A Nodal Transmission Pricing Model based on newly developed expressions of Real and Reactive Power Marginal Prices in Competitive Electricity Markets

Ashish Saini and A.K. Saxena

Abstract-In competitive electricity markets all over the world, an adoption of suitable transmission pricing model is a problem as transmission segment still operates as a monopoly. Transmission pricing is an important tool to promote investment for various transmission services in order to provide economic, secure and reliable electricity to bulk and retail customers. The nodal pricing based on SRMC (Short Run Marginal Cost) is found extremely useful by researchers for sending correct economic signals. The marginal prices must be determined as a part of solution to optimization problem i.e. to maximize the social welfare. The need to maximize the social welfare subject to number of system operational constraints is a major challenge from computation and societal point of views. The purpose of this paper is to present a nodal transmission pricing model based on SRMC by developing new mathematical expressions of real and reactive power marginal prices using GA-Fuzzy based optimal power flow framework. The impacts of selecting different social welfare functions on power marginal prices are analyzed and verified with results reported in literature. Network revenues for two different power systems are determined using expressions derived for real and reactive power marginal prices in this paper.

Keywords—Deregulation, Electricity markets, Nodal pricing, Social welfare function, Short run marginal cost.

I. INTRODUCTION

In this price based competition, a fair, transparent and predictable transmission pricing framework of electricity is one of the major issues. From the economic point of view, a nodal pricing based on SRMC (Short Run Marginal Cost) presents a good potential for providing economic signals for system

(e-mail: aksaxena61@hotmail.com).

operation [1].

First, Schweppe et al. [2] proposed the concept of marginal price of microeconomics to be extended to power systems and taken as the nodal price of electricity to induce efficient use of both the transmission and generation resources by providing correct economic signals. The marginal prices are obtained within an OPF (Optimal Power Flow) framework, as they are the sensitivities (dual variables) associated with the active power balance equations. Further, as proposed in [3]-[5], reactive marginal price is defined as the sensitivity of the generation production cost to the reactive power demand with reactive power production cost neglected. It represents a small portion of the true cost, as it only includes the fuel costs of the generators. It is suggested by Chattopadhyay et al. [6] that reactive power price should recover operational cost and capital investments of capacitors, but the reactive power production cost of generators is neglected. In the studies [7] on reactive power services, it is stressed that the capital costs should be included in reactive power price. Dai Y. et al. [8] introduced an opportunity cost as a reactive power production cost of generator along with capital investment cost of capacitors. Both of these costs are included in the objective function of the total system operation cost and sequential quadratic programming is applied to solve the OPF problem to obtain real and reactive marginal prices for five-bus system.

The utility industry restructuring has enhanced the role and importance of OPF tools. Although Newton method is well developed method for OPF, but more recently advanced optimized techniques such as genetic algorithms (GAs), simulated annealing method and interior point (IP) methods have been employed to solve power system optimization problems.

In present paper, section 2 is a brief introduction of GA-Fuzzy optimization method is given. The GA-Fuzzy OPF is tested and found better than various OPF methods based on classical optimization techniques and GA variants by authors and already reported in reference [9]. A proposed nodal pricing model based on SRMC method is discussed in section 3. The new expressions of real and reactive power marginal prices for all buses are developed for final optimal values of all control variables obtained from GA-Fuzzy OPF. Section 4 deals with a computer study made for 5-bus system and IEEE 30-bus data, by using expressions of real and reactive marginal

Ashish Saini is with the Department of Electrical Engineering, Faculty of Engineering, Dayalbagh Educational Institute, Agra 282005, U.P., India (corresponding author phone: +91-562-2801224; fax: +91-562-2801226; e-mail: ashish_711@rediffmail.com).

A.K. Saxena is with the Department of Electrical Engineering, Faculty of Engineering, Dayalbagh Educational Institute, Agra 282005, U.P., India

power prices in section 3. A study is made to know the impact of different social welfare functions (with base electric power loads and bilateral power transactions) on real and reactive marginal prices SRMC method for 5-bus power system data [8]. The first two cases have different social welfare functions with same base electric power loads. The last two cases represent actual electricity market scenarios having same welfare functions with same base electric power loads but two different bilateral power transactions. Optimal values of real power generation, reactive power generation of generators and reactive support of shunt capacitors are obtained by GA-Fuzzy OPF. Real and reactive power marginal prices using newly developed expressions are determined for nodal transmission pricing. Another computer study is made on completely deregulated IEEE 30-bus system with pool loads, bilateral and multilateral transactions. Network revenues are determined for both 5-bus and IEEE 30-bus power systems. Section 5 concludes the paper.

II. GA-FUZZY APPROACH FOR OPF SOLUTION

The GA-Fuzzy optimization technique has been already validated by Saini *et al.*, (2006) for OPF on 26-bus power system data, 6-bus power system data and IEEE 30-bus power system data. In this approach the ranges of crossover probability (P_c) and mutation probability (P_m) are divided into LOW, MEDIUM and HIGH membership functions and each function is given some membership values.



Fig. 1 GA-Fuzzy approach for OPF problem solving

Fig. 1 is a diagrammatic representation of an approach to incorporate fuzzy logic to GA based OPF solution. The GA parameters (P_c and P_m) are varied based on the fitness function values as per the following logic:

(1) The values of the best fitness for each generation (*BF*) is expected to change over a number of generations, but if it does not change significantly over a number of generations (*UN*) then this information is considered to cause changes in both P_c and P_m .

(2) The diversity of the population is one of the factors, which influences the search for a true optimum. The variance

of the fitness values of objective function (VF) of the population is a measure of diversity which is used to change P_c and P_m .

In this approach the ranges of P_c , P_m , BF, UN and VF are divided into three triangular functions and each is given some membership values.

III. PROPOSED NODAL TRANSMISSION PRICING MODEL

In this model, all schedule firm electric power transactions are added to the system. The following assumptions are considered for proposed pricing model.

i) All the power pool generators are required to bid their generation cost characteristics to the power pool along with maximum generation.

ii) There are no non-firm bilateral electric power transactions. iii) The real and reactive power of power pool loads are known from electric load forecasting and kept constant during optimization. Therefore, there is no bidding from single auction power pool demands shown in Fig.2. and instead of rectangular block bids from power pool generators quadratic generation cost bids are considered in the present paper.



Fig. 2 Single Auction Power Pool

iv) The other costs of system like maintenance and different overheads etc. are not being included in proposed model.

v) The losses taking place in transmission network due to transactions as well as power pool are considered to be supplied from power pool itself. They are not supplied by electric power transactions generators or cope up with transaction loss supply contracts which are complex to setup and coordinate [10].

The proposed model has single auction power pool with bilateral and multilateral power transactions in which there are no power pool demand bids. Therefore, in this case a maximization of social welfare function becomes total system cost minimization problem.

A. Objective functions and constraints

The objective function for the optimization problem is to minimize the system cost. Based on the assumption of constant loads, the minimization of system cost is equivalent to maximize the social benefits. Therefore, two suggested objective functions in [8] to maximize social benefit are given by (1) and (2) as follows:

$$\min \sum_{i=1}^{ng} \left[C(Pg_i) + C(Qg_i) \right]$$
(1)

and

$$\min \sum_{i=1}^{ng} \left[C(Pg_i) + C(Qg_i) \right] + \sum_{j=1}^{ncap} C(Qc_j)$$
(2)

Let the real power generation cost curve bid of the generator at i^{th} bus = $C(Pg_i)$

Equivalent reactive power generation cost of generator at i^{th} bus