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Abstract:

This report summarises the achievements and work performed during the first year of MuCol, in the frame of the wider International Muon Collider Collaboration (IMCC). A brief summary per work package (WP) is presented, referring to the more extended description contained in the IMCC Interim Report to be provided to CERN Council in the next few weeks.

MuCol Consortium, 2024

For more information on MuCol, its partners and contributors please see <https://mucol.web.cern.ch/>

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1. INTRODUCTION

The present document gives a concise description of the status and progress of the MuCol Consortium. MuCol is contributing a very important part of the overall R&D effort of the International Muon Collider Collaboration (IMCC).

The IMCC Interim Report details the technical achievements and the R&D goals toward the next update of the European Strategy for Particle Physics (due to start in 2026). It also describes the key R&D activities that should receive funding in the near future. This Interim Report will be submitted to the Laboratory' Director's group, a subcommittee of CERN Council, and it is currently undergoing scientific review by the IMCC and MuCol Advisory Committee. An excerpt of the report that contains the MuCol contributions is attached in Annex 2.

2. STATUS OF THE MUCOL CONSORTIUM

As of today, 29 out of the 32 Institutes that proposed the project signed the Consortium Agreement (CA). The University of Bologna (IT) and the Brookhaven National Laboratory (US), both Associated Partners, decided not to sign the CA for administrative reasons. Also, the Royal Holloway University (UK) had a significant administrative delay, but the signature is now under way. Despite that, the three Institutes continue to work on the project participating actively to the meetings and performing the technical work expected from them, so there was no need to redistribute their work among the other partners.

Considering the new deadlines agreed with the EU Project Officer after the start of the project, all Milestones and Deliverables of the first year have been achieved in time or even earlier, even though hirings were delayed due to the delayed start of the project. At present, several positions have been filled and the students are starting to produce results.

MuCol has been very active in terms of publications and dissemination in the scientific community, with talks provided at several conferences/workshops. The list of papers and talks is in Annex 1.

A Dissemination and Communication plan is in preparation and will be submitted by the end of March 2024.

Finally, a few workshops were organized in the framework of MuCol, with the enthusiastic participation of many scientists participating to the project, and also from Institutes not members of the Consortium. In particular, the list of past and upcoming workshops includes:

- Muon Collider Synergies workshop (22-23 June 2023, Orsay)¹
- MuCol training on detector design and physics performance tools (5-6 July 2023, CERN)²
- MuCol WP8 Cooling Cell Workshop (18-19 January 2024, CERN)³
- IMCC and MuCol MDI Workshop (11-12 March 2024, CERN)⁴
- MuCol Mini-Workshop on pulsed magnets (15 May 2024, CERN)⁵

In 2023, MuCol activities were also included in the second International Muon Collider Collaboration (IMCC) annual meeting⁶, that took place from 19th to 22nd June 2023 at the Irene Joliot-Curie Laboratory in Orsay (FR) under the coordination of CEA. The EU Project Officer also participated to the meeting in person to show their support to the Consortium. After the kick-off meeting held remotely on 28th March 2023⁷, the first official MuCol annual meeting will take place at CERN from 12th to 15th March 2024⁸ joint with the third IMCC annual meeting.

¹ <https://indico.cern.ch/event/1260921/>

² <https://indico.cern.ch/event/1277924/>

³ <https://indico.cern.ch/event/1335151/>

⁴ <https://indico.cern.ch/event/1353612/>

⁵ <https://indico.cern.ch/event/1388830/>

⁶ <https://indico.cern.ch/event/1250075/>

⁷ <https://indico.cern.ch/event/1219912/>

⁸ <https://indico.cern.ch/event/1325963/>

3. SCIENTIFIC AND TECHNICAL ACHIEVEMENTS AND OUTLOOK FOR THE NEXT PERIOD

In the following the main achievements for each work package (WP) are outlined. A more extensive description is included in the Interim Report.

3.1. WP1: COORDINATION AND COMMUNICATION

WP1 performed a work of coordination on both the scientific, technical, and administrative matters. In particular, monthly meetings were organized among the WP leaders, the Dissemination officer and the Gender advisor. During the first year two Governing Board meetings have taken place, and the members were invited to participate to the IMCC International Collaboration Board (ICB) during the IMCC annual meeting 2023 to meet and discuss with the other institutes representatives of the Collaboration.

From the point of view of Study Coordination, a document detailing all the preliminary parameters⁹ to be used as start of the Study has been published in the MuCol website¹⁰, which is available online and where resources are constantly updated. Moreover, a peer review process for scientific publications has been setup in conjunction with the IMCC structure¹¹. In particular, MuCol and the IMCC share the same Scientific Publication Committee and the same Publication policy, detailing the different types of publication and the reviewing process they have to undergo. As for the Dissemination and Exploitation plan, the project management is in contact with communication professionals to develop and implement an effective strategy to disseminate the project results and transfer the knowledge to the scientific community in order to maximise the impact of the research.

The MuCol Gender Advisor core activities have been structured around three impact areas:

- increasing awareness, e.g., providing resources and one-on-one support related to 50 ways to fight common implicit biases,
- developing wellbeing vision and action, e.g., engaging with the monthly MuCol management committee meetings and regularly share a possible framework for specific action plans on workplace wellbeing,
- targeting relevant topics, e.g., keeping the MuCol management committee informed on current challenges, opportunities, and optimal solutions related to gender-related issues, such as work-life balance for physicists with young children to attend workshops and meetings.

For what concerns the implementation scenarios, a cost review process is being setup, while for an implementation at CERN work will be done once the technical baseline is sufficiently stable.

⁹ <https://mucol.web.cern.ch/results/milestones/tentative-parameters>

¹⁰ <https://mucol.web.cern.ch>

¹¹ https://indico.cern.ch/event/1342402/contributions/5659123/attachments/2746426/4778968/PSC-October-2023_clean.pdf

3.2. WP2: PHYSICS AND DETECTOR REQUIREMENTS

A detector concept has been developed for an experiment with a center-of-mass energy of 3 TeV. The starting point was the detector design proposed by CLIC at the same center-of-mass energy. Major modifications to the tracker system have been implemented to accommodate two double-cone-shaped shielding absorbers made of tungsten coated with borated polyethylene, each with an opening angle of 10° . This structure is necessary to mitigate the impact of the beam-induced background on the detector.

The detector performance has been assessed by reconstructing the physics objects with the beam-induced background overlaid and utilizing detailed simulations of each sub-detector.

The design of a detector suitable for muon collisions at a center-of-mass energy of 10 TeV began by defining the main physics requirements.

Key challenges have been identified for both the 3 TeV and 10 TeV center-of-mass energies, and a prioritized schedule of activities for the next review has been prepared.

A general assumption has been made for each sub-detector technology to ensure a functional detector at present. The individuals working on physics and detector activities are active members of the DRD ECFA collaborations and the CPAD in the US, hence the most promising technologies will be utilized in future detector configurations.

A software and computing infrastructure are in place with resources provided by INFN and in minor part by CERN.

3.3. WP3: PROTON COMPLEX

WP3 focused its efforts in the first year in assessing the state of the art to understand the performances that can be reasonably expected.

For instance the development and exploitation of the LINAC4 H- source at CERN is being followed up closely in order to understand the limitations and needs for the source for a future Proton Complex. The new redesigned source is close to achieve the peak current required for the 2 MW version on the Muon Collider and substantial progress in the source brightness was achieved. The new source was installed and is in operation since 2023. The next step in achieving high charged bunches is a redesign of the LINAC4 RFQ in order to improve transmission.

A compilation of the literature on past projects, with special attention to US Muon Acceleration Program (MAP) and design of a Neutrino Factory at CERN, was done. A baseline lattice for the accumulator and compressor for the 5 GeV case, based on the studies for the Neutrino factory at CERN, was revised and fully transferred to XSuite. Basic beam physics parameters are being collected and compiled and a parametric study is underway. A first look at the transport between ring and target of a 2 ns high current bunch has started.

Since both the accumulator and compressor rings are strongly space charge limited machines, an evaluation of available codes for space charge dominated beam simulation is being carried out. In order to complement this evaluation a collection of data from CERN PS bunch rotation and Booster

bunch recombination, both with high density bunches, was carried out. Data analyses and plans for future measurements are underway.

Concerning the hirings, WP3 hired a 2 years post-doc to work the proton complex, this person started on February 1st 2024. That is the only hiring foreseen for WP3 for the whole grant time. As for the articles, WP3 submitted an overview article for IPAC24 (poster) on the proton complex initial design ideas.

3.4. WP4: MUON PRODUCTION & COOLING

The target team have designed a radial build for the baseline graphite pion production target, taking into account radiation flux into the surrounding solenoid, heat load on the graphite target itself and appropriate cooling systems for the target and shielding. A 3D FLUKA model for the target area has been constructed and the pion and muon yield through the target system has been assessed. The team have supported magnet experts to assess the associated radiation load. Work has begun on studies of liquid metal and powder targets as higher power alternatives.

Beam physics designs have been made for the ionisation cooling systems.

The rectilinear cooling system, used at high and intermediate emittances is the focus of the MuCol study. A preliminary system optimisation has been performed yielding potentially improved performance, subject to assessment and refinement of the design requirements by hardware experts. A first attempt at developing an improved simulation tool using the BDSIM code has been performed, with better handling of dipoles than existing simulation codes.

3.5. WP5 : HIGH ENERGY COMPLEX

In order to limit muon losses due to decays along the high-energy RCS (Rapid Cycling Synchrotrons) chain, acceleration has to be fast with large average RF gradients. Longitudinal tracking simulations have given a minimum required number of RF stations per RCS to keep the longitudinal emittance. We have optimized the layout of the hybrid RCS to minimize the orbit length variation. The effect of multi-turn wakefields due to higher-order modes on the longitudinal stability was investigated and the power induced into these HOMs was studied as a function of their quality factors.

The design of a lattice for a 10 TeV center of mass collider lattice has significantly progressed but still work is required to get a lattice working for nominal beam parameters. Relaxing slightly requirements would allow finding such a lattice. Progress on studies of radiation at Earth's surface caused by neutrinos generated by muon decays comprise FLUKA studies, an improved "source term" describing radiation from a decaying muon beam without divergence and a procedure to take the properties of the lattice into account.

The muon beam fast acceleration and the collider ring have been presented at the international accelerator school, which took place in Erice in July-August 2023.

The next milestones are the organization of a mini-Workshop on pulsed magnets (the fixed date is 15 May at CERN) for the RCSs, and a tentative optics of the collider ring and RCSs. The lattice of the

collider already exists. Some work is still required to work with the nominal parameters. A first lattice of the RCS is under development.

3.6. WP6: RADIOFREQUENCY SYSTEMS

The RF system for the muon cooling complex consists of approximately 8000 RF cavities operating in the frequency range starting from a few hundred of MHz. The majority of the cavities operate at 352 and 704 MHz in the initial and 6D-cooling channels. The main peculiarity of the RF system is that the RF cavities are interleaved with strong solenoidal magnetic fields, which enhance the cavity breakdown rate. This also limits the choice of the RF cavities to normal conducting ones since SRF cavities cannot operate in magnetic field. In order to reach high gradient on the order of a few tens of MV/m in normal conducting cavities, high peak RF power on the order of few MWs per one single cell cavity is needed. This results in very high peak power requirements of a few tens of GW.

Integration of the RF cavities together with high-field superconducting solenoids and absorbers in the common vacuum vessel is another engineering challenge. The superconducting solenoids operate at cryogenic temperature whereas RF cavities and the associated RF network operate at room temperature. Combining all the subsystem in a compact way is a key challenge in the engineering design of the muon cooling channel.

Several experiments on breakdown rates in cavities under high magnetic field have been carried out in the frame of dedicated programs (International Muon Ionization Cooling Experiment (MICE) and Muon Accelerator Program at Fermilab (MAP)). Dedicated test stands have been studied and designed to analyze the improvements that may be obtained in the choice of bulk materials and surface finishing procedures. A first one, allowing to carry out breakdown tests at static electric field values up to 10 MV/m with a magnetic field up to 1.3 T is close to be put in operation. A second one, designed to operate a 3 GHz cavity in a 7 T magnetic fields, is ready to be submitted for funding.

Design and construction of prototype cavities at nominal RF frequency is part of the next year program.

3.7. WP7: MAGNET SYSTEMS

A design of the magnet system, for muon beam production, involving HTS cable at 20 K has been developed, and analyses performed thus far indicate a magnet roughly half the size radially and with better energy efficiency when compared to the US-MAP LTS coil, while maintaining similar muon capture efficiency. The main objective in the coming year will be to iterate on this design to resolve the optimal radial dimensions of the target, shield, and magnet while mitigating radiation heat load and damage to the magnet, and further optimization in terms of cost.

Recent achievements toward the magnet system for muon cooling include an analysis of the magnet geometries proposed by US-MAP in the rectilinear cooling chain and a proposed alternative design of magnets, optimized in terms of cost and engineering considerations. In the coming months further analyses will be performed including quench protection and magnet design for a new beam optics.

Advances have been made towards the magnetic design of compact and high field final cooling solenoids, with potential to reach and exceed 40 T. Planned work this year includes detailed multi-physics evaluations and supporting experimental activity using HTS tapes and pancakes to provide an experimental basis.

Large progress toward the design of the pulsed NC magnet configurations in the acceleration chain has been realized, concluding ‘H’ and ‘Hourglass’ shaped iron cores as the best options. Further magnetic analysis of these and the SC magnets is planned this year and a relevant mini-workshop on pulsed magnets will be organized in collaboration with WP5.

Lastly, specifying the performance limits of the collider dipole and quadrupole magnets has been underway, producing a series of design charts which can be iterated with beam optics. In the coming year, we plan to finalize these design charts and extend the analysis to combined function magnets.

3.8. WP8: COOLING CELL INTEGRATION

WP8 has organized several meetings also in collaboration with WP4 to define a baseline for the cooling cell to be designed. All the specifications and criticalities of the different technical systems have been reviewed and a workshop has been organized in December 2023 to present all the knowledge acquired and discuss the pros and cons of all the possible options.

At the moment, a proposal for the initial configuration of a cell to be design is being finalized and will be presented in March 2024 at the annual meeting to get the agreement of the Consortium and IMCC Collaboration. Once approved, the design work will start steadily. In the meanwhile, WP8 is collaborating with WP6 and WP7 to design a facility to test RF structure in a magnetic field of several T. Such a facility has many commonalities with a cooling cell and therefore is serving as training for the engineers involved.

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ANNEX

ANNEX 1 : LIST OF MUCOL PAPERS AND TALKS

List of papers and talks in which the acknowledgment to MuCol is explicit (as of 29/02/2024)

PAPERS

- 1) K. Skoufaris et al., "First design of a 10 TeV centre of mass energy muon collider", in Proc. IPAC'23, Venice, Italy, May 2023, pp. 690-693. doi:10.18429/JACoW-IPAC2023-MOPL064.
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- 12) C. Accettura et al., Conceptual design of a target and capture channel for a Muon Collider, accepted for publication in IEEE Transactions on Applied Superconductivity, DOI 10.1109/TASC.2024.3368387.

TALKS

- 1) R. Losito, Challenges in the Design of Muon Colliders, 12th Course - Challenges in Radiation Damage and Radiation Protection during Design and Operation of Accelerator Facilities and Space Missions, Erice (Sicily), Italy, 23-30/10/2023.

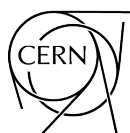
- 2) R. Losito, The Muon Collider Study: Challenges and perspectives, 8th High Power Targetry Workshop (HPTW2023), RIKEN Wako campus, Japan, 6-10/11/2023.
- 3) D. Lucchesi, Higgs Prospects at Muon Collider, UK HEP Forum 2023: Completing the Higgs-saw puzzle, Abington Oxfordshire, UK, 21-22/11/2023.
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ANNEX 2: DESCRIPTION OF PROGRESS AND PLANS

You can find below an excerpt of the IMCC Interim Report that will be used as description of the progress and plans for IMCC and MuCol

Description of the progress and plans for IMCC and MuCol

Editors: M. Lancellotti, R. Losito, D. Schulte, the MuCol Consortium,
the International Muon Collider Collaboration (IMCC)



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Description of the progress and plans for IMCC and MuCol

*Editors : M. Lancellotti, R. Losito, D. Schulte, the MuCol Consortium,
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Abstract

This document summarises the technical progress of MuCol and the IMCC and the status of the muon collider R&D programme.

Keywords

Collider, muon, accelerator physics, technology, etc.

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1 Introduction

This report summarises the achievements and work performed during the first year of MuCol, also in collaboration with the wider International Muon Collider Collaboration. The report provides an overview of the collider including the injectors, the section for muon production and fast acceleration. We then provide a complete overview of all the main technical systems, providing the status and outlook for future developments.

2 Physics, Detector and Accelerator Interface

2.1 Physics and detector needs

2.1.1 Overview

The vast physics potential can be translated into requirements for the machine and the experiments that will harvest data from it.

The most notable requirements on the machine are: the mitigation of the beam-induced backgrounds (discussed in Section 2.2), the amount of delivered integrated luminosity and the ability to precisely measure it, and a precise determination of the beam energy.

The requirements on the detectors situated at the main interaction points are set in terms on “baseline” and “aspirational” targets. They include requirements on the detector acceptance, particle detection and identification efficiency, as well as resolutions on the various particle properties inferred by the instrumental measurements. The baseline requirements are set by the need to separate collision products from energy depositions from beam-induced backgrounds and the need to identify and measure particles over a wide range of energies with a precision at least comparable with the experiments taking data at the LHC. The aspirational targets are set with the goal of fully exploiting the physics potential of the machine. They aim at a reconstruction performances comparable to those targeted by Higgs factories while extending to significantly higher energies. Furthermore, these requirements are set with the goal of maintaining sensitivity to unconventional signatures as well as profiting from the unique potential of muon colliders to use forward muons to study vector boson fusion processes. The preliminary targets for several key metrics discussed more in detail in the next Section are reported in Table 2.1.

Table 2.1: Preliminary summary of the “baseline” and “aspirational” targets for selected key metrics, reported separately for machines taking data at $\sqrt{s} = 3$ TeV and $\sqrt{s} = 10$ TeV. The reported performance targets refer to the measurement of the reconstructed objects in physics events after, for example, background subtraction and not to the bare detector performance.

Requirement	Baseline		Aspirational
	$\sqrt{s} = 3$ TeV	$\sqrt{s} = 10$ TeV	
Angular acceptance	$ \eta < 2.5$	$ \eta < 2.5$	$ \eta < 4$
Minimum tracking distance [cm]	~ 3	~ 3	< 3
Forward muons ($\eta > 5$)	–	tag	$\sigma_p/p \sim 10\%$
Track σ_{p_T}/p_T^2 [GeV^{-1}]	4×10^{-5}	4×10^{-5}	1×10^{-5}
Photon energy resolution	$0.2/\sqrt{E}$	$0.2/\sqrt{E}$	$0.1/\sqrt{E}$
Neutral hadron energy resolution	$0.5/\sqrt{E}$	$0.4/\sqrt{E}$	$0.2/\sqrt{E}$
Timing resolution (tracker) [ps]	$\sim 30 - 60$	$\sim 30 - 60$	$\sim 10 - 30$
Timing resolution (calorimeters) [ps]	100	100	10
Timing resolution (muon system) [ps]	~ 50 for $ \eta > 2.5$	~ 50 for $ \eta > 2.5$	< 50 for $ \eta > 2.5$
Flavour tagging	b vs c	b vs c	b vs c , s -tagging
Boosted hadronic resonance ID	h vs W/Z	h vs W/Z	W vs Z

Initial considerations on the interplay between the accelerator complex and detectors dedicated to the study of neutrino physics are reported in Section 2.3.

2.1.2 Key challenges

The requirements on a detector that can successfully extract physics from collision data at a muon collider are set by two categories of constraints: the rejection of the reducible beam-induced backgrounds and the need for (precision) physics observables. These two categories can lead to conflicting choices that require an overall optimisation to be performed. A quantitative assessment of these requirements is being carried out based on a preliminary set of physics benchmark channels that are used to study the overall performance of a detector design on selected key metrics.

The requirements on the detector acceptance, summarised in terms *angular acceptance* and *minimum tracking distance*, have to balance the need to maximise the sensitive volume for a high rate SM measurements, retain sensitivity to a broad range of non-prompt physics, while suppressing the BIB to a manageable level. For example, the presence of large absorber nozzles located in the forward region of the detector is key to reducing the high-energy showers from the beam decays to a soft, diffused, energy contribution in the detector volume. At the same time, especially when considering a machine operating at a centre of mass energy of 10 TeV, a sizeable fraction of the interesting events will include outgoing particles within the uninstrumented volume of the absorbers. The precision determination of the Higgs boson couplings in single and multi-Higgs boson production events are used as main benchmark to set the angular acceptance requirements. The requirements on the minimum tracking distance will be studied on high-rate Higgs boson studies exploiting flavour-tagging as well as searches for long-lived particles [17].

Thanks to their highly penetrating nature, muons offer a unique possibility to discriminate charged and neutral vector boson fusion processes. Dedicated *forward muon* ($\eta > 5$) detectors that could be placed beyond the detector shielding and the accelerator components. The needs of a comprehensive vector boson scattering measurement and BSM searches (e.g. extended Higgs sectors) programme set the goals of measuring not only the presence of the outgoing muons, but also their momenta with good resolution. A preliminary study of the placement of the detectors, their technology and the effects of BIB still needs to be performed.

It is assumed that excellent (>90%) detection efficiencies must be achieved for energies between $\mathcal{O}(1)$ GeV to $\mathcal{O}(1)$ TeV for all measured particle species. The requirements on the resolution of the measurements of *transverse momenta* and *energies* are driven by the high rate Higgs and SM measurements. In particular, these requirements are set by the need of rejecting irreducible SM backgrounds that share the same final state signature. Searches for high-mass objects, where searches for heavy vector triplets (HVT) are being used as a benchmark, contribute with looser requirements since these are naturally less affected by both BIB and irreducible SM backgrounds. The same physics benchmarks are currently used for the determination of the requirements in terms of flavour tagging of hadronic jets.

The identification of boosted hadronic resonances is an important feature, required for the full exploration of the SM electroweak sector and several searches for new heavy particles. In particular, the ability to distinguish hadronically-decaying Higgs bosons from Z and W bosons in the whole detector acceptance is crucial. High-mass searches, e.g. searches for HVTs, would benefit from the ability to distinguish W and Z bosons for centrally-produced resonances.

The availability of timing information from each of the sub-detectors of a next-generation collider experiment is taken to be the norm. Requirements on *timing* resolutions are set by background

suppression considerations. The time of arrival of BIB particles on the sensitive elements of the detector spreads over a few ns after the bunch crossing, providing a powerful handle for rejection. In the future, these requirements could be relaxed when improved reconstruction algorithms with alternative mitigation strategies (e.g. based on the event topology) become available. The search for heavy (meta-)stable massive particles was identified as a benchmark channel that would profit directly from a precise determination of the time of flight by each of the detector systems. A minimum goal of retaining sensitivity to slow-moving particles with a relativistic velocity $\beta \geq 0.5$ was taken as baseline model-independent benchmark. The use of timing and time-of-flight information for particle identification is a potentially promising tool that has yet to be studied.

Unconventional signatures and the search for long-lived states still need to be explored in detail at a muon collider. However, it is reasonable to assume that they would impose requirements on the ability to reconstruct displaced decays using only a subset of the available detector systems. Foreseen benchmarks are for example a search for anomalous showers in the calorimeter systems, or searches for displaced decay vertices in the tracking detectors or the muon system.

The requirements on the detector acceptance and performance are less stringent when considering an energy stage at $\sqrt{s} = 3$ TeV. The differences are driven by the smaller contribution of vector boson fusion processes to the total cross-section and by the lower maximum energy of the collision products.

A key part of the physics programme at a muon collider is the measurement of several cross-sections and branching ratios with percent-level precision. This immediately sets a stringent requirement on the determination of the delivered integrated luminosity. The current assumed target is a measurement with an uncertainty at the permille-level.

2.1.3 *Recent achievements*

There has been a great deal of work since the roadmap on the physics requirements of a muon collider detector. Much of this was documented in the Muon forum report [?] and a recent review [?]. There have been two main directions of research undertaken since the roadmap in the pursuit of better understanding detector needs: those focused on phenomenological studies and those based on full detector simulation. Phenomenological studies have been performed at a variety of levels of sophistication, from background free studies on truth level events, to fast detector simulation in DELPHES with all relevant backgrounds. The utility of these studies is that they are able to cover a large array of physics possibilities and to focus on what is needed for detectors to disentangle the hard scattering physics backgrounds. The studies based on full simulation allow one to also quantify the potential in the presence of beam-induced backgrounds. As focused on in [?,?], there have also been a small amount of studies of the same physics cases, where both fast and full detector simulations were performed. While ultimately it would be ideal to have all studies that impacted detector performance requirements done at a full simulation level, in cases where there is overlap between fast and full simulation studies good agreement has been found. This in turn gives confidence in the use of fast simulations to help better delineate the physics performance goals that have been reported.

Notable highlights were the studies performed on Higgs measurements and dark matter searches with disappearing tracks.

The Higgs measurements [16] serve as a general purpose benchmark for low-energy Standard

Model processes. These were used to evaluate the effects of the detector acceptance on the final Higgs boson coupling precision, as well as to perform an initial study of the resolution and instrumental effects related to the presence of beam-induced backgrounds.

The search for disappearing tracks [?] is a unique probe to definitively test the WIMP dark matter paradigm at a collider experiment. The signature consists of short tracks formed by a few (3-4) tracking detector hits. As such, it is uniquely sensitive to the detector layout, technology and the levels of beam-induced background.

Furthermore, recent fast simulation studies [15, 16] have been crucial in demonstrating the need for not just forward muon tagging, but also the aspirational goal of forward muon measurements and how the physics performance changes.

2.1.4 Planned work

The effort in view of the evaluation report will be focused on extending the list of preliminary benchmarks mentioned in Section 2.1.2 by assembling a list of representative benchmarks that will allow judging the physics performance more globally.

As a part of this effort, a broad survey of measurements and searches will be conducted to identify a list of high-priority benchmarks to be studied in more detail with full simulation. The result of the survey will be a prioritised target list. The list should be short (tentatively not be longer than ten elements) to be compatible with the limited resources of the collaboration. The primary target of the evaluation will be a collider operating at $\sqrt{s} = 10$ TeV. The list should specify for which benchmarks a dedicated assessment for a lower energy stage at $\sqrt{s} = 3$ TeV should be performed.

The second key task follows directly from the first and consists in performing the detailed studies for as many of the benchmarks extracted from the target list as feasible to update to the requirements on the key metrics.

The last key task will consist in developing a concept for automating the evaluation of the prioritised benchmarks to efficiently re-evaluate the results for any change in assumed detector design or data-taking conditions.

2.1.5 Important missing effort

A precise determination of beam energy is necessary for extracting physics results from the experiments. While it is assumed that techniques foreseen and used at other collider facilities will be compatible with the requirements, no work on the design of the instrumentation, the conceptual evaluation of the expected performance or the evaluation of any interplay with the detectors can be performed with the available resources.

Similarly, only preliminary studies have been performed to study luminosity determination using large-angle Bhabha scattering [?]. The feasibility of reaching the required precision needs to be systematically assessed, and possible dedicated detectors need to be designed, if required. No effort is ongoing and this will likely remain uncovered.

2.2 Machine-Detector Interface

2.2.1 System Overview

The beam-induced background (BIB) poses a significant challenge for the physics performance of a multi-TeV muon collider. The background is dominated by the decay of stored muons, with additional contributions from incoherent electron-positron pair production and possible beam halo losses on the aperture. These particles interact with surrounding materials and generate a mixed radiation field composed of secondary electrons, positrons, photons, as well as hadrons (photo-nuclear interactions) and muons (Bethe-Heitler pair production). Without dedicated mitigation measures, the beam-induced background would severely impede the reconstruction of collision events in the detector and would lead to significant radiation damage in detector components.

An optimized design of the Machine-Detector Interface (MDI) is hence critical for minimizing the impact of machine operation on the physics performance reach, and for reducing the ionizing dose and displacement damage in the detector. The MDI design must include an elaborate absorber configuration, consisting of masks inside the final focus region and a conical shielding, which penetrates deeply into the detector region, up to a few centimeters from the interaction point. The optimization of these masks and absorbers must be done jointly with the detector and interaction region (IR) design. A conceptual MDI layout for a 1.5 TeV muon collider has been devised previously within the MAP collaboration, by means of the MARS Monte Carlo code [1–3]. Based on this configuration, first MDI design studies for higher-energy muon colliders (3 TeV and 10 TeV) were carried out within the IMCC [4–6] using the FLUKA code [7–9].

2.2.2 Key Challenges

The main challenge for the design of the machine-detector interface is the short lifetime of muons. This intrinsic source of radiation distinguishes a muon collider from other high-energy colliders. One of the key requirements is the design of a sophisticated shielding configuration at the interface between final focus magnets and detector. As shown in previous studies by the MAP collaboration for 1.5 TeV [1–3], the number of secondary particles entering the detector can be suppressed by orders of magnitude by placing massive absorbers in close proximity of the interaction point (IP). The innermost part consists of a nozzle-like shielding, which defines the inner detector envelope and hence the angular acceptance of the detector (10° in MAP). The shape and material budget of the nozzle determines the entry points, directions and energy spectrum of particles reaching the detector. The nozzle must be made of a high- Z material to efficiently shield the electromagnetic showers induced by muon decay products or by beam halo losses on the aperture. In addition, it must embed a layer of borated polyethylene or a similar material to moderate and capture secondary neutrons produced in photo-nuclear interactions. The nozzle must be carefully optimized for different center-of-mass energies. Besides the conceptual design, one also faces engineering challenges including assembly and support of the nozzle, as well as integration of the nozzle inside the detector. In addition, an adequate cooling system must be devised, to evacuate the heat deposited by decay products and beam halo losses.

While the characteristics (e.g. spectra) of the decay and halo-induced background are mainly determined by the nozzle, the amount of background particles is also influenced by the interaction region layout, i.e., by the lattice design and the placement of mask-like absorbers inside IR magnets. For

example, the previous studies by MAP for a 1.5 TeV collider suggested that a dipolar component in the final focus configuration can be beneficial for reducing the background flux into the detector [3]. Designing and optimizing the IR layout is one of the key challenges for the collider design, in particular for 10 TeV (a 3 TeV and 6 TeV IR design was previously devised within MAP [10–12], although no background simulations were published). Furthermore, the flux of secondary particles is also influenced by the presence of a solenoid field in the detector region. This concerns not only the decay-induced background, but also incoherent electron-positron pairs, which are produced in the vicinity of the IP and are not directly intercepted by the nozzle. While the choice of the solenoid field strength is primarily driven by the particle detection efficiency in the detector, it must also take into account the benefits for background suppression.

Even with an optimized MDI and interaction region design, a suitable choice of detector technologies and reconstruction techniques is needed to reduce the effects of the remaining background (see Chapter 3). The signatures of background particles often exhibit distinct differences with respect to collision products, which can be exploited for background suppression. This concerns, for example, the arrival time of background particles with respect to the bunch crossing, as well as the directions of background particles when they enter the detector. The shielding requirements and MDI design will hence strongly depend on detector R&D efforts to suppress the effect of background particles.

2.2.3 Recent Achievements

A full simulation framework based on the FLUKA Monte Carlo code was developed for computing the beam-induced background entering the detector. First muon decay studies for 1.5 TeV, replicating the MAP interaction region, exhibited a good agreement with the previous MAP results derived with MARS15 [13]. The studies were further extended to 3 TeV and, in particular, to a higher collision energy of 10 TeV [4–6]. At the same time various simulation techniques were improved, like the sampling of decays from a fully matched beam phase-space distribution, which provided a more accurate description of the transverse beam tails. While the 1.5 TeV and 3 TeV studies were still based on the interaction region lattice from MAP, a new lattice was developed for the 10 TeV collider, considering a triplet configuration as final focus scheme [20]. The 10 TeV lattice allows for β^* values of a few millimeters and incorporates an adequate chromatic compensation without sacrificing the physical and dynamic aperture. Using the FLUKA simulation framework, a comparison of decay-induced background for 1.5 TeV, 3 TeV and 10 TeV were performed [4–6, 13]. As one of the key findings, these studies demonstrated that the secondary spectra and multiplicities of particles entering the detector are not substantially different for a 10 TeV collider. Figure 2.1 illustrates the distribution of arrival times and energy spectra of decay-induced background particles for 3 TeV and 10 TeV, respectively [6]. The results were obtained with the different IR lattices (MAP lattice for 3 TeV and IMCC lattice for 10 TeV), as described above.

In order to explore the impact of lattice design choices on the decay-induced background, a series of studies was performed for 10 TeV [4]. Three alternative triplet layouts were considered, one based on pure quadrupoles, one based on combined-function dipole-quadrupoles and one using short dipoles placed between triplet magnets. In the two latter cases, the dipolar component strongly alters the azimuthal distribution of e-/e+ impact positions on the vacuum aperture, yet the massive nozzle dilutes any azimuthal dependence of the particle flux into the detector. In general, the studies showed that the dipolar component suppresses only marginally the contribution of decays in the final focus region, but

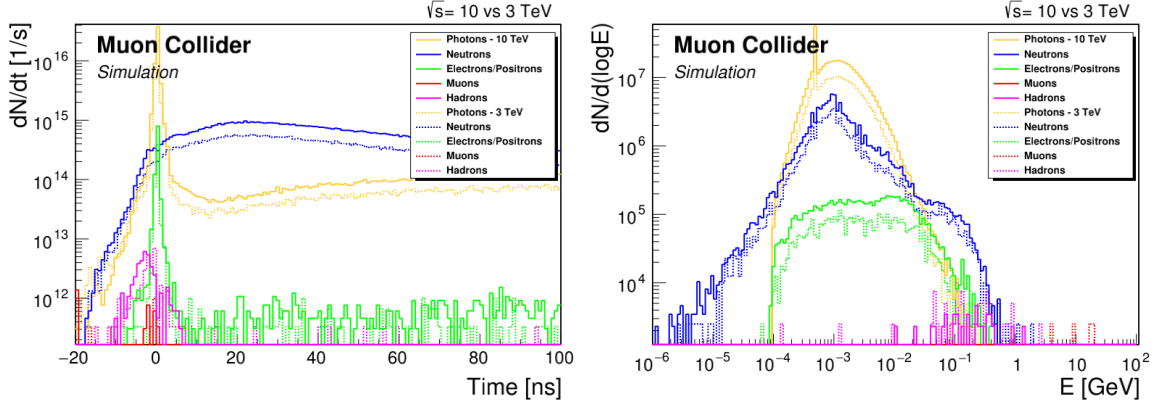


Fig. 2.1: Left: Distribution of the arrival time of decay-induced background particles entering the detector. Right: Energy spectra of particles arriving within the time window $[-1 : 15]$ ns with respect to the bunch crossing (photons, electrons and positrons below 100 keV were discarded). The figures were taken from Ref. [6].

nevertheless is beneficial for reducing the contribution of distant decays. The latter can yield a non-negligible contribution if the final focus is followed by a long drift section. Such a drift might be needed to allow for a smoother reduction of the beta function at the end of the final focus scheme. The studies showed that in this case, a dipolar component in the triplet can help to reduce the background.

In addition to the above studies, the impact of L^* on the decay-induced background was explored for the 10 TeV collider [5]. The solenoid in the detector region traps the electrons and positrons, which travel in the beam vacuum until they reach the other side of the interaction region, depositing their energy in the machine components. As a consequence, muon decays between the final focus magnets ($s < L^*$) contribute several orders of magnitudes less to the background than those in final focus quadrupoles. A longer L^* implies larger beta functions in the magnets, therefore increasing the magnet aperture. On the other hand, the quadrupole gradient decreases if the maximum field at the coil aperture is kept the same, thus implying a longer final focus scheme. A comparative study of two different lattices with $L^* = 6$ m and $L^* = 10$ m showed only a moderate background reduction by a few tens of percent, but at the expense of a more complex lattice design. Increasing L^* is hence not considered a viable option for reducing the background.

All the studies listed above were still based on the MAP nozzle design, which was optimized for 1.5 TeV. First attempts to adapt the nozzle for 10 TeV suggest that there is potential to reduce the decay-induced particle flux into the detector [5]. For example, the simulations showed that particle flux into the inner tracker depends on the internal angle of the nozzle tip. The studies also indicated that changing the external shape of the nozzle and adapting the placement of the borated polyethylene layer can reduce the neutron and photon flux. Optimizing the nozzle for 3 TeV and 10 TeV remains one of the key tasks for future studies.

Preliminary assessments of background sources beyond muon decay were performed for 10 TeV. In particular, a first comparison of incoherent electron-positron pairs against decay-induced spectra was carried out [5]. Although some electrons and positrons from pair production will be trapped by the solenoid, a non-negligible fraction of particles with energies up to about 1 GeV is expected to enter the

Table 2.2: Maximum values of the ionizing dose and the 1 MeV neutron-equivalent fluence (Si) in a CLIC-like detector. All values are per year of operation (10 TeV) and include only the contribution of muon decay.

