lower. Because the array is 30 km in diameter, we do not have much information from depths greater than about 30 km and cannot determine whether the anomaly continues into the mantle.

Though this main low-velocity feature is relatively compact, it does appear to be somewhat asymmetric. In particular, the center shifts significantly between layers 3 and 4, suggesting an east dipping structure. This dip is apparent in the east-west cross section of Plate 1a and in similar cross sections (not shown) of a set of models with differing block arrangements. The easterly dip probably is not an artifact of the inversion since more west dipping than east dipping rays are used in the inversion. The resolution matrix (Figure 6b, discussed in the next section) confirms this interpretation. The observed dip suggests that the east dipping Sierran frontal fault zone or an eastward (outward) dipping zone of weakness associated with the mylonitized cataclastic border of a Cretaceous pluton beneath Pumice Valley [e.g., *Kistler*, 1966] may influence the location of the low-velocity anomaly.

In addition to this low-velocity anomaly, some smaller features are visible. A high-velocity region in the northwestern

corner of the model lies beneath the Sierra (layers 1 and 2) and may be caused by high-velocity basement rock. Similar highvelocity features were observed by Iyer et al. [1981a, b] and Evans [1982] under the Idaho Batholith. A second highvelocity anomaly is centered near the south end of the Mono Craters in layers 1 and 2. It coincides with a magnetic low [U.S. Geological Survey, 1974] which may be caused by carbonate metasediments in Sierran roof pendant rocks (R. Bailey, personal communication, 1985). Such rocks crop out nearby and in other areas along a larger north-south magnetic low of which this one is a part. Where they appear nearby along the crest of the Sierra Nevada, these rocks have higher density than the neighboring granitic rocks [Oliver, 1977] and may therefore have higher seismic velocities than the granitic rocks which crop out west of the Mono Craters. The thickness of this roof pendant is uncertain but could be as great as 5 or 6 km, based on observed variations in hypocenter patterns with depth south of Long Valley (R. Cockerham, personal communication, 1985). Finally, a low-velocity feature appears beneath Mono basin in layers 1 and 2 and may continue to depth. Since it lies on the edge of the model and is poorly resolved (diagonal elements of  $\mathbf{R} < 0.4$  or 0.5), its interpretation is uncertain. It may reflect deeper down-faulted material in Mono basin contrasting with faster surrounding granitic rocks, or strictly speaking, it even might be shallow magma beneath the northernmost Mono Craters. There is, however, no compelling reason to believe this feature is anything but an artifact of the inversion's modeling of the shallow sediments of Mono basin. Since there is abundant evidence for such sediments, we perfer not to overinterpret the data by looking too far for alternative, less probable sources.

### Inversion Model Resolution

An examination of the model resolution helps in evaluating the significance of features seen in the inversion result. The resolution matrix calculated by the inversion is best understood by

$$\hat{m} = \mathbf{R}m\tag{7}$$

[e.g., Ellsworth, 1977], which relates the "true" model m to the inversion result  $\hat{m}$ . The "truth" of m, which ideally is the real earth structure, is limited largely by the model parameterization (i.e., the selection of block sizes and boundaries). Each element of the symmetric singular matrix  $\mathbf{R}$  is between -1 and +1 (>0 on the diagonal) so that each row of the matrix is an averaging kernel relating all of m to one block in  $\hat{m}$ . That is,  $\hat{m}$  is some average, hopefully local, of the parameterized real earth structure m.

Thus in most cases large diagonal elements in **R** indicate that the velocity estimates in  $\hat{m}$  are dominated by velocities in the same regions in *m*, that is, that  $\hat{m}$  is a good representation of *m*. Figures 6a-6c shows that the diagonal elements of **R** are  $\geq 0.6$  for most of the central parts of our models. Figure 6*b* and Plate 1*b* show the row of **R** for the block in model B believed to contain the most anomalous material. This row of **R** is typical of the blocks in this central part of the velocity model. The averaging kernel for this block is compact, so the velocity estimate probably is not strongly influenced by anomalies outside the block. Thus we believe that the models presented are well resolved on the block level and generally are interpretable if their velocity perturbations are significantly larger than the standard errors, which average about 0.8% (Figures 6a-6c).



