ZirTiDiS: an implicit finite difference code for the calculation of apparent Zr-in-Titanite (ZiT) temperatures

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Here we describe the application of ZirTiDiS (Zirconium in Titanite Diffusion Software), a set of MATLAB routines designed to calculate apparent Zirconium-in-Titanite temperatures in function sample's pressure-temperature-composition evolution using the of a thermobarometer of Hayden et al. (2008). Using Hayden et al.'s equation, the equilibrium Zr concentration in titanite (sphene) is calculated for a custom pressure-temperature-time path by specifying start- and end conditions, a cooling rate and the activities of TiO₂ and SiO₂ required for the thermobarometer. Alternatively, activities can be calculated using bulkcomposition-specific phase diagrams (pseudosections) and lookup-tables containing chemical potential data from which the activities of TiO₂ and SiO₂ are calculated. The Zr concentration and the respective effective Zr-in-titanite (ZiT) temperature is calculated for spherical grains considering thermally activated diffusion, using experimentally derived diffusion coefficients for Zr in titanite (Cherniak, 2006). We then present a worked example and benchmarks detailing the main features of ZirTiDiS.

The following routines must be located in the same directory:

- ZirTiDiS_fun.m:
- ZirTiDiS_exe.m:
- ZirTiDiS_CR_exe.m
- data.dat:
- main function calculate cooling histories calculate apparent ZiT Temperatures vs. cooling rates chemical potential database

and the main code is executed by typing ZirTiDiS_exe or ZirTiDiS_CR_exe in the MATLAB command window.

The code is written in a general way to allow for a transparent presentation of the results and is provided free of charge¹. All software and documentation presented here is intended for research and didactic purpose and comes without warranty.

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GOVERNING EQUATIONS

The Zr-in-titanite thermobarometer

Hayden et al. (2008) experimentally calibrated the pressure–temperature–activity relationship for the Zr concentration in titanite. Their thermobarometer is sensitive to the activities of TiO_2 and SiO_2 , which can be either specified by the user or calculated for a chosen bulk rock composition.

The equilibrium Zr concentration in titanite as a function of temperature, pressure and activities is given by:

$$log(Zr_{ppm}^{titanite}) = 10.52 - \frac{7708}{T(K)} - 960 \frac{P(GPa)}{T(K)} - log(a_{TiO2}) - log(a_{SiO2})$$
(1)

(Hayden et al. 2008). Rearranged for temperature, equation (1) becomes:

$$T(^{\circ}C) = \frac{7708 + 960P(GPa)}{10.52 - \log(a_{TiO2}) - \log(a_{SiO2}) - \log(Zr_{ppm}^{titanite})} - 273$$
(2)

The thermobarometer was calibrated using Zr contents in titanite crystals synthetized in the presence of zircon, quartz and rutile at 1–2.4 GPa and 800–1000°C in a piston cylinder apparatus. The estimated uncertainty is ± 20 °C within the range of 600–1000°C (Hayden et al. 2008).

Diffusion in a sphere

For one-dimensional diffusion in a spherical geometry, the change in concentration with respect to time is proportional to the radial derivative of the concentration gradient:

$$\frac{\partial C}{\partial t} = \frac{D(T)}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial C}{\partial r} \right)$$
(3)

Where t is time, r is the radial direction, C(r,t) is the concentration and D(T) is temperaturedependent diffusivity of the Arrhenius-type:

$$D(T) = D_0 \exp\left(-\frac{Q}{RT}\right) \tag{4}$$

With D_0 (5.33*10⁻⁷ m²/sec) being the diffusivity at infinite temperature (pre-exponent factor) and Q (325*10³ J/mol) the activation energy that are experimentally determined for titanite under anhydrous, pO₂-buffered conditions (Cherniak, 2006). T is the absolute temperature and R is the gas constant (8.314 J/mol/K). No pressure dependence on the diffusivity is reported. These are currently the only available estimates for diffusivity in titanite; however, the code can be easily updated if required.