	Dose	1 MeV neutron-equivalent fluence (Si)
Vertex detector	200 kGy	3×10^{14} n/cm ²
Inner tracker	10 kGy	1×10^{15} n/cm ²
ECAL	2 kGy	1×10^{14} n/cm ²

inner tracker. The studies suggest that contribution of incoherent pairs corresponds to a few ten percent of the total number of electrons and positrons entering the detector in the vicinity of the IP (within ± 50 cm). On average, the incoherent pairs have a higher energy than the decay-induced background component since the latter is strongly diluted by the nozzle.

Through the same simulation framework and by using a simplified model of a CLIC-like detector as well as the MAP nozzle (for the detector description, see also Sec. 3), the cumulative radiation damage in the detector could be calculated for different collider energies (so far for muon decay only). Two quantities were evaluated, the total ionizing dose and the 1 MeV neutron-equivalent fluence in Silicon. The former describes the ionization damage in organic materials and compounds, while the latter is related to the displacement damage. The highest dose values occur around the vertex detector, reaching about ~ 200 kGy/year (10 TeV collider). The 1 MeV neutron-equivalent fluence is highest in the inner tracker due to increased leakage of neutrons from the nozzle, with a peak value of around 10^{15} n/cm²/year (10 TeV collider). Table 2.2 provides a summary of the maximum values in different parts of the detector.

2.2.4 Planned Work

One of the key tasks for the evaluation report is the optimization of the shape and material composition of the nozzle using the FLUKA simulation framework. The studies will be carried out separately for the 3 TeV and 10 TeV machines. The optimization will rely on simple key figures (e.g. hit densities in the vertex detector) in order to avoid the need of a full detector simulation for each design iteration. For certain reference configurations, a full evaluation of the background in dedicated detector simulations will be essential, to provide a feedback for the nozzle design. Where applicable, alternative optimization techniques (machine learning) will be explored. The nozzle optimisation will mainly focus on decay-induced beam losses, but the contribution of other background sources (incoherent pair production and beam halo losses) will be assessed through the same simulation framework. This requires input from other codes (GuineaPig) and machine studies (beam dynamics simulations). In this context, it is foreseen to improve the description of incoherent pair production by muons in GuineaPig.

Although a full-scale engineering design of the nozzle is out of the scope of the present studies, it is foreseen to address some of the most important engineering and integration aspects. This includes in particular the evacuation of the deposited heat by means of a cooling system, the nozzle support structure, the nozzle segmentation and assembly, as well as the integration of the nozzle inside the detector and solenoid. Furthermore, the feasibility of instrumenting the nozzle will be evaluated in close collaboration with detector experts.

Another key task will be the optimization of the interaction region layout, under consideration of the beam-induced background, optics-related constraints, shielding requirement for magnets (heat load to cold mass, radiation damage in the coils), as well as magnet technology limitations (coil aperture versus peak field). The team is prioritizing this optimization for a 10 TeV machine, but will apply lessons learned to a reoptimization of MAP's 3 TeV interaction region if more resources become available. An important design specification is the minimum acceptable vacuum aperture in the interaction region (in terms of transverse beam sigma). A smaller aperture of the masks embedded in the final focus magnets and the nozzle is beneficial for reducing the decay-induced background, but can lead to enhanced halo losses in the interaction region. It is essential to quantify the permissible level of beam halo losses per bunch crossing, which must remain below the decay-induced background. Based on these studies, the interaction region aperture will be revisited and the need of other mitigation measures for halo losses (e.g. halo scraping system far from the IP) will be assessed.

Complementing the background studies, updated estimates for the cumulative radiation damage in the detector will be provided for the optimized interaction region and nozzle layout. These estimates shall include all background contributions, including incoherent pairs and halo losses, which have been neglected so far in the radiation damage studies.

2.2.5 *Important Missing Effort*

Considering the present resources, the MDI and IR studies described in the previous sub-section will be given priority until the evaluation report planned for 2026. Although the foreseen design studies will be mainly of a conceptual nature, they will prepare the path towards a fully integrated MDI and IR design. With the present resources, integrated engineering can only be performed for a very limited subset of the systems; however, a detailed design and integration of all technical systems can be elaborated once more resources become available. At that stage, important aspects, like the alignment of the nozzle and correction schemes for possible misalignments, can be addressed in detail. Furthermore, beam instrumentation like beam position or loss monitors, as well as luminosity monitoring, can be studied once resources are increased.

In addition to the MDI and IR design studies, it will be important to design a collimation or scraping system, which reduces the halo-induced background in the detector and also protects the interaction region in case of accidental beam losses. Multi-turn tracking studies will be needed to assess the efficiency of collimation techniques. In addition, it might be necessary to explore novel collimation schemes. The studies described in the previous sub-section will provide the necessary input concerning the acceptable amount of halo losses in the interaction region. It will therefore establish specifications for future design studies of a halo cleaning system, which can be addressed once more resources become available.

2.3 Neutrino physics

The collider target parameters foresee a single bunch of $N_{\pm} = 1.8 \times 10^{12}$ muons (and one of anti-muons) injected in the 10 TeV muon collider every $1/f_r = 0.2$ sec. Assuming 10^7 sec of operation per year, this corresponds to a current of 9×10^{19} muons per year. The muons circulate until they decay, and those that decay in a straight section of the collider ring give rise to a collimated beam of neutrinos that could be used for physics measurements in a dedicated detector. The fraction of usable muons is the length L

of the straight section divided by the collider circumference, of 10 km, and a region of at least $L = 10$ m without fields is required for the installation of the detector close to the Interaction Point (IP). This gives 9×10^9 neutrinos of each species per second and 9×10^{16} per year at the 10 TeV collider. At the 3 TeV collider, a similar estimate gives $2.4 \times 10^{10(17)}$ neutrinos per second (year). Notice that our estimate only accounts for the muons that decay in the detector region. The total length of the straight section is about 100 m in the current versions of the collider lattice design, and most of the muons decaying in this longer region should produce usable neutrinos. At the real collider we could thus expect few or 10 times more neutrinos than our estimate.

The neutrinos are very collinear to the decaying muons, with an angle that is typically below 0.1 mrad already at the 3 TeV MuC, and even smaller at 10 TeV because of the larger muon energy (see e.g. [?]). The muon beam angular divergence is typically much above 0.1 mrad, hence the distribution of the neutrino angle relative to the beam axis is driven by the dynamics of the muon beam and it cannot be estimated without reference to the lattice design, which is still preliminary. Fortunately, the beam angular divergence in the detector region equal to 0.6 mrad, both for the 3 and 10 TeV colliders is a rather robust design parameter because it is directly related to the luminosity at fixed emittance. Our estimate of the neutrino angle (and energy) distribution thus assumes a constant 0.6 mrad angular spread¹ for the decaying muons, and nominal beam energy of 1.5 and 5 TeV for the 3 and 10 TeV muon collider, respectively. This simplified simulation of the neutrino angle and energy distribution has been found in qualitative agreement with the complete simulation based on a preliminary design of the lattice.

The relevant parameter for physics studies is the rate of neutrino interactions, which in turn depends on the geometric acceptance and on the mass per unit area of the neutrino target. There are good perspectives to attain order-one geometric acceptance: around 30% of the neutrinos would intercept a small 10 cm radius cylindrical target placed at a realistically large (200 m) distance from the IP. The target density is harder to estimate, because it is intertwined with the capabilities of the detector to record the products of the neutrino interactions. In Ref. [?], a detector concept was developed in order to study the neutrinos produced by a dedicated 250 GeV muons ring. The concept foresees a 1 m target (with 10 cm radius) composed of a stack of tracking CCD planes, with a mass per unit area of $50 \text{ g}\cdot\text{cm}^{-2}$. Assuming this value, and a neutrino cross section of $10^{-35} \text{ cm}^2 \cdot E[\text{TeV}]$, results in $4 \times 10^{0(7)}$ and $3 \times 10^{0(7)}$ neutrino interactions per second (year) and the 10 TeV and at the 3 TeV muon collider, respectively, for each neutrino species. The expected energy spectrum of the interactions corresponding to this specific detector is reported on the left panel of Figure ???. Only muon neutrinos are considered in the figure for a direct comparison with the neutrino rates at past and future facilities, from Ref. [?]. Both the neutrinos from the μ^- decay and the anti-neutrinos from the decay of the μ^+ are included in the figure. Two different detectors would be needed to collect both species, since they fly away from the IP in opposite directions.

Despite the promising potential discussed in Section ??, no resources are currently available within IMCC for the design of dedicated neutrino detectors beyond the refinement of the estimation of the neutrino flux from updated accelerator lattice designs.

¹Specifically, we smear $p_{x,y}/p_z$, with p the muon momentum, by independent Gaussians with $\sigma = 6 \times 10^{-4}$.

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3 Detector

3.1 Concepts

3.1.1 System overview

The detector concept for a $\sqrt{s} = 3$ TeV muon collider is based on the detector design proposed by CLIC [1], modified to adapt it to the machine-detector interface. To accommodate the broad physics program expected, an angular coverage close to 4π would be required. The angular coverage is limited by the presence of the nozzles, two double-cone shielding absorbers made of tungsten and borated polyethylene having an opening angle of 10° , which are necessary to mitigate the impact of the beam-induced background. The nozzles are placed along the beam axis, in the region between 6 and 600 cm away from the interaction point. The innermost system closest to the beam-pipe is a full-silicon tracking system, that includes a vertex detector made of silicon pixels with double layers, and inner and outer trackers respectively composed of silicon macropixels and microstrips. The tracking system is surrounded by a calorimeter system consisting of an electromagnetic (ECAL) and a hadronic (HCAL) calorimeter, the former composed of alternating layers of tungsten absorber and silicon sensors, and the latter having alternating layers of steel absorber and scintillating pads. A solenoid with an inner bore of 3.5 m radius, provides a magnetic field of 3.57 T, whose flux is returned by a magnet iron yoke instrumented with muon chambers (resistive plate chambers). A scheme of the full detector is shown in Figure 3.1.

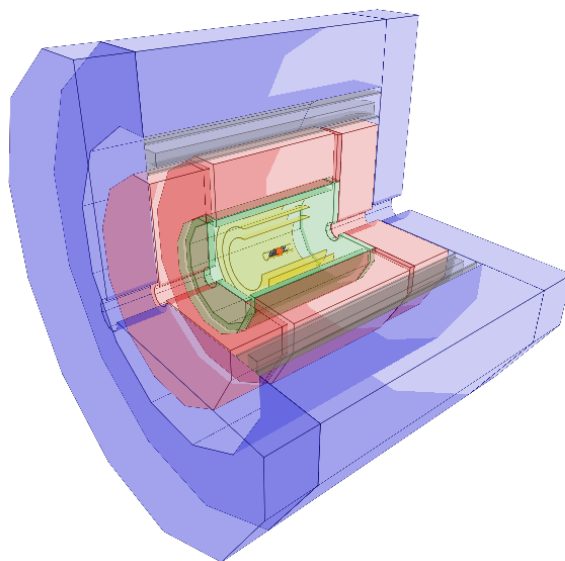


Fig. 3.1: Muon collider detector concept. From the innermost to the outermost regions, it includes the tracking system (yellow), the electromagnetic calorimeter (green), the hadronic calorimeter (red), the superconducting solenoid (gray), and muon detectors (blue).

3.1.2 Key challenges

As for the accelerator, the main technological challenges for the detector arise from the short lifetime of muons. In fact the beam-induced background produced by the decay in flight of muons in the beams

and subsequent interactions potentially poses a serious limitation to detector operations. All kinds of particles are produced, like photons, electrons, and neutrons, that can be partially mitigated by a proper design of the machine-detector-interface, as described in Section 2.2. Nevertheless, on order of 10^8 particles enter the detector at this center of mass (CoM) energy, therefore the detector design, the technology choices, and the reconstruction strategies must primarily take into account the beam-induced-background impact.

It is important to study the features of the beam-induced background by using simulation, to take the proper directions for the detector development. Figure 3.2 shows two key distributions, the arrival time (normalized to the bunch crossing time) and the energy of the beam-induced background particles when they enter the detector. These distributions have been obtained by using MARS15 simulation at $\sqrt{s} = 1.5$ TeV [22]. It can be seen that a large part of beam-induced background particles are asynchronous with respect to the bunch crossing, and they usually have low energy. Therefore timing measurements and appropriate energy thresholds are important handles to suppress them at the detector level.

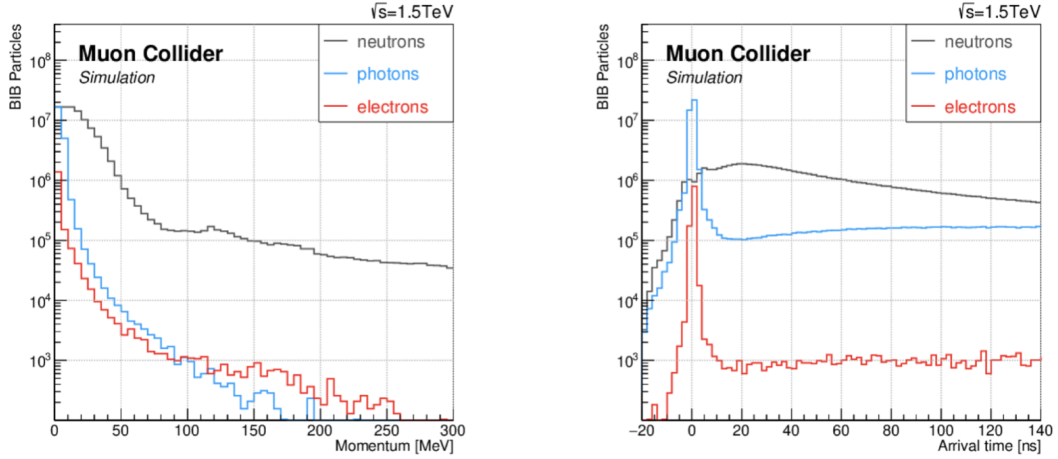


Fig. 3.2: Energy and arrival time, normalized to the bunch crossing time, of the beam-induced background particles when they enter the detector.

The following general requirements have been identified for the detector, driven by the necessity of suppressing the beam-induced background and keeping the signal efficiencies as high as possible:

- time measurements with excellent resolution: at this CoM energy resolutions ranging from 30 to 60 ps for the tracking system, and around 100 ps for the calorimeters are evaluated to be appropriate with the detector technologies available at the time of HL-LHC; the time resolution due to the primary vertex uncertainty has not been studied yet, but a resolution below 10 ps can be easily assumed by considering the beam size in z ;
- energy measurements, to apply a proper threshold for rejecting the beam-induced background soft component;
- high granularity, to reduce the overlaps between beam-induced background and signal hits, and consequently reducing the occupancy;
- radiation hard devices, since the radiation level is similar to what is expected at the High Luminosity LHC (HL-LHC) [2].

The research and development for these technologies will be performed in synergy with the existing programs, from HL-LHC to other future colliders.

The muon collider detector should ensure the physics reaches from low energy (*e.g.* Higgs and standard model physics) to the highest achievable energy scale for new physics searches (Section 2.1). This is particularly challenging in the detector for $\sqrt{s} = 10$ TeV collisions and beyond, where particle momenta from few GeV to several TeV have to be measured. The detector layout and design should satisfy physics requirements, and at the same time, it has to accommodate the MDI requirements and geometry. In this context, the magnetic field value plays an important role. High magnetic fields, around 5 T, could help in improving tracking momentum resolution of high energy particles but it could generate inefficiencies for those with low momentum. In addition, there are significant challenges to achieve the mechanical and electrical stability of the superconductive solenoids needed to reach such values of the field, including the technology transfer from previous HEP projects and the availability of experts.

Another challenge is the simulation of the detector for reconstruction and performance studies. The propagation of millions of beam-induced background particles through the detector volume, done with software based on GEANT4 [4], is heavily CPU-time consuming. Dedicated software and algorithms that tackle this problem in the proper way have to be developed since the muon collider environment is different from that of other well-known collider machines. Adequate computing resources should also be allocated for the detector studies.

3.1.3 Work progress since Roadmap

An important progress since the LDG roadmap is the initiation of the studies for the design of the detector at $\sqrt{s} = 10$ TeV. To properly understand the requirements, three major macro-categories of physics processes for muon collisions at $\sqrt{s} = 10$ TeV have been identified:

- low energy: typical examples are Electroweak (EW) and Higgs boson production, with energy in the range of a few hundreds of GeV; a sample of Higgs bosons decaying to $b\bar{b}$ jets is used for the studies;
- high energy: New Physics (NP) processes can create heavy resonances at the order of TeVs; simulated Z' boson with a mass of 9.5 TeV is taken as a representative case;
- unconventional signatures like long-lived particles. Disappearing tracks and emerging jets are just a few examples.

The transverse momenta, p_T , of the decay products of Higgs and Z' bosons are shown in Figure 3.3 to illustrate the difference among them.

The requirements set on the detector by the selected physics benchmarks at $\sqrt{s} = 10$ TeV are determined by optimizing the different sub-detectors. For the tracking system, a parametric study has been done looking at the relation between the depth of the tracking system and the magnetic field. Figure 3.4 (left) shows the results of momentum resolution for tracks with a transverse momentum $p_T \sim 5000$ GeV, as a function of the maximum tracker radius for different magnetic field values where it is evident that a deeper tracker with an high magnetic field value is necessary to keep a good track reconstruction resolution. A preliminary discussion with experts on detector magnets has been organized with a dedicated workshop [10], that set the basis for the studies.

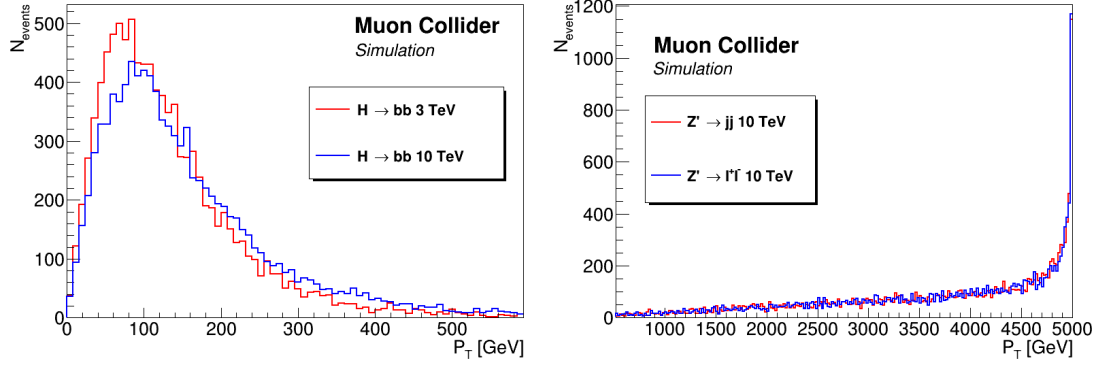


Fig. 3.3: Left: p_T distributions of b -quark coming from the $H \rightarrow b\bar{b}$ decays at $\sqrt{s} = 3$ and 10 TeV, as obtained at generator level. Right: distribution of leptons and jets p_T coming from the decay of a Z' boson produced at $\sqrt{s} = 10$ TeV with a mass of 9.5 TeV, as obtained at generator level.

Studies with photon/protons/pions particle guns have been performed to determine the calorimeter characteristics. Deeper calorimeters to contain high energy particles showers are necessary as shown in Figure 3.4 (right), where it is visible that a fraction of photon energy (with energies greater than 1 TeV) leaks into HCAL. For the muon reconstruction, studies on muons with $p_T \sim 5000$ GeV have shown that more inclusive algorithms that also use calorimeters information should be used in order to collect the energy released by muons.

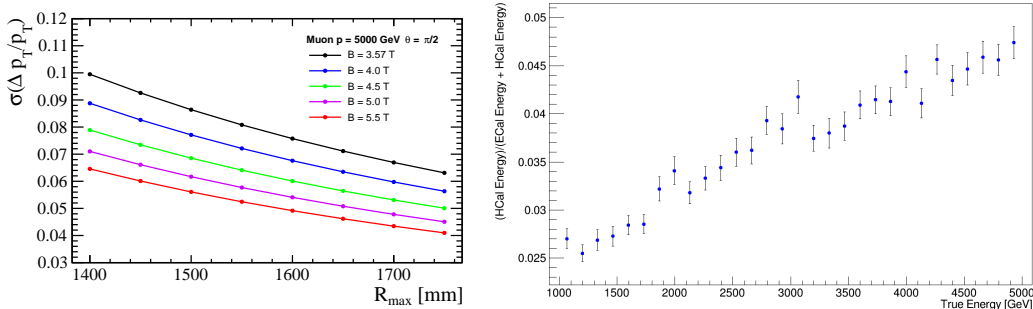


Fig. 3.4: Left: track momentum resolution for muons with $p = 5$ TeV and $\theta = \pi/2$, as a function of the tracker radius (R_{max}) and for different values of magnetic field (B). Right: fraction of photon energy measured in HCAL with respect to the total energy measured in ECAL+HCAL, as a function of the true photon energy.

3.1.4 Work planned for Evaluation Report

The magnet layout and magnetic field intensity will be one of the first items to be tackled for the next activities. This choice will drive the design of the detector sub-systems. The tracking, calorimeter, and muon detector system geometries will be defined, considering the available space (limited by the magnet, MDI, and cavern dimensions).

The assessment of the beam-induced background effects on the detector at $\sqrt{s} = 10$ TeV is another important activity for the upcoming Evaluation Report. It will include the study of incoherent electron-positron production, a physics process that could become relevant at high center-of-mass energies, such as 10 TeV. Once the simulation samples of the beam-induced background described in

Section 2.2 are validated, the studies at the detector level will start. First, the interactions of the beam-induced background with the detector have to be simulated; a preliminary detector design will be used, considering different configurations and values of the magnetic field. Several important physics quantities, like detector occupancy and distributions of hit position, time, and energy will be studied, including the determination of the radiation levels. The detector requirements will be reviewed, to verify if important changes for the layout and the technology choices are necessary, with respect to the $\sqrt{s} = 3$ TeV concept. The reconstruction performance of the main physics objects will be studied. Initially, using the same algorithms reported in Section 3.2, and subsequently, with algorithms tuned specifically for the $\sqrt{s} = 10$ TeV case. Feedback will be provided to the MDI study group to assess the possibility of improving the detector acceptance (*e.g.*, reducing the nozzle angle) while maintaining excellent reconstruction performance. The technology choice will be made by considering physics requirements and costs.

A first detector concept description at $\sqrt{s} = 10$ TeV will be delivered and made available in one of the next releases of the muon collider simulation framework and will serve as the starting point for all future studies. The simulation of the beam-induced background in this detector will be provided, along with a version of the reconstruction algorithms with an initial tune specifically tailored for this concept.

3.1.5 *Important missing effort*

An important missing study is the feasibility of a detector system for the identification and measurement of very forward muons. These muons are emitted outside the detector acceptance, but they are important for physics measurements. As an example, muons from $Z^0 Z^0$ fusion processes are mainly emitted in these regions, therefore their detection could be employed to tag such events and distinguish them from the $W^+ W^-$ fusion. These muon detectors have to be placed along the beam line, where also the accelerator magnets are placed. The propagation of the very forward muons through the magnetic fields configuration due to the accelerator components is not trivial, and a dedicated study with FLUKA has to be performed.

3.2 Performance

This section presents an overview of the performance of the 3-TeV detector concept for the reconstruction of the primary physics objects in the presence of beam-induced background.

3.2.1 *Overview of the physics object reconstruction*

The high levels of beam-induced background in the detector pose unprecedented challenges for the reconstruction and identification of the particles produced in muon collisions, which are referred to as physics objects. To fully exploit the physics potential of a muon collider and accomplish its physics program, it is essential to reconstruct all the physics objects with high efficiency and determine their properties with the greatest precision, even in the presence of beam-induced background.

A campaign of studies, based on a detailed detector simulation, was carried out to assess the effects of the background on the detector response and possibly develop the appropriate mitigation measures. The outcome was that the reconstruction algorithms for all the considered physics objects required revision or fine-tuning. However, the results indicate that the background effects on the detector response

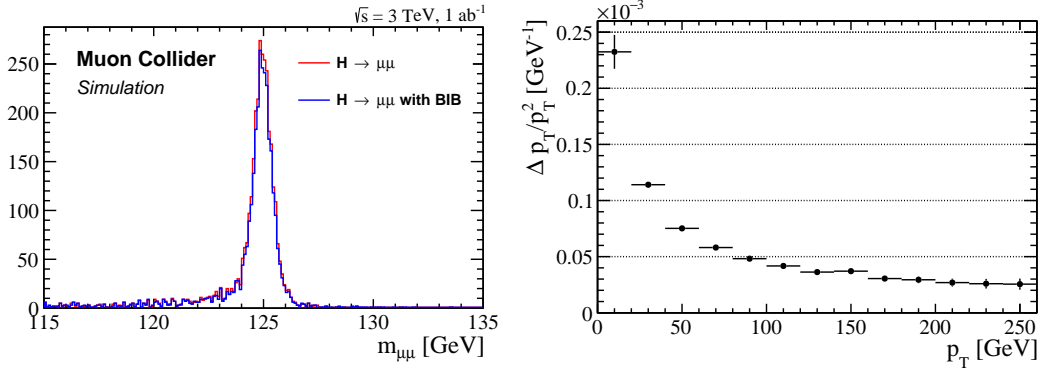


Fig. 3.5: Left: Invariant mass distribution of the muon pairs produced in the $\mu^+\mu^- \rightarrow H\nu_\mu\bar{\nu}_\mu \rightarrow \mu^+\mu^-\nu_\mu\bar{\nu}_\mu$ process without the beam-induced background (red line) and with the beam-induced background overlaid to the physics events (blue line). Right: Transverse momentum resolution as a function of transverse momentum for the reconstructed muons entering in the plot on the left with the beam-induced background (BIB) overlaid.

can be minimized to a degree that does not compromise the detector performance. This performance was then estimated reconstructing a set of benchmark Higgs boson channels at a 3 TeV muon collider.

The beam-induced background causes very high hit multiplicities in the detector’s tracking system, making the track finding process highly challenging, since the number of hit combinations to be considered increases exponentially, and a uniform diffuse energy deposition in the calorimeters, which makes it difficult to identify and accurately measure the energy of particles from collisions.

In general, the physics object reconstruction involves combining information from different detector sub-systems. Tracks, calorimeter clusters, and muon detector hits are combined to achieve an optimal performance in terms of identification efficiency, background rejection, and momentum resolution. For this purpose, a particle flow algorithm is employed, PandoraPFA [7], which takes as an input the reconstructed tracks and the hits of the calorimeters and muon detectors.

The initial focus of the detailed simulation studies was on muons, electrons, photons, and jets. Muons are identified by matching tracks with hits in the muon detector system. This sub-detector, located far from the beamline, is not significantly affected by the beam-induced background, except for the forward and backward regions with respect to the beam direction. Electrons and photons are reconstructed by matching tracks with clusters in the electromagnetic calorimeter. Isolated clusters are classified as photons, while clusters matched with a track are classified as electrons. The energy of electrons and photons is corrected to take into account inefficiencies and radiation losses. The reconstruction efficiency of the electromagnetic objects as a function of the energy reaches around 95% for high energy but drops at low energies due to the beam-induced background. For the jet reconstruction, tracks and calorimeter hits are filtered to remove the beam-induced background contamination and then are given as input to the PandoraPFA algorithm. The particles reconstructed by PandoraPFA are used as input to the jet clustering algorithm, which aims to group together particles produced in the fragmentation process of the same quark or gluon, by exploiting their correlations. The resulting jet energy is corrected to recover the losses due to particles escaping the detector, detector inefficiencies, and also for beam-induced background contamination. The jet reconstruction algorithm has been tested with simulated samples of different jet flavours: gluons and u , d , s , c , and b quarks. Despite the presence of the

beam-induced background throughout the detector, the efficiency ranges between 80% and 95%, with a negligible fake jet probability. In order to identify the jets originating from heavy quarks, secondary vertices compatible with the decays of b - and c -hadrons are reconstructed by combining tracks. A jet is identified as a heavy-flavour jet if one of these secondary vertices is reconstructed within the jet cone. The b -jet identification probability is approximately 45% at low p_T (20 GeV) and increases to 70% at 120 GeV, while keeping a misidentification rate of about 20% for c -jets and from 1% to 5% for light jets. This level of performance is similar to what is currently achieved at hadron colliders. At lepton colliders, a higher efficiency is expected. The current algorithm is mainly limited by the presence of the beam-induced background. In the future, artificial intelligence-based methods will be implemented to minimize the effects of BIB and further enhance efficiency.

The physics objects described above were used to reconstruct the Higgs boson decay modes into the final states $b\bar{b}$, $\gamma\gamma$, $\mu^+\mu^-$ and derive the reconstruction performance in the momentum range defined by these processes. The invariant mass depends on the magnitude and the direction of the decay particle momenta. The peak position at the nominal mass of the Higgs boson indicates a well-calibrated energy of the objects, while the peak width reflects the accuracy with which the object properties are measured. Figure 3.5 (left) shows the distribution of Higgs boson reconstructed mass for $\mu^+\mu^- \rightarrow H\nu_\mu\bar{\nu}_\mu$ with H decaying into $\mu^+\mu^-$. The reconstruction of high-energy muons produced in this decay is not significantly affected by the beam-induced background, as shown in the figure. The width of the mass peak is 0.4 GeV, comparable to electron-positron colliders. Figure 3.5 (right) demonstrates that relatively high-energy muons are reconstructed with high momentum resolution. In Fig. 3.6, the invariant mass of the $H \rightarrow \gamma\gamma$ for the $\mu^+\mu^- \rightarrow H\nu_\mu\bar{\nu}_\mu$ process is plotted. As for the muons, high-energy photon reconstruction is not heavily impacted by the beam-induced background. In fact, the di-photon mass distribution has a peak with a width of 3.2 GeV, with a small tail at higher masses that does not have an impact on the $H \rightarrow \gamma\gamma$ measurements. These events are then used to evaluate the energy resolution achieved with the current calorimeter. This range of energy is dominated by the constant term, which is about 3%.

The case is different for hadronic jets that are also reconstructed with low-energy objects. The reconstruction performance of low-momentum tracks and low-energy calorimeter clusters is impacted by the beam-induced background. The di-jet mass resolution is critical, for example, to separate the H and Z peaks as shown in Fig. 3.7. The current value of the Higgs boson mass resolution is about 18%, being dominated by beam-induced background effects, *i.e.* the energy thresholds set on the calorimeter hits. The dijet mass resolution is sufficient for determining the Higgs and Z bosons yields on a statistical basis, but in the future improving the jet energy resolution will be fundamental for several measurements. This can be achieved by optimizing the filters for removing the beam-induced background contamination, and subsequently by lowering the calorimeter energy thresholds.

3.2.2 Key challenges

The first studies with the detailed detector simulation have shown that the effects of the beam-induced background on high-energy objects in the central region of the detector are negligible. One of the key challenges in event reconstruction is dealing with physics objects that have low energy and physics objects that are in the forward or backward regions of the detector.

The beam-induced background mitigation measures must be refined and perfected to improve the reconstruction of the low-energy objects. For instance, the energy thresholds on the calorimeter hits

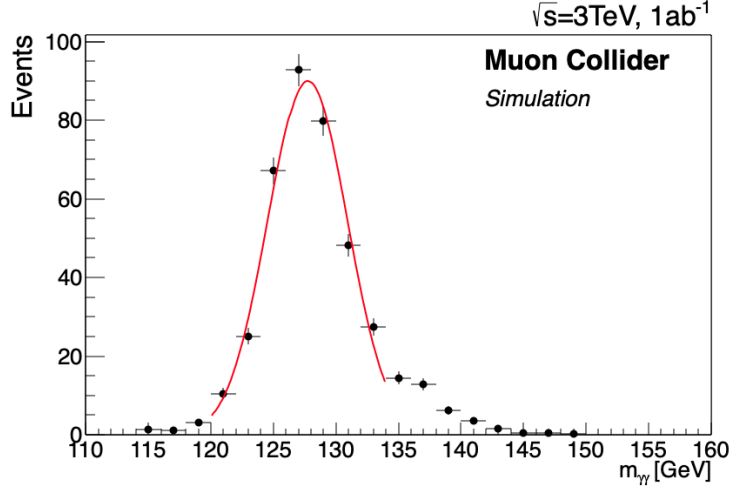


Fig. 3.6: Invariant mass distribution of the photon pairs produced in the $\mu^+\mu^- \rightarrow H\nu_\mu\bar{\nu}_\mu \rightarrow \gamma\gamma\nu_\mu\bar{\nu}_\mu$ process with the beam-induced background overlaid to the physics events.

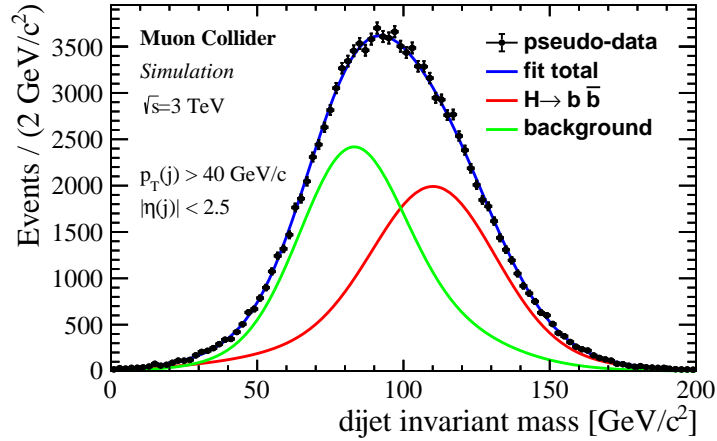


Fig. 3.7: Invariant mass distribution of the jet pairs produced in the $\mu^+\mu^- \rightarrow H\nu_\mu\bar{\nu}_\mu \rightarrow b\bar{b}\nu_\mu\bar{\nu}_\mu$ process with the beam-induced background overlaid to the physics events: the reconstructed mass peak of the Higgs boson is indicated in red, while the background from $Z \rightarrow b\bar{b}$ and $Z \rightarrow c\bar{c}$ is in green.

affect the energy resolution of jets and low-energy photons and electrons. In the detector forward and backward regions closer to the beamline, the beam-induced background levels are higher. At multi-TeV collision energies, all the standard model particles are highly boosted in the forward region and their decays may produce particles that are very close to each other in space or even overlapping in the detector. Dedicated algorithms must be developed for those cases.

3.2.3 Work progress since Roadmap

Since the Roadmap, an assessment has been performed of the reconstruction performance for tracks, muons, electrons, photons, and jets in the presence of the beam-induced background with a detailed detector simulation at a 3 TeV collider, as discussed in Section 3.2.1. The reconstruction algorithms of the physics objects were revised and fine-tuned to preserve their reconstruction efficiency and the accuracy in the determination of their properties.

Moreover, such physics objects were used to carry out sensitivity studies on the Higgs boson

production cross sections at a 3 TeV collider. Although preliminary, the results [8] are competitive with respect to the corresponding full-fledged estimates from the CLIC Collaboration at the same collision energy.

3.2.4 *Work planned for Evaluation Report*

The work plan for the Evaluation Report follows two main directions: the completion of the physics objects studies at the 3 TeV center-of-mass energy and a preliminary evaluation of the reconstruction performance for the main physics objects at a $\sqrt{s} = 10$ TeV collider.

At 3 TeV center-of-mass energy, a refinement of the electron and photon reconstruction is planned: the energy resolution is currently limited at low energies by the high thresholds set for the electromagnetic calorimeter hits and at high energies by the spillage of the electromagnetic showers into the hadronic calorimeter; electron reconstruction would also benefit from the recovery of the radiated bremsstrahlung photons. Furthermore, the tau leptons are still missing to complete the set of available physics objects and their reconstruction algorithms must be studied. In addition, only preliminary studies were conducted on the missing energy determination due to the issues on the calorimeter object reconstruction. The improvements already discussed on this sub-detector will open the possibility also to tackle the missing energy resolution.

3.2.5 *Important missing effort*

Some efforts are still missing to get a complete picture of the detector performance at 3 TeV and to have a full set of reconstructed objects to be used in physics studies:

- a study of the reconstruction algorithms for tau leptons with the beam-induced background and an assessment of their performance;
- an optimization of the jet reconstruction, taking advantage of an improved reconstruction of low-momentum objects and possibly the identification of jet substructure;
- development of dedicated algorithms to reconstruct and identify boosted physics objects;
- an improvement of the jet flavour identification, exploiting more sophisticated algorithms based on artificial-intelligence techniques;
- an assessment of the most suitable particle identification techniques and algorithms in the muon collider environment.

The major part of the resources will be dedicated to the study of the $\sqrt{s} = 10$ TeV performance. The algorithms studied for the 3 TeV case will optimize and adapted where needed, to the higher center-of-mass energy. New methods may be developed to reconstruct physics objects that exhibits different properties at high energy.

3.3 **Technologies**

3.3.1 *System overview*

The detector concept described earlier serves as a starting point for evaluating the expected detector performance in different physics scenarios by building an efficient full-simulation workflow to study various beam-induced background mitigation strategies. At this conceptual stage, only general assumptions

about the relevant detector parameters were made, such as dimensions, material composition, granularity, and spatial and time resolution. This approach simplifies the process of iterative variations towards an optimised detector design for which specific technology details can be implemented at a later stage. These studies allow the identification of the key features of different sub-detectors at a Muon Collider experiment, which are summarised in the recent review for Snowmass 2021 on the promising detector technologies and R&D directions [9].