Fig. 7. Magmatic model of Bailey [1982], by permission.

The sediments filling Mono basin, on the other hand, form a relatively thin horizontal layer and are near the edge of the models. Because resolution is usually poor near the edges of models and because thin horizontal layers are parasitic cases and always are modeled badly by the "ACH" method, it is best to take a different approach to interpreting the resolution of this anomaly. Comparing the uncorrected (model A) and corrected (model B) cases (Figures 5a-5e and Figures 6a and 6b) one can see the strong influence of the first layer sediments on the second layer; deeper layers are less affected by this "smearing out" of the sediment velocity anomaly. In the corrected case the remaining perturbations in the first layer are only about 4%, compared with 12% for the uncorrected case. Nevertheless, the shape of the first-layer anomaly is similar in both cases, suggesting that the sediment corrections around Mono Lake should be larger than the ones used or, alternatively, that the second layer also may be slow under Mono Lake. The models' resolution of this feature is insufficient to discriminate between these possibilities.

The third layer, however, clearly is decoupled from these effects. There is no significant change in the pattern in layer 3 between the corrected and uncorrected cases. Similarly, layer 4 is very similar in all the models. Layer 5 differes in model C, presumably because of the greater depth of this layer in model C.

# Interpretation

Bailey [1982] inferred from geological and geochemical arguments that the Mono Craters are fed by a shallow ring dike from an active midcrustal magma chamber. Even though it is somewhat smaller, shallower, and displaced eastward, we interpret the low-velocity anomaly beneath the Mono Craters as this chamber. Many rock properties can produce low velocities, but the location of this feature beneath a young, increasingly active volcanic chain and the observed and predicted velocity decreases due to melt and partial melt in crystalline materials [e.g., *Goetze*, 1977; *Mavko*, 1980] support this interpretation. Also, the intensity of the anomaly and its depth, similar to low-velocity anomalies found under other small young silicic centers, support our interpretation that the low velocities are caused by melt or partial melt [e.g., *Iver*, 1984].

The bulk melt fraction present in the chamber is much more difficult to estimate. The gross distribution of melt in the chamber, the geometry of the melt fraction itself (whether it wets crystal faces, for example), the melt viscosity, and the relative importances of phase change, melt squirt, and other proposed attenuation mechanisms all are poorly known and all affect such estimates strongly. A low-viscosity melt wetting crystal faces could produce the observed velocity perturbation with on the order of 1% melt [e.g., *Mavko*, 1980]. On the other hand, the very low phenocryst content of erupted magmas suggests that at least part of the chamber may be as much as 100% melted (R. Bailey, personal communication, 1986).

Given such gross uncertainties, we propose only the following elementary estimate. The velocities of rhyolite melt [Murase and McBirney, 1973] and dacite melt [Hayakawa et al., 1957] seem to be about 4 km/s, which would provide a 36% velocity contrast with country rock (6.25 km/s) if present in layer 3. If the velocities of the solid and melt part average in a simple volume-weighted fashion (they may well not), then the melt fraction to produce a 7% velocity anomaly would be of the order of 20%.

The volume of the chamber is somewhat difficult to estimate accurately because it is similar to the size of the blocks (about 200 km<sup>3</sup>). The anomaly does appear to involve at least one full block, since it also seems to affect several blocks neighboring the most anomalous one. It does not appear to involve fully more than about three blocks. We conclude that the magma chamber is between about 200 and 600 km<sup>3</sup> in volume. This volume is less than that of the Bisho Tuff erupted from Long Valley [*Bailey*, 1982] and presumably is much smaller than the magma chamber that produced that tuff. Coupled with the youth of the Mono Craters, this relatively small magma chamber volume suggests that a major ash flow event is not now likely (e.g., R. Bailey, personal communication, 1985).