Numerical solution of the diffusion equation

The diffusion equation (3) is solved using an implicit finite difference scheme yielding

$$C_i^n [1 + S(r_{CR}^2 + r_{CL}^2)] - SC_{i+1}^n r_{CR}^2 - SC_{i-1}^n r_{CL}^2 = C_i^o$$
(5)

where r_{CR} and r_{CL} is the midpoint to the right and left of the evaluated grid node *i*, respectively.

While

$$S = \frac{D(T)\Delta t}{r^2 \Delta r^2} \tag{6}$$

combines thermally activated diffusivity (equation 4) with the spatial- (Δr) and temporal discretization (Δt). The initial condition is given by the Zr concentration calculated for the starting temperature and allocated to the entire grain (i.e., homogenous concentration). The concentration is calculated for a spherical half-grain and symmetry is achieved via a zero-flux (Neumann) boundary condition at the grain center. The (Dirichlet) boundary condition at the grain rim is updated at each time step and given by the Zr concentration at the new pressure–temperature–activity conditions calculated for the user-specified cooling rate, decompression rate and/or changing activities using equation (1).

PRESSURE-TEMPERATURE-ACTIVITY PATHS & EXAMPLES

User-specified activities

Table 1 shows the main user input required to execute the program:

```
Table 1 – Code snipped from ZirTiDiS_exe.m showing the main user input data.
```

```
clear, clc, close all
<u>_____</u>
% ZirTiDiS - Zirconium-in-Titanite Diffusion Software
% S. Schorn & E. Moulas - Mainz, 18.05.2024
%for more details see Zenodo documentation
%doi: 10.5281/zenodo.11184086
&CALCULATE COOLING HISTORIES
%IMPLICIT SOLVER
£_____
plot now = 1;
                    %[0,1] - 1 for plotting on the fly
                    %[0,1] - 1 to load precompiled data
lookuptable = 0;
safe data = 0;
                      %[0,1] - 1 to safe data
%define your system here
                      %grain radius [µm]
grsz = 50;
Tin
     = 800;
                    %initial temperature [°C]
Tfin = 600;
                    %final temperature [°C]
cool r = 20;
                     %cooling rate [°C/myr]
                %time step (~1e10 - 1e11)
%convert °C to K
tstep = 1e10;
     = 273;
C2K
myr2sec = 60*60*24*365*1e6; %milion year [s]
%if isobaric: set Pin = Pfin
Pin
     = 1.0;
                     %initial pressure [GPa]
     = 0.4;
                      %final pressure [GPa]
Pfin
%set activities - used if lookup tabel == 0
                     %starting activity TiO2
aTi in = 1.0;
                    %ending activity TiO2
%starting activity SiO2
aTi fin = 1.0;
aSi in = 1.0;
            %ending activity SiO2
asi fin = 1.0;
```

A typical cooling history output using ZirTiDiS_exe.m for fixed activities (lookuptable = 0) is presented in Figure 1. The program calculates the initial Zr concentration of ~276.5 ppm for the specified starting conditions which is allocated to the entire grain. Due to the imposed cooling rate, the temperature decreases for each time step and the associated Zr concentration is calculated and allocated to the grain rim. This results in a Zr concentration gradient which drives diffusion from the core towards the rim to equalize the concentration. At high temperature diffusion is efficient and the Zr concentration at the center approximates the equilibrium concentration imposed at the rim. Therefore, the recorded ZiT core temperature remains close to the actual temperature during cooling – the red line ('T in titanite') does not significantly depart from the blue line ('real T'). However, with decreasing temperature the diffusive equilibration between core and rim becomes increasingly ineffective, resulting in an incremental departure of the ZiT core temperature from the actual one. The final Zr concentration throughout the grain describes a characteristic bell-shaped profile, with a maximum at the core (~136.7 ppm) and minimum at the rim (~17.8 ppm), corresponding to an apparent ZiT temperature of ~692°C and ~600°C, respectively (Fig. 1).



Figure 1 - Example calculation for $aTiO_2$ and $aSiO_2$ of unity. The red line is the calculated apparent ZiT core temperature.

Some key results are prompted in the command window:

Table 2 – Command window prompt for previous calculation.