From the technology perspective the present $\sqrt{s} = 3$ TeV detector model can be divided into six sections ordered by increasing distance from the interaction point:

1. **vertex detector (VXD):** *Si* sensors with $25 \times 25 \mu\text{m}^2$ pixels and time resolution of $\sigma_t = 30$ ps arranged in double layers with 2 mm spacing;
2. **inner (IT) and outer (OT) tracker:** *Si* sensors with $50 \mu\text{m} \times 1$ mm (IT) and $50 \mu\text{m} \times 10$ mm (OT) macro-pixels and time resolution of $\sigma_t = 60$ ps;
3. **electromagnetic calorimeter (ECAL):** sampling design with *W* absorber and *Si* sensors arranged in $5 \times 5 \text{ mm}^2$ tiles;
4. **hadronic calorimeter (HCAL):** sampling design with steel absorber and plastic-scintillator tiles arranged in $30 \times 30 \text{ mm}^2$ cells;
5. **superconducting solenoid:** magnetic field strength of 3.57 T with a *Fe* return yoke;
6. **muon detector:** Resistive Plate Chambers (RPC) divided into $30 \times 30 \text{ mm}^2$ cells interleaved in the magnet's return yoke.

Description of this geometry is implemented in the DD4hep [5] framework, which provides interface to GEANT4 [4] simulation software and to Marlin [6] framework for detector digitization and event reconstruction. Two generic types of hits are used in the detector simulation:

- **tracker hit:** corresponds to a single energy deposited by a particle in the sensitive volume, with associated energy, time and position of the deposit within the volume;
- **calorimeter hit:** corresponds to the integrated energy deposited by one or more particles in the sensitive volume during the fixed integration time, with only the total energy and time assigned to the hit associated with the volume.

Tracker-type hits are used for VXD, IT and OT detectors, while calorimeter-type hits are used for the ECAL, HCAL and muon detectors, which have the actual granularity implemented in the geometry.

3.3.2 Key challenges

High-intensity beam-induced background that survives after passing through the MDI nozzles poses significant challenges for most of the sub-detectors by inducing high levels of radiation and by creating excessive amount of background hits. Projected levels of total ionizing dose (TID) and neutron fluence at Muon Collider are comparable to those expected at HL-LHC, while the background hits have signatures unique to Muon Collider and require dedicated treatment in each sub-detector to achieve the necessary physics performance.

In the tracking detectors, the beam-induced background causes very high hit density, up to 5×10^3 hits/cm² in the innermost layers of VXD, when integrating over a 15 ns readout window. Combinatorial background arising from such a large number of hits makes track reconstruction unfeasible

unless the amount of background hits entering the pattern recognition algorithm is significantly reduced. The primary beam-induced background suppression methods in the tracking detectors are:

1. **timing:** rejection of hits outside of a very narrow time window of about 100 ps (exploiting the characteristic time distribution of beam-induced background hits, as shown in Fig. 3.8;
2. **direction:** rejection of hits inconsistent with pointing at the interaction region by estimating their direction from a stub of two hits in a double-layer;
3. **cluster shape:** rejection of beam-induced background hits represented by wider clusters of pixels due to crossing the sensors at a shallower angle;
4. **goodness of fit:** rejection of fake track candidates due to bad χ^2 .

Considering these aspects, the great challenge for tracking-detector technology is to provide extreme time resolution and on-detector hit filtering while maintaining low material budget and high radiation tolerance. A low material budget indirectly requires low power density of the readout electronics such that it can be cooled without introducing additional heat-exchanging materials. We should also note that these beam-induced background suppression methods could potentially limit the performance of long-lived particles, for which a dedicated strategy should be defined in the future.

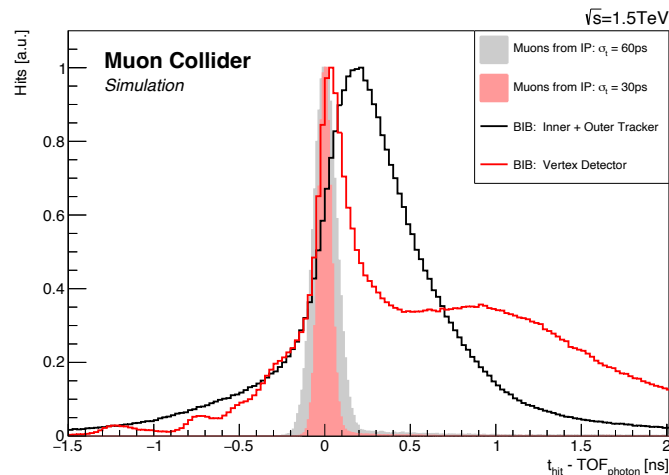


Fig. 3.8: Time distribution of hits in the tracking detector corrected for the expected photon's time of flight from the interaction point. Hits from the beam-induced background (BIB) are shown by solid lines, while hits from single muons smeared by corresponding time resolutions are shown by filled areas.

In the ECAL and HCAL sub-detectors beam-induced background contribution comes primarily from low-energy photons and neutrons respectively, which have a relatively uniform angular distribution across the detector volume. Yet, their distribution in time and depth is different from the shower signatures produced by the hard collision, as shown in Fig. 3.9. Given that the beam-induced background contribution partially overlaps with the signal hits, with the current configuration and technology of the calorimeters, it can't be excluded from the readout completely and has to be subtracted instead at a later stage. To minimise the effect of such beam-induced background subtraction on the resulting energy resolution the corresponding detector should possess high spatial granularity and time resolution, allowing to measure the corresponding time and depth profiles of the shower. In particular fine depth segmenta-

tion implies a large number of sensitive layers in the detector, making the cost of the technology also an important factor. Thus, the main challenge for the ECAL and HCAL technologies is to provide excellent time resolution in a finely segmented detector at a low cost, while being compatible with the radiation-hardness requirements.

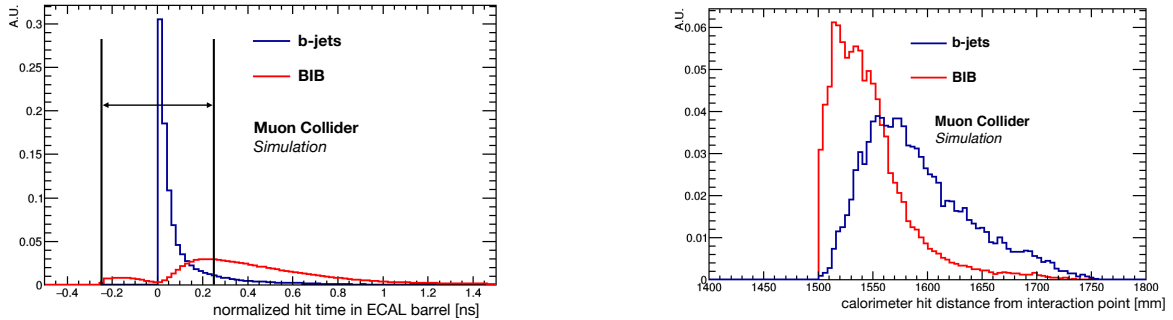


Fig. 3.9: Difference between the time (left) and depth (right) of the hits produced by beam-induced background (BIB) and signal b-jets.

The muon system is relatively unaffected by the beam-induced background contribution except for the very forward region, where high-energy neutrons and photons create hits near the MDI nozzles. While this does not pose any serious challenge for muon detection itself, it is nevertheless important to have high spatial and time resolution to allow matching of standalone muon tracks with hits in the tracking detector. Such seeding of muon tracks from the muon system would greatly improve muon-reconstruction speed given the high combinatorial background in the tracking detector.

3.3.3 Work progress since Roadmap

Several developments have been done for different sub-detectors towards a better definition of their technical characteristics.

A realistic digitization algorithm for pixel sensors of the tracking detectors has been implemented and integrated into the Muon Collider simulation software. With a configurable pixel pitch for the sensor together with other readout parameters like noise and threshold it provides realistic pixel clusters that can be used for beam-induced background suppression. On the hardware side several technologies have the potential to meet the requirements of the tracking detectors, such as AC- and DC-coupled LGAD, trench-isolated LGAD, as well as MAPS technology thanks to its particularly low material budget. Estimates of the data rate induced by the beam-induced background hits underline the importance of fast and radiation-hard data-transfer links, such as LpGBT, and careful design of the data acquisition logic. Reduction of the amount of data directly in the readout chip is particularly important in this respect.

For ECAL a new conceptual design has been implemented in the simulation based on Crilin technology [19], which is a semi-homogeneous calorimeter with finely segmented Cherenkov-radiating crystals providing high time resolution at relatively low cost. After showing a good performance in simulation studies several physical prototypes have been built and tested to experimentally validate this technology. The latest beam test [20] of a multi-layer prototype at CERN demonstrated a time resolution of $\mathcal{O}(20\text{ ps})$ and good agreement with Monte Carlo simulations, as shown in Fig. 3.10.

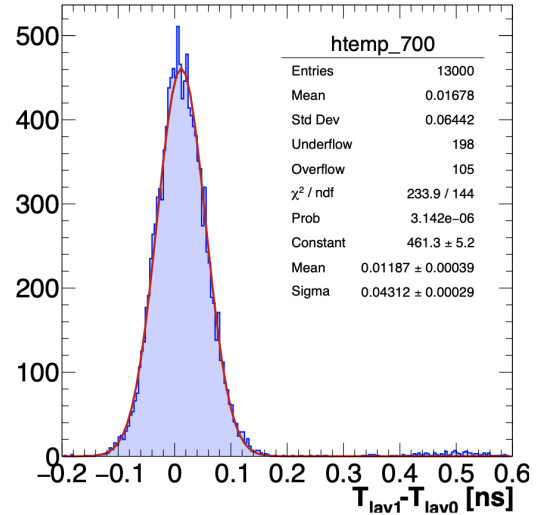
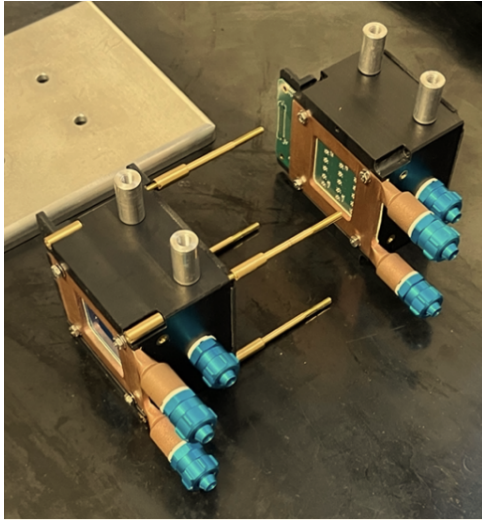


Fig. 3.10: Left: two out of three detection layers of the Crilin prototype tested at CERN. Right: Distribution of the time difference between two neighbouring layers of the prototype.

For HCAL the use of Micro-Pattern Gas Detectors (MPGD) [17] as an active layer is under study, which offers good energy and time resolution at high rate and low cost for instrumenting such a large area. The corresponding design has been implemented in the detector geometry for full-simulation studies, which showed performance comparable to that of the current baseline. The technologies being considered are μ RWell, RPWell and MicroMegas, for which initial digitization logic for digital readout has been implemented in the simulation software. Physical prototypes for each technology have been also produced and two test-beam campaigns have been carried out at CERN during 2023 (see Fig. 3.11), which showed good results in terms of MIP detection efficiency.

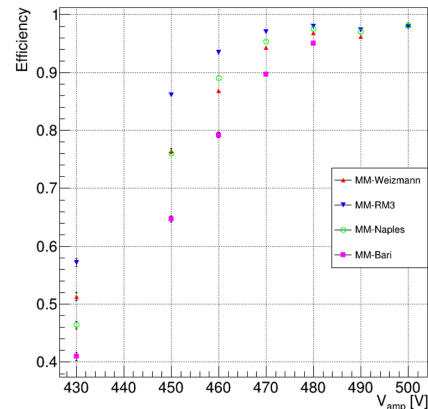


Fig. 3.11: Left: MPGD-based HCAL prototype tested at CERN having multiple layers built with different technologies. Right: measured MIP-detection efficiency of different MicroMegas layers as a function of the applied high voltage.

For muon detector, the Picosec technology [18] is being studied as a better-performing alternative to the RPC layers. It uses a crystal Cherenkov radiator, coupled to a UV-transparent photocathode and a two-stage amplification by Micromegas, providing a time resolution comparable to that of the tracking detector. This would be of great importance for rejecting out-of-time beam-induced background hits,

especially in the forward region of the muon system where the rates are high. Several prototypes have been tested with different photocathode materials and gas mixtures, with very promising preliminary results, as shown in Fig. 3.12. Finally, the tested Picosec geometry has been interfaced with the full-simulation framework to study its performance in the forward region in the presence of beam-induced background.

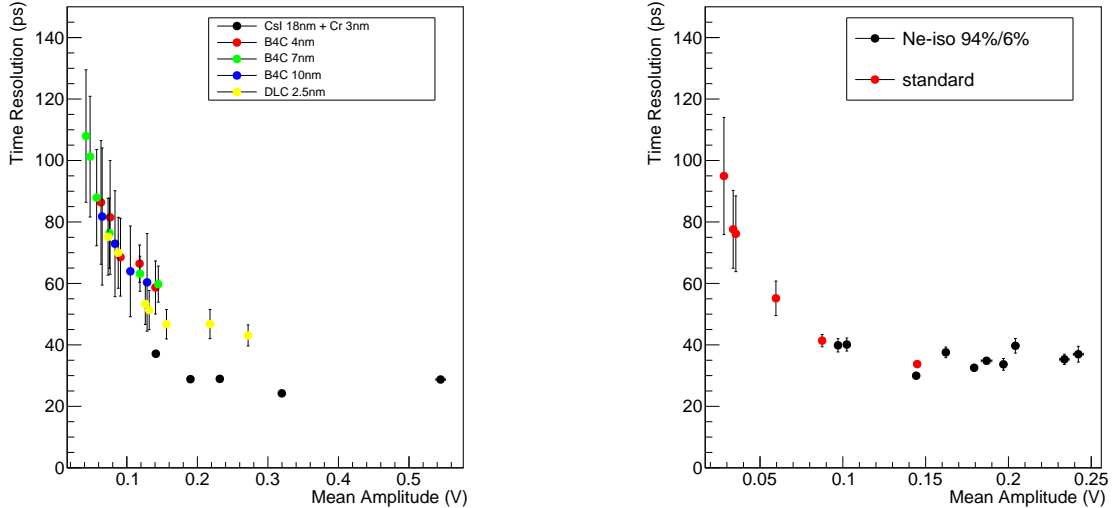


Fig. 3.12: Time resolution obtained by the Picosec prototypes as a function of the mean signal amplitude compared for different photo-cathode materials (left) and gas mixtures (right).

It should also be noted that the Detector and Physics community of IMCC has been deeply involved in the ECFA planning, making sure that all the mentioned technologies relevant for each sub-detector are included in the corresponding DRD collaboration roadmaps. Similar efforts are also taking place within CPAD. A comprehensive list of all the relevant technologies can be found in [9].

3.3.4 Work planned for Evaluation Report

A number of developments are planned to progress towards a well-defined conceptual detector design. Important input is expected from experimental tests of the first production batches of DC-RSD sensors [21], which is a promising technology for the tracking detector. In particular its ability to achieve low occupancy by controlling the extent of charge sharing will be validated and implemented in the simulation software. R&D on the technologies considered for the ECAL, HCAL and muon detector will continue according to their working plans, which are part of the coordinated DRD and CPAD efforts in Europe and U.S. respectively.

3.3.5 Important missing effort

All the sub-detectors have one candidate technology that is being worked on, which is sufficient to move forward. Yet the lack of alternative new technologies developed in the context of Muon Collider makes it less likely to achieve the best possible physics performance.

This lack of new technologies is particularly important in the tracking detector, where the technology is at a very early stage and multiple technical aspects need to be addressed. These include the possibility of having long pixels in the Inner and Outer Trackers, where hit density is lower, which is

challenging to implement in DC-RSD technology. Different possible readout implementations can have great impact on the sensor's efficiency, granularity of the timing information and the resulting power consumption. An integrated approach to the tracker design that also includes the mechanics and cooling will be very important in the future.

The integration of all sub-detectors, currently missing, will be studied once the technology for each individual sub-detector is defined.

3.4 Software and Computing: Concepts

3.4.1 System overview

The muon collider software framework [3] is based on CLIC's iLCSoft. It includes the DD4hep toolkit [5] to model the detector geometry, the GEANT4 [4] program to simulate the detector response, and the Marlin package [6] for the event digitization and reconstruction. Stable particles are generated by external packages and given as input to the aforementioned software. Signal and physics background events are produced by users with common packages like WHIZARD [13] and MADGRAPH [14]. The beam-induced background bunch-crossings, instead, are produced by using the FLUKA [15] and Fluka-LineBuilder [16], as described in Section 2.2. The programs workflow proceeds as:

- generation of $\mu^+\mu^-$ interactions and beam-induced background bunch crossings;
- simulation of the interaction of the generated particles with the passive and active elements of the detector; the results are stored as SimHits;
- overlay of beam-induced background SimHits to the $\mu^+\mu^-$ interaction events;
- reconstruction of the energy deposits in each sub-detectors, i.e. tracker, calorimeters, muon system producing RecHits;
- reconstruction of high-level physics objects e.g. charged particle tracks, jets, secondary vertices, muons, electrons, etc.

The physics objects are then used in the analysis measurements, as presented in Section 3.2.1. The software infrastructure is currently supported and maintained by two INFN experts.

The computing infrastructure is formed by:

- CPU: accessed via cloud services provided by INFN and CERN;
- storage: disk space of about 600 TB at INFN sites and about 100 TB at CERN.

3.4.2 Key challenges

The major challenges identified so far are the following:

- production of the beam-induced background bunch-crossing events, see Section 2.2 for a description;
- simulation of the beam-induced background particles in the detector; this task requires a significant amount of CPU time, in Ref. [3] such a time is quantified depending on the configuration used to track particles throughout the material;

- the overlay of the beam-induced background hits with the $\mu^+\mu^-$ interactions particle hits; this process demands a significant amount of computing memory (RAM) per event, for a detailed discussion see Ref. [3];
- tracks and calorimeter object reconstruction from RecHits including the beam-induced background; it can be performed only under particular conditions, for example by filtering tracker hits depending on their arrival time on the sensor and subtracting a tuned amount of energy in the calorimeter cells.

3.4.3 Work progress since Roadmap

The software has been improved significantly since the roadmap to reduce the amount of computing resources and the time necessary to simulate and reconstruct a complete bunch-crossing event. A complete description of the improvements can be found in Ref. [11]. The notable optimisations include the early exclusion of irrelevant beam-induced background particles from GEANT4 simulation by filtering tracker-hit collections based on the arrival time on the sensor, as well as the integration of ACTS (A Common Tracking Software) track-reconstruction framework [12].

Another important step forward is the transition to the common Key4hep software stack that is almost completed, but not yet in production.

From the point of view of the code distribution to the users, two major software releases have been done since the the roadmap, in June 2022 and April 2023. The software is available with its distribution via docker images and CERN CVMFS.

3.4.4 Work planned for Evaluation Report

The major activities currently in progress and likely to be ready at the time of the evaluation report are:

- complete transition to Key4hep and distribution of a production release, depending on the person-power available;
- definition of the release validation workflow;
- definition of a user support, with voluntary personnel, to help newcomers to use the software structure ;
- expansion of computing infrastructure to include additional European and US sites.

3.4.5 Important missing effort

The computing infrastructure is distributed in different sites, a federation is needed with an authentication and an authorization method common to the IMCC. A similar problem is present on data management, where different architectures are used by different sites and within IMCC there is no data management system in place. Both these activities are not pursued due to the lack of person-power.

The usage of advanced artificial intelligence methods for physics object reconstruction like tracks and jets and their identification could significantly improve the performance by helping to minimize the impact of the beam-induced background. These activities require a significant increase of the person-power.

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4 Accelerator Design

This chapter describes the whole accelerator chain of the proposed muon collider complex. The challenge of the proton complex is to provide the few MW proton with very short bunch lengths of a few ns and low repetition rate of 5 Hz. The Muon Production Cooling part consists of a target inside an as high as possible magnetic field and standing the drive beam power, a decay channel with decreasing magnetic fields and comprising a chicane to remove unwanted particles, a section for longitudinal capture of the muons and, finally, several ionization cooling channels interleaved with a section merging several muon bunches into one bunch. The acceleration to high energy has to be fast requiring large average RF gradients at all stages; the baseline solution consists of a sequence recirculating Linacs followed by very rapid cycling synchrotrons accelerating the beam within a few tens of turns. Finally, the muons are injected into the muon collider ring, which has to provide sufficient luminosity leading to a challenging design with β^* and rms bunch length of a few mm and large rms momentum spread of around $1 \cdot 10^{-3}$.

4.1 Proton Complex

4.1.1 System Overview

The proton complex is the first piece in the Muon Collider complex. It comprises of a high power acceleration section; an accumulator and compressor; and a target delivery section. The high power acceleration section can take many shapes. In our baseline design we will study a final energy linac. This section is responsible for delivering high power, high intensity bunches to the accumulator and compressor section. At the end of the high power acceleration section the pulse total charge is distributed among a high number of bunches with a small energy spread. Such a long train of bunches do not reach the desired instantaneous power for intense pion production on the target.

In order to achieve the high proton intensities in a short pulse, an Accumulator and Compressor ring will be used to combine and compress the protons into very short bunch, with a length of the order of ~ 2 ns rms. The first storage ring, the Accumulator, accumulates the protons via charge stripping of the incoming H^- beam from the linac section, preserving the energy spread. The incoming beam is chopped to allow a clean injection into the ring circumference. The second storage ring, the Compressor, accepts between 1 and 6 intense bunches from the Accumulator and performs a 90° -bunch rotation in longitudinal phase space, shortening the bunches to the limit of the space-charge tune shift just before extraction. The Compressor ring must have a large momentum acceptance to allow the storage of the beam with a momentum spread of a few percent, which arises as a consequence of the bunch rotation.

The target delivery section transports the final intense short bunches from the compressor to the target, ensuring that neither the transverse nor longitudinal properties of the beam are compromised in the process. To achieve optimal luminosity, the final collider will work in single bunch colliding mode. Therefore, in the multi-bunch solution, short bunches extracted from the Compressor must be recombined and hit the pion production target simultaneously.

The primary requirement of the Proton Complex is to enable the production of a high number of useful muons at the end of the decay channel after the target. The production rate, to good approximation, is proportional to the primary proton beam power, and (within the 5–15 GeV range) only weakly dependent on the proton beam energy. Considering a conversion efficiency of about 0.013 muons per proton-GeV, a proton beam in the 1–4 MW power range at an energy between 5 GeV and 10 GeV will

provide the sufficient number of muons required.

4.1.2 Key Challenges

The critical challenges for the Proton Complex include the determination of proton final energy on the target with significant implications for particle creation, the layout of the high power acceleration section, and the choice of target material and size. Two final proton beam energies, 5 GeV and 10 GeV, will be investigated during the length of the grant.

A comprehensive study is required to identify key parameters for the Proton Complex, including a compression scheme and the final number of bunches, thus influencing the layout of compressor ring lattice and the required number of turns for compression. The minimum number of bunches needed will affect the layout of the *ring-to-target* delivery design. The beam parameters on the target surface will impact the design of the expense beam dump, which can be challenging due to target geometries and constraints.

Determining the linac chopping scheme is another key parameter, which will directly influence the linac pulse length and current, and subsequently, the accumulator and further accelerator design.

Other important challenges include the design of the accumulator lattice for both energies to be studied, investigation of the instability thresholds in the accumulator and compressor rings, error analysis across the entire complex with a focus on bunch recombination at the target delivery system, and continuous development of the H^- source to meet the needed pulse current and length for the Muon Collider's requirements, including potential upgrades.

4.1.3 Recent Achievements

A baseline lattice for the accumulator and compressor for the 5 GeV case, based on the studies for the Neutrino factory at CERN, was revised and ported to XSuite. Basic beam physics parameters are being collected and compiled and a parametric study is underway. A first look at the transport between ring and target of a 2 ns high current bunch has started. A compilation of the literature on past projects, with special attention to US Muon Acceleration Program (MAP) [1,2] results, was done.

Since both the accumulator and compressor rings are strongly space charge limited machines, an evaluation of available codes for space charge dominated beam simulation is under way. In order to complement this evaluation a collection of data from CERN PS bunch rotation and Booster bunch recombination, both with high density bunches, was carried out. Data analyses and further plans are underway.

4.1.4 Planned Work

The majority of the planned work for the following year is concentrated on the compressor lattice design, refinement, and target delivery parameters. We plan to explore possibilities at a beam energy of 5 GeV, including the definition of minimum number of bunches possible and a rotation scheme. Also for the 5 GeV case, we plan to narrow down the beam parameters that are possible to be delivered to the target. A second step in the process will be the design of a 10 GeV compressor ring and the re-design of the target delivery section, in case the 5 GeV solution is unable to achieve the required beam quality.

Other planned work regarding the Proton Complex includes:

- Compilation of linac technologies and main parameters
- Study on H^- source capabilities (current and pulse length)
- Study on H^- stripping for injection into the Accumulator
- Definition of a possible chopping scheme for the linac and final accumulator setup
- Definition of RF requirements for bunch rotation
- Initial study of main instabilities in the accumulator and compressor rings

4.1.5 Important Missing Effort

Several crucial efforts will remain incomplete given the current resource constraints. Notably, the study proposal does not encompass work on the accumulator or further acceleration (beyond the linac final energy of 5 GeV). Exploring alternatives to the final energy linac and finding a way to elevate the 5 GeV linac energy to the 10 GeV case are not feasible with the existing resources. Moreover, limitations in resources will not allow in-depth error and instability studies in various sections of the complex. Integrated engineering activities, as well as the detailed RF design for the rotation scheme, will be lacking. Alternative rotation setups will also remain unexplored. In depth work on the linac lattice design and alternatives to a full energy linac option will also not be covered. Many R&D topics regarding H^- source development, H^- stripping, high efficient acceleration, design of high-gradient Super Conducting (SC) cavities for the linac will be either partially covered or not at all developed at this stage, and we will use already proven schemes and setups for the SC linac in the baseline design.

4.2 Muon Production and Cooling

4.2.1 System Overview

The muon production and cooling system comprises several subsystems. The protons provided by the proton complex intersect a target to produce pions. The target is immersed in a 20 T solenoid field, yielding a high pion flux. The field is rapidly tapered to 1.5 T. Pions and muons traverse a solenoid-focused chicane where high momentum beam impurities are removed followed by a Beryllium absorber which ranges out remnant low energy protons. The remaining beam passes through a longitudinal drift where any remaining pions decay. The beam is then captured longitudinally. A multi-frequency RF system that captures the beam into 21 bunches is required owing to the initially large longitudinal beam emittance. Another solenoid chicane system splits the beam by charge species, in preparation for the ionisation cooling system.

The ionisation cooling system comprises a series of solenoids, which focus the beam onto energy absorbers where the beam momentum is removed. The momentum is restored longitudinally using RF cavities resulting in a reduction in the beam's emittance (volume in position-momentum space). An initial rectilinear cooling system reduces the beam emittance sufficiently that the many initial bunches can be merged into one single bunch. The beam is then cooled further to the final emittance, using a continuation of the rectilinear cooling system followed by a sequence of high field solenoids operated ultimately with a low momentum (non-relativistic) beam. The beam is finally reaccelerated to relativistic speeds so that it can be delivered to the acceleration system.

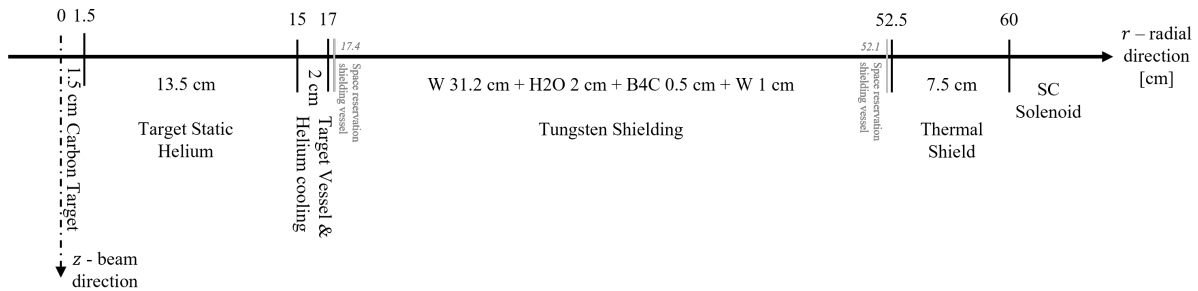


Fig. 4.1: Target radial build.

4.2.2 Key Challenges

Critical challenges have been identified in the muon production and cooling system.

- An outline cooling system was prepared by the US Muon Accelerator Program (MAP) [1] that yielded an emittance that did not meet our requirement by a factor 2. The MAP system used conservative equipment parameters, but more demanding parameters may yield improved performance while remaining practical. Significant risk was identified associated with heating in the final cooling absorbers. The MAP system must be assessed and optimised to get a better understanding of the potential system performance including thorough assessment of engineering challenges.
- A detailed design for the pion production target, solenoid and surrounding infrastructure must be performed. This target is as demanding as state-of-the-art horn-based pion production targets. Solenoid focusing at high beam powers in this environment has not yet been done in practice. Assessment of the associated issues must be performed, building on the work done by MAP, including detailed assessment of solenoid feasibility accounting for radiation and thermal loads in liaison with the magnet team. Handling of the spent proton beam must be studied in detail.

Other important challenges have been identified.

- A system to separate the charge species has not been designed. In the baseline design the system must accommodate very large emittance which is not readily manageable using a conventional system, while maintaining the bunch structure.
- A design for the longitudinal capture system exists. In order to enable pion yield optimisation studies to continue, the sensitivity to incident beam parameters must be understood.
- A design for the bunch merge system was done but the lattice is no longer available. A new lattice must be generated and sensitivity to parameters must be performed.
- It is very likely that the overall system performance may be greatly increased by looking at alternative designs to the baseline described above. This could dramatically improve the facility performance.

4.2.3 Recent Achievements

The target team have designed a baseline radial build for the pion production target, taking into account radiation flux into the surrounding solenoid, heat load on the graphite target itself and appropriate cool-

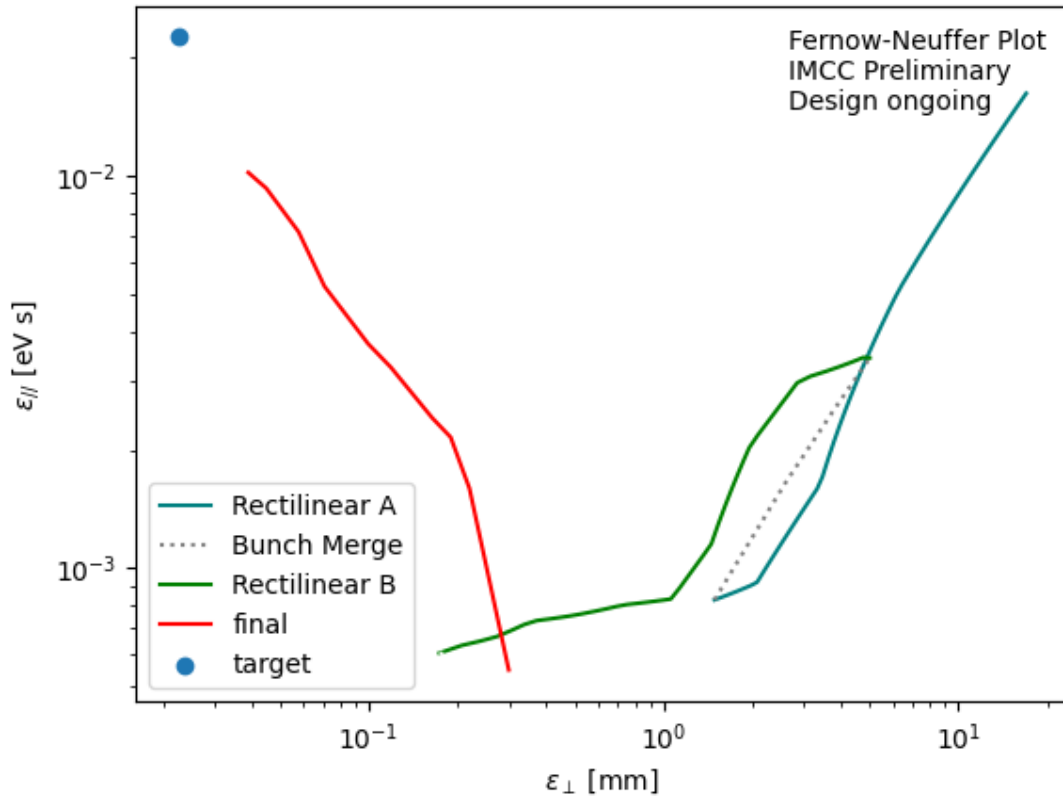


Fig. 4.2: System performance of the muon cooling system, including an updated rectilinear and final cooling system. Optimisation continues; in particular the rectilinear cooling system final emittance has not been integrated with the final cooling system.

ing systems for the target and shielding (detailed in 5.4 and 5.5). The radial build is shown in Fig. 4.1. A 3D FLUKA model for the target area has been constructed and the pion and muon yield through the target system has been assessed. The magnet team have identified HTS technology as having greater tolerance to radiation issues. The target team have updated the design with reduced shielding. Preliminary concepts for the spent proton beam handling have been studied.

Beam physics designs have been made for the ionisation cooling systems. Two cooling systems have been studied, the rectilinear cooling system, used at high and intermediate emittances, and the final cooling system, used for low emittances. The optical parameters of the solenoid system have been assessed and parameter dependencies established, including non-linear optics dependencies on momentum and transverse emittance. Possible lattices using different RF technologies have been assessed. A preliminary system optimisation for both lattices has been performed yielding potentially improved performance. The current performance estimate for the ionisation cooling system is shown in Fig. 4.2. The performance of both the rectilinear and final cooling systems have been improved yielding significantly smaller transverse and longitudinal emittance compared to previous baselines. Optimisation continues and it is expected that the simulated performance will improve further.

4.2.4 *Planned Work*

The target design will continue with increasing detail. Systems for cooling of the shielding, moderation and absorption of neutrons will be refined. Improved models for the incident proton beam will be considered and the design for the upstream beam window will be updated. Preliminary studies for the handling of the spent proton beam have been envisaged but a detailed design does not exist. The existing beam physics design for the chicane and proton absorber will be refined and an engineering design for handling of the significant spent proton beam in this region will be developed. The 1.5 T solenoid field in this region will likely require superconducting technology. An appropriate collimation and shielding system will be designed to protect the solenoids in this region.

The intermediate emittance rectilinear cooling system design will be further optimised. The optimisation will be extended to include the high emittance rectilinear cooling system. The optimisation will be refined to include a more detailed assessment of the limitations of solenoid and RF fields, taking into account the required field profiles and highly compact nature of the lattice. An integrated design will be completed for a small subset of the cooling lattices that are proposed.

The final cooling system design will be further optimised. The lattice design will be refined in collaboration with magnet and RF experts. An integrated design will not be completed. Absorber heating increases rapidly at lower beam emittance and lower momentum characteristic of the downstream end of this system. Schemes to mitigate the impact on the liquid hydrogen will be assessed. Impact of misalignment and field errors will be assessed. Other collective effects will be assessed. The final cooling system will be integrated with the final emittance of the rectilinear cooling system. A system to reaccelerate the beam to relativistic speeds will be studied.

Limitations arising from space charge and beam loading will be assessed to estimate a maximum beam current that can traverse the cooling system. A preliminary estimate of tolerances to alignment will be performed. A preliminary design for the absorber will be made including a preliminary heat load assessment. A preliminary assessment of radiation load from muon decays will be performed and collimation systems will be considered. Beam instrumentation requirements will be considered. Simulation in alternate codes will be performed to validate the performance estimates.

For all systems, a future R&D path will be developed including an assessment of necessary equipment tests. Detailed studies of a rectilinear cooling channel cell for a cooling Demonstrator are described below.

4.2.5 *Important Missing Effort*

Several important studies with lower priority will not be carried out, assuming current resource levels continue. In the target region, effects of misalignments and field errors will not be studied. Mitigation schemes, to handle the case that the baseline design can not accommodate the required beam power or the requirements change, will not be studied in detail. Equipment tests will not be possible but a plan will be developed.

Integrated engineering will be performed for only a subset of the rectilinear cooling cells. Beam instrumentation will not be studied in detail. Correction schemes for misalignments will not be studied. Low frequency acceleration systems such as induction linacs, that may be advantageous for the final cooling system, will not be studied.

Integration systems, key for a start-to-end simulation, will not be developed. Consequently the muon production system will carry significant performance, risk, cost and power uncertainty. These integration systems are unconventional and technically challenging. In particular, the charge separation system, which has no current design, will not be developed. This system must separate muon charge species before cooling, where the beam that has transverse and longitudinal emittances that are expected to be too large for a conventional dipole-based scheme to manage without significant beam degradation.

The longitudinal capture and bunch merge system, which have beam physics designs, will not be developed further. Both of these systems have complex arrangements of RF cavities, operating at several frequencies, for simultaneous manipulation of several bunches. The schemes would benefit from analysis of the challenges in the RF systems. The bunch merge system additionally incorporates a challenging transverse funnel.