Bailey [1982] speculates that Long Valley and the Mono Craters may have a common mafic magmatic source in the mantle, which supplies heat to the individual shallower midcrustal silicic chambers (Figure 7). Our observations do not contradict this model; in fact, they tend to confirm at least the shallower part of it. However, they do suggest that the active fluid volume of magma is located more directly beneath the Mono Craters themselves, rather than beneath Pumice Valley, centered within the ring fracture zone.

Unfortunately, there are few other geophysical data to help constrain our Mono Craters model. The data reported by Kissling et al. [1984], who derived a tomographic model for depths of 0-14 km at Long Valley using local earthquake travel times, extend north to the Mono Craters, but resolution is poor in that area. This tomographic model shows moderately low-velocity material beneath the Mono Craters throughout the sampled depth range and is generally similar to the teleseismic result. However, the tomographic anomaly extends to shallower depth than the teleseismic anomaly. In particular, it shows low velocities from 3 to 9 km depth near the south end of the Mono Craters, whereas the teleseismic model, which appears to be well resolved in this area, shows faster than average velocities at these depths (Figure 5b). Closer examination of the stations and sources used by Kissling et al. suggests that the region may be sampled mostly by subparallel roughly north striking rays arriving at a station at the north end of the Mono Craters, near our station MD2. MD2 exhibits a 0.2-s sediment anomaly. Thus the tomographic model for this area partly may reflect an ill-resolved sediment anomaly and therefore may be less reliable locally than the teleseismic model. However, because of these differing results the presence of a high-velocity anomaly near the south end of the Mono Craters suggested by teleseismic data cannot be considered proven.

Other geophysical data are less applicable. Only one heat flow measurement [Lachenbruch et al., 1976] is available for the Mono Craters area. It is west of the craters at Aeolian Buttes and has a normal Basin and Range value (91 mW m<sup>-2</sup>) [Lachenbruch et al., 1976; A. Lachenbruch, written communication, 1982]. A. Lachenbruch (personal communication, 1984) indicates that this result does not preclude the presence of a young magma chamber at depth, because if it is as young as it appears, heat flow from it should not have perturbed surface temperatures yet. For example, a magma chamber less than 700,000 years old and more than 10 km deep, or less than 150,000 years old and 6 km deep would not perturb surface temperatures significantly even directly above the chamber.

The gravity data are equally inconclusive. The regional Bouguer gravity map [Oliver and Robbins, 1978] shows a small 5-mGal low at the southern end of the Mono Craters, but the feature represents data from only one gravity station. A simple model (a 200 km<sup>3</sup> upright cylinder with its top 10 km beneath the Mono Craters, a diameter of 6 km, and a height of 7.5 km) would produce a 1.5-mGal anomaly if it had

a density contrast of  $0.2 \text{ g/cm}^3$ . This gravity signature would be swamped by larger local features and might not be separable from uncertainties (which easily could exceed 3 mGal) in the Bouguer reduction density for the volcanic pile.

Finally, Hermance et al. [1984] report a magnetotelluric study in Pumice Valley. They did not observe a decrease in resistivity at shallow depths and concluded that the magma chamber for the Mono Craters is either too thin or too deep (>10 km) to be resolved or is significantly displaced from the center of the ring fracture. Since the teleseismic results show that the low-velocity feature is 5–10 km east of Pumice Valley and below about 10 km depth, the magnetotelluric observations do not contradict our results.