Elapsed time is 4.824951 seconds. Initial Zr concentration in the grain is 276.5125 ppm. Final rim Zr concentration is 17.818 ppm. Final core Zr concentration is 136.6765 ppm. Zr-in-titanite temperature at the core is 692.1365 °C. fx; >>

The equilibrium Zr concentration in titanite calculated using equation (1) as a function of pressure and temperature for activities equal to unity is shown in Figure 2 (left), while the effect of variable activities is displayed in the panel to the right. Similar concentrations are used as boundary condition for the grain rim.



Figure 2 – Pressure–Temperature space contoured for equilibrium Zr concentration in titanite and concentration at a fixed P-T point in function of aTiO₂ and aSiO₂ (log₁₀ units ppm).

It is pointed out that the choice of activities affects the absolute Zr concentration (Fig. 3, left), but not the apparent ZiT temperature (Fig. 3, right). However, this is only true if the activities are kept constant throughout the calculation run (cf. yellow line).



Figure 3 – Calculation showing the effect of activities. Blue: $aTiO_2 = aSiO_2 = 1.0$. Red: $aTiO_2 = 0.8$, $aSiO_2 = 0.5$. Note that the blue and red line overlap in the right panel. Yellow: starting conditions are the same as for the blue line, final conditions are those of the red line. Other parameters are identical to those in Figure 1.

Activities from pseudosections

As alternative to user-specified activities, a lookup table ('data.dat' in the current example) containing precomputed chemical potential data can be used (lookuptable = 1) to calculate activities from bulk-composition specific phase diagrams (aka pseudosections). In this example, we base our calculations on a MOR basalt (SM89 104–16; Sun & McDonough 1989), carried out using the Perple_X software bundle (Connolly, 2005, 2009). Details on the construction of the phase diagram and activity calculation can be found in the Appendix. Figure 4 shows the activities for TiO₂ and SiO₂ and the respective Zr concentration in titanite.



Figure 4 – Activities and equilibrium Zr concentration for the SM89 MORB.

Cooling rates

ZirTiDiS can be executed repeatedly for increasing cooling rates to calculate apparent temperatures depending on grain size and initial temperature (Fig. 5). This is done in the routine ZirTiDiS_CR_exe.m. It should be noted that this type of calculation is independent of the choice of pressure and activities, so long as the values are kept constant during cooling.



Figure 5 – ZiT core temperature as function of cooling rate & initial temperature (colored lines). Grain size = $25 \,\mu m$.

CODE TESTING

Numerical resolution and convergence

In ZirTiDiS, the diffusion equation is solved using an implicit finite difference scheme; as such, it is unconditionally stable for any choice of time step tstep (which is set by the user). Depending on the type of calculation, it may be useful to increase tstep to speed up the calculations. In this case it is recommended to perform a convergence test (e.g., Fig. 6) to ensure that the calculated ZiT temperatures approximate a unique value (~740°C in this example). In the current example and depending on the machine used, a calculation takes ~4 seconds for tstep = 1e10. Such small time steps are only required to produce a smooth cooling history (e.g., red line on Fig. 1), but can be increased to ~1e11 without significantly affecting the calculated final ZiT core temperature (Fig. 6, left). With this tstep a typical calculation takes ~0.5 seconds (Fig. 6, right).



Figure 6 – Left: ZiT core Temperature (°C) vs. timestep (log₁₀ units seconds). Right: Runtime (s) vs. timestep. Pressure is 1 GPa and activities are unity. Other parameters are identical to those in Fig. 1.