The baseline subsystems were chosen as they have the most mature design. Alternative schemes are likely to improve performance significantly, but have lower Technology Readiness Level. For example an emittance exchange scheme, employing a wedge absorber and dipole, could yield better performance compared to the final cooling scheme with simpler technology. A combined ‘HFoFo’ channel would be capable of cooling two charge species simultaneously, potentially yielding a more cost- and power-efficient cooling system. Frictional cooling, ring coolers, Parametric Ionisation Cooling channels and helical cooling channels may all yield improved cost, power or luminosity performance. None of these alternatives will be studied.

4.3 Acceleration

4.3.1 Low-energy acceleration

System overview

The low energy section involves three superconducting linacs operating at 352 MHz and 1056 MHz: a single pass linear pre-accelerator (PA) followed by a pair of multi-pass ‘Dogbone’ recirculating linacs (RLA). In the presented scenario, acceleration starts after final cooling at 255 MeV/c and proceeds to 63 GeV, where the beam is going to be injected into an first rapid cycling synchrotron. A schematic of the low energy section is shown in Fig. 4.3. The 352 MHz linac, which has a large aperture, is sufficient to transmit a beam that has received relatively little cooling. The 1056 MHz cavities linearise the RF waveform to minimise the growth of uncorrelated energy spread in the beam.

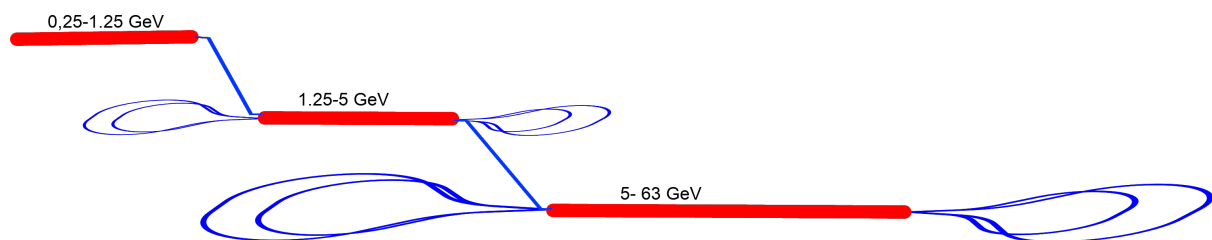


Fig. 4.3: Layout of a two-step-Dogbone RLA complex. Pre-accelerator, Dogbone I and Dogbone II are stacked up vertically; μ^\pm beam can be transferred between the accelerator sections by the vertical dogleg.

Key challenges

To ensure that the survival rates of muons are sufficient, the acceleration must be done at high average gradient. Since muons are generated as a secondary beam they occupy large phase-space volume. In addition to providing high average gradient, the accelerator must have very large transverse and longitudinal accelerator acceptances.

For the given longitudinal emittance, in order to accelerate of the muon beam within the given transverse and longitudinal emittance tolerances, the beamline must be designed to minimize transverse chromatic effects, thus tight focusing in bending plane with weak quadrupoles. In addition to preservation of the longitudinal emittance, the bunch length needs to be precisely controlled in the arcs.

The weak FODO channel chosen to minimize chromatic effects for first passages (where the beam energy is low) will lead to large betatron amplitudes at high energies, making the linac vulnerable to transverse wakefield effects. Considering the high bunch charge to be accelerated, the initial offset of the beam needs to be controlled precisely.

Another key challenge is the beam loading effect due to the high bunch charge. The following bunch will always gain less energy due to the beam loading effect of the the preceding bunch. Since both bunches will be recirculating in the same arc, the energy difference will lead to a transverse orbit deviation from the reference orbit in the arc, which will in turn lead to a transverse beam offset in the following linac pass. This offset will create a wakefield in the linac that will amplify the beam offset and potentially lead to beam loss or degradation. Therefore the beam loading effect needs to be controlled either by exchanging bunch positions or some other methods.

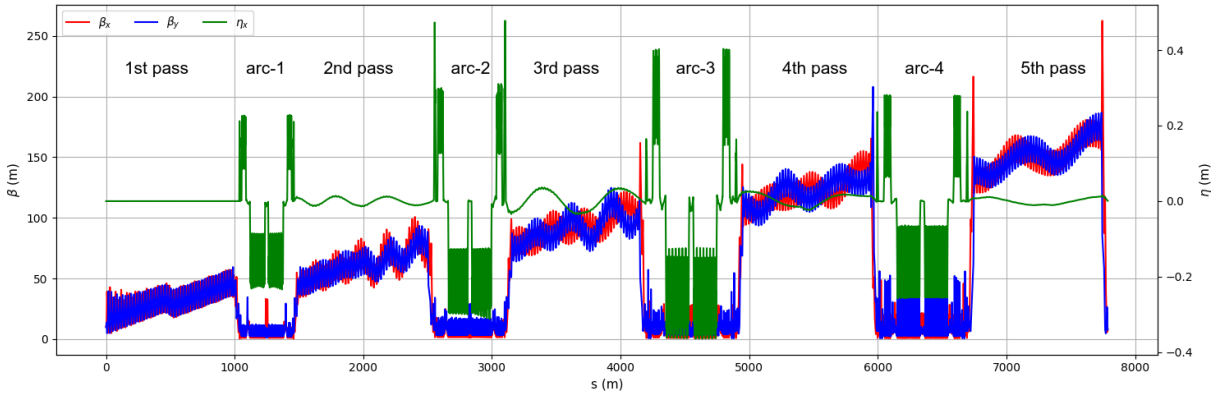


Fig. 4.4: Start-to-end Twiss functions along RLA2

Work progress since Roadmap

We created a preliminary lattice design for RLA2. We used a FODO focusing structure in the linac to reduce chromatic effects at low energy. Several lattice configurations were considered for the recirculating arcs including FODO, Triplet, Theoretical Minimum Emittance (TME) and Double Bend Achromat (DBA). The DBA showed better performance. An initial bunch with 100 mm.rad longitudinal and 40 mm.mrad transverse emittance could be accelerated from 5 GeV to 63 GeV while preserving longitudinal emittance, a 25% increase in transverse plane, and a better than 90% muon survival rate. Figure 4.4 shows the linear lattice functions along the RLA2. Because the quadrupole gradients in the linac are the same for each linac pass, the increasing beam energy in later passes leads to large beta func-

tions in later passes. Table 4.1 contains the main parameters for the simulated RLA2 and the predicted RLA1.

Parameter	Unit	PA	RLA1		RLA2	
Injection energy	[GeV]	0.255	1.25		5	
Ejection energy	[GeV]	1.25	5		63	
RF Frequency	[MHz]	352	352	1056	352	1056
Number of cavities	#	30	25	2	320	56
RF gradient	[MV/m]	25	25	30	25	30
Energy gain / pass	[GeV]	0.955	0.8		11.6	
Passes	#	1	5		5	

Table 4.1: Preliminary parameters for low energy acceleration

Work planned for Evaluation Report

Following works are planned as a next step as voluntary effort and provided resources can be made available.

- No work has been performed for PA and RLA1. Our next step will be to create designs for these lower energy parts. The large acceptance of especially in PA, requires large apertures and tight focusing. Combined with moderate beam energies, this favors solenoid rather than quadrupole focusing for the entire PA linac.
- We had have made significant progress with the lattice design in RLA2. However, the design still does not meet our performance requirements (see above) even without machine imperfections. We will therefore continue to improve this design until it meets our requirements.
- The gradients estimated in simulations are somewhat optimistic. All simulations will be repeated for lower acceleration s: 16 MV/m for 352 MHz, 30 MV/m for 1056 MHz.
- The impact of machine imperfections and operation strategies balancing contradicting requirements will be implemented in simulations

Important missing effort

The expected gradient and balancing beam loading effect for the accelerating gradient plays a main role on the muon survival rate in the low energy section.

An initial 6D phase space distribution is essential for performing more realistic simulations in the low energy acceleration chain of muon collider. Our simulations have thus far assumed a Gaussian distribution, but the upstream systems could deliver a beam very different from that. Simulations that provide that distribution will not be available during this study, if for no other reason than the systems upstream of the PA will not be fully designed.

4.3.2 High-energy acceleration

System Overview

For the high-energy acceleration from 63 GeV to the TeV range, a chain of rapid cycling synchrotrons (RCS) is foreseen to accelerate the two counter-rotating bunches with a repetition rate of

5 Hz. One option, inspired by the US Muon Acceleration Program (MAP) [1, 2], includes intermediate stages of 0.30 TeV, 0.75 TeV and 1.5 TeV to finally reach 5 TeV before injecting the muons into the separate collider ring. This scenario is illustrated in Fig. 4.5. The first two RCS share the same tunnel,

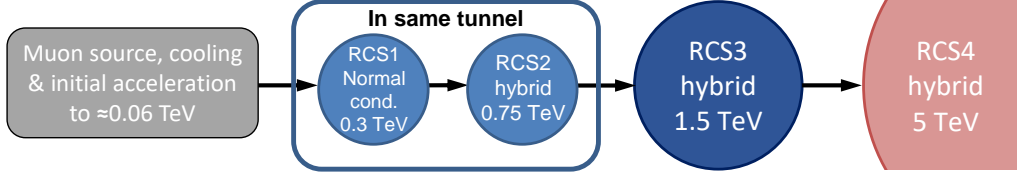


Fig. 4.5: Sketch of the chain of rapid cycling-synchrotrons for the high-energy acceleration complex. From [3].

meaning that they have the same circumference and layout [4]. The bending in the first RCS is provided by normal conducting magnets. The RCS2 to RCS4 are planned as hybrid RCSs where strong fixed-field, superconducting magnets are interleaved with normal conducting magnets cycling from $-B_{nc}$ to $+B_{nc}$. This combination allows for a large energy swing combined with a high average bending field to minimize the radius and thus the travel time and decay of the muons.

Key Challenges

To keep decays acceptably low, the RCSs must have high average gradients G_{avg} , as high as 2.4 MV/m. The average gradient is the energy gain in one turn divided by the circumference; since most of the ring does not contain RF, the gradient in the RF sections must be significantly higher than that average gradient. Assuming a survival rate of 90% per RCS, ultra-fast acceleration with tens of GeV energy gain per turn is required. The RF voltage has therefore to be provided by hundreds of superconducting cavities. To both provide large gradients, ILC-like 1.3 GHz cavity structures, also known as TESLA cavities [5], have been assumed for the simulations. As a result of the tens of GV of RF voltage, the number of synchrotron oscillations per turn is much larger than the conventional stability limit for stable synchrotron oscillations and phase focusing of $1/\pi$ [6] in a synchrotron with one or few localized RF sections. As a consequence, the RF system must be distributed over the entire RCSs in order to reduce the synchrotron tune between two consecutive RF stations to a value much smaller than that instability limit.

As a direct result of the decay and ultra-fast acceleration, the acceleration times are in the millisecond range and the number of turns in each RCS is between 17 and 66. In the RCS chain, the ramp rate of the normal conducting magnets is on the so far unprecedented order of kT/s, a particular challenge. Further, due to the hybrid structure of the three downstream RCSs, beam orbits and radii are not constant anymore, but change locally, as depicted in Fig. 4.6. Special attention is therefore being paid to the lattice design in order to minimize the orbit length change during acceleration. Fast cavity detuning on the kHz scale to match the RF frequency with the changing revolution frequency have to be developed.

With the special beam structure of counter-rotating, intense single μ^+ and μ^- bunches, large transient beam loading for both fundamental and higher-order modes must be expected.

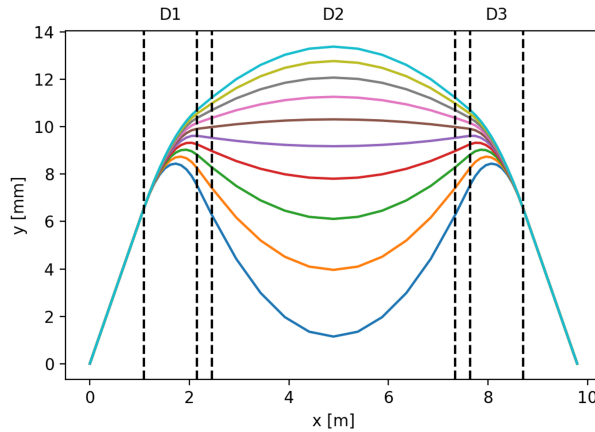


Fig. 4.6: Trajectories in a half-cell of RCS2. The injection/extraction orbits are respectively in the inner/outer side (in blue/cyan). From [7].

Recent achievements

To simulate longitudinal beam dynamics, we use the longitudinal macroparticle tracking code BLoND [8, 9]. The code was successfully extended to model multi-turn wakefields in the multiple RF stations per ring. A plot of the longitudinal phase space at injection for RCS1 is displayed in Fig. 4.7(a).

Tracking simulations on the influence of the number of RF stations on the longitudinal emittance and beam stability have been performed for all RCSs. As shown in Fig. 4.7, their minimum number is around 32 RF stations for RCS1 and RCS4, and 24 stations for RCS2 and RCS3 [3]. This allows to

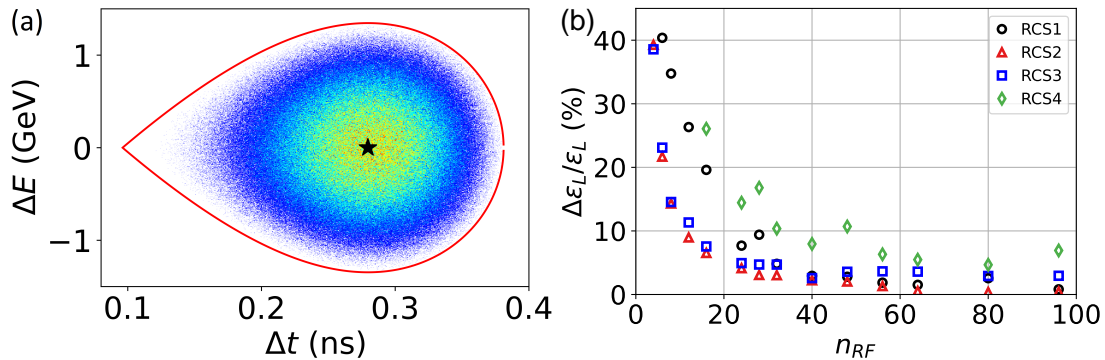


Fig. 4.7: (a) Longitudinal phase space for a μ^+ bunch in RCS1 for $n_{RF} = 32$ at injection. The red line indicates the separatrix (with continuous energy approximation) for $f_{RF} = 1.3$ GHz. (b) Relative emittance growth at the end of the cycle of each RCS with respect to the emittance at injection versus n_{RF} for RCS1 to RCS4 from simulations without intensity effects.

keep the longitudinal emittance growth close to the required 5% level (not taking into account intensity effects nor phase and energy errors at injection).

A first lattice of the RCS2 has been developed with Xsuite [10]. In the current version (see Figure 4.8, the RCS2 consists of 26 arcs. 24 out of the 26 insertions between the arcs host some cavities. The two remaining insertions will be dedicated to injection and extraction. The arc half-cells house three dipoles: two superconducting dipoles (10 T) on the outside, and a pulsed normal conductor with a peak field of 1.8 T in the middle.

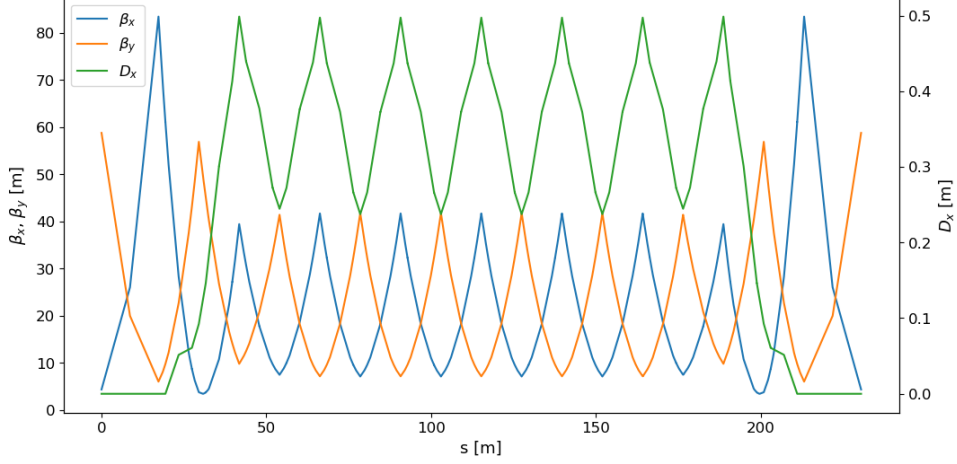


Fig. 4.8: Twiss functions in one out of 26 arcs of RCS2.

Simulations that include the intensity effects of the single but intense muon bunch show the effect of short-range and long-range induced voltages. The short range wakefields, calculated once following the theory of K. Bane [11] and once using a resonator model for all fundamental and higher-order modes of an ILC-like cavity, show induced voltages on the order of 1 MV per meter (and per cavity), i.e., stay below 10% of the cavity voltage without beam. The effect of multi-turn wakefields due to HOMs (higher-order modes) on the longitudinal stability was investigated and the power which is induced into these HOMs was studied as a function of their quality factors [12].

The orbit length variation $\Delta\mathcal{C}$ has been minimized by optimizing the layout of the FODO cells [7] so as to reduce the range of tuning required for the RF cavities and their power sources. With the current design, values reach $\Delta\mathcal{C}/\mathcal{C} \cdot f_{\text{RF}} \approx 2 \text{ kHz}$ in RCS2, resulting in a tuning requirement of $\Delta\mathcal{C}/\mathcal{C} \approx 1.5 \times 10^{-6}$, equivalent to a peak tuning speed of approximately 10 MHz/s.

At this state, giving some tolerances on the magnets and thus $\Delta\mathcal{C}$ becomes very challenging. Due to the fast acceleration, it becomes very difficult to correct any dynamic errors like a jitter on the powering of the magnets. The lattice should enable some passive mitigation of this jitter. The task is even more challenging because it should work also for a counter-propagating beam. A main concern is the eddy currents generated in the pulsed magnets like the normal conducting dipoles.

Planned Work

The longitudinal tracking and RF studies are well advanced for a single beam, but the transient beam loading in the RF cavities due to the counter-rotating beams remains to be investigated. The impact of fundamental and higher-order mode voltages induced in the RF cavities on the longitudinal beam dynamics will be studied in detail. We will not place RF cavities at points where the two opposite sign muon beams cross to prevent the short range wakefield induced in the cavities by one beam from affecting the other one.

The present parameter set for the RCS chain (Table 5.3) has been derived assuming the same muon survival rate for each of the stages. This results in very different requirements for the total RF voltages. While the first RCS must be equipped with almost 21 GV, the RF voltage is smaller for the following

two stages, despite the fact that RCS3 is significantly larger than the first two accelerators. Parameter optimization of the sequence of RCSs, in particular with respect to survival rate and the energy levels at which beam is transferred, will be performed to reduce the overall RF voltage installed in the entire chain and to maintain the same average accelerating gradient through the entire RCS chain.

The required RF voltage for a given transmission is smallest for a perfectly linear energy ramp. This would require that the current driving the pulsed magnets in the RCS varies linearly with time. While a close approximation to this is possible, that would require a very costly power source for the magnet. It would be less costly to drive the magnets with a current pulse that is closer to a portion of a sine wave. However, a nonlinear rise of the field must be compensated by additional RF voltage to reach the same muon survival. First discussions on cost models for the RF system and the bending magnets with their power converter have started, but there are not yet at the level of detail and consistency to allow cost optimization. This effort will continue in 2024, adding also software tools to extract cost estimates.

The work on RCS lattice, started only recently, will be continued and extended to cover the whole RCS chain and possible limitations. Special emphasis will be to ensure a sufficient energy acceptance and a careful evaluation of possible synchro-betatron resonances. The effect of deviations in the magnetic field strength of fast ramping magnets on the beam and possible mitigation method have to be studied. Code development will be pushed to enable start-to-end simulations and integrate the magnetic ramp. Such simulations will give a first estimate of the emittance growth during the acceleration.

Important missing effort

While the RCS injection chain accelerates the bunch to the energy required for the collider ring, its current design does not deliver the longitudinal bunch parameters required. The short bunches required pose tight constraints on the longitudinal emittance growth in the entire RCS chain. Scenarios where the longitudinal bunch parameters for the collider are not achieved during the normal course of acceleration in the final RCS should be designed and simulated (for example, a longitudinal phase space rotation could be performed on the bunch in less than one turn).

Furthermore, the present RF frequency for the muon acceleration of 1.3 GHz has been taken as an assumption, as detailed cavity designs are available for the International Linear Collider (ILC). Although the frequencies around 1.3 GHz are well suited in terms of achievable gradient, further studies considering bucket area, beam loading and wakefields could force to move to a lower RF frequency. Once the suitable frequency range has been fixed, the exact RF frequency remains to be determined based on arguments like the matching in frequency with the muon pre-acceleration and cooling stages.

While the focus has been on the optimization of separate beam dynamics simulations for the transverse and the longitudinal planes, full simulations of the beam dynamics in six dimensions (6D) have yet to be performed and it remains to be clarified which tracking tool is suitable or could be extended to the parameters of the muon RCS chain.

The strong transient beam loading with the high-intensity single bunches also poses challenges to the low-level RF feedback systems. A gated 1-turn delay feedback is being considered, but the conceptual design must be made to estimate its benefit and RF power requirement.

The extremely fast acceleration of muons in RCSs extends the synchrotron concept in uncharted

territory in terms of parameters, which are beyond those of present accelerators. Already the conventional design tools had to be carefully scrutinized and extended to make sure that they remain applicable for the muon RCSs. No existing RCS has a comparable circumference, accelerates similarly fast and with such a large synchrotron tune. In addition the concept of interleaving super- and normal-conducting magnets with its consequences on the orbit length has not yet been demonstrated. The future effort should therefore cover the design study of a moderately-sized hybrid RCS demonstrator to be constructed and commissioned from 2030 to 2033.

We could use existing accelerators to test operation with parameters at least beginning to approach the parameters required for the muon RCSs. For example, synchrotron tunes as large as 0.1 could be tested with ions at injection energy in the CERN SPS, to benchmark the consequences of discretised synchrotron motion. Further beam tests may be possible in the existing RCS at JPARC or the 8 GeV Booster synchrotron at Fermilab, both accelerating proton beams within few 10^4 turns.

4.4 Collider Ring

Present work on the muon collider ring design focuses on a 10 TeV center of mass machine.

4.4.1 Collider Design Overview

The optics design of the collider design comprises:

- The Interaction Regions (IR) with a straight section housing the detector and an inner focusing triplet. This is followed by a longer (almost) straight section possibly with weak bendings and/or quadrupoles. In the present scenario, injection, extraction for beam dumping, RF and other systems will use the straights available in this region.
- A Chromatic Compensation Section (CCS) correcting chromatic aberrations generated due to the small β^* required to achieve sufficient luminosity.
- A Matching Section (MS) connecting the CCS to the arc cells. Present efforts aim at designing an MS with sufficient tuning margin for the betatron phase advances to allow adjustments of the working point.
- The arc will be made of negative momentum compaction cells required to tune the momentum slip factor of the whole collider ring to very small values required to keep the bunches short (≈ 1.5 mm) over about 1000 turns contributing to luminosity.

The following effects related to muon decays have to be mitigated:

- Electrons and positrons lead to showers either by synchrotron radiation generated by them towards the outside of the ring or where they impact on the inside of the ring. Tungsten absorbers installed inside the magnet aperture together with residual heat load and radiation to the magnet are described in section 5.5. The cryogenic system is dimensioned to cope with the residual heat load from muon decays and is described in 5.7.
- Neutrinos leave the ring almost tangential to the design trajectory and reach Earth's surface close to the plane defined by the collider ring with hot spots in the direction of straight sections. Dose levels generated by these muons reaching Earth's surface or rather showers created by them are described in section 5.10. Measures to ensure that dose levels remain at negligible levels are

described and comprise to limit the length of straight sections outside the IR and mechanical system described in section 5.12 to periodically deform the machine in vertical direction.

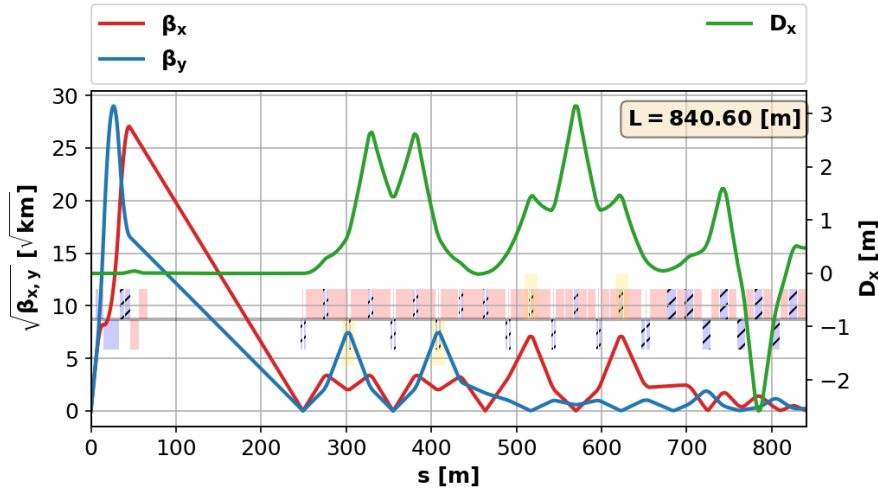


Fig. 4.9: Twiss functions in the collider ring from the IP through the final focusing, the CC section up to the beginning of the matching section.

4.4.2 Key Challenges

A major challenge of the optics design are the chromatic aberrations caused by the small Twiss betatron function at the interaction point $\beta^* = 1.5 \text{ mm}$ and the large rms momentum spread of $\sigma_\delta = 10^{-3}$ together with the high beam rigidity and maximum quadrupole gradients. Twiss parameters in the most challenging part of the muon collider ring are shown in Fig. 4.9. The design of the local CC section to correct these aberrations and, in particular, the control of higher order effects is underway. The small β^* and the large beam rigidity unavoidably leads to large Twiss betatron functions at location of strong magnets around the final focusing structure and, to a lesser extent, in the CC section. A consequence is stringent requirements on unwanted multipolar components to be evaluated once a working lattice for a perfect machine is available. The rms bunch length has to be kept short (rms $\approx 1.5 \text{ mm}$) for about 1000 revolutions contributing to luminosity production. This leads to stringent requirements for the momentum compaction factor including higher order contributions and the need to control the (average) dependence of the path length from the betatron oscillation amplitudes using sextupoles. It has not yet been decided whether a high gradient high frequency RF system will be used to slightly mitigate these constraints.

Pushing the luminosity requires to push the fields of the magnets (see section 5.1) to the maximum possible with existing technologies or, if feasible, to develop new concepts. This is necessary to reduce the machine circumference allowing to increase the number of revolutions contributing to luminosity production and for a compact design of the final focusing structure.

The dose levels, where neutrinos reach Earth's surface, will be kept at negligible levels with the help of mitigation measures as installation of the collider ring deep underground, avoidance of straight sections in regions outside the straights housing the experiments by adding dipolar components to quadrupoles and higher order multipoles (becoming combined function magnets) and wobbling,

i.e. periodic deformation of the ring in the vertical direction as described in section 5.12, of the machine. Challenges are the required high precision movement system and to ensure that adverse effects on the machine optics and performance can be controlled.

Challenges generated by muon decay products (electrons and positrons and synchrotron radiation generated by them) and showers generated by them and their interception by tungsten absorbers is described in 5.5. Challenges due to the heat load from residual shower particles not intercepted by the absorber are described in section 5.7 on the cryogenic system.

The Machine-Detector-Interface (MDI) with tungsten absorbers and nozzles to minimize beam induced background seen by the detector is described in a dedicated section 2.2.

4.4.3 *Work since Roadmap*

Substantial progress has been made on the design of a lattice for a 10 TeV center of mass collider [13]. Despite significant improvements of the transverse acceptance for off-momentum particles, a lattice working for nominal beam parameters is not yet available even for a perfect machine. Nevertheless, relaxing slightly requirements (increasing β^* and the bunch length and decreasing the momentum spread by the same factor) would allow to find such a lattice.

Progress of Beam Induced Backgrounds (BIB) studies and Machine Detector Interface (MDI) design optimizations are described in section 2.2. BIB mitigation strategies elaborated with the collider lattice design are described there.

Progress on studies of radiation at Earth's surface caused by neutrinos generated by muon decays comprise FLUKA studies, an improved "source term" describing radiation from a decaying muon beam without divergence and a procedure to take the properties of the lattice into account. A detailed description is given in section 5.10.

4.4.4 *Work planned for Evaluation Report*

Optimization aiming at designing a lattice with sufficient transverse acceptance over the whole relevant momentum with the nominal β^* will be continued. If no such lattice is identified, parameters may have to be slightly relaxed (increase of β^* and bunch length leading to smaller momentum spread).

Starting with a working lattice for a perfect machine without machine imperfections, realistic scenarios will be investigated. Imperfections to be added comprise component misalignments, magnet strength errors (possibly caused by limited precision of power converters) and unwanted multipolar components of magnets. Initially, a lattice without β^* squeeze will be assumed. Afterwards, correction of imperfections based on observations with the beam will be simulated. As a result of these simulations, specifications for component alignment tolerances, maximum magnet strength uncertainties and maximum unwanted multipolar components will be obtained. In case some of these conditions, e.g., maximum unwanted higher magnetic field multipolar components cannot be met in practice, an optimized lattice design may allow to improve and parameters may have to be relaxed.

The impact of periodic machine deformations to mitigate radiation from neutrinos reaching Earth's surface described in sections 5.10 and 5.12 on beam dynamics will be studied. Machine deformations introduced by design vertical dispersion inside the challenging CC section with large betatron functions and strong sextupoles possibly leading to a substantial impact on the dynamic apertures and

machine performance.

4.4.5 *Missing Effort*

Present studies concentrate on a 10 TeV center of mass collider and no further investigations on a lower energy machine are underway. In case a staged implementation of muon collider facility with a lower energy collider as first stage is envisaged, thorough studies in addition to the existing 3 TeV center of mass muon collider design from MAP [1] are necessary.

Interplay of machine nonlinearities and beam-beam effect have not yet been looked into in detail but drive the design and alignment tolerances to ensure that the expected performance is reached. Further studies on beam-beam effect have to be clarified.

4.5 **Collective Effects**

4.5.1 *System overview*

Collective effects are a general concern over the whole muon collider, from the proton driver to the collider ring. Different mechanisms will dominate the system, depending on the particle's type, their energy, the bunch emittance and intensity.

In the proton system, the high-intensity and medium energy of the proton bunches will make them prone to collective instabilities from space-charge effects and interplay with impedance, in particular in the accumulator and compressor rings. In the muon cooling system, collective effects created by beam-matter interaction in the ionisation cooling system could make the muon bunches unstable or lead to an increase of the emittance. These effects will be investigated as part of muon production and cooling described in Section 4.2. In the muon acceleration system, the two high-intensity, counter-rotating muon and anti-muon bunches will undergo fast acceleration to meet the survival rate goal. The numerous RF cavities required for acceleration will generate strong wakefields that could degrade the bunch emittance and lead to intensity losses. Beam-beam effects will also be present in the droplet arcs of the Recirculating Linacs, at two crossing points in the Rapid Cycling Synchrotrons (RCS) and at the two interaction points in the collider ring. In the latter, the beam chamber will generate resistive-wall wakefields whose magnitude will be determined by the chamber radius and materials used.

4.5.2 *Key challenges*

In the first RCS, an energy gain per turn of 14.7 GeV is required to reach the 90% survival rate of the muon beams. To obtain such large accelerating gradient, $O(700)$ TESLA superconducting RF cavities operating at 1.3 GHz [14] and with an individual accelerating gradient of 30 MV m^{-1} will be needed, as described in Section 4.3. The cavities High-Order Modes (HOMs) will generate short and long-range wakefields. Combined with the high bunch intensities of 2.7×10^{12} , 2.4×10^{12} , 2.2×10^{12} and 2.0×10^{12} muons per bunch at injection of RCS1, RCS2, RCS3 and RCS4 respectively, the strong wakefields could disrupt the beam motion and lead to emittance blow-up and particle losses. Moreover the fast acceleration the two bunches will undergo in the RCS (only 17 turns for RCS1) would require the transverse damper to have a fast response to efficiently mitigate the coherent beam instabilities. Sextupoles magnets could be introduced to correct and control the RCS lattice chromaticity and mitigate potential head-tail instabilities, but this would however require further space in the RCS lattice.

In the 3 TeV and 10 TeV collider rings the beam chamber will generate short-range resistive-wall wakefields. To reach the highest possible magnetic field in the dipole, the magnet aperture should be as small as possible and must host a 4 cm thick tungsten shielding to intercept muon decay products, as described in Section 5.1 and Section 5.5 for the 10 TeV collider. Because of the absence of synchrotron radiation damping mechanism, the transverse normalised beam emittance of $25 \mu\text{m rad}$ must be preserved over the storage time to reach the target luminosity. The inner radius of the tungsten shield and its material properties, such as the operating temperature or the use of a low electrical resistivity coating, will influence the resistive-wall wakefield and determine the coherent stability threshold. At the interaction points, strong beam-beam effects will arise from the high bunch intensity of 1.8×10^{12} muons per bunch at injection and the small β^* target of 1.5 mm. The short bunch length of $\sigma_z = 1.5$ mm could also lead to beam induced heating in some devices. However the strength of collective effects will reduce over the beam storage time in the collider thanks to the muon decay. With a 5 TeV beam, the Lorentz factor $\gamma = 47323$ and the muon lifetime in the laboratory frame τ is $\tau = \gamma\tau_0 = 47323 \cdot 2.2 \mu\text{s} = 104$ ms, equivalent to 3121 turns in the 10 km long ring.

4.5.3 Recent achievements

A transverse impedance model for the RCS1 was created using the PyWIT framework [15], assuming the accelerator comprises 670 superconducting TESLA type RF cavities. The HOMs used are those of the Low Loss type TESLA cavities described in Ref. [16]. The three modes with the largest shunt impedance R_s are reported in Table 4.2. Figure 4.10 shows the real part of the transverse horizontal dipolar beam coupling impedance obtained with this model. The vertical impedance is assumed to be identical to the horizontal one.

Table 4.2: List of transverse HOMs from the Low Loss TESLA cavity, as described in Ref. [16].

Frequency f_{res} [MHz]	Shunt Impedance R_s [$\text{M}\Omega/\text{m}$]	Q factor [10^4]
1927.1	3865.11	1.5
2451.07	6155.63	10.0
2457.04	4314.02	5.0

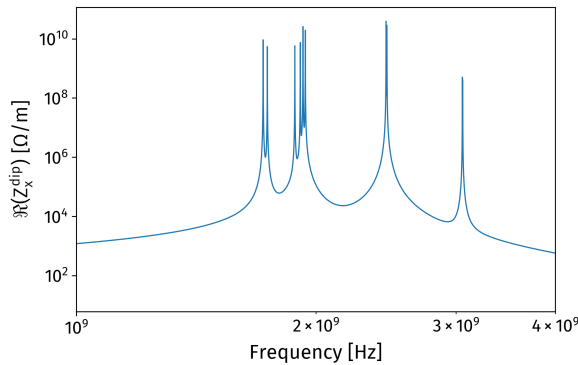


Fig. 4.10: Real part of the horizontal dipolar impedance for the RCS1, including the HOMs created by 670 TESLA type RF cavities. The plot is zoomed on the 1 GHz to 4 GHz range to highlight the HOMs.

Transverse beam dynamics simulations were performed with the PyHEADTAIL [17] macroparticle tracking code. To handle the large acceleration gradient present in the RCS, the RF cavities must be distributed over multiple RF stations along the ring as detailed in Section 4.3. Specific modules were developed to handle in PyHEADTAIL simulations of this particular configuration of the RF cavities [18–20].

A first stability criterion was established through tracking simulations to find the maximum single High-Order Mode shunt impedance R_s , resonance frequency f_{res} and quality factor Q admissible in a cavity. To guarantee single bunch stability with a single HOM, in single-turn wakefield regime $R_s < 100 \text{ M}\Omega \text{ m}^{-1} Q / f_{res}^2$ where f_{res} is expressed in GHz whereas in multi-turn regime $R_s < 10 \text{ T}\Omega \text{ m}^{-1}$. When all the cavity HOMs are included in the impedance model, tracking simulations show that there is a factor 2 margin on the total transverse shunt impedance $R_{s,tot}$ of the modes, assuming that all modes shunt impedance can be summed as we remain in the single-turn wakefield regime.