#### **CONCLUSIONS**

The relative residual patterns obtained from teleseismic compressional wave arrivals recorded in the Mono Craters area imply the presence of a low-velocity feature under the southern part of the Mono Craters. Inversion of these data provides a moderate resolution three-dimensional velocity image of the feature. The velocity structure modeled predicts the observed travel time delays to within their expected reading errors. It reveals a small low-velocity anomaly in the middle crust mostly between about 10- and 20-km depth and with a maximum velocity decrease of about 7%. The lowvelocity anomaly may continue to the Moho as an east dipping feature.

A proposed explanation for the feature is the presence of silicic melt or partial melt under the Mono Craters in a magma chamber partly controlled by the Sierran frontal fault zone or the mylonitic border zone of a Cretaceous pluton. This hypothesis is largely consistent with the geologic observations of Kistler and Bailey but does not support the notion of a larger midcrustal chamber centered beneath Pumice Valley and within the Mono Craters ring fracture zone (Figure 1). The volume of the interpreted magma chamber is greater than 200 km<sup>3</sup> but is substantially smaller than the chamber that existed under Long Valley before eruption of the 600 km<sup>3</sup> Bishop Tuff. The melt fraction in the Mono Craters magma chamber is poorly constrained by these teleseismic data but may be of the order of 20%.

#### Appendix

The "remaining variance" in Table 2*a* is, strictly speaking, only an estimate of the data variance left unexplained by the model  $\hat{m}$ . The equation used, however, can be derived from equations (5) and (6) with only the approximations already implicit in those equations and the assertion that the remaining variance is

$$\sigma r^2 = \frac{e^T e}{(N_{\rm obs} - N_{\rm ev})} \tag{A1}$$

where the error  $e = d - A\hat{m}$  and  $N_{obs}$  and  $N_{ev}$  are the number of observations and events, respectively (D. A. Stauber and D. Oppenheimer, personal communication, 1986). The sum square error is

$$(d - \mathbf{A}\hat{m})^{T}(d - \mathbf{A}\hat{m}) = d^{T}d - x^{T}\hat{m} - \hat{m}^{T}x + \hat{m}^{T}(\mathbf{G} - \theta^{2}\mathbf{I})\hat{m}$$
(A2)

where the solution  $\hat{m}$  obeys equation (6) rewritten as

$$\hat{m} = \mathbf{G}^{-1} \mathbf{x} \tag{A3}$$

with  $\mathbf{G} = (\mathbf{A}^T \mathbf{A} + \theta^2 \mathbf{I})$  and  $x = \mathbf{A}^T d$ . Since  $x^T \hat{m} = \hat{m}^T x$ , equation (A2) rearranges to

$$e^{T}e = d^{T}d - \hat{m}^{T}x - \hat{m}^{T}\theta^{2}\hat{m} + \hat{m}^{T}(\mathbf{G}\hat{m} - x)$$
(A4)

where equation (A3) implies that the last term vanishes. The inversion uses equations (A1) and (A4) to estimate the remaining variance, so this estimate is exact within the linearity assumptions in equation (5) and the assertion that the system has  $N_{obs} - N_{ev}$  degrees of freedom.

Ellsworth [1977] compares the value  $\sigma r^2$  obtained from (A1) and (A4) with values obtained by raytracing through  $\hat{m}$ . He estimates that  $\sigma r^2$  leads to variance reduction estimates that are about 5% optimistic in complex models. Our conclusions in the text based on the variance reduction and  $\sigma r^2$  are not affected by differences of this magnitude.

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U. Achauer, Geophysikalisches Institut, Universität Fridericiana Karlsruhe, Hertz Str. 16, Bar 42, Karlsruhe, D-7500, Federal Republic of Germany.

J. R. Evans, L. Greene, and H. M. Iyer, U.S. Geological Survey, 345 Middlefield Road, MS 977, Menlo Park, CA 94025.

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Plate 1 [Achauer et al.]. (a) Vertical cross section of model B along a line (Figure 5c) through the suspected magma chamber. Velocity perturbations are coded by color with low velocities in magenta. (b) The row of the resolution matrix corresponding to the most anomalous block in Plate 1a.