Analytical benchmark

The numerical solution is benchmarked against an analytical expression (Crank, 1979, eq. 6.18) for time-dependent diffusivity and a linear cooling path (i.e., a constant cooling rate) as shown in Figure 6a. According to eq. (4), the effective diffusivity exponentially decays with decreasing temperature (Fig. 6b). It was shown that by defining a new 'compressed time' variable τ (after Lasaga, 1983; Fig. 6c, d), the problem involving temperature-dependent diffusivity (\tilde{D}) effectively reduces to one with constant diffusivity (i.e., isothermal). This is graphically highlighted by the colored areas under the curves in figures 6c and d being equivalent. The analytical solution is given by:

$$C(r,\tau) = -\frac{2LC_0}{\pi r} \sum_{n=1}^{n=\infty} \frac{(-1)^n}{n} \exp(-n^2 X) \sin\left(\frac{n\pi r}{L}\right)$$
$$X = \frac{\pi^2}{L^2} \tau D_{max}$$
$$\tau = \int_0^t \frac{\widetilde{D}(t')}{D_{max}} dt'$$
$$\widetilde{D} = D(T(t))$$

where *C* is the concentration at a given radial coordinate *r* and time *t*, *C*₀ is the starting concentration throughout the grain, D_{max} is the diffusivity at maximum temperature and *L* is the total grain radius. This solution applies for a constant (Dirichlet) boundary condition of 0 concentration at the grain rim where *r* = *L* (Fig. 6e). The infinite sum is truncated after 30 terms, after which the residuals become negligible (~10⁻²⁰; Fig. 6f).



Figure 7 – Numerical vs. analytical solution for time-dependent diffusivity.

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APPENDIX

Pseudosection calculation

Pseudosection calculations were performed using Perple_X v.7.0.11 (Connolly, 2005, 2009) and the thermodynamic dataset hp62ver.dat (Holland & Powell, 2011). The employed activity–composition relationships are Fsp(C1) for feldspars (Holland & Powell, 2003), cAmph(G), Augite(G) and melt(G) for clinoamphibole, augitic clinopyroxene and mafic melt, respectively (Green et al., 2016), Gt(W), Chl(W), Bi(W), Mica(W), Opx(W) and IIm(DS6) for garnet, chlorite, biotite, white mica, orthopyroxene and ilmenite, respectively (White et al., 2014), Ep(HP11) for epidote (Holland & Powell, 2011) and O(HP) for olivine (Holland & Powell. 1998). The whole rock composition (MORB 104–16 of Sun & McDonough, 1998) is converted to the model system of Na₂O–CaO–K₂O–FeO–MgO–Al₂O₃–SiO₂–H₂O–TiO₂–O₂ (NCKFMASHTO) by omitting minor MnO and converting 30% of the total FeO to Fe₂O₃ (Table S1). Similarly, phase diagrams are constructed for pure TiO₂ (rutile) and SiO₂ (quartz) to calculate the reference chemical potentials (see below). Input- & output datafiles and phase diagrams can be found in the supplementary materials. For additional details on phase diagram calculations and using WERAMI visit https://www.perplex.ethz.ch/.

Table S1 – Whole rock bull	composition of MORB	104–16 (wt.%) used for	thermodynamic modelling.
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SiO ₂	TiO ₂	AI_2O_3	FeO	MgO	CaO	Na ₂ O	K ₂ O	O ₂	H ₂ O	Sum
50.22	1.34	14.79	9.33	8.17	10.92	2.58	0.34	0.31	2.00	100.00

Calculating activities from chemical potentials

The chemical potential of a component *i* is related to the activity and the absolute temperature via the relationship

$$\mu_i = \mu_0 + RT \ln a_i \tag{A1}$$

where μ_0 is the reference chemical potential at the standard state. Rearranged for activity this yields

$$a_i = exp\left(\frac{\mu_i - \mu_0}{RT}\right) \tag{A2}$$

For the calculations at hand, the chemical potentials of TiO₂ and SiO₂ can be easily computed using WERAMI from the Perple_X software bundle. In this case, μ_i is the chemical potential of component *i* (e.g., TiO₂) calculated for the specified bulk rock composition (MORB 104–16 here) while μ 0 relates to the chemical potential of component *i* in the pure reference phase (i.e., rutile). For μ_{SiO2} this corresponds to pure quartz. The compiled datatable ('data.dat') feeds into the 'activity_data_function', which calculates the activities using equation (A2). Reasonably, where the calculated mineral assemblages contain rutile and quartz, μ_i and μ_0 are equal and therefore $a_{TiO2} = a_{SiO2} = 1.0$ (Fig. 4).

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