These simulations were performed assuming that the chromaticity Q' is corrected to zero (i.e. using sextupoles). Assuming the RCS lattice will be a FODO type and an average Twiss beta function of $\bar{\beta}_{x,y} = 50 \text{ m}$, the transverse tunes can be approximated to $Q_{x,y} \approx C_0 / (2\pi\bar{\beta}_{x,y}) = 19$ with $C_0 = 5990 \text{ m}$ the machine circumference. The chromaticity $Q'_{x,y}$ was scanned from -19 to $+19$. With the impedance model pictured in Fig. 4.10, no transverse emittance blow-up was found after 17 turns of acceleration, both with $Q' = -19$ and $Q' = 0$. Applying a factor two on the impedance, a large emittance blow-up appears with $Q' = -19$ and $Q' = +19$. With smaller chromaticity values such as $Q' = -4$ or $Q' = +4$, the transverse blow-up is still present but limited to a few percent. Simulations including a small initial transverse offset of the beam were also started in order to assess the impact of injection errors on transverse coherent stability, scanning the initial horizontal beam offset in the $0.1 \mu\text{m}$ to $1000 \mu\text{m}$ range. A transverse damper located in the second RF station after the injection point would be required to damp the bunch centroid motion. For larger offset such as 1 mm , either the damper strength should be quite strong (in the 4-turn range) or multiple damper units should be used.

In the 10 TeV collider ring, the resistive-wall impedance from the dipole magnets vacuum chambers would be the main source of wakefields. Impedance and beam stability simulation results performed for the 10 TeV collider are described afterwards. Similar studies were also done for the 3 TeV collider and can be found in Ref. [21]. Assuming that the innermost surface seen by the beam is the tungsten shield, impedance models were created for a range of radii between 10 mm and 40 mm . To reduce the chamber impedance, the inner surface of the tungsten shield would be copper-coated. The material temperatures are assumed to be 300 K , as described in Section 5.7. A scan on the copper coating thickness was also performed, from $0.1 \mu\text{m}$ to $100 \mu\text{m}$ to find the minimum thickness required to shield the tungsten material. The impedance models were generated using the ImpedanceWake2D code [22]. The chamber and material parameters used in simulations are reported in Table 4.3. Figure 4.11 shows the transverse dipolar impedance for a 23 mm radius chamber, and for different copper coating thicknesses.

Table 4.3: Chamber parameters used in simulations for the 10 TeV collider.

Chamber length and geometry		10 km, circular	
Copper coating thickness	μm	0.1, 1, 10, 100 + no coating + infinite	
Copper resistivity at 300 K	$\rho_{Cu,300K}$	$\text{n}\Omega \text{ m}$	17.9
Tungsten resistivity at 300 K	$\rho_{W,300K}$	$\text{n}\Omega \text{ m}$	54.4

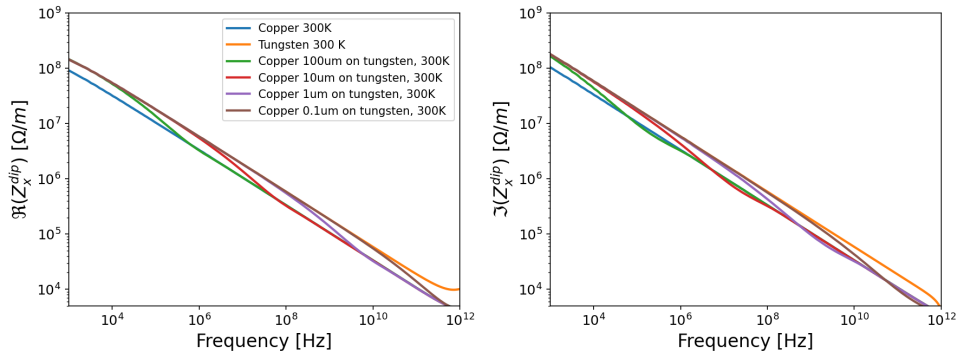


Fig. 4.11: Transverse dipolar impedance for a 23 mm radius tungsten shield in the 10 TeV collider. Left plot shows the real part, right plot the imaginary part. Different copper coating thickness are assumed, and are represented alongside two models assuming an infinite copper thickness (orange curve) or tungsten thickness (blue curve).

Tracking simulations using PyHEADTAIL were performed with these impedance models [20,23]. They allowed to find the minimum chamber radius needed to ensure transverse coherent beam stability, as well as the copper coating thickness that should be used to reduce impedance effects. The muon decay effect has to be included in simulations since the bunch intensity reduction over time will reduce the coherent effects strength. A PyHEADTAIL module was therefore implemented to reproduce this effect in simulations.

Figure 4.12 summarises the results of the tracking simulations. The minimum chamber radius required to keep the beam stable is plotted as a function of the transverse damper strength. Each curve corresponds to a different copper coating thickness. For coating thickness larger than 1 μm , the curves are superimposed on the pure copper case. It shows that a copper coating of at least 1 μm is required to shield the tungsten. Results of simulations showed that if a tungsten chamber with a 10 μm copper coating is used, with a 50-turn transverse damper gain, the minimum chamber radius required is 13 mm, smaller than the 23.5 mm currently assumed for radiation shielding studies.

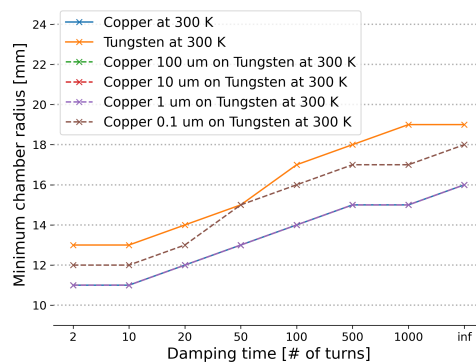


Fig. 4.12: Minimum chamber radius required to keep the emittance growth below 10% after 3000 turns, for the different copper coating thickness considered and pure copper or pure tungsten (no copper coating).

For both RCS and collider rings the impedance models and beam dynamics codes are made available on a dedicated Git repositories and can be found at <https://gitlab.cern.ch/>

[muc-impedance/muc-impedance](#). A web page was also developed to visualise the developed impedance models and is available at <https://muc-impedance.docs.cern.ch/>.

4.5.4 *Planned work*

Impedance models for the RCS2, RCS3 and RCS4 will be created, following the machine parameters reported in Section 5.3. Simple models for the resistive-wall impedance of the RCS are also currently being investigated, in particular for the pulsed magnet chambers. Because of the fast magnet ramping, in the order of $\dot{B} = 4200 \text{ T s}^{-1}$ for the RCS1 for example, ceramic chambers with outer RF shielding stripes such as those used in the J-PARC RCS [24] must be considered. The tracking simulations will be ported to the XSuite [10] framework. This will allow to perform start-to-end tracking simulation in the different RCS as well as in the collider ring, without and with collective effects. The study of the effect of an initial transverse offset of the beam will be refined to better assess the required strength and location of the transverse damper. Beam-beam effects will also be included in simulations performed within this framework.

The tracking simulation framework for the collider ring will also be migrated to XSuite. This will allow to investigate the coherent beam-beam effects in 10 TeV collider, and their possible interplay with impedance effects. Similarly to the RCS studies, the effect of an initial bunch offset at injection will be studied through simulations. The impact on coherent stability of the quasi-isochronicity of the ring caused by the very small momentum compaction factor α_p will also be investigated, as well as the effect of the higher-order momentum compaction factors.

Collective effects studies for the proton driver part will also be started, in association with the Linac, Accumulator and Compressor ring developments exposed in Section 4.1, as well as the collective effects during the ionisation cooling developed in Section 4.2. In particular the effect of space-charge, and its interplay with impedance, on the coherent beam instability thresholds should be investigated.

4.5.5 *Missing efforts*

The transverse tracking simulations for the RCS are for now limited to a simple linear optics model. The development of a detailed lattice model would allow to refine the coherent beam stability simulations in the RCS and ensure through start-to-end simulations the choice of beam parameters for the RCS chain. In particular collective effects in the hybrid synchrotrons, which will see large horizontal beam excursions in certain sections of the ring, could be investigated.

In collaboration with the vacuum and the magnet design teams, the technology options for the RCS normal and super-conducting dipole vacuum chamber should be investigated to have a better estimate of the resistive-wall impedance in the RCS.

In the collider ring, an RF system design should be investigated in collaboration with the lattice design and RF design teams in order to evaluate its impact on the coherent beam stability.

Experimental study of space-charge could be performed in machine development sessions in the CERN PS to investigate beam dynamics effects that could arise in the proton driver Accumulator and Compressor rings. Moreover these sessions could also be used to study coherent beam dynamic effects close to transition for isochronous rings.

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5 Accelerator Technologies

5.1 Magnets

Prior to the IMCC, the US Muon Accelerator Program (MAP) study [1,2] provided the most complete concept of a MuC, including an overview of the magnet requirements. The IMCC has hence taken MAP as a starting point, identified the key magnet challenges and technology options, and evolved the magnet configurations to provide a current set of main magnet performance parameters. These parameters extend the feasible performance space by considering recent advances in superconductor and magnet technology.

Work carried out so far to evolve the MAP configurations has a strong focus on HTS. A driving reason for this are the higher field reaches possible with HTS. But, equally important are considerations of efficient cryogenic operation and helium inventory. Operation in helium gas at temperatures in the range of 10 K to 20 K can provide a coefficient of performance up to a factor four higher than a cryoplant producing liquid helium at 4.2 K. This improved energy efficiency will reduce the impact of energy depositions from muon decay and triggered cascades, which applies throughout the MuC complex, and vital to the sustainability of the accelerator complex.

The sections below describe the magnet systems for the main parts of the MuC complex, namely the muon beam production (target, decay and capture channel), muon cooling, acceleration and collision. We will expand on the concept and magnet engineering, making reference to specific technologies such as Low Temperature Superconductors (LTS, Nb-Ti or Nb₃Sn), High Temperature Superconductors (HTS, mainly considering REBCO) as well as normal conducting (NC) iron dominated magnets. More extensive descriptions can be found in the publications cited. We also bring the attention to the internal review of magnet technology options that was organized during the 2023 IMCC Annual Meeting (<https://indico.cern.ch/event/1250075>), with a final report presented at the Accelerator Design Meeting of 30 October 2023 (<https://indico.cern.ch/event/1337221/>).

5.1.1 Magnet system for muon beam production

System Overview

Muons are produced from the decay of pions generated from the collision of a short, high intensity proton pulse with a target. The target, varying in outer diameter dimensions from 150 mm to 250 mm depending on technology, is placed within a steady-state, high field “target solenoid”, whose purpose is to capture and guide pions into a “decay and capture channel”, also embedded in solenoid magnets. An approximately 18 m long magnetic field profile from the target to the end of the capture channel enables the capture of pions and has a characteristic shape with a peak field of 20 T on the target and an adiabatic decay to roughly 2 T at the exit of the channel [3].

To prevent heating and radiation damage from the interaction of the multi-MW proton beam with the target, a radiation shield is necessary for the target, decay, and capture solenoids. This shield comprises a combination of a dense metal such as tungsten (to intercept highly energetic photons generated by the decay electrons) and a moderator like water (to reduce neutron fluence). The shield thickness dictates the magnet bore and is chosen to reduce to acceptable levels the radiation damage and heat load on the solenoid coils and surrounding infrastructure. Calculations show that with a shield approximately 500 mm thick, radiation induced heating in the coils would fall within the range of 5 kW, local radiation

dose in the range of 80 MGy, and a yearly peak DPA in the range of 10^{-3} . These values, and especially the radiation damage, are at the limit of present magnet technology, thus setting a minimum magnet bore dimension of 1200 mm used for the design of the target, decay and capture solenoids. A larger bore dimension implies higher stored magnetic energy, influencing electromagnetic forces, magnet protection, and cost.

To achieve the peak 20 T field profile at the target, MAP considered a hybrid normal conducting (NC) and superconducting (SC) target solenoid configuration, consisting of a rad-hard resistive NC insert (approximately 5 T with a 150 mm bore), within a large bore Low Temperature Superconducting (LTS) magnet (approximately 15 T with a 2400 mm bore) [4–6]. While this concept remains a possibility and can be built based on the extrapolation of known technology, the system’s stored energy (approximately 3 GJ), coil mass (about 200 tons), and wall-plug power consumption (around 12 MW, dominated by the resistive insert) are substantial.

Key Challenges

The main challenge in our proposed design (see below) is radiation damage of the superconductor and insulation, both requiring further analysis and measurements, and especially advances in understanding the damage mechanism in HTS. Other challenges include magnet engineering (field performance, mechanics, stored energy and protection) and infrastructure and operating cost (power and cooling), including integration/maintenance in a high-radiation environment. These challenges appear manageable, and overlap broadly with those of magnets for high magnetic field science (e.g. user facilities based on hybrid SC and NC solenoids and all-SC solenoids), as well as magnets for fusion devices (e.g. the central solenoid magnets for a Tokamak) [7].

Recent Achievements

Following recent advancements in HTS magnets for fusion [8], we have proposed an alternative design involving an HTS cable operating at 20 K. The cable considered is shown in Fig. 5.1, an internally cooled conductor inspired by the VIPER developed at MIT [9]. The analysis performed thus far indicates the potential to eliminate the resistive insert, thus reducing the magnet bore to the minimum of 1200 mm, roughly half the size of the US-MAP LTS coil, while still maintaining the desired field profile for efficient muon capture. If compared to LTS, operating at a temperature higher than liquid helium diminishes the need for radiation heat shielding and maintains good overall energy efficiency. The proposed system is shown schematically in Fig. 5.2. It has a stored energy of ~ 1 GJ, a coil mass of around 100 tons, and a wall-plug power consumption of approximately 1 MW. This represents a significant reduction compared to the previously suggested hybrid solution from the MAP study. Our future focus will be on identifying specific HTS conductor and winding technologies suitable for magnets of this class. The details of the electro-magnetic and mechanical design can be found in ref. [10], while the cooling and quench analysis can be found in ref. [11].

Planned Work

After completing a first iteration on the electro-magnetic, mechanic, cooling and quench protection designs, we plan now to iterate on the free bore to resolve known mechanical interference with target and shield, and mitigate radiation heat load and damage. Alternative cable designs and coil geometries are

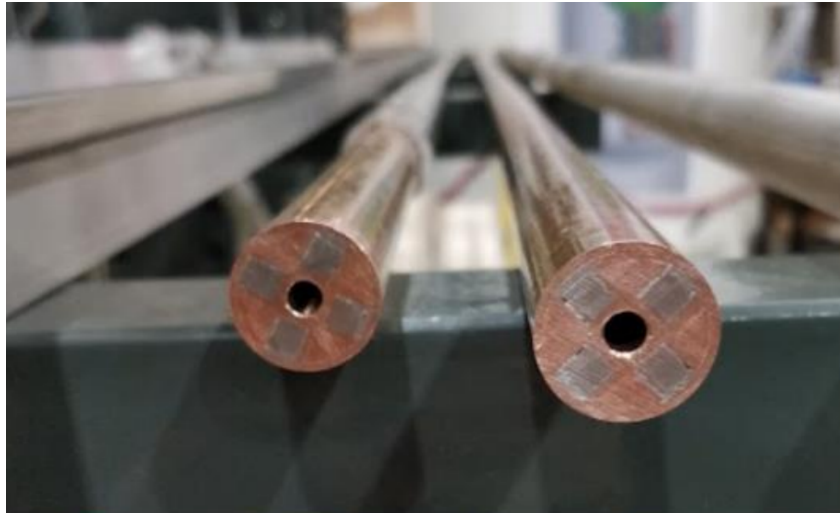


Fig. 5.1: MIT VIPER cable, image taken from ref. [9].

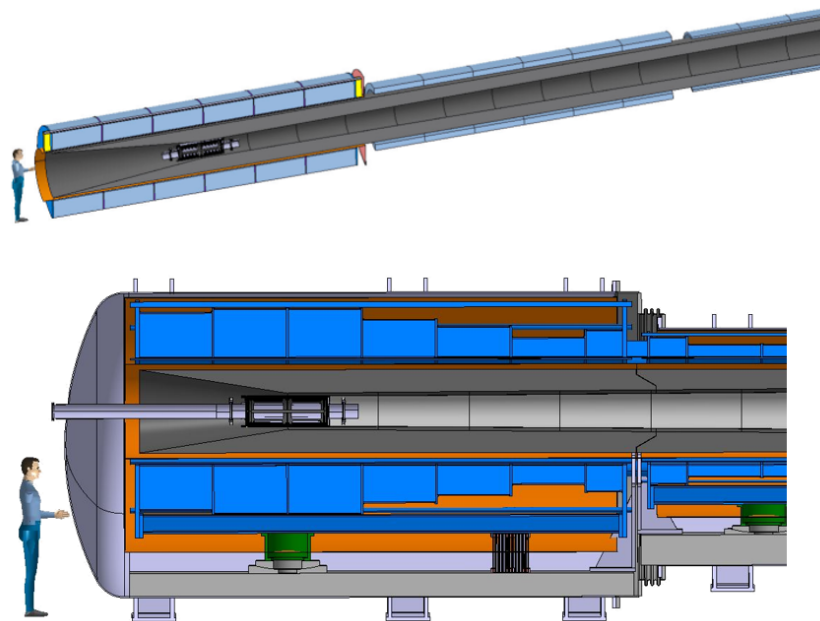


Fig. 5.2: Schematic view of the HTS target, decay and capture channel proposed (top), with a detail of the high field solenoids around the proton target area (bottom).

being considered, to see whether a better cost optimum can be found. We will then integrate the design in an engineering concept, including considerations of manufacturing, installation and maintenance. This effort can be completed within the planned timeline. It will then be important to plan for technology demonstrators, from cable to coil, including testing efforts. Given the size of this magnet, this work will require considerable material and personnel investment.

Important Missing Effort

Besides the technology demonstrators already quoted earlier, the most crucial missing effort is the characterization and understanding of radiation damage in HTS. This is a recent field of research, data is scarce and we still lack a sound understanding of the mechanism by which particle radiation induces

degradation of the critical properties of the superconductor. Such understanding is mandatory to extrapolate measurements to the conditions experienced by the magnets in a MuC, and thus reliably predict the lifetime.

5.1.2 Magnet system for muon cooling

System Overview

Muons exiting the target, decay and capture channel have a large spatial and energy spread, and thus must be cooled in both dimensions to reach values suitable for a collider. This 6D “beam cooling” process occurs over a long (almost 1 km) sequence of tightly integrated absorbers (consisting of light elements such as hydrogen), solenoids, and RF cavities. The solenoids create a broadly increasing oscillating magnetic field in the beam direction, that when combined with absorbers and re-acceleration (RF cavities), cools the beam in the six dimensions of the beam phase space (position and momentum). The final emittance of the muon beam is inversely proportional to the strength of the final cooling solenoids. To achieve maximum cooling efficiency and minimize the emittance there is hence a clear interest in very high field final cooling solenoids.

The MAP design study provided a baseline of magnets (geometry and number) over the entire cooling chain (up to the final cooling solenoids) which could produce the desired on-axis field profile [12]. However, it is important to note that these solenoids were created purely to best fit a desired field profile, rather than from a magnet engineering point of view, and therefore present un-optimized parameters (stresses, forces, volume of conductor) which pose significant challenges. In the MAP version, in total there are approximately 2400 solenoids in cooling channels of approximate 1 km length (excluding the final cooling), which are divided into a total of 826 cooling cells. There are 12 types of cooling cells (labeled A1 to A4, B1 to B8) composed of an absorber, one or two RF modules, and two, four or six solenoids in split pairs (depending on cell type).

For the final cooling solenoids, the MAP scheme consisted of 17 solenoids with a bore field up to 30 T. With this field, an emittance of about 50 μm , roughly a factor of two greater than the transverse emittance goal (25 μm), can be achieved [12, 13]. However, other analyses [14] show that higher fields (in the range of 50 T) offer further gains in the final emittance and beam brightness.

Key Challenges

As detailed in the next section, individual solenoids and cells based on the MAP configuration pose challenges in terms of peak fields, high forces and stresses, and quench management. The range of specifications is however within what can be manufactured already with present technology. Indeed, it is rather the integration of solenoids within a cell containing RF cavities and absorbers, as well as in a series (where the field of one cell affects neighboring ones), which poses the primary difficulty in this aspect of the overall MuC. Furthermore, the large number of solenoids in the 6D cooling section will require standardization and effective industrialization.

For the final cooling, in the scope of improving upon the design by the US-MAP study, the fundamental challenge will be developing ultra high-field solenoids (as explained in the next section) with magnetic fields reaching beyond the current state of the art, more than 40 T in a 50 mm bore. The number of these solenoids, which are nearly free standing, is limited. We hence expect that in this case

it will be the peak field that will pose the main challenge.

Recent Achievements

Starting from the MAP baseline, the first step has been to characterize the parameters of all of the solenoids during operation, as shown in Table 5.1.

Cell	J_E (A/mm ²)	B_{peak} (T)	E_{Mag} (MJ)	e_{Mag} (MJ/m ³)	σ_{Hoop} (MPa)	σ_{Radial} (MPa)
A1	63.25	4.1	5.4	20.5	34	-4.6/0.0
A2	126.6	9.5	15.4	76.3	137	-28.3/0.0
A3	165	9.4	7.2	72.8	138	-28.5/0.0
A4	195	11.6	8.4	91.5	196	-49.4/0.0
B1	69.8	6.9	44.5	55.9	95	-13.5/0.0
B2	90	8.4	24.1	61.8	114	-20.1/0.0
B3	123	11.2	29.8	88.1	174	-36.6/0.0
B4	94	9.2	24.4	42.4	231	-23.5/19.7
B5	168	13.9	12	86.3	336	-55.7/21.1
B6	185	14.2	8.2	68.3	314	-43.1/22.3
B7	198	14.3	5.7	59.6	244	-37.4/20.7
B8	220	15.1	1.4	20.3	119	-22.9/22.1

Table 5.1: Summary of main cooling solenoid characteristics for the 6D cooling cells of a Muon Collider, based on the US-MAP configuration. For a given cell type, B_{peak} is the peak on axis field, σ_{Hoop} is the maximum hoop stress seen by a solenoid, and σ_{Radial} shows the minimum/maximum radial hoop stress seen by a solenoid.

The solenoids from the MAP optics exhibit a diverse range of parameters, from large-bore variants with a diameter exceeding 1.5 m and a modest on-axis field of 2.6 T, to smaller-bore with a 90 mm diameter and a high on-axis field of 13.6 T. This diversity features substantial stored magnetic energy (up to 44 MJ in the single cell B1), notable associated stresses (hoop stress up to 300 MPa and radial tensile stress reaching 20 MPa in cells B5 and B6), and quench management challenges (energy density approaching 100 MJ/m³ of a coil in cell A4).

While the MAP study provides a baseline, the magnets were created from a beam physics point of view (find solenoid geometries which best fit a desired on-axis field) rather than from a magnet engineering point of view. This is evident in Table 5.1, i.e. large volumes of conductor (and therefore larger cost) are paired with lower current density, when larger current densities/lower volumes can be considered. Therefore, significant work has gone into creating an optimization program to revise the coil configurations to address identified challenges while fitting the desired on-axis field to within some error percentage. This is currently a work in progress, and will incorporate advancements from beam optics studies.

For the final cooling solenoids, to improve upon the results obtained by the US-MAP study, we are considering a solenoid design with the potential to reach and exceed 40 T, a clear bore of 50 mm, a magnet length of 500 mm, and compact enough in size to reduce overall footprint, mass, and cost. See Fig. 5.3. We are studying in particular a non-insulated HTS winding solution, where the cooling solenoid is built as a stack of soft-soldered pancakes. To reduce the coil size, forces, and stored energy, and meet

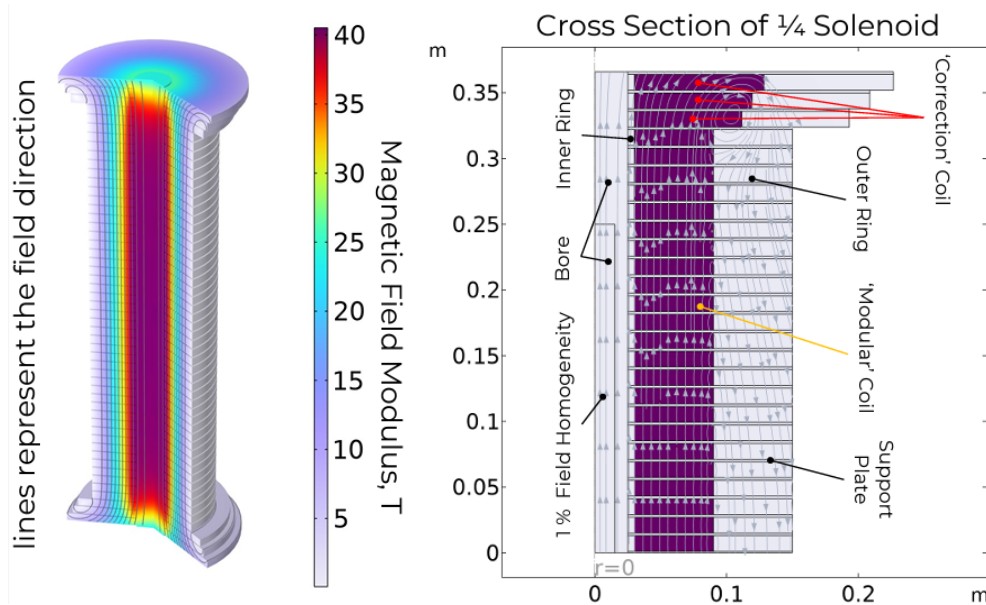


Fig. 5.3: The current 40 T and beyond conceptual design for the final cooling solenoids. It consists of 46 identical 'modular' and six 'correction' pancakes, with a bore aperture of 50 mm. Figures courtesy of B. Bordini.

the field target, the operating current density target is high, 650 A/mm^2 . The coil size is exceptionally small, with a 180 mm outer diameter.

Two critical parameters were identified in the conceptual design phase of a final cooling solenoid, the stress state and the selection and control of the transverse resistance which must be a good balance between the required ramp-rate and quench management. The mechanics design features a maximum hoop stress of 650 MPa, ensuring no tensile stress under any operating condition. To achieve this, the wound and soldered pancakes undergo radial loading from a rigid external ring, providing a radial pre-compression of 200 MPa at room temperature. This radial pre-compression is carefully chosen to nearly offset the outward electromagnetic stress at 40 T, a field range identified as the stress limit for a single pancake. Beyond this point, higher fields would necessitate segmenting the coil into concentric layers with independent support, introducing added complexity and size.

Efforts are underway to address the transverse resistance, with ongoing work focused on reducing values typically associated with soldering tapes. Given that most current transfer in REBCO tapes occurs through the copper coating on the tape sides, it has been observed that minimizing or eliminating this copper component significantly enhances transverse resistance [15]. Our objective is to achieve protection through a low transverse resistance (potentially with mechanisms to actively trigger a quench), while still enabling a full ramp in less than six hours and maintaining field stability at a flat-top better than 10 pm/s. Further details on the concept, design studies, and recent advancements are available in ref. [15].

Planned Work

For the evaluation of the MAP baseline 6D cooling solenoids, one important aspect is ongoing - the quench protection analysis. In parallel, optimization and revision of all magnets from an engineering perspective (stress, cost, protection, etc.) as mentioned above is underway. Tight collaboration with

beam physicists is necessary to incorporate new magnet configurations to fit evolving on-axis field profiles. Specific manufacturing options will be explored, and the possibility of standardization will also be considered to manage the substantial number of solenoids slated for construction.

The final cooling solenoid is a case by itself. Besides the design and analysis work, which will include multi-physics evaluation of electrical, magnetic (screening currents), mechanical and thermal (quench) performance, we have initiated supporting experimental activity. Tests are planned on HTS tapes and pancakes to provide an experimental basis for the electro-mechanical performance limits (stress and strain, as well as in-field measurement of delamination) and prove the feasibility of concepts. Stacks and windings are being manufactured to establish mechanical properties, and eventually perform tests in field to probe performance in the range of 20 T to 40 T.

Important Missing Effort

The cryogenic cooling system needs to be defined both in concept, as well as in practical engineering solutions. For various reasons, such as paramagnetic effects on helium, cooling by a bath of helium is not practical. Direct and indirect cooling need to be considered to find the optimal baseline. A second matter that will require attention is to explore manufacturing routes for the large number of solenoids needed by the cooling channel. Finally, a full-size demonstration of a 6D cooling cell integration, as well as the final cooling solenoid, will be required to validate the designs.

5.1.3 Magnet system for muon acceleration to TeV energies

System Overview

To extend their lifetime in the laboratory reference frame, the muons must be accelerated rapidly to relativistic momentum. The acceleration begins with an initial linear accelerator and sequence of recirculating linear accelerators followed by a sequence of rapid-cycling synchrotron (RCS) and hybrid cycling synchrotrons (HCS) [16, 17]. The RCS employs fast-ramped normal conducting (NC) magnets, swinging from an injection to an extraction field level. In a HCS, static superconducting (SC) magnets establish a field offset, while NC fast-ramping magnets are powered from peak negative to peak positive field, enabling a full field swing. This design results in a more compact accelerator compared to an equivalent RCS.

Design concepts of NC fast-ramped magnets with a peak operating field of 1.5 T were developed by US-MAP [18]. SC dipoles for HCS were not studied in depth, besides setting target value for bore field and magnet length.

In the current IMCC baseline configuration, the NC dipoles in the initial RCS need to sweep from 0.36 T to 1.8 T within 0.35 ms (equating to a rate of 4 kT/s). In the concluding HCS, the dipoles sweep from -1.8 T to 1.8 T in 6.37 ms (equating to a rate of approximately 560 T/s). Studies are ongoing to evaluate the possibility of realizing the final slower HCS pulsating magnets with HTS REBCO based tapes and ferric core. The SC dipoles in the first two HCS have a nominal field of 10 T, while in the final HCS the assumption is of 16 T field. All dipole magnets, NC and SC, have a rectangular nominal aperture of 30 mm (vertical) x 100 mm (horizontal).

Key Challenges

Beyond magnet engineering, a fundamental challenge in constructing an accelerator ring of the required dimensions is the substantial stored energy, reaching several tens of MJ. Efficiently powering at a high-pulse rate with effective energy recovery between pulses necessitates expertise in managing peak power in the range of tens of GW. Resonant circuits combined with energy storage systems appear to be the only viable solution. This is described in detail in the next section, devoted to power converters.

A second challenge will be mitigating the losses originating from the iron hysteresis, eddy currents in the lamination and coils, as well as any other metallic component exposed to field changes. For example, the vacuum chamber is inserted into a gap where the $\frac{dB}{dt}$ is of the order of few thousands of Tesla per second. Standard metallic vacuum chambers cannot be used, as the induced losses would be not sustainable leading to severe overheating or, in the worst case, melting of the chamber. Alternative concepts are needed to reduce the impact of these losses.

Recent Achievements

As noted in the previous section, the primary challenge of the RCS and HCS magnets lies in effectively managing the multi-GW power necessary to pulse them while maintaining precise control of the field ramp shape, homogeneity, and maximizing energy efficiency. The power required for pulsing, given a specified ramp time and shape dictated by beam design and RF limitations, is directly proportional to the magnetic energy stored in the ramped magnets. A lower bound for stored energy is the magnetic energy within the beam aperture, nominally defined as 30 mm (gap) x 100 mm (width). To limit saturation, which can impact losses and field quality, an upper design field limit of 1.8 T has been set for the resistive magnets. This corresponds to a magnetic energy of 3.9 kJ/m in the beam aperture, with the energy stored in the magnet being higher. Analysis of various resistive magnet configurations, considering different iron cross-sections, materials, coil designs, and current densities, indicates that the lowest magnet stored energy is in the range of 5.4 kJ/m, representing a 1.4-fold increase compared to the magnetic energy in the beam aperture [19].

The present strategy is to realize the dipoles as single turn magnets without return connections and let the power converters connect the ends and starts for the coils from subsequent magnets (see section on power converters). Two type of conductors are analysed, either flat bars cooled at the ends or hollow direct cooled conductors.

A secondary concern involves the magnitude of resistive, eddy current, and hysteresis losses — power drawn from the grid and dissipated. Although a definitive target has not been established, a suitable range is considered to be 200 to 500 J/m per pulse. After analyzing multiple configurations, it has been determined that the best compromise between stored energy, losses, and field quality is achieved with "H" and "Hourglass" shaped iron cores [18]. These configurations will be used in further magnetic analysis, including 3D and end effects. It is important to note that the design of the power converter is intricately linked with magnet design and analysis, aiming for an optimal cost solution (CAPEX+OPEX), while considering beam dynamics and RF. The exploration of various powering configurations has given way to identifying two main cost drivers: capacitor-based energy storage and the active power converters necessary for controlling ramp linearity and reproducibility.

Finally, the steady state SC dipole magnets of the HCS's are only in the early stages of develop-

ment. While specification of these magnets is still an active discussion, it is accepted that the aperture will be similar to that of the pulsed resistive magnets, i.e. 30 mm x 100 mm rectangular, necessitating non-conventional windings. Rejecting the cos-theta coil geometry due to its inefficiency for a rectangular aperture, we have shifted our conceptual focus toward flat racetrack coils. These coils are simpler and more suitable for winding HTS tapes. It appears feasible to achieve a target magnetic field of around 10 T while operating at temperatures significantly above liquid helium (10 to 20 K) in case HTS is used. This approach would be highly advantageous to help with operating margin and efficiency requirements in HCS's, which tend to experience higher beam losses and operational challenges.

Planned Work

Further detailed magnetic analysis, including 3D and end effects, of the possible NC magnet configurations (“H” and “Hourglass” shaped iron cores) is ongoing. This will lead to a final optimized design. Tests are planned on soft magnetic steel in a range of frequency centered around 1 kHz, and field up to saturation, where the experimental database is sparse. These tests will provide input for the NC magnet design.

An initial design study of magnet configurations and parameters of the SC dipole magnets is underway, with 2D and 3D analysis. This study combined with consideration of more complex geometries, quench protection analysis, and engineering (mechanics, cryogenics, etc.) will provide the basis for selecting the most suitable configuration.

Important Missing Effort

Besides the design and analysis work, and the limited experimental activity, also in the case of the fast pulsed accelerators the program would need a validation of the integrated system made of magnet and power converter. Given the modular nature of the design, one such test could be performed on a single powering cell. The configuration for this test is not yet defined, but as a minimum it should consist of NC dipoles and power converters, including the energy storage units. Such a set-up would allow measurement with accurate field tracking, including field quality, losses, as well as overall efficiency of powering and energy storage.

5.1.4 Magnet system for muon collision

System Overview

The final stage of the muon accelerator complex is the collider ring, where two counter-rotating bunched beams of positive and negative muons collide. A critical design parameter for the collider ring is to maximize collisions of stored muon beams in their limited lifetime. This is achieved by minimizing the collider ring circumference [20], translating into a requirement of the highest possible field in the arc dipoles. At the same time, luminosity depends critically on the strength and aperture of the quadrupoles in the Interaction Region (IR). In fact, not only high gradients and aperture are important for luminosity, but also a short IR length reduces the cumulative neutrino flux generated by muon decays in the straight sections around the experiments and reduces chromatic aberrations. Effective radiation shielding is essential to protect against substantial radiation and heat loads generated by muon decay and collisions. To give representative figures, the heat load originating from muon decay (electrons) and synchrotron

radiation in the arc, initially at 500 W/m at the level of the beam chamber, is reduced to below 5 W/m at the level of the coil, with a radiation dose below 40 MGy, by inserting a 40 mm thick tungsten shield. The need of thick shielding results in exceptional demands on magnet aperture [21, 22].

Assumptions in the present study of the 10 TeV collider optics include the generation of a steady-state magnetic field up to 16 T within a 160 mm aperture by the main arc magnets. To minimize straight sections and address effects from the high neutrino flux, these arc magnets are assumed to serve combined functions (e.g., dipole/quadrupole and dipole/sextupole) [20]. The latest optics necessitate dipole fields in the range of 10 T and gradients of the order of 300 T/m. While these field requirements combined with aperture constraints are part of an initial assessment, they currently exceed practical limits and will necessitate iteration. As for the IR quadrupole magnets, the assumption from optics studies is a peak field of 20 T, also associated with large apertures, up to 300 mm.

It should be noted that the US-MAP study investigated a reduced collider energy of 3 TeV, which could stand as a fast-track option leveraging Nb₃Sn technology nearing demonstration.

Key Challenges

As detailed in the next section, the present optics demands high field and large bore combined function arc and IR magnets. While this study is evolving and practical limits being developed for these magnets, they must be designed to withstand large stresses (mechanics), with large stored energy (quench), and deal with significant energy deposition and radiation dose from muon beam decay and interaction debris.

Recent Achievements

To advance the study, specifying the performance limits of accelerator dipole and quadrupole magnets is crucial. We have initiated this effort through analytical evaluations of operating margin, peak stress, hot-spot temperature, and magnet cost, assuming a sector coil geometry [23]. While the results are specific to this coil, extending them to other coil geometries is possible and would not significantly alter the main outcomes.

The analytical evaluation was utilized to create design charts with maximum magnet aperture (A) versus bore field (B) (see Fig. 5.4), a format convenient for iteration with the beam optics. These A-B charts were generated for various superconductors and operating points, including Nb-Ti at 1.9 K, Nb₃Sn at 4.5 K, and REBCO at either 4.5 K or 20 K. For a 10 TeV collider, Nb-Ti at 1.9 K appears sub-optimal due to a low operating margin (considering the substantial energy deposition), cryoplant efficiency, and energy consumption concerns. Similarly, Nb₃Sn at 4.5 K falls short of the required field performance for arc magnets, providing feasible solutions only up to 14 T, being limited by mechanics when considering the necessary 160 mm aperture. Our initial evaluation of REBCO indicates that also in this case the available design space does not meet the required performance. However, for REBCO, operating margin is not a concern, and operation in the range of 10 K to 20 K could be considered. The main limitations for REBCO arise from the cost of the superconductor and quench protection. Cost considerations drive the current density in an all-HTS coil toward high values where standard detect-and-dump protection strategies are not sufficiently fast. Therefore, alternative protection schemes need to be devised to leverage the large current carrying capacity and margin of present REBCO conductors. Assuming a reduction in the cost per meter of REBCO tape by a factor of three to four, and relaxing the

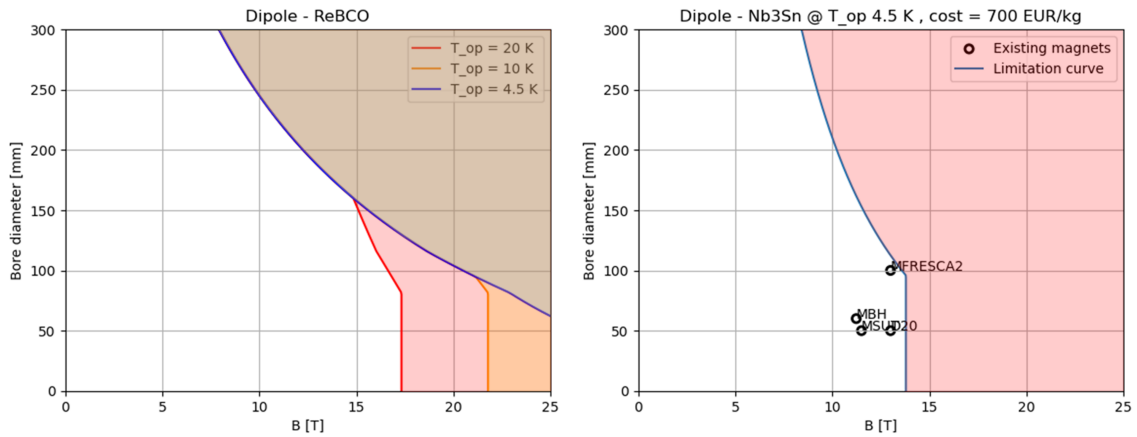


Fig. 5.4: Dipole limitation curves as a function of stress, protection, and margin shown against bore diameter vs. magnetic field for different conductor material and temperature. Left: ReBCO at different operating temperatures (Top), assuming an aspirational cost of 2500 EUR/Kg, a peak stress of 300 MPa, and a hot spot temperature of 200 K. For example, the red line represents the limit assuming an operating temperature of 20 K plus 2.5 K margin. Right: Nb₃Sn at 4.5 K, assuming an aspirational cost of 700 EUR/Kg, a peak stress of 150 MPa, and a hot spot temperature of 350 K. Plots are advanced versions from ref. [23].

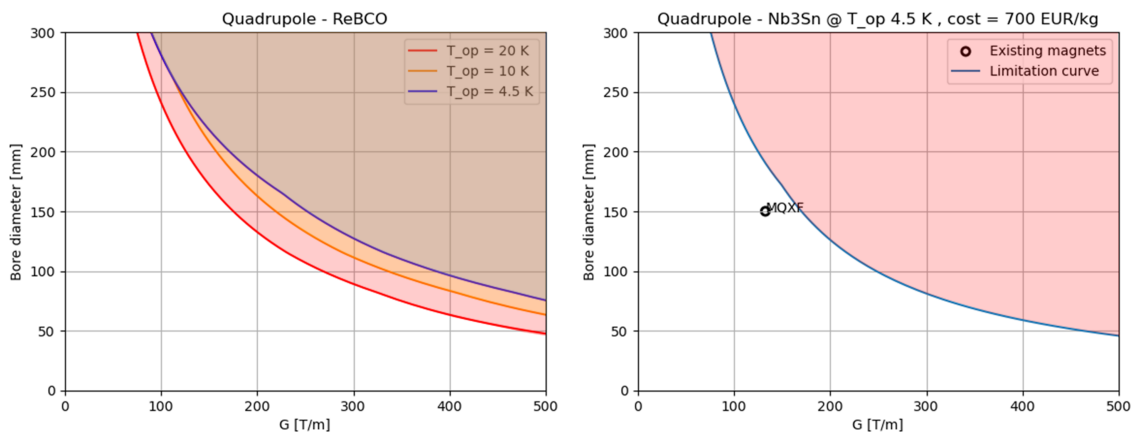


Fig. 5.5: Limitation curves as a function of stress and margin shown against bore diameter vs. magnetic field gradient of collider quadrupoles consisting of ReBCO at different operating temperatures (left) or Nb₃Sn at 4.5 K (right). This is a current work in progress, with final design targets still being decided and protection limits created. Plots courtesy of D. Novelli.

need for very high values of current density, a suitable design range for the arc magnets can be defined. This range spans from a nominal aperture of 160 mm at a reduced bore field of 12 T to a nominal bore field of 16 T but with a reduced aperture of 100 mm. The entire range can be achieved with REBCO at 4.5 K and 20 K, while the low field range can also be reached with Nb₃Sn at 4.5 K, providing at least two technology options.

The analysis for quadrupoles, using the same method outlined above and in [23], is presently in progress (see Fig. 5.5). The range of feasible designs in this case covers gradients of 300 T/m, with an aperture of 100 mm, down to gradients of 100 T/m, and aperture of 250 mm. This is only marginally short of the present requirements for the IR optics, which indicates that the arc dipoles are actually the most demanding magnets.

Planned Work

We will pursue the analysis of quadrupole performance limits (for the design of the interaction regions) and combined function magnets, necessitated by neutrino flux mitigation. We plan to finalize the "A-B" charts for the Superconducting (SC) dipoles and quadrupoles in the collider, incorporating an assessment of the feasible range of combined function gradient versus dipole strength. The main difficulty will be to extend the analysis to combined function magnets. We will most likely need to resort on parametric Finite Element Analysis (FEA) for this.

Following an iteration on the beam optics, we will then advance to the examination of engineering designs for the collider arc dipole and combined function magnets. This study will encompass stress management strategies aimed at enhancing robustness and compensating for inevitable stress peaking factors. Additionally, it will be of interest to explore a fast-track line for a reduced collider energy, specifically in the range of 3 TeV, as investigated by US-MAP, leveraging the Nb₃Sn technology nearing demonstration.

Important Missing Effort

The engineering design of the arc and IR magnets would require a considerable amount of personnel resources, well beyond what is presently allocated in the study. Although we will focus on the most challenging elements (arc dipoles and IR quadrupoles), other magnets may need due attention. One striking example is the Nb₃Sn option that could be used to fast-track the construction of a first collider at 3 TeV. This design is presently beyond the foreseen scope.

As noted in Sec. 5.1.1, the effect of radiation on HTS can be an issue. The radiation effects of the harsh and unique environment of a Muon Collider cannot be reproduced and tested in an existing installation, thus an evaluation of material response will need an understanding and scaling of existing and future data. For this specific issue we plan to rely on advances in material characterization for magnetically confined fusion.

5.2 Power Converters for the muon acceleration to TeV energies*System Overview*

The quick acceleration times can only be achieved with considerable electric power provided by the power converter. The fast $\frac{dB}{dt}$ also carries huge voltages with it. In order to deal with both huge power and voltages (5.2), the power converters of the RCS are based on resonant circuits and must be divided into several series/parallel connected power cells. A power cell is the basic power converter block. Many such power cells are connected to power one sector of the accelerator. One sector is formed by series of connected magnets, i.e. with the same current flowing through. The RCS is divided into a given number of sectors, each supplied by an independent power converter. Inside one Sector, the power cells can be connected in Cell-Load cascade or Unified Cell to load connection mode, as illustrated in Fig. 5.6. The magnets and power converters will need to be designed such that they possess the same number of independent circuits and series connected power cells and magnets. Figure 5.6 shows the case of one sector with four separated magnets each possessing four independent circuits and four series connected power cells per circuit.

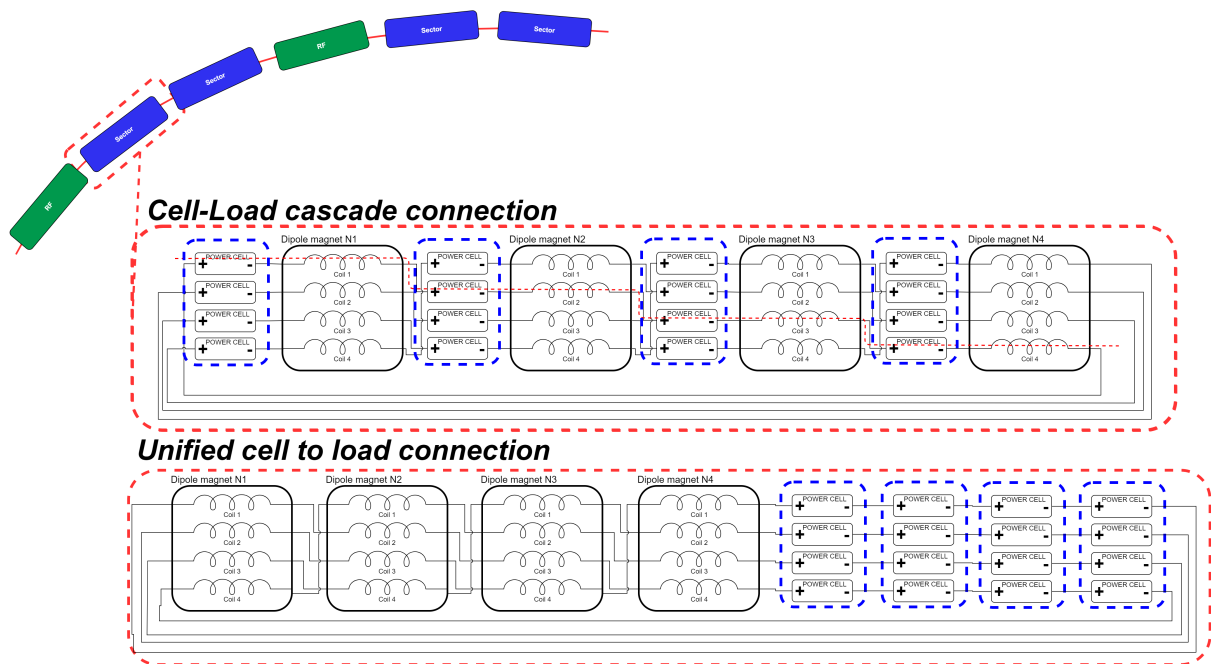


Fig. 5.6: Connection of the power cells with the magnets.

The choice of the connection depends upon the voltage insulation level of the magnets and the location of the power cells. The Cell-Load cascade connection allows a much smaller voltage insulation to ground but only makes sense if the power cells are located close to the magnets i.e. in the tunnel. The Unified cell to load alternative, has higher insulation requirements but power cells can be installed on the surface without having too much cable routing.

The power cell design is based on a discontinued resonance approach where the energy is stored in one or more capacitor banks and then discharged on the magnets with a combination of several semiconductor switches. Two different topologies have been identified and are shown in Fig. 5.7. In both cases, the LC resonance starts by bringing the current (Field) on the negative polarity at the injection and continues the oscillation towards positive values during the real particle acceleration phase. It then returns back to zero where the resonance is actively stopped by the semiconductor switch. Capacitors are then recharged to the initial value and the power converter waits to be restarted for the next pulse. The concept is illustrated in Fig. 5.8.

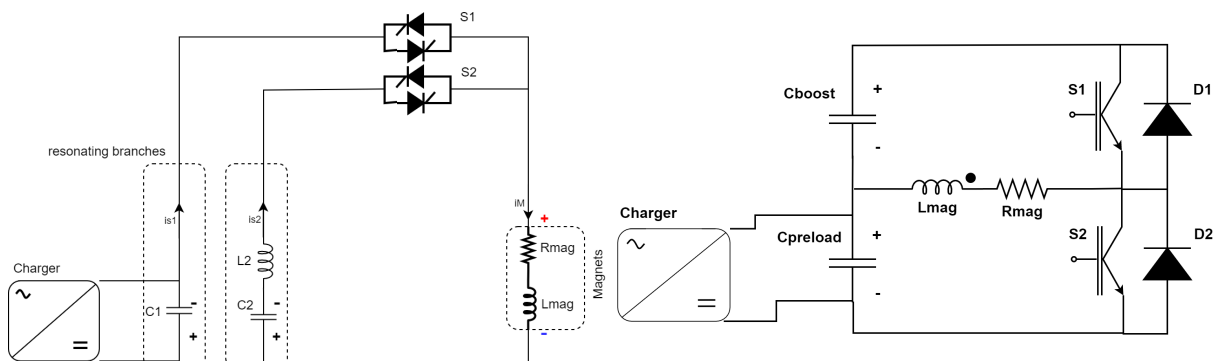


Fig. 5.7: Full wave (left) and switched (right) discontinued resonance principles

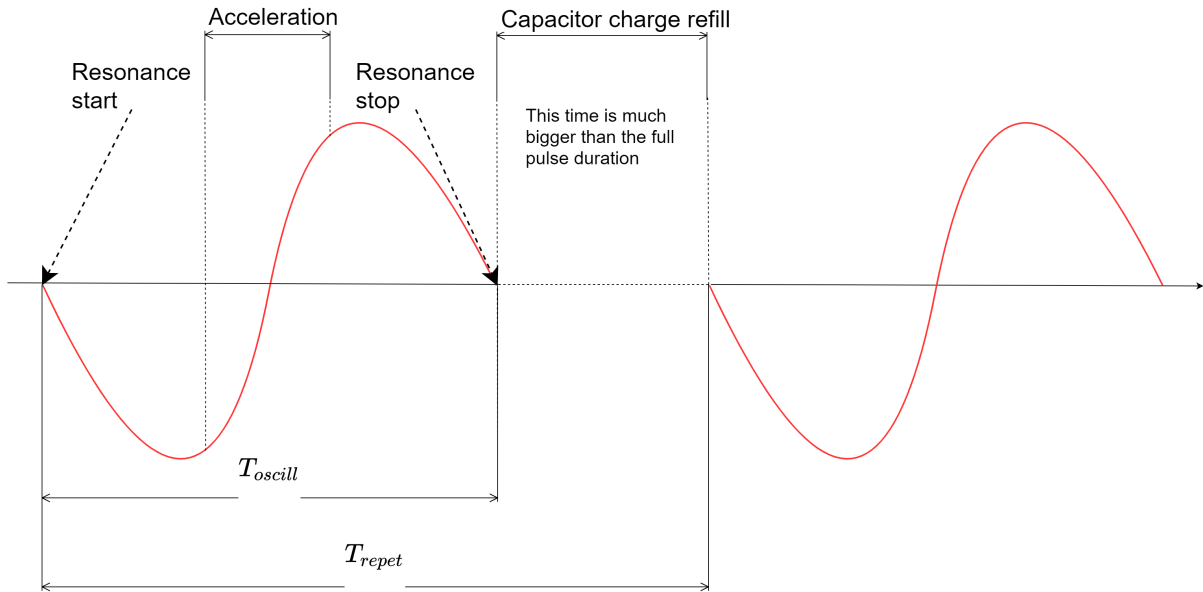


Fig. 5.8: Discontinued resonance approach

5.2.0.1 Key Challenges

The quick acceleration requires extremely high peak power sources that can only be economically guaranteed by making large use of resonance circuits such as the one proposed in the previous paragraph. On the other side, resonant circuits are not very easily controllable and it is difficult to assure high precision among the different sectors (see Fig. 5.6) and high repeatability from pulse to pulse. In addition, LC resonance doesn't match with linear acceleration profiles as required to minimize the RF requested power. The above parameters will have to be carefully analysed to avoid overrating of the power converters.

Table 5.2: RCS peak power and voltages for a linear Bref ramp.

	RCS1	RCS2	RCS3	RCS4
Inj Energy [GeV]	63	314	750	1500
Acc. length [km]	5.99	5.99	10.7	35.0
Res. mags length [km]	3.65	2.54	4.37	20.38
Binj in gap [T]	0.36	-1.8	-1.8	-1.8
Bextr in gap [T]	1.8	1.8	1.8	1.8
B ramp time Tramp [ms]	0.35	1.10	2.37	6.37
Dipoles Pmax [GW]	111	54	43	74
Dipoles Vmax [MV]	2.4	1.1	0.9	1.5

5.2.0.2 Recent Achievements

The two resonating circuits reported in Fig. 5.7 are a concept generalization of two possible approaches for the power converters. The full wave resonator is the approach by which it is possible to get close to the desired linear acceleration profile, by adding two or more resonant circuit. The most efficient approach is to use the first and second harmonics (Fig. 5.9), but other approaches are possible. The circuit is very simple and, in theory, the cost of the power electronic switch, (two thyristors) is limited.

However, the circuit doesn't offer any clear possibility to make a regulation and therefore to control the current among the different sectors of the accelerator. To overcome this limitation, additional

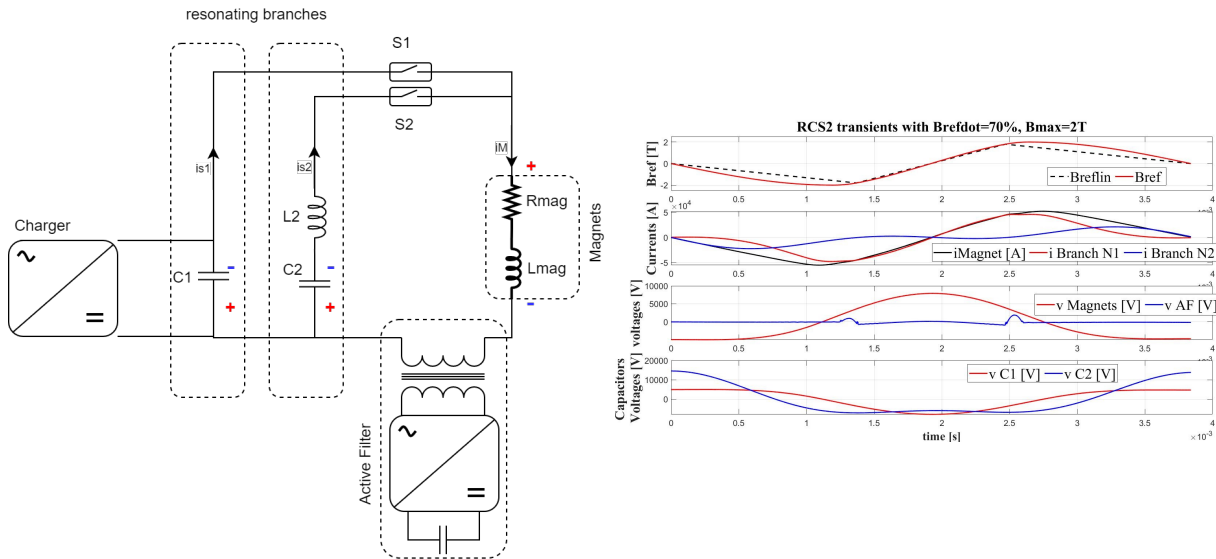


Fig. 5.9: Full wave resonance with active filter contribution

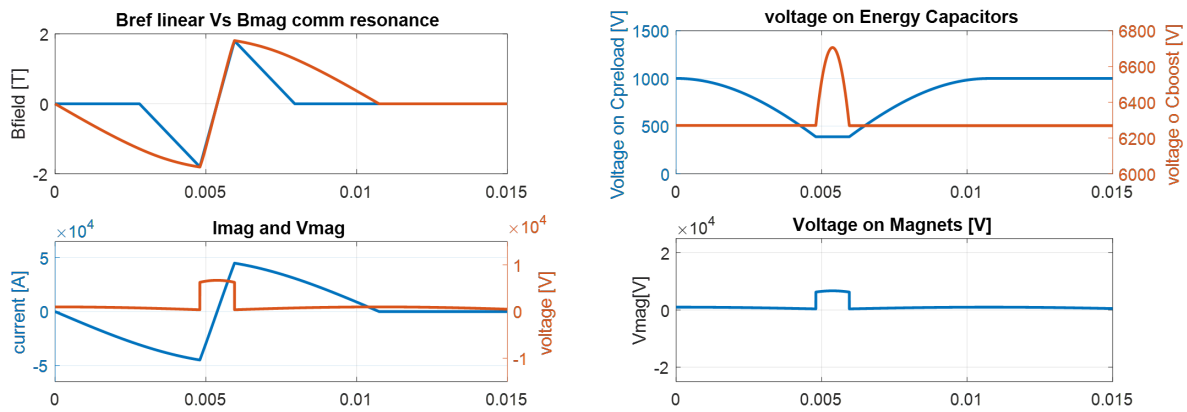


Fig. 5.10: Simulation of a switched resonance case

hardware would have to be installed (Active filter) whose cost can be high. In addition, energy storage capacitors oscillate with bipolar voltage thus leading to a considerable less energy dense design (and therefore higher cost). The introduction of the switched resonance circuit makes the circuit more complicated and costly from the power electronics point of view, but no additional magnetic components (L2 in Fig. 5.7) are required and energy storage capacitors only oscillate on positive voltage so that a more favorable design is possible for these (Fig. 5.10).

Even more important, it is possible to act on the switching on-off time instants to play with the equivalent output voltage. When this is done using several tens of power cells (as in the configuration shown in Fig. 5.6) one realizes that it is possible to have basic control of the currents in each sector and possibly avoid using an active filter. The control concept would be based on an "Iterative Learning Controller" approach, which acts on the reference voltage of each power cell to achieve matching of the current profile across the different sectors. The study of the control algorithm feasibility is part of the important missing efforts listed in the next paragraphs.

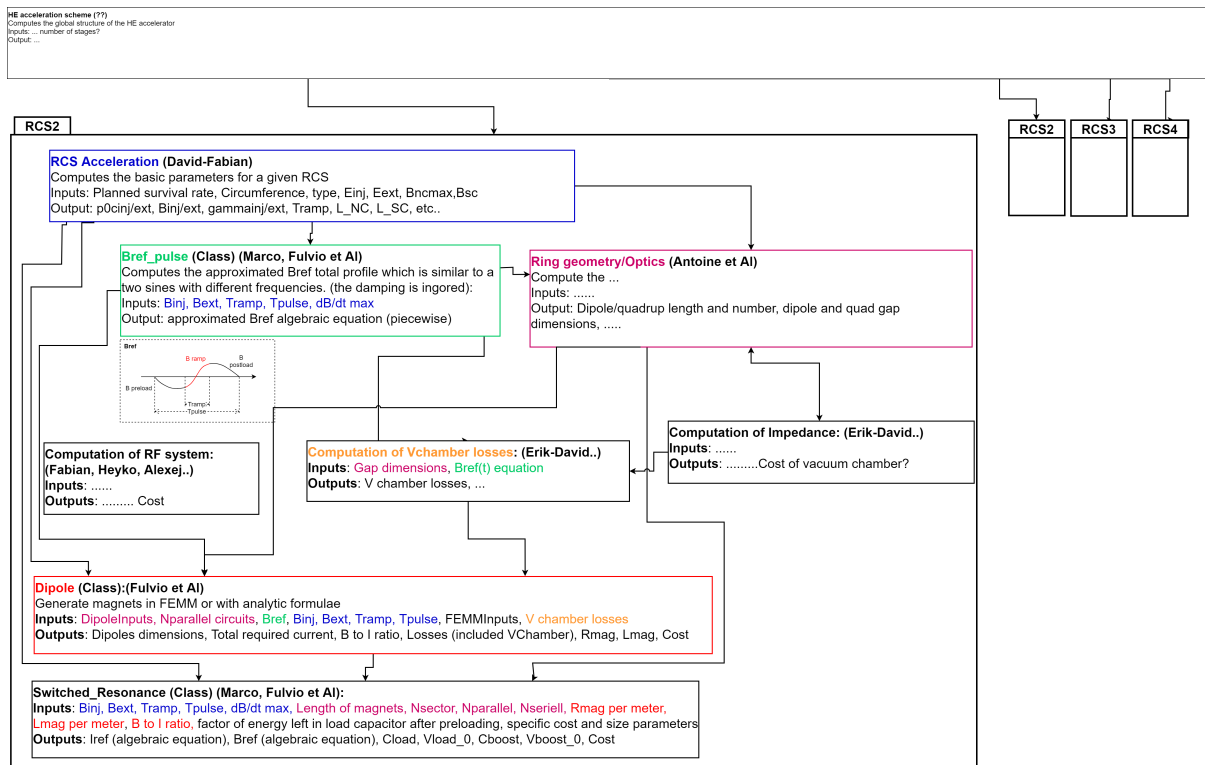


Fig. 5.11: Python Accelerator simulation suite schematic

Planned Work

Because of the strong links with the design of the resistive magnets and with other technological areas of the accelerator, it is difficult to determine the design of the power converters alone. Instead a combined python based design suite is being developed. A preliminary sketch is reported in Fig. 5.11.

Different Python classes shall perform the necessary computations to design the relative parts and compute the cost of it. An integrated optimization can then lead to a cost effective design of the accelerator as a whole.

Another very important part in the design of the power converters is with the study of the ILC controller to verify if such an approach would allow controlling the current among sectors with the required accuracy.

5.2.0.3 Important Missing Efforts

Throughout our analysis we have assumed many design values that have a remarkable impact on the cost and carbon footprint of the final design. As the application is very peculiar, our assumption cannot be justified by existing similar applications. In particular the limits of the IGBTs could be different from that assumed in the design. As the systems only works for few ms every 200, the DC maximum voltage and peak switched current values may be higher than normally assumed with "standard" power converters, thus reducing the equivalent IGBT number. Also the energy density design value of the capacitors may be higher (or lower) than assumed. It is therefore essential to build (after the design optimization effort) a full scale power cell and study the limits of the different components. In addition, the system behaviour and control of several connected power cells has to be demonstrated with a string

test using a limited number of full scale power cells.

5.3 RF

5.3.1 RF system for muon cooling

System Overview

The RF system for the muon cooling complex consists of approximately 8000 RF cavities operating in the frequency range starting from a few hundred of MHz. The majority of the cavities operate at 352 and 704 MHz in the initial and 6D-cooling channels. The main peculiarity of the RF system is that the RF cavities are interleaved with strong solenoidal magnetic fields, which enhance the cavity breakdown rate. It has been proven to affect the high gradient operation of the RF cavities necessary to re-accelerate muons as fast as possible due to their short life time. This also limits the choice of the RF cavities to normal conducting ones since SRF cavities cannot operate in magnetic field. In order to reach high gradient on the order of a few tens of MV/m in normal conducting cavities, high peak RF power on the order of few MWs per one single cell cavity is needed. This results in very high peak power requirements of a few tens of GW. On the other hand, the single (or few) bunch operation mode results in relatively short pulse lengths of $\approx 10 \mu\text{s}$ and relatively low duty factor of $\approx 10^{-4}$.

Key Challenges

Several experiments on breakdown rates in cavities under high magnetic field have been carried out in the frame of dedicated programs (International Muon Ionization Cooling Experiment (MICE) [28], Muon Accelerator Program at Fermilab (MAP) [2]). Higher breakdown rates leading to lower achievable accelerating gradients were observed in copper cavities operating at 805 MHz. A model based on the "beamlet" principle obtained good correlation with experiments [31]. That model predicts the appearance of breakdown when the local temperature rise exceeds a threshold beyond, which plastic deformation and surface damage may affect cavity behavior. Additionally, it also relates the local temperature rise to the magnetic field. The same study predicted an improvement for cavities made of beryllium, which is corroborated by measurements: a maximal gradient of nearly 50 MV/m is kept in presence of 3 T, while for copper the gradient drops from 24 MV/m at 0 T to the 13 MV/m at 3 T [31].

Integration of the RF cavities together with high-field superconducting solenoids and absorbers in the common vacuum vessel is another engineering challenge. The superconducting solenoids operate at cryogenic temperature whereas RF cavities and the associated RF network operate at room temperature. Combining all the subsystem in a compact way is a key challenge in the engineering design of the muon cooling channel.

Recent Achievements

A simplification of the "beamlet" model for short pulses ($< 10 \mu\text{s}$) has been developed, where the heat diffusion in the cavity walls can be neglected. It showed that reducing the pulse duration should strongly increase the maximal acceptable B field, for the same accelerating field. Moreover, materials other than copper (beryllium, aluminum, copper alloys such as CuAg) with different mechanical properties could give other solutions to mitigate this effect. Lower temperatures could also mitigate this effect, as it affects the field emission of the cavity, as well as increasing the surface hardness and the thermal

conductivity . Further, the external magnetic field may affect elliptical cavities less than pillbox cavities.

Planned Work

Further simulations involving thermal studies must be performed in order to estimate the local thermal diffusion and its potential effect on the breakdown limit in different configurations. These simulations must include multiple physics, including RF, particle tracking, and thermodynamics. A dedicated test stand is needed for studying these possibilities, which must include a high-power (some MW) RF source, one or several cavities and a strong magnet (some Tesla).

On the design side, based on the input from the muon cooling beam dynamics design, a consistent set of parameters for all of the RF cavities and their associated RF systems will be elaborated creating the backbone of the conceptual design of the RF system for the muon cooling complex. For certain specific cases, starting with the cavity which will be used for the demonstrator, more advanced engineering design will be performed including 3D RF design and thermo-mechanical simulations, as well as integration into the cooling cells for operation at very high gradients in strong solenoidal magnetic fields. The impact of the beam loading on the muon energy spread will have to be investigated and appropriate mitigation measures to be proposed.

Important Missing Effort

The conceptual design of all of the cavities for the whole muon cooling complex including front end, rectilinear initial and 6D-cooling, bunch merge and final cooling will not be covered due to the large number of different cavities. Design and construction of prototype cavities at nominal RF frequency as well as testing at high gradients in strong magnetic fields is required.

5.3.2 RF system for acceleration

System Overview

After the cooling channel, a linear accelerator and two Recirculating Linear Accelerators (RLAs) provide an initial acceleration up to 63 GeV. The linacs operate at the RF frequency of 352 MHz and accelerating gradient of 25 MV/m. Downstream from the RLAs, four Rapid Cycling Synchrotrons (RCSs) will gradually increase the energy of the two muon bunches within a few tens of turns each up to the collision energy of 5 TeV. During the transition from the second RLA to the first RCS, the bunches are split and continue as counter-rotating bunches. The design choices for the RF system will be guided by the requirements resulting from the beam dynamics simulations and the short muon lifetime. As a result, a high RF voltage per turn are required, supplied by hundreds of superconducting 1.3 GHz cavities operating at accelerating gradient of 30 MV/m per RCS. A more detailed description of the acceleration chain can be found in section 4.3.

Key Challenges

All accelerators following the first RCS will be implemented as hybrid RCSs with both normal- and superconducting magnets. Due to the nature of this hybrid magnet design, the orbit length and, thus, the revolution period changes during the acceleration, leading to the necessity of fast frequency tuning capabilities for the cavities.

The large bunch charge of up to 2.7×10^{12} muons per bunch in the RCS chain will lead to significant transient beam loading and HOM-induced power within the cavities. While the instantaneous requirements for cavity powering and HOM power extraction are high, the machine's duty cycle is low. The cavities will, therefore, be operated in a pulsed mode. The requirements for powering and HOM extraction further increase in the RLAs. The number of passes is ≈ 5 , while the beam current is higher than in the first RCS due to the higher bunch charge and lower travel time between cavity passages.

Additionally, the impact of the beam loading will not be consistent in all cavities in an RCS due to the differing time between the passages of the counter-rotating μ^+ and μ^- bunches. The same challenge applies to the extraction of the HOM power and cavity powering. In the RLAs, the HOM power and cavity powering need to be investigated in detail, as the bunches are planned to pass in buckets directly after each other, which might significantly impact HOM power extraction requirements. In the cavity shape design, the cavity HOMs performance has to be carefully balanced against the fundamental mode performance, which might lead to different designs for each ring due to the different beam currents. In the cavity design for the low-energy acceleration, one also has to take the particle speed into account, as some of the accelerators operate in an energy regime where the particles are not ultra-relativistic.

Recent Achievements

A first approximation of the power requirements for the RCS chain has been performed using the ILC cavities, cryomodules, and powering infrastructures [24] as a baseline. The results of which can be found in Table 5.3. The 9-cell ILC cavity operates at a fundamental frequency of 1.3 GHz with an accelerating gradient of 30 MV/m. While the ILC features the same repetition rate (5 Hz) as the muon collider, the beam current and bunch structure differ significantly. The requirements do not consider transient beam loading, HOM power contributions, cryogenic loss, impact of orbit change detuning, and counter-rotating beams.

Planned Work

Within the work package, optimised cavity geometries for the specific cases of the muon collider RCSs and the low-energy acceleration complex are planned to be designed. Due to the different beam- and machine parameters in the low- and high-energy acceleration, the impact of this optimisation will be significant. The target parameters, such as the fundamental mode frequency or HOM stability requirements, will be discussed with the other working groups involved. For the final choice of the frequency, the power requirements of the acceleration and cryomodules might play a significant role.

During the acceleration, muons will constantly decay, resulting in many seed particles for multipacting, which might lead to breakdowns. The magnitude of this effect needs to be studied in detail and be included in the shape optimisation.

For the chosen cavity geometry, the development of an HOM damping scheme as well as HOM coupler and FPCs (Fundamental Power Couplers) design will be conducted according to the requirements of the collective effects and beam dynamic studies. Depending on the powering and beam dynamics requirements, it might be necessary to adjust the number of cells per cavity to stay within the power limits of the couplers. In addition to the design of the cavities, an uncertainty quantification is planned to be conducted in order to investigate the impact of fabrication imperfections on the performance of the cavity. The results of this analysis will serve as a requirement for the fabrication precision in the cavities.

Table 5.3: RF parameters for the RCS chain. The average and peak RF power includes losses from the cavity to the klystron, while the wall plug power also includes the klystron efficiency.

	Unit	RCS1	RCS2	RCS3	RCS4	All
Synchronous phase	[°]	135.0	135.0	135.0	135.0	-
Number of bunches/species	-	1	1	1	1	-
Combined beam current (μ^+ and μ^-)	[mA]	43.3	39.0	19.8	5.49	-
Total RF voltage	[GV]	20.9	11.2	16.1	90.0	138.2
Total number of cavities	-	700	380	540	3000	4620
Total number of cryomodules	-	78	42	60	334	514
Total RF section length	[m]	990	530	760	4230	6510
Combined peak beam power (μ^+ and μ^-)	[MW]	640	310	225	350	-
External Q-factor	[1×10^6]	0.94	1.04	2.05	7.42	-
Cavity detuning for beam loading comp.	[kHz]	-0.69	-0.62	-0.32	-0.09	-
Max. detuning due to orbit length change	[kHz]	0	2.0	0.33	0.20	-
Total number of klystrons	-	88	42	30	47	207
Cavities per klystron	-	8	9	18	64	-
Beam acceleration time	[ms]	0.34	1.1	2.37	6.37	-
Cavity filling time	[ms]	0.23	0.25	0.50	1.81	-
RF pulse length	[ms]	0.57	1.35	2.87	8.18	-
RF duty factor	[%]	0.29	0.68	1.44	4.09	-
Peak cavity power	[kW]	910	820	420	120	-
Total peak RF power	[MW]	850	410	300	460	-
Average RF power	[MW]	2.42	2.76	4.27	19.0	28.4
Average wall plug power for RF System	[MW]	3.72	4.25	6.56	29.2	43.7
HOM power losses per cavity	[kW]	9.75	12.14	6.74	2.77	-
Total HOM power losses	[MW]	6.83	4.61	3.64	8.3	23.38

The power consumption of the system will be determined for the different frequencies under consideration. To achieve a good compromise between power consumption and voltage stability under the different conditions in each accelerator, simulations will be used to determine an optimal value for the loaded quality factor Q_L and the cavity detuning $\Delta\omega$.

Important Missing Effort

The work package will focus on the design of the cavities and couplers for both the high- and low-energy acceleration. The integration of the cavities into cryomodules is not part of the work package. Possible improvements to the fabrication procedure could enhance the accelerating gradient for the accelerating cavities and should be examined, as these could significantly reduce the number of required cavities.

5.3.3 RF power sources

System Overview

The muon cooling system will require a significant amount of RF power to supply around 8000 cavities each with around 3 MW, summing up to around 10 GW of peak power. The frequencies required are likely to be around 352 MHz and 704 MHz. This will be driven by klystrons at this power and frequency

range.

Key Challenges

Klystrons at 352 or 704 MHz are rather large devices which are typically located in a surface building. Using a standard commercially available 3 MW klystron for each cavity will require a surface building on the order of 180 m by 30 m, as well as requiring shafts for large waveguides. A key requirement is to reduce the size of the physical footprint. This can be achieved either by using fewer higher power klystrons to feed multiple cavities or by making the klystrons more compact using improved technologies. For example, the E37503 Multibeam Klystron is a 1 GHz, 20 MW klystron has an RF circuit length of 1.5 m, including the collector and gun, it would have a total length in excess of 2 m. A 352 MHz klystron would be significantly longer than this. Another issue is the wall-plug electrical power required to drive the klystrons. Klystrons are typically around 60% efficient at their saturated output power, however, they are typically operated at lower power to provide a low-level RF overhead to cope with RF transients, which further reduces the efficiency. The duty cycle of a muon collider is likely to be around 0.015%, and including HVDC system and modulator efficiency and RF losses the total power is close to 2 MW of average power. This could be halved to under 1 MW if the operating efficiency could be increased to closer to 80%. An advantage of having a higher efficiency is also a reduction in the power handling of the collector further reducing space and cooling requirements.

Recent Achievements

There has been significant developments in high efficiency, compact klystrons for LHC, FCC & CLIC at CERN and Lancaster University. The use of two stage klystrons where the gun is operated at a lower voltage and beam power making the bunching process occur in a much shorter distance. This in turn allows better collection of particles into a well focused bunch improving the efficiency, while at the same time reducing the length of the klystron. A two stage (TS) multi-beam klystron has been designed for the CLIC drive beam that operates at 1 GHz and an output power of 24 MW, which has an efficiency of 82% and an RF circuit length of only 0.9 m.

Planned Work

Specific design work on 352 MHz and 704 MHz klystrons for MuCol will start in 2024 at Lancaster University. This will most likely be a two-stage klystron to minimise the size. The number of cavities fed by each klystron will be optimised to minimise the size of the surface building while also increasing the efficiency.

Important Missing Effort

A prototype two-stage klystron should be constructed and demonstrated, however this could be for LHC, FCC or CLIC.

5.4 Target

System Overview

The production of muons in the muon collider front-end involves the collision of a proton beam with a target material. This interaction triggers deep inelastic reactions that generate kaons and pions, subsequently decaying into muons. To effectively capture these particles and maintain control over their emittance, a robust solenoidal magnetic field is crucial. This magnetic field confines the charged particles along helical trajectories within the production target and subsequent beamline. To sustain the megawatt-class production target, active cooling is essential, requiring separation from the primary vacuum through beam windows. Moving downstream through the tapering sector before reaching the muon-cooling section, provision for an extraction channel for the unspent proton beam is required to accommodate a high-power dump absorber.

Initially, a graphite target is being considered as the primary option due to its suitability. Graphite allows operation at high temperatures and exhibits remarkable resistance to thermal shock. Its extensive usage in various facilities attests to its reliability for 2 MW operation. However, two other distinct technological alternatives are currently under investigation. The first alternative involves a heavy-liquid metal (HLM) target made of pure lead. This option addresses concerns regarding radiation damage and could potentially eliminate the necessity for integrated active target cooling within the cryostat of the superconducting (SC) solenoid. The second alternative explores a fluidized tungsten target that circulates micro-scale spheres in a closed loop. Notable features include high thermal-shock resistance and reduced susceptibility to cavitation, corrosion, and radiation damage. Both options present a possible pathway for even higher beam power delivery.

Key Challenges

The MAP study has laid the groundwork for a muon collider but has left certain crucial aspects unexplored. One significant gap is the lack of an integrated system design and optimization for the target systems for production of a high-charge, high-quality muon beam essential for achieving the desired luminosity. Similarly, detailed specifications for other front-end beam-absorbers, such as beam windows and a proton dump, were not addressed until now within the IMCC.

The integration of a MW-class production target, radiation shielding, and their respective cooling systems within the cryostat of the SC Solenoid poses significant challenges. For instance, in a 2 MW facility utilizing a graphite muon production target, around 110 kW of thermal power are deposited on the target. Additionally, up to 34% of the stored beam energy is deposited onto tungsten shielding near the target, necessitating efficient heat extraction and isolation from the surrounding solenoid. Addressing these issues requires dedicated vessels and the routing of multiple services. The ability to align and perform target exchanges independently, without removing the surrounding shielding of over 20 tonnes, needs consideration. Furthermore, residual radiation doses on the target systems necessitate designs compatible with remote handling.

Whether employing a carbon, HLM, or fluidized tungsten target, the high-intensity 2 ns pulse on target results in a very high adiabatic temperature rise of the bulk material. This temperature rise can lead to dynamic stress-strain responses in solid targets, potentially surpassing material limits. HLM targets, though free of structural concerns, may induce extreme loads on the containment vessel due to pressure

waves in the liquid, necessitating in-depth design and modelling of this complex multiphase problem. Understanding erosion management and powder handling for a fluidized tungsten target is imperative, particularly due to limited operational experience in present facilities.

The substantial levels of radiation exposure, encompassing hadronic and electromagnetic showers, as outlined in section 5.5, pose a significant challenge for the target system and its adjacent components. A comprehensive study of target and beam window materials against radiation damage is required. High integrated fluence of protons can induce atomic changes in the crystalline structure of the target materials, resulting in conductivity loss and increased brittleness, potentially reducing the lifespan of the device. For graphite, radiation annealing via operation of the target at high-temperature, coupled with larger beam sizes on target, is considered a mitigation strategy. Proton beam windows, separating the primary vacuum from the target confinement atmosphere, benefit from low Z materials such as beryllium, in order to reduce their integrated dpa (displacement per atom).

Effective cooling is essential to maintain reasonable temperature conditions for the entire system and minimize heat dissipation towards the superconducting magnet. Simultaneously, designing a sustainable facility requires optimal sizing of auxiliary services.

Lastly, a major challenge involves designing a proton absorber capable of fully absorbing the entire beam if necessary at a regular dumping power, alongside the intricate design of a beam extraction channel.

Recent Achievements

The culmination of current studies has resulted in a baseline target design featuring an 80 cm-long isotropic graphite rod of 30 mm in diameter, enclosed within a titanium vessel for hermetic confinement. A carbon composite frame holds the rod in the central position of the vessel. Internally, static helium gas at 1 bar prevents sublimation of the graphite during expected high-temperature operation (around 2000°C). Additionally, it facilitates heat dissipation through natural convection, as opposed to a radiation-only cooled target. While direct cooling (in contact with the rod) could lower the graphite temperature, the baseline solution was preferred due to its capacity for enhancing radiation defect annealing and reducing erosion concerns.

Active cooling of the inner vessel utilizes a helicoidal helium cooling circuit operating at room temperature and 20 bar. Although this setup offers a lower heat transfer coefficient compared to a liquid coolant, it mitigates the formation of pressure waves due to energy deposition on the coolant and concerns regarding water radiolysis. Positioned within the bore of the shielding assembly, the target vessel is planned to be supported on the cryostat's upstream side, allowing easy replacement of the target without interfering with the shielding assembly.

The assembly's protection from radiation has been developed in detail (see also 5.5). A tungsten shielding surrounding the pion capture solenoid is required. To address the dissipation of heat (680 kW for a 2 MW facility), the approach shifted from contemplating water cooling, which posed complexities and handling limitations, towards utilizing helium gas cooling. This transition aims to resolve technological challenges associated with corrosion, erosion, and hydrogen embrittlement on the shielding material. The tungsten shielding design has evolved to adopt pie-shaped segments, perforated for improved cooling efficiency, together with the engineering design of the shielding vessel.

The IMCC studies have been focused on refining the target design and optimizing the pion/muon yield towards the cooling section. After careful consideration, a beam size of 5mm (1σ) was determined as the optimal compromise to ensure that the graphite's dynamic response remains within acceptable limits. This solution aligns with the requirements of a 2 MW production target facility and is compatible with a proton injection of 5 GeV and 2 ns (1σ) pulses at a frequency of 5 Hz.

The proton beam window, currently envisioned to be made of beryllium due to its low density and reduced interaction with the primary beam, will be located outside the cryostat. This component will undergo extensive radiation damage and necessitates dedicated cooling. Initially, materials such as titanium were considered for windows but were dismissed due to an expected accumulation of 10s of displacement per atom (DPA) per year. After several iterations, the decision was made to position it outside the solenoid assembly, ensuring improved accessibility for inspections, potential replacements, and increased availability of service space.

Focused research on an HLM lead target emphasized defining a high-level concept while addressing critical obstacles. An initial concept involving flow in a pipe was discarded due to high magnetohydrodynamic (MHD) losses and concerns regarding shock waves on the retaining target pipe. The current model under consideration involves a free-flow of lead in the vertical direction (similar to a curtain), aiming to eliminate the concerns posed by the initial concept. Ongoing work involves further modelling and development of this concept.

Planned Work

The plan includes defining a layout for the proton dump extraction along with its conceptual design. Additionally, there will be a comprehensive focus on fully integrating the target assembly system inside the cryostat, encompassing detailed aspects of its supporting structure. Concurrently, the design of the proton beam window, especially its cooling system, will be developed in conjunction with a high-level integration design study. Careful considerations will be made regarding the installation, dismantling, and maintenance of the frontend target systems equipment. Lastly, comprehensive physics simulations, spanning from muon production to the cooling section, are scheduled to be conducted.

Important Missing Effort

The ongoing conceptual studies lack vital engineering data essential for the expected operational conditions in a muon collider. There is a need for extensive material characterization and beam tests to complement these studies adequately. For instance, prototyping key components and carrying out beam tests in facilities such as HiRadMat at CERN would provide valuable feedback. Additionally, it is imperative to include the dimensioning of auxiliary services along with respective high-level costing.

5.5 Radiation shielding

System Overview

Radiation to equipment poses a significant challenge for all stages of the muon collider complex, from the front-end up to the collider ring. Dedicated shielding configurations must be designed for the different machines in order to dissipate the radiation-induced heat and protect equipment against long-term radiation damage. This concerns in particular the protection of superconducting magnets in different

Table 5.4: Muon decays in the collider ring (one bunch per beam), assuming an injection frequency of 5 Hz and 1.2×10^7 s (=139 days) of operation per year.

	3 TeV	10 TeV
Muons per bunch	2.2×10^{12}	1.8×10^{12}
Circumference	4.5 km	10 km
Muon decay rate per unit length	$4.9 \times 10^9 \text{ m}^{-1} \text{ s}^{-1}$	$1.8 \times 10^9 \text{ m}^{-1} \text{ s}^{-1}$
Power per unit length carried by decay e^\pm	0.411 kW/m	0.505 kW/m
Total decays per unit length and per year	$5.87 \times 10^{16} \text{ m}^{-1}$	$2.16 \times 10^{16} \text{ m}^{-1}$

parts of the complex, like the target and capture solenoids of the muon source as well as the superconducting magnets in the RCS and collider rings. The radiation shielding must prevent beam-induced magnet quenches, reduce the thermal load to the cryogenic system, and prevent magnet failures due to the ionizing dose in organic materials (e.g. insulation, spacers) and due to atomic displacements in the superconductors. In most cases, dedicated absorbers need to be embedded inside the magnet aperture in order to attenuate secondary radiation showers before they can reach the coils.

The proton-driven MW-class muon source is one of the areas in the muon complex where massive shielding elements are needed for equipment protection. The solenoids near the production target are exposed to the secondary radiation showers generated by inelastic collision products in the target. The front-end design elaborated within MAP considered a combination of resistive copper magnet inserts and larger-aperture solenoids made of low-temperature superconductors. The latter are more sensitive to radiation than resistive magnets and were foreseen to be shielded by a thick layer of helium gas-cooled tungsten beads. A new solenoid configuration, based entirely on high-temperature superconductors (HTS), has been developed within the IMCC, combined with a new arrangement of tungsten shielding inserts for absorbing electromagnetic and hadronic showers.

Dedicated shielding configurations are also needed in the accelerators and the collider, protecting equipment against the radiation load due to muon decay. The power carried by decay electrons and positrons is on average about 35% of the energy of decaying muons (the rest is carried away by neutrinos, which are irrelevant for the radiation load to the machine). With the presently assumed beam parameters, this amounts to about 500 W/m dissipated in the collider ring; the collider parameters are chosen such that the power load is about the same at 3 TeV and 10 TeV (see Table 5.4). The decay electrons and positrons can have TeV energies and emit synchrotron radiation while travelling inside the magnets. The energy is then dissipated through electromagnetic showers in surrounding materials. In addition, secondary hadrons can be produced in photo-nuclear interactions, in particular neutrons, which dominate the displacement damage in magnet coils. Shielding studies for muon colliders have been previously carried out within MAP, indicating that a continuous liner (few centimeters of tungsten) is needed inside magnets and magnet interconnects. The shielding requirements for collider energies up to 10 TeV have been studied more recently within the IMCC.

Absorbers and shielding configurations might also be needed for the protection of other accelerator systems like RF cavities. In addition, massive absorbers are also required for the Machine-Detector Interface (MDI), in order to reduce the beam-induced background and radiation damage in the detector. The MDI shielding is discussed in more detail in Sec. 2.2 and will not be covered here.

Key Challenges

Designing shielding configurations for a harsh radiation environment like in the muon collider target complex requires a good understanding of radiation damage limits for equipment components like superconductors, insulation materials, etc. The shielding requirements will strongly depend on R&D efforts towards more radiation-hard solenoids and accelerator magnets. Radiation damage effects in superconductors, in particular in HTS, are also of critical interest for other applications like fusion reactors. The irradiation tests and theoretical studies carried out by the fusion community are highly beneficial for the muon collider design study. One of the key challenges is to derive a relation between radiation damage quantities, e.g., displacement per atom (DPA), and relevant macroscopic material properties like the critical temperature. This is crucial for establishing a relationship between irradiation experiments and radiation environments in the muon collider complex. Despite the still existing uncertainties, it is expected that the understanding of radiation effects in HTS magnets, including the possible benefits of annealing, will significantly improve in the coming decade.

The shielding blocks inside the superconducting solenoids around the pion/muon production target need to be tens of centimeters thick (radially), in order to sufficiently reduce the heat load and radiation damage in the magnets. The shielding has to be efficiently cooled since it has to dissipate a significant fraction (about 35%) of proton drive-beam power (2 MW). Other important aspects are the machining, handling, assembly and support of the shielding blocks. Optimizing the shielding configuration around the target and in the downstream capture section is crucial, since the shielding will determine the final aperture requirements for the solenoids. Another challenge is the overall integration of the heavy shielding inside the cryostats. Furthermore, the shielding needs to be thermally insulated from the cryostats, considering the significant heat dissipation in the shielding.

One of the key challenges for the collider shielding design is the overall optimization of geometrical aspects (beam aperture, shielding thickness, coil aperture) and thermal aspects (shielding and coil temperature, thermal insulation, cooling scheme). This optimization critically depends on technology choices, e.g., low-temperature versus high-temperature superconductors, and requires a multidisciplinary design approach including radiation and beam physics, magnet engineering, cryogenics and vacuum. A careful optimization of the absorber thickness is important since the absorbers significantly impact the aperture requirements for magnets. An essential design parameter for the shielding is the maximum allowed heat deposition in the cold mass of collider magnets and the resulting cooling requirements, which will be an important cost factor for facility operation due to the associated power consumption (see Sec. 5.7 for details). Besides the conceptual shielding design, one also faces different engineering challenges. The shielding needs to be equipped with a cooling circuit in order to extract the heat deposited by the particle showers. In addition, the vacuum chamber needs to support the weight of the shielding absorbers (>100 kg/m). Another important aspect is the raw material and manufacturing cost of the shielding. Considering the length of the collider (10 km for the 10 TeV machine), the shielding cross section hence needs to be carefully optimized.

Recent Achievements

A conceptual radiation shielding design was conceived for the target area and the downstream capture section and chicane. Dedicated shielding studies were performed with the FLUKA Monte Carlo code, in order to quantify the heat load and radiation damage in the solenoids. The shielding was assumed to

Table 5.5: Radiation load on the target solenoid in terms of the maximum displacement per atom (DPA) and the maximum absorbed dose per year of operation for various shielding configurations. The studies considered a graphite target. The inner aperture of the shielding around the target vessel was 17.8 cm. A gap of 7.5 cm was assumed between the shielding and the coils (supports, thermal insulation).

Inner radius of the magnet coils	Shielding thickness around the target	DPA/year [10^{-3}]	Dose [MGy/year]
60 cm	W 31.2 cm + H ₂ O 2 cm + B ₄ C 0.5 cm + W 1 cm	1.70 ± 0.02	10.0 ± 0.3
65 cm	W 36.2 cm + H ₂ O 2 cm + B ₄ C 0.5 cm + W 1 cm	0.90 ± 0.02	5.6 ± 0.2
70 cm	W 41.2 cm + H ₂ O 2 cm + B ₄ C 0.5 cm + W 1 cm	0.49 ± 0.01	3.1 ± 0.1
75 cm	W 46.2 cm + H ₂ O 2 cm + B ₄ C 0.5 cm + W 1 cm	0.29 ± 0.01	1.9 ± 0.1
80 cm	W 51.2 cm + H ₂ O 2 cm + B ₄ C 0.5 cm + W 1 cm	0.16 ± 0.01	1.0 ± 0.1
85 cm	W 56.2 cm + H ₂ O 2 cm + B ₄ C 0.5 cm + W 1 cm	0.09 ± 0.01	0.6 ± 0.1

be composed of helium gas-cooled tungsten segments. In order to thermalize and capture neutrons, the shielding around the target was assumed to embed a layer of water and boron carbide. This can reduce the cumulative displacement damage in the coils by about a factor of two. Table 5.5 shows the annual DPA and dose in the target solenoid for different tungsten shielding thicknesses. The studies indicate that a thickness of about 40 cm is needed for reducing the DPA in the coils to 10^{-3} DPA/year and the dose to about 5 MGy/year. Considering the beam aperture requirements, the target vessel size and the space required for supports and thermal insulation, the minimum coil aperture (radius) for the target solenoid is hence expected to be about 60-70 cm. The maximum allowed DPA in the coils per year of operation needs to be further assessed, and will depend on the expected effect of annealing cycles. A dose of 5 MGy/year could possibly be acceptable for insulation materials.

In order to estimate the general shielding requirements for superconducting arc magnets in the 3 TeV and 10 TeV colliders, generic shielding studies were performed with FLUKA. The main focus of these studies was on muon decay, whereas other source terms like beam halo losses still have to be addressed in the future. As in the MAP studies, tungsten was assumed as absorber material due to its high atomic number and density. For engineering reasons, pure tungsten may be substituted by tungsten-based alloys without significantly affecting the shielding efficiency if the alloy has a similar material density. The simulations indicated that the total power penetrating through the shielding is similar for all collider energies, despite the harder decay spectrum at 10 TeV. On the other hand, the maximum power density and dose in the coils was found to be a factor of 1.5–2 higher at 10 TeV than at 3 TeV.

Table 5.6 summarizes the calculated power load and radiation damage in collider arc magnets as a function of the radial tungsten absorber thickness (for the 10 TeV collider option). The power penetrating the absorber, mostly in the form of electromagnetic showers, amounts to almost 20 W/m in the case of a 2 cm shielding, and decreases to 4 W/m in the case of a 4 cm shielding. Most of this power is deposited in the cold bore and cold mass of the superconducting magnets. As a design criterion, the beam-induced heat load due to muon decay shall not exceed 5 W/m, considering the additional static heat load in the magnet cold mass and the resulting cooling requirements and power consumption (see Sec. 5.7). This suggests that the tungsten shielding thickness needs to be at least 4 cm. With such a thickness, the cumulative radiation damage in magnets (dose and DPA) is expected to be acceptable, even for 10 years of operation. This shows that the heat load in the cold mass remains the driving factor for the shielding design. Together with the required beam aperture of 2.35 cm (see Sec. 4.4) and other space requirements (supports etc.), the performed shielding studies indicate that the inner coil aperture

Table 5.6: Power load and radiation damage in collider ring arc magnets (10 TeV) as a function of the radial tungsten absorber thickness. The power penetrating the shielding does not include neutrinos, since they are not relevant for the radiation load to the machine; the percentage values are given with respect to the power carried by decay electrons and positrons. The results include the contribution of both counter-rotating beams.

	2 cm	3 cm	4 cm
Beam aperture (radius)	23.5 mm	23.5 mm	23.5 mm
Outer shielding radius	43.5 mm	53.5 mm	63.5 mm
Inner coil aperture (radius)	59 mm	69 mm	79 mm
Power penetrating tungsten absorber	19.1 W/m (3.8%)	8.2 W/m (1.6%)	4.1 W/m (0.8%)
Peak power density in coils	6.5 mW/cm ³	2.1 mW/cm ³	0.7 mW/cm ³
Peak dose in Kapton (5/10 years)	56/112 MGy	18/36 MGy	7/14 MGy
Peak dose in coils (5/10 years)	45/90 MGy	15/30 MGy	5/10 MGy
Peak DPA in coils (5/10 years)	8/16 × 10 ⁻⁵ DPA	6/12 × 10 ⁻⁵ DPA	5/10 × 10 ⁻⁵ DPA

(radius) of the collider arc magnets needs to be about 8 cm, which is a key figure for the magnet design.

Planned Work

The shielding studies for collider magnets performed so far were mostly of conceptual nature, with the goal to establish key parameters like the required shielding thickness. It is foreseen to progress towards a more realistic absorber design, by optimizing the transverse absorber cross section for dipoles and quadrupoles. Besides the contribution of muon decay, also beam halo losses have to be studied. In addition, it is planned to repeat the shielding studies for a wobbled machine configuration, which is essential for mitigating the environmental impact of neutrinos. Furthermore, material and engineering aspects have to be studied, including the choice of absorber material (pure tungsten versus other heavy tungsten-alloys), machining and handling, as well as the design of supports. Another important aspect is the definition of the operating temperature and the design of the cooling circuit, which requires a close collaboration between various experts (cryogenics, vacuum). So far, the studies focused mainly on the collider arcs, but they have to be extended to the experimental insertions, in particular the final focus regions. Besides the studies for the collider, shielding studies are also foreseen for the accelerators.

Important Missing Effort

In several cases, a detailed engineering design of the shielding configurations will not be possible. In addition, it is out of the scope of the present activity to proceed with the prototyping of radiation absorbers or mock-ups of entire shielding configurations. Furthermore, with the present resources it is not feasible to perform dedicated irradiation tests for probing the radiation effects in superconductors like HTS. However, possible synergies with other activities, for example within the fusion community, can be exploited.

5.6 Muon Cooling Cell

The Cooling cell is the building block of a Muon Cooling section as described in Section 4.2 and is considered one of the highest priority for prototyping efforts towards the demonstration of the feasibility

of a Muon Collider. The cooling of muons requires in fact a very compact assembly comprising room temperature RF cavities, superconducting solenoids and either Liquid Hydrogen or Lithium Hydride absorbers (more details in chapter 5.8). All those components will require space for services, power feeds and other ancillaries which will make the mechanical integration extremely complex. Within the European Project MuCol it has therefore been decided to have a dedicated work package (WP8) to produce a complete 3D model of a representative cell among the several types that will be necessary for the cooling sections. In this chapter we describe the strategy on how we intend to proceed in phases towards the full integration of a cell, and on the rationale behind the choice of the cooling cell type that will be implemented. We expect to validate the choice at the annual meeting of the IMCC collaboration that will be held in March 2024.

System Overview

A cooling cell, in its simplest version, is defined as the assembly of an RF structure made of several cells, surrounded by two or more superconducting solenoids, and one absorber at each end of the cavity (See Fig. 5.12 for a conceptual drawing).

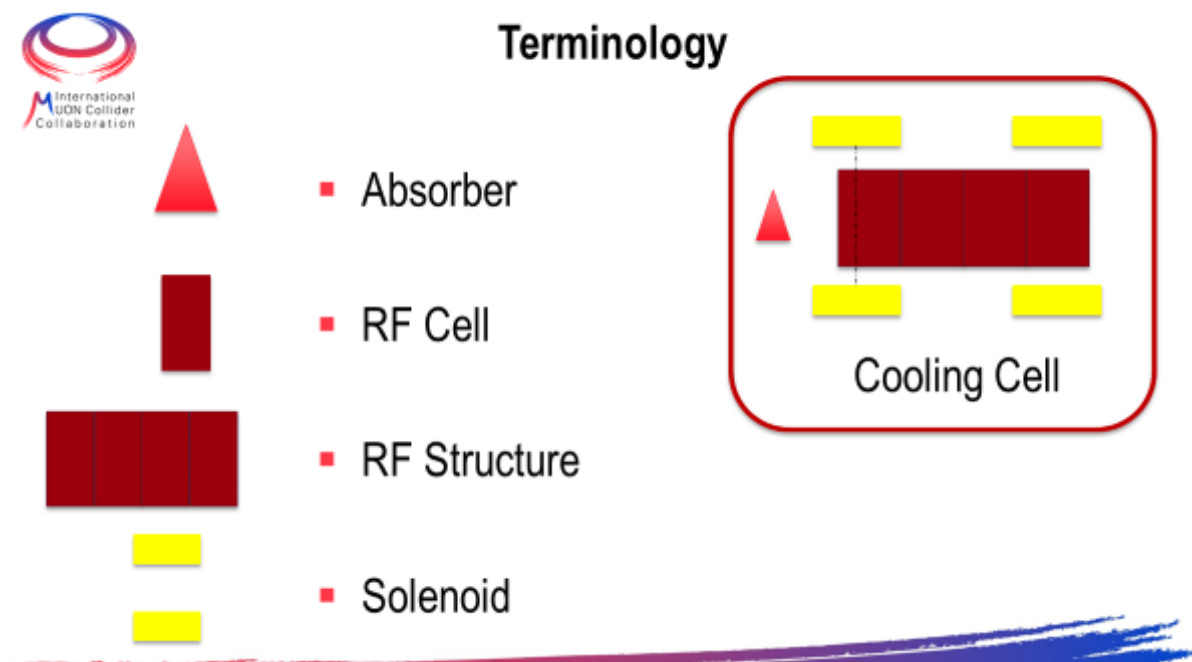


Fig. 5.12: Terminology adopted for the different components of the Cooling Cell

Different types of cooling cells will be necessary to cope with the muon beam characteristics along the cooling section of the complex. A description of the layout of a possible implementation of the 6D cooling section can be found for instance in the cooling section and in papers from the MAP programme [12, 13]. Such layout will be further optimised as discussed in Section 6.3. We will choose the cell that can yield

- an excellent cooling performance; and
- an appropriate level of technical challenge.

In order to acquire the necessary experience to properly design a cooling cell, it was agreed that the WP8 design team would be in charge as well of the design of the "Radio Frequency cavity in a Magnetic Field Test Facility" (RFMFTF) which encompasses a pillbox type cavity inside a superconducting solenoid. This is considered a somewhat simpler integration exercise yet including most of the difficulties presented by the cooling cells.

Key Challenges

The main challenges for the integration of a cooling cell are related to the limited space available in order to fulfil the requirements. The design will have to cope with the following constraints:

- have a large magnetic field on axis (order of a few Tesla),
- have a large electric field (25 MV/m) in the RF cavity,
- decide the technology to be used to limit the breakdown rate in the RF cavity under high magnetic field,
- decide whether all solenoids are in a single cryostat or in separate cryostats,
- decide whether services and ancillaries for the RF cavity (cooling, RF power couplers, HOM damping couplers will come radially or longitudinally ,
- in case the absorber, or the mitigation strategy for high breakdown rate in the RF cavity requires the use of Liquid or Gaseous Hydrogen, understand the safety issues and study a proper distribution network around the cell,
- provide the shortest cell to cell coupling space.

Recent Achievements

A preliminary conceptual design of the RFMFTF has been presented and discussed, and will be the object of further studies. The parameters of such test facility are listed in Table 5.7 :

Table 5.7: Parameters for the RFMFTF

	Unit	Parameter	Comment
Magnetic Field on Axis	[T]	7	-
RF Frequency	[MHz]	3000	-
Number of solenoids	-	2	In order to allow working in phase or antiphase
Number of cryostats	-	1	Both solenoids will be in the same cryostat
Position of RF power coupler	-	Longitudinal	RF Power Coupler will come from the front as all the services

Planned Work

In the next few months we are going to complete the design of the RFMFTF that is planned to be mostly built by INFN and placed at INFN - LASA in Milan. An initial funding has been granted by

INFN, although a full estimate of the cost has to be established taking into account that some parts might come from in kind contributions (e.g. cryogenics, power converters and RF power source) of some of the labs participating to the collaboration. On January 18 and 19, 2024, a workshop on the cooling cell technology has been organised at CERN. We presented to the community and some experts in the field the choices taken by the team and collected feedback, in order to prepare a proposal for the Governing board of MuCol about the type of cell for which the detailed design will be performed. After the endorsement of the GB, the design work will start at full speed.

Important Missing Effort

At the moment, the project misses the resources to build a cooling cell. The cost is estimated to be between 5 and 10 MCHF for the first prototype.

5.7 Cryogenics

Overview

A cryogenic infrastructure that enables the operation of superconducting magnets and radio-frequency (RF) cavities is an essential part of the Muon Collider complex. Systems requiring cryogenics will be present at most stages of the complex, including but not limited to:

- Proton Driver: cooling of high-Q RF cavities;
- Front End: cooling of the target solenoid;
- Cooling Channel: cooling of the magnet array, operation of the H₂ absorbers;
- Accelerator and Collider rings: cooling of superconducting magnets.

With sustainability in mind, one of the main drivers for the design of the cryogenic system will be the overall electrical power consumption. The various challenges of each part of the complex shall be tackled while keeping the highest possible thermodynamic efficiency (*i.e.* temperature levels as high as feasible) and the complexity to a minimum.

Key challenges

Several key challenges have been identified at the level of the Cooling Channel, and the Accelerator and Collider rings. For the moment, the Proton Driver and the Front End systems have not been assessed from a Cryogenics standpoint.

Cooling channel: the aim is to economise the overall cryogenic system investment and operation by harmonizing the demands of the various magnets that make up the channel. The most demanding magnets of the chain are the final cooling solenoids, where a substantial heat load needs to be extracted from each structure. Here, the challenge is rather on designing the local heat extraction rather than coping with the overall generated heat load. Solutions are strongly dependent on chosen time constant and ramp scheme for the magnets. The heat load profile and peak heat load generated during ramping varies significantly with these two parameters; a lower time constant reduces the heat load during ramp, but also reduces thermal and electrical stability during operation.

Accelerator ring: the focus for the accelerator ring is to investigate sustainable cryogenic system possibilities in a heterogeneous magnet environment such as the accelerator ring, which will have inter-

leaved normal conducting (warm) and superconducting (cold) magnets, and to design a cooling layout to cope with such arrangement. The fast ramping magnets will most likely generate significant ramping losses, and the sheer number of cold-to-warm transitions calls for careful design to keep heat in-leaks manageable. Another challenge is that of magnet cooling over long distances: with the aim of minimizing cost and complexity, one should strive to maximize the distance required between the accelerator's continuous-cryostat's cryogenic-service feed points and re-cooling stations. Considering the rather short field-free regions between magnets (*i.e.* interconnects), the internal routing of cryogens in the cryostat while satisfying minimum magnet interconnect distances needs careful consideration.

Collider ring: Convergence on a radial build that can be achieved from both the magnet point of view (aperture *vs.* field) and cryogenic/thermal design is crucial. It has to support appropriate mitigation strategies for the heat load deposited on the coil, such as a heat intercept between the coil and absorber and the shielding thickness of the absorber so that the total heat load stays below 10 W/m. As with the accelerator ring, magnet cooling over long distances needs to be optimised: with the aim of minimizing cost and complexity one should strive to maximize the distance required between the collider's continuous-cryostat's cryogenic-service feed points and re-cooling stations. Optimization of very short magnet interconnects compliant with magnet movement for neutrino flux mitigation is necessary: the internal routing of cryogens in the continuous collider cryostat and the integration of cryogenic-service feed-points has to be solved while satisfying minimum magnet interconnect distances and allowing for magnet movement.

Recent achievements

Since the definition of the road map, the principal achievement has been the identification of the main drivers for the cryogenic design and operation of the Muon Collider complex. The collider ring has been the subject of a more focused study, due to the stringent conditions regarding power deposition on the superconducting magnets. An estimation of the heat loads has been carried out for collider ring magnets as function of operating temperature and absorber thickness, including static heat loads from radiation and conduction via mechanical supports. This assessment will be completed with the presently missing contribution from resistive splices, current leads and ramping losses. The heat load estimation evidenced the need for a heat intercept (thermal shield) in the radial build between the absorber and the coils. This intercept is a necessary component to reduce the heat in-leak from thermal radiation to manageable levels. Also from the heat load estimation, the electrical power-consumption was estimated for the collider ring at the refrigerator interface as a function of the temperature level of the magnets and absorber circuits. Boundaries were defined for operating temperature, cryo-related power consumption and heat load to coil for collider-type magnets. These cryogenic, sustainability-driven, operational-landscape mappings contribute to facilitating the magnet/coil-cable design options.

Planned work

Most of the planned work will focus on the accelerator ring, namely to carry out an exercise similar to what has been done for the collider ring: heat load estimation and corresponding proposals of cryogenic options for the accelerator ring, considering the overall cryogenic electrical consumption. Concerning the Proton Driver, Front End and Cooling Channel, work will focus on heat load estimation and identification of potential showstoppers/challenging magnets. A common thread while working on the several

systems that make up the complex will be the cryogenic distribution and the exergetic analysis of the accelerator and collider rings, with the overall sustainability of the cryogenic system in mind.

Important missing effort

At the moment, resources are insufficient to carry out an in-depth assessment of the cooling solution for the radiation absorbers in the collider ring, namely to investigate the trade-off between water and CO₂ as coolant. It should be discussed if hydrogen as a coolant for the collider ring's superconducting magnets is an option worth investigating, and if so a preliminary evaluation into safety considerations for hydrogen use should be started. In view of the considerable heat load deposited onto the collider magnets via the absorber and cold mass supports, a thermal design optimisation of the supports along with appropriate integration of heat intercepts (thermal shield) will reduce the incoming heat loads to the temperature level of the magnets, which can have a significant impact on the overall power consumption of the 10 km collider ring. At the moment resources are also insufficient to carry out an individual thermal design optimisation of the extensive Muon Collider magnet family.

5.8 Vacuum System

5.8.1 Overview

The vacuum technology of a muon collider will encompass the vacuum system of the different elements of the accelerator complex: proton driver, cooling cells, beam acceleration and collider. Each element of the accelerator complex will have different vacuum requirements and specific constraints. Due to the short storage lifetime of the muons the pressure requirement of a muon collider will be more relaxed than in existing electron and proton storage rings [32].

The accelerator complex will require a vacuum system for beam transmission, including superconducting cavities with specific dust-free requirements, thermal insulation for the superconducting magnets, and several barriers between vacuum and absorbers in the cooling cells.

Starting at the proton driver, the pressure requirement would be $< 10^{-9}$ mbar, assuming a similar concept as the SPL machine [33]. To achieve this pressure level, only conventional vacuum equipment is required and no specific challenges are expected in this area. The presence of superconducting cavities would require dust management during the assembly and clean pumpdown and venting procedures.

After the muon production at the target, the cooling section will be dominated by the presence of drift pipes, absorbers and RF cavities inside strong solenoidal fields. Despite the pressure requirement may not be challenging, the configuration and integration of the cooling cells will be very demanding. The presence of strong magnetic fields will limit the use of mechanical pumps and difficult the integration of ion pumps and vacuum instrumentation. This area can be pumped using chemical pumping, i.e., with NEG coatings or cartridges, cryopumping (taking advantage of the availability of cryogenics for the superconducting magnet cooling), or ion pumps in special configurations like shown in [34], taking advantage of the magnetic fields available in the area.

The cooling section will need to integrate either lithium hydride or high density hydrogen (liquid or gas) as absorber to reach the target emittance (see Section 5.6). Multiple windows will be required to separate the absorbers from the vacuum of the beam line along the cooling channel.

Finally the beam acceleration and the collider will also integrate conventional vacuum equipment to reach a modest vacuum, as showed in [32]. The vacuum chamber of the collider would be integrated

with a thick tungsten shield (see Section 5.5) that have to dissipate a significant amount of the muon decay power. Assuming an aperture of 47 mm, as shown in Table 5.6, the optimal pump distribution requires 10 l/s pumps spaced 90 m to reach an average pressure $<10^{-6}$ mbar, not considering beam induced desorption.

5.8.2 Key challenges

The main challenges that have been identified are the production of very thin windows for the final stages of the cooling, the integration of liquid hydrogen as absorber in contact with thin windows, and the integration of the collider beam screen to intercept the power produced by the muon decay, having low resistive wall impedance (see Section 4.5.3).

The kinetic energy of the muon beam at the final cooling will be as low as 20 MeV at the entrance of some stages [35], reaching a few MeV at the exit. At this energy, the typical thickness used for accelerator windows (tenths of mm) will significantly perturb the beam. 1.3 mm of beryllium are enough to stop the muon beam completely at 5 MeV. The development of thin windows ideally below 10 μm and able to survive high intensity beams is required.

The presence of liquid hydrogen in those last stages poses another challenge. A cooling cell where the beam kinetic energy inside the absorber is reduced from 20 to 5 MeV involves the deposition of 9.6 J. For a small beam of σ_{RMS} equal to 0.6 mm, it will produce a pressure excursion inside the hydrogen of several hundred bars. Under these conditions the integrity of a thin window is questionable. If the muon beam has a repetition rate of 5 Hz, the power deposited in the liquid hydrogen is approximately 50 W. The evacuation of this power will be also challenging, considering the very limited bore radius of the solenoid (see Section 5.1.2).

The superconducting dipole magnets of the muon collider will require a thick tungsten shielding to protect the coils from the muon decay products. The vacuum chamber should integrate this shielding, it should be able to evacuate a significant heat load from the muon decay (in the order of 500 W/m), and have an acceptable resistive-wall impedance. The high heat load excludes running this beam screen at cryogenic temperature. On the other hand, the modest vacuum required is achievable with distributed pumping with lumped pumps separated by tenths of meters.

5.8.3 Recent achievements

Different materials used for the production of thin windows for x-ray transmission, like Be, C, and Si_3N_4 have been evaluated. Among them, silicon nitride is easily available with several suppliers. A setup for mechanical characterization of silicon nitride windows at different temperatures, from 77 K to 500 K, by bulge testing has been build and commissioned. The measurement campaign has started. Several windows of 1 μm thick Si_3N_4 with a 6 by 6 mm aperture on a silicon frame of 10 by 10 mm were tested at room temperature and at liquid nitrogen temperature. All the membranes were leak tight and survived a differential pressure of more than 5 bar at room temperature and more than 2 bar at cryogenic temperature.

One silicon nitride window has been irradiated with HiRadMat beams at SPS. The objective of the experiment was to prove the window could survive to proton intensities equivalent to those of the final cooling with a mechanical load of 1 bar of differential pressure. Assuming all the power remains in the window (using Bethe-Bloch equation) 4×10^{12} muons at 5 MeV and σ_{RMS} 0.6 mm is equivalent to

440 GeV/c protons with 0.25 mm beam size and 3×10^{12} protons. The membrane survived intensities 20 times higher than this threshold with a significant deformation, but still leak tight (see Figure 5.13).

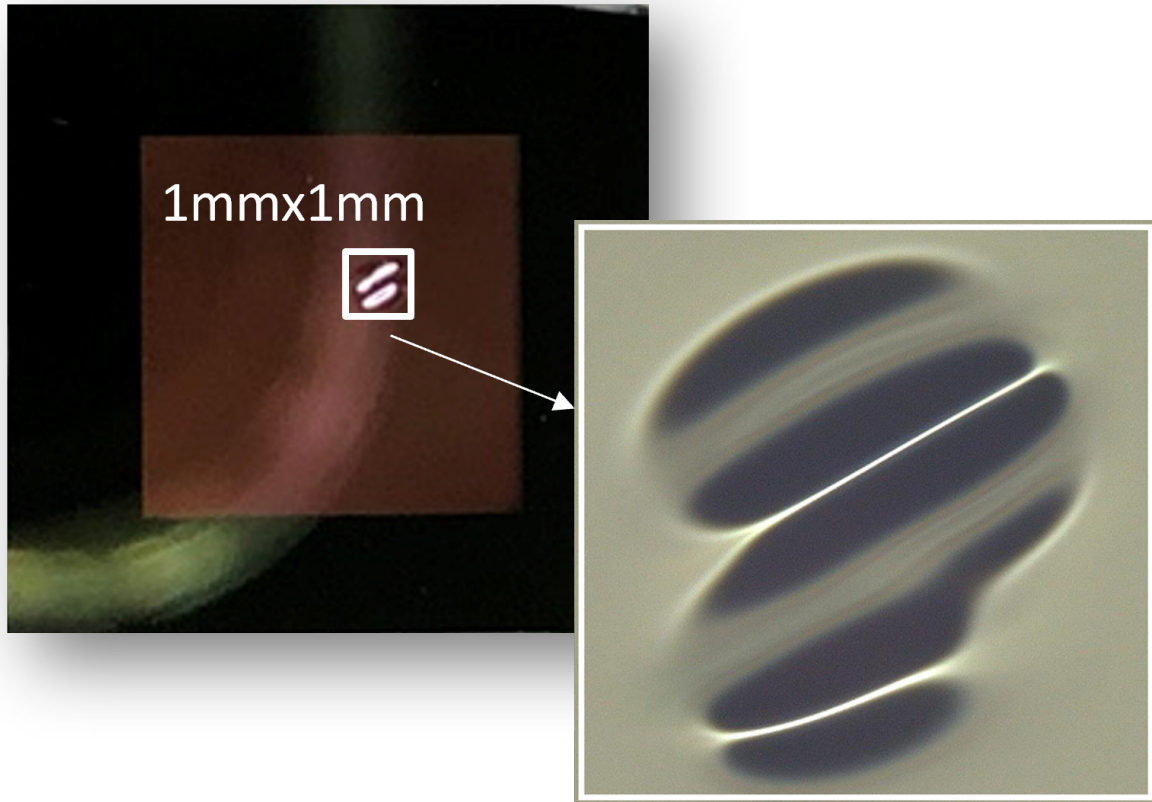


Fig. 5.13: Deformation of Si_3N_4 membrane after exposure to several pulses of a proton beam at 440 GeV/c and $> 5 \times 10^{14} \text{ p}^+/\text{mm}^2$.

5.8.4 Planned work

The main efforts are being focused on the development of very thin windows for the muon cooling. The mechanical characterization of the Si_3N_4 membranes will continue. The setup is shown in Figure 5.14. The setup consist on a window holder made of copper that can be heated or immerse in liquid nitrogen, a cover flange that allows to create a vacuum for thermal insulation and an confocal optical sensor to measure the deflection of the membrane when pressurised. With this setup will be possible to measure the mechanical performance of the membrane at different temperatures.

A HiRadMat experiment called SMAUG2 has been approved for 2024, and will allow to irradiate six membranes with different proton beams. The aim of the experiment is to gain a better understanding of the membrane behaviour during irradiation and the mechanism that generate the strong deformation shown in Figure 5.13 and test the performance at maximum beam brightness.

On top of the window characterization studies, the work will include the proposal of new concepts that could allow the integration of hydrogen as absorber for low emittance and low energy beams. Another topic that will progress in the coming months and years is the definition of the beam screen of the collider

including the cooling scheme and possible coatings for reduction of the resistive wall impedance.

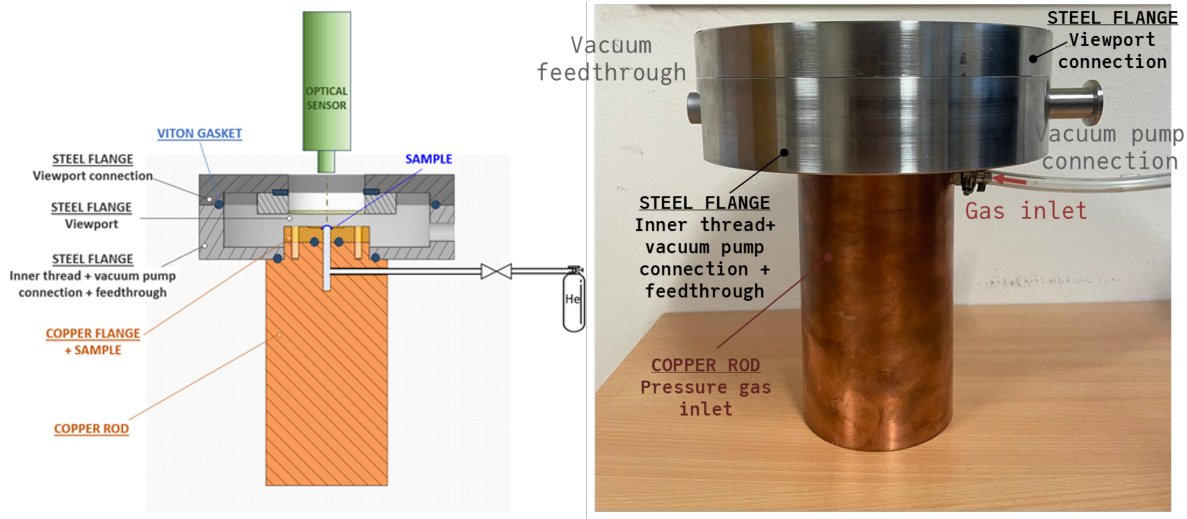


Fig. 5.14: Experimental setup for mechanical characterization of Si_3N_4 by bulge testing

5.8.5 Important missing effort

The present amount of resources limits the studies of thin windows to commercial available Si_3N_4 membranes. No development or optimization of the membrane properties will be carried out. Other candidate materials like silicon carbide, carbon, etc. are not included in the study either. No investigation about the mechanical integration of the window is being carried out. All the tests are carried out gluing the silicon frame to the support. A future application would require to develop different radiation hard joining techniques and/or a way to remove the membrane from the silicon frame

One of the driver specifications of the final cooling window is the absorber material and pressure excursions after each beam passage. The integration of the absorber in the final cooling will not be pursued more than at conceptual level.

5.9 Instrumentation

No specific studies have been launched to address the design of beam instrumentation for the Muon Collider since the expected intensities do not seem unfeasible with the presently available technologies. In particular instrumentation already used in existing muon beam facilities as well as other type of test beams are considered to be adaptable to the requirements as they are presently understood. Once the layout will be frozen, studies will be performed to confirm such hypothesis. The main difficulties will be related to the space available (very limited in the Ionisation Cooling channels), and to the radiation levels and background due to muons decay. The IMCC will strive to provide at least a roadmap for the most challenging instruments, with detailed specifications and corresponding proposed devices

5.10 Radiation Protection

Overview

The Radiation Protection (RP) aspects of the Muon Collider can be separated into two main, intrinsically different topics. One is related to the conventional RP aspects connected to prompt and residual radiation, air, water and soil activation, as well as radioactive waste produced in the whole facility starting from the proton driver up to the collider ring. These aspects are principally well understood and can be mitigated to acceptable levels as long as they are addressed in the design phase. The second topic is related to the flux of high energy neutrinos emitted from the Muon Collider that have a very small probability to interact far away in material near the Earth's surface producing secondary particle showers. This aspect is most relevant for the collider ring.

Key challenge

Muons circulating in the muon collider decay and generate neutrinos within a small solid angle that may lead to a large local flux of neutrinos in the plane of the collider ring. Due to their particularly low interaction cross section, the attenuation of TeV-scale neutrinos traversing the Earth's matter is very low (e.g. 0.01% for 100 km). A large flux of neutrinos may therefore reach the Earth's surface even far away from the collider, where rare single events of these high-energetic neutrinos create secondary particle showers. One of the challenges of a high energy muon collider is therefore to reduce the small amount of radiation created by these showers so that it is negligible.

A refined neutrino dose model has been developed. It comprises FLUKA Monte Carlo simulations that allow study of the expected neutrino and secondary-particle fluxes and evaluation of the main parameters for the effective dose predictions. The results are then folded with a realistic neutrino source term taking into account the given real collider lattice. The findings are further used to develop a map in which the dose is projected on the Earth's surface subsequently used for the final dose assessment. Next to the dose assessment also the uncertainties are to be studied and methods allowing to demonstrate compliance. This is an iterative process where optimization is addressed at the various working steps.

The goal is to ensure that the neutrino-induced effect does not entail any noticeable addition to natural radioactivity and that the environmental impact of the muon collider is negligible, i.e. an effective dose of the order of 10 $\mu\text{Sv}/\text{year}$, similar, for instance, to the impact from the LHC. Below this constraint, the optimisation requirement is considered as fulfilled and public acceptance can be expected.

Recent achievements - Neutrino dose model

Exhaustive FLUKA simulations were performed to evaluate the effective dose in soil, resulting from the interaction of the neutrinos emerging from the decay of 1.5 TeV and 5 TeV mono-directional muons. The angular and energy distributions of the neutrinos were sampled according to the respective distributions expected from the muon decays. It was found that after only a few meters of path in soil the sampled neutrino-induced showers reach a plateau condition, where the effective dose saturates and remains constant farther ahead. This condition is considered the conservative worst-case scenario since the neutrino-induced showers rapidly decrease in the transition between soil and air, as further demonstrated with additional simulations. The effective dose kernel has been evaluated on the basis of a Gaussian fit to the radial projection of the saturated effective dose. These kernels, characterised by a peak dose

and a lateral width, were evaluated for a wide range of neutrino interaction distances from the decay point (5, 10, 15, 20, 40, 60, 80, 100 km) and further interpolated to obtain a kernel shape for any distance between 5 km and 100 km. It was found that the widening of the neutrino radiation cone due to the lateral extension of the shower is very small compared to the effect of the neutrino flux angular divergence. The results additionally allowed for a general verification of simplified analytical expressions showing good agreement.

In order to evaluate the effective dose due to neutrinos reaching the Earth's surface, the "source" term given by the effective dose kernel needs to be further combined with the properties of the accelerator lattice taking the divergence of the muon beam into account. This has been performed based on numerical evaluations for half an arc cell of the latest version of the 10 TeV center-of-mass energy collider. The results show that sharp dose peaks are expected to be caused by short straight sections of 0.3 m length between magnets. Focusing and chromaticity correction based on combined function magnets helps avoiding even higher peaks. Even though the length of all straight sections is identical, the height of the peaks are lower at the beginning of the cell than towards the end of the cell. The dipolar magnetic field of combined function magnets is lower than the one of pure dipoles leading to slightly increased radiation levels. The variations of dose from different positions along the quadrupoles is caused by variations of the beam divergence.

Obvious mitigation measures are to minimize the length of straight sections in regions outside the long straight section housing the experiments and to install the device deep underground leading to large neutrino distance from the Earth's surface so that the divergence of the neutrino flux leads to dilution of the resultant shower. Careful lattice design avoiding straight sections without horizontal beam divergence due to dispersion derivative may allow the radiation dose peaks from the arcs to be mitigated. The present plan for the 10 TeV collider is to implement an additional mitigation method, which implies that the beamline components in the arcs are placed on movers to deform the ring periodically in small steps such that the muon beam direction would change over time (for details see Section 5.12). It has been found that such vertical deformation of the beam within ± 1 mrad by the movers would result in a reduction of the dose kernels by a factor 80 to 90 for distances between 5-100 km.

Higher neutrino fluxes arising from the long straight sections are unavoidable. A tool to determine the location on the surface corresponding to the neutrino flux position and to easily adjust the positioning of the machine is being developed. This tool can be used to optimize the position of the collider ring such that higher radiation levels are localized in regions such as rock face, which may be owned by the laboratory and fenced, or at the sea. A first Proof of Concept (POC) to identify the intersection points with the Earth's surface with such a tool has been achieved by simulating straight line exit points in the case SPS & LHC. It was a static simulation to validate the methodology and the potential results, but without allowing dynamic change of the position of the accelerator. Following this POC, it was decided to add this functionality to 'Geoprofiler', a decision-support web application for future accelerator localisation study. This functionality allows users to move dynamically the position of the collider via 2D placement with specification of the altitude as well as the ability to "tilt" the collider around two axes, and to then perform an analysis of the main radiation lines of the collider for this position. The objective was to show the intersection between these lines and the surface of the Earth (Digital Elevation Model). Due to the large range of action of the radiation lines, we chose to use European Space Agency Copernicus DEM, which covers the whole European territory. At this point, because of performance issues, it

was decided as a first step, to restrict the number of radiation lines to the two main ones. An analysis of the positioning with the tool allowed us to identify at least one potential option in the local CERN area that would direct the neutrino flux of the IPs to a limited non-built-up area in the mountains on one side and a far away area in the Mediterranean Sea on the other side. In addition, this configuration has the advantage of having a single exit point in the mountains from each of the two IP's located with a steep exit angle thanks to the collider inclination and ground profile.

Generally, for the dose assessment all possible exposure pathways have to be taken into account. In the case of the neutrino induced radiation far away from the collider, it has been found that the only pathway to consider is the external exposure directly from the secondary particle showers induced by the neutrinos. It has been demonstrated with FLUKA simulations that the exposure due to activated or contaminated soil and air is negligible. FLUKA simulations were furthermore used to investigate the composition of the secondary particle showers created by the neutrino interactions, which is relevant for identifying methods to demonstrate compliance. It was found that the effective dose stemming from the neutrino interactions is dominated by neutrons and the electromagnetic component. Moreover, various dosimetric quantities were compared to each other allowing to evaluate the field-specific conversions factors. Finally, it was concluded that the exposures resulting to biota, i.e. animals and plants, are expected to be orders of magnitude below the respective reference levels.

Recent achievements - Conventional RP aspects

A first investigation of the conventional RP aspects of the collider ring arcs was performed based on FLUKA simulations. The studies comprised the evaluation of the residual ambient dose equivalent levels in the arc dipoles region for different cool-down times. The radiation levels after 5 years of beam operation were found to be better than in the inner triplet region of the HL-LHC and are thus considered acceptable assuming optimization of interventions. The residual dose rates after the commissioning phase, assumed to be of three months with 20% beam intensity, were found to be more than one order of magnitude lower and complying with a Supervised Radiation Area ($< 15 \mu\text{Sv/h}$) after one week of cool-down, thus facilitating for interventions. Furthermore, the radioactive soil thickness around the tunnel was investigated and found to be similar to that of the LHC. With suitable collider placement deep underground the level of soil activation is expected to be acceptable.

Planned work - Neutrino dose model

For the dose kernel evaluation the plan is to investigate more realistic neutrino interaction scenarios, taking into account different exit angles of the neutrino flux at the Earth's surface, interactions in various materials and more realistic geometries. Additionally, various sensitivity studies are foreseen to be conducted in a systematic manner. For the folding with the collider lattice, further studies will be carried out to investigate the feasibility of the lattice, understand the impact of the machine "wobbling" on beam dynamics and to refine the model around transitions between magnets and straight sections. The Geoprofiler tool is planned to be further improved allowing a more in-depth analysis of the areas impacted by the neutrinos, including a height/depth clearance taking into account the respective neutrino flux width. Next to that, the feasibility of the potential option in the local CERN area will be investigated more closely. For the dose assessment the evaluation of more realistic exposure scenarios and potential dose modification factors that are location dependant will be further investigated.

Planned work - Conventional RP aspects

Depending on the advancement of the target area and the test facility designs, an RP assessment may be conducted in the future to evaluate shielding requirements and provide input relevant for the optimization of the conventional RP aspects.

Important missing effort

The full evaluation of the feasibility of a collider option will not be possible in view of its dependence on the approval by the authorities of the impacted States. Furthermore, the project is lacking the resources to evaluate the potential to reuse the LHC.

5.11 Civil Engineering**5.11.1 Overview**

Civil Engineering (CE) represents a significant proportion of the implementation budget for tunneling projects such as the Muon Collider at CERN. As a result, CE studies are of critical importance to ensure a viable and cost-efficient conceptual design from the beginning.

5.11.2 Layout and placement study

The civil engineering design and planning is a key factor in establishing the feasibility of the Muon Collider. Experience from previous construction projects at CERN has shown that the existing sedimentary rock in the Geneva Basin, known as molasse, provides favourable tunneling conditions. Regions of limestone geology are also present, and cause more challenging tunneling conditions. During the excavation of the LEP tunnel, water ingress from the limestone formations caused significant problems. For this reason, the underground structures should be located as much as possible in the molasse and avoid the limestone. Another priority is to orientate the tunnel to minimise the depth of the shafts and reduce the overburden pressure on the underground structures.

Recent achievements

To plan the tunnel alignment and analyse the geological constraints, an application called ‘Geoprofiler’ has been developed. This application provides geographical visualisation of the accelerator’s footprint alongside detailed geological profiles. Within the application, user can modify the location of the tunnel alignment as well as its depth and tilt. To ensure a productive user experience, the resulting geology of the accelerator placement is displayed in real-time.

Key challenges

A key requirement of the application is to be able to freely modify the footprint of the accelerator and determine the most favourable position in terms of risk and cost. Additionally, radiation analysis requires high precision to position the accelerator and was added to the tool as well. Many key advancements were made during the development of the Geoprofiler tool:

- Integration of the alignment data. Although currently there is no official alignment, it is likely that a MAD-X file format will be provided. Therefore, it has been made feasible to upload a MAD-X

file to ‘Geoprofiler’.

- Several geodetic challenges were encountered. The available data in the MAD-X file first needs to be converted from a Cartesian coordinate system to a geographic one. Once the accelerator is in a geographic system, the coordinates must remain accurate even when the alignment is moved or rotated.
- The geological data used for the tool was collected from UNIGE (University of Geneva). There are two main components in the application to assess the geology:
 - Firstly, the profile of the alignment, which displays the geological data. This includes the depth of each geological layer, the depth of the accelerator and the surface height.
 - Secondly, the geology surrounding the shafts is displayed, from which the depths of each geological layer can be determined.
- For radiological analysis, a feature to compute the intersection of radiation lines with earth surface was added.

5.11.3 Muon Test Facility

A beam test facility was proposed to demonstrate the feasibility of muon ionisation cooling in order to prove that the required luminosity could be achieved in the Muon Collider. A preliminary civil engineering study has been carried out, investigating the possibility of constructing the Test Facility at the two different locations.

TT10 option

The first option is to use the existing TT10 tunnel, an existing transfer line to SPS. From TT10 a new beamline would be extracted via a tunnel to the proposed Muon Collider Demonstrator Facility. A conceptual layout of the facility includes a target hall, cooling tunnel, service gallery and access shafts, as shown on the image 5.15.

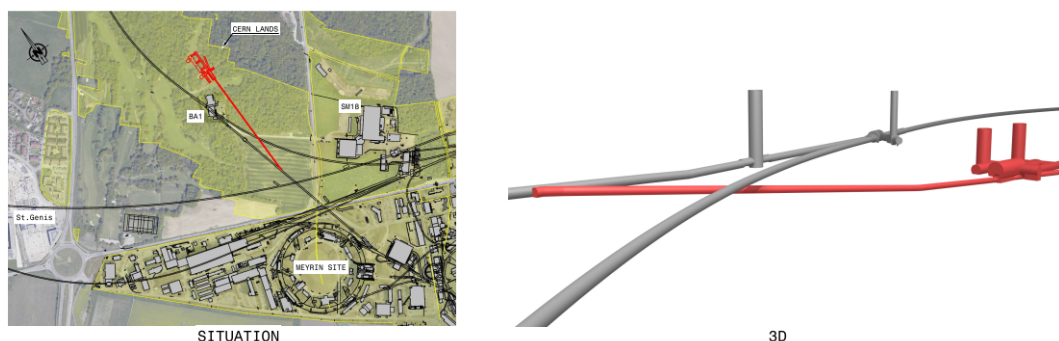


Fig. 5.15: General layout of the proposed test facility at TT10 area.

Due to the complexity and excessive cost of the required works a second option was proposed and studied implementing the proposed facility in an already existing facility at CERN.

TT7 option

A second option proposes the extension of the existing TT7 transfer tunnel up to building 181. The new surface test facility building would be connected to the underground tunnel through waveguides located every 10 m, as shown on the Fig. 5.16.

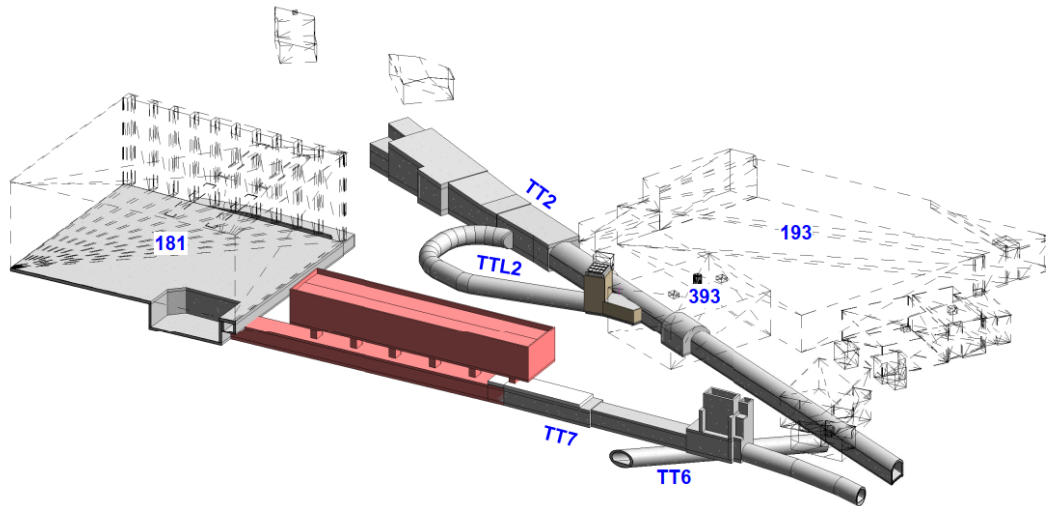


Fig. 5.16: General layout of the proposed test facility at TT7 area.

Currently, existing steel shielding blocks can be found at the end of TT7 tunnel. The blocks are proposed to be either fully or partially removed during the construction of the facility, and if possible, reused at CERN. Preliminary civil engineering cost estimates have been prepared for the two scenarios.

5.11.4 Planned work

The main goal for the following year is to choose a suitable position for the machine, that satisfies multiple constraints, such as the geological situation, territorial, and environmental aspects.

A more detailed understanding of the experimental requirements and integration studies is required, to feed into the civil engineering design and define tunnel/cavern dimensions. The aim is to have a typical cross section for the main tunnels and access shafts, to allow the feasibility studies to advance.

5.12 Movers

The neutrino flux created by the decaying muon beam in the collider is to be distributed on the surface by deforming the collider in vertical direction periodically, say every 12 hours. The collider deformation patterns are a combination of pieces of parabola with opposite curvature depicted in Fig. 5.17. The wavelength and the period of the deformation pattern are adjusted such that the slope of the tangent varies by ± 1 mrad allowing to reduce the peak doses due to neutrinos reaching earth's surface by almost two orders of magnitude.

During operation, the vertical position and the pitch of all collider magnets (pure bendings and combined function magnets) must be changed to vary the orientation of the tangent to the beam trajectory, that represent the cone of radiation induced by the neutrino flux. Several collider ring vertical deformation patterns, each to be used during typically 12 hours, are depicted in Fig. 5.18.

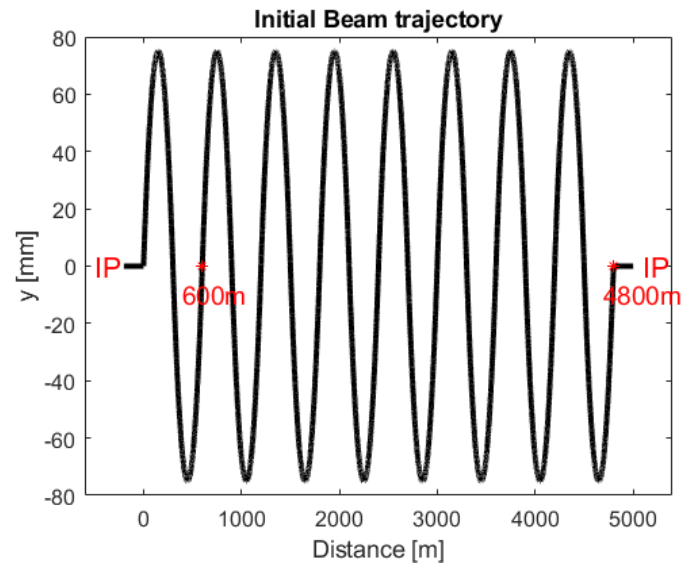


Fig. 5.17: Typical muon collider deformation pattern to mitigate radiation from neutrinos reaching Earth's surface.

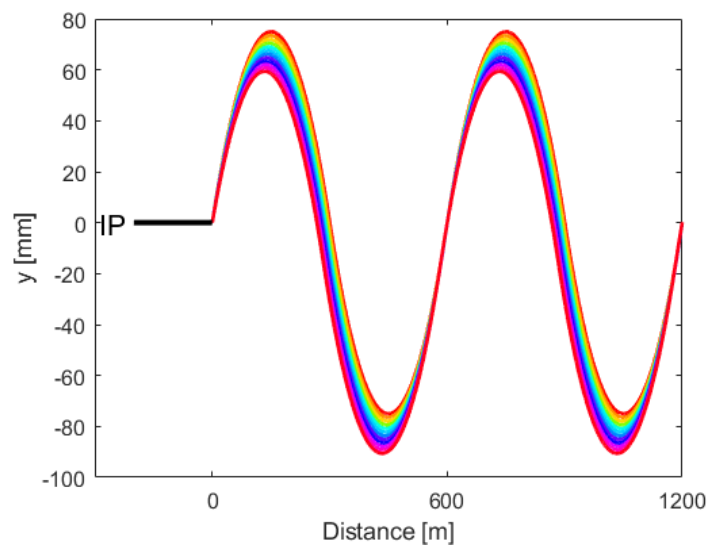


Fig. 5.18: Several collider ring vertical deformation patterns.

Several machine deformation "wobbling" patterns resulting in ± 1 mrad variations of the slope of the tangent are plotted in Fig. 5.19. To keep the radiation level at an acceptable level, the tangent to the beam trajectory should change between -1 mrad and +1 mrad. If we assume a period of 100 m, thus correspond to vertical movement required of the magnets is ± 25 mm with respect to the horizontal beam trajectory. Two adjacent magnets cannot be allowed to have opposite maximum deviation in order to protect the interconnection bellows. It should also be noted that increase of the required movement of the magnets will lead into a larger tunnel diameter.

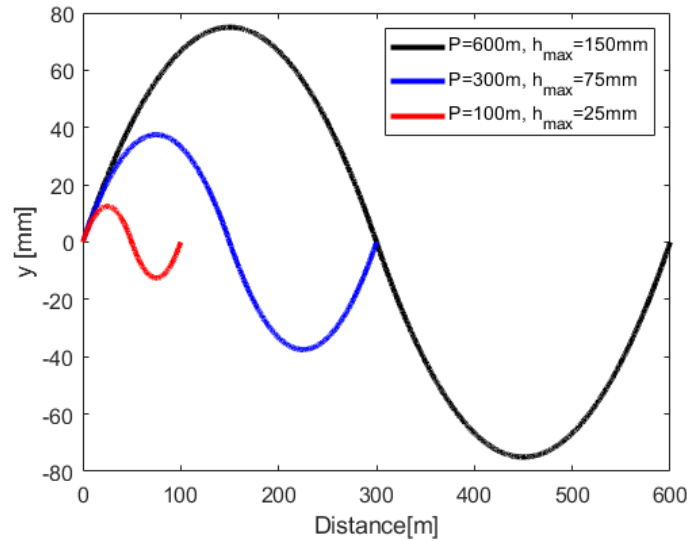


Fig. 5.19: Proposed deformation patterns with different amplitudes and periods.

5.12.1 Key Challenges

Specifications of positioning accuracy will become available only after thorough beam dynamics studies based on a working based on the collider lattice. The required positioning accuracies are expected to be stringent, in particular, for the chromatic correction and matching sections. For the present studies, positioning tolerances of ± 0.1 mm with respect to the theoretical position are assumed.

The control system of the system may need both sensors on the magnet moving components (i.e. jacks, gearboxes) and on the magnets themselves to confirm the position of the magnets after each movement. This will lead to controlling of several hundreds of electrical motors in closed loop feedback from up to couple of thousands of sensors.

The time required for the change from one magnet lay-out to another is dependent on the maximum number of motors that can be driven in parallel. The parallel movement of all magnets would require even hundreds kW of power – its realistic scenario for the movement operation, and thus time impact, remains to be studied in detail.

The collider magnets will be served by a cryogenic supply system. We have used the existing scheme of the LHC machine as reference. This involves a connection between the static cryogenic and magnet assemblies at approximately every 100 m. The beam trajectory of the muon collider does not allow a rigid connection between the cryogenic supply and the magnets at the same interval; thus, development is required.

5.12.2 Planned Work

A mock-up of the first concept is planned to study the movement system, Fig. 5.20 shows the mock-up 3D model. The plan is to test it over one interconnection. This involves two dummy magnets, the LHC type jacks for their alignment and jacking system for the re-positioning.

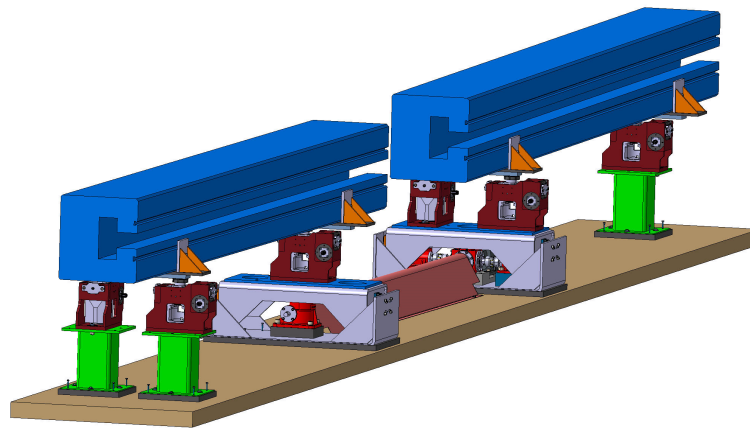


Fig. 5.20: Mock-up of the proposed magnet movement system.

5.13 Infrastructure

The study of the technical Infrastructures of the Muon Collider complex has not started yet as the configuration of the machines is still in evolution. A survey of expected energy consumption will be performed during 2024 and presented towards the end of the year with the main goal to identify the main drivers of energy consumption and provide a basis to optimise the design of the machines taking into account not only the performance but also the use of energy. For what concerns HVAC, the systems will be very likely similar to what is being operated in the present CERN complex. An optimisation will have to be done to limit the energy consumption. Particular attention will be devoted to the target area and the muon cooling section, where special requirements might be applied, due to the high level of radiation expected and the eventuality of using liquid or gaseous hydrogen as absorbing material or as gas used to inert the secondary emission yield of the RF cavities surfaces. A study will be launched as soon as decisions on the technologies to be used will be assessed. At the same time, at the moment it is not considered a priority to look in details into logistic aspects such as transport of magnets and other equipment, remote handling etc... such studies will be performed once the design of the machines will be stable. A conceptual design of the remote handling in the target area will be part of target studies as during the lifetime of the complex it is to be expected that several targets and surrounding solenoids might have to be exchanged. In this sense the civil infrastructure shall have to foresee a proper area for the radiation cooling of spent targets and surrounding equipment and hot-cells for the treatment of radioactive waste.

5.14 General Safety Considerations

The safety of people and environmental protection are priorities in the concept of a muon collider complex. Collaboration with CERN's Occupational Health & Safety and Environmental Protection (HSE) Unit is established to assure the satisfaction of the regulations and applications of best practice in these domains.

Many standard industrial hazards will need to be considered for working in such a facility, such

as noise, lighting, air quality, working in confined spaces, which can be satisfied by applying existing CERN safety practices and the Host State's regulations for workplaces. The ambient temperature in the facility will be of particular interest for access and work.

The creation of a muon collider complex will involve civil works, including tunnels, concrete structures and buildings. At CERN, all infrastructure shall be designed in accordance with the applicable Eurocodes to withstand the expected loads during construction and operation, but shall also consider accidental actions, such as seismic activity, fire, release of cryogenics and the effect of radiation on the concrete matrix and other tunnel construction fabric.

All buildings, experimental facilities, equipment and experiments installed at CERN shall comply with CERN Safety Code E and other relevant fire safety related instructions. In view of the special nature of the use of certain areas, in particular underground, and the associated fire risks, CERN's HSE Unit is considered to be the authority for approving and stipulating special provisions. As the muon collider complex study progresses, detailed fire risk assessments will have to be made, in line with the evolution of the study of the technical infrastructures. The most efficient protection strategy is one that uses complementary 'safety barriers', with a bottom-up structure, to limit fires at the earliest stages with the lowest consequences, thus considerably limiting the probability and impact of the largest events. In order to ensure that large adverse events are only possible in very unlikely cases of failure of many barriers, measures at every possible level of functional design need to be implemented:

- In the conception of every pieces of equipment (e.g. materials used in electrical components, circuit breakers, etc.);
- In the grouping of equipment in racks or boxes (e.g. generous cooling of racks, use of fire-retardant cables, and fire detection with power cut-off within each racks, etc.);
- In the creation and organisation of internal rooms (e.g. fire detection, power cut-off and fire suppression inside a room with equipment);
- In the definition of fire compartments;
- In the definition of firefighting measures, including smoke extraction and fire suppression systems;
- Access and egress sufficiently sized in an acceptable range for evacuation and fire service intervention.

With the proposed technology solutions for equipment items, personal and process safety aspects, as well as environmental concerns, must be taken into account across the full life cycle from design, fabrication, testing, commissioning, use and dismantling. For example, extensive use of cryogenics will require considerations of cryogenic and mechanical safety, as well as risk evaluations with regard to potential oxygen deficiency hazards and potential mitigation means compatible with the complex. The potential use of gaseous and/or liquid hydrogen will also require particular study, in terms of explosion and flammable gas risk assessments, potential ATEX zoning and particular mitigation measures. The electrical hazards present in the complex will need to be assessed and mitigated through sound design practice and execution. The CERN Electrical Safety Rules, alongside NF C18-510, shall be followed throughout the design process; where exceptions are required, this shall be subject to an appropriate level of risk assessment to evaluate the residual risk, and determine the mitigation strategies required. For all aspects concerning non-ionising radiation (magnetic fields, electromagnetic compatibility, etc.) the relevant CERN Safety Rules shall be followed.

For environmental aspects, efforts will be made to economise of the use of energy and water.

- Atmospheric emissions shall be limited at the source and comply with the regulations in force.
- There will be a rational use of water with the discharge of effluent water into the relevant networks in accordance with the regulations in force.
- Use of energy will be made as efficiently as possible, with thermal efficiency for all new buildings
- The natural physical and chemical properties of the soil will be preserved. All the relevant technical provisions related to the usage and/or storage of hazardous substances to the environment shall be fulfilled to avoid any chemical damage to the soil. Furthermore, the excavated material shall be handled adequately and prevent further site contamination. All excavated material must be disposed of appropriately in accordance with the associated waste regulations.
- The selection of construction materials, design and fabrication methods shall be such that the generation of waste is both minimised and limited at the source, with the appropriate waste handling and traceability of the waste in place.

Noise generated at CERN shall comply with safety requirements of the CERN Safety Rules.. Emissions of environmental noise related to neighbourhoods at CERN shall comply with CERN's Noise footprint reduction policy and implementation strategy.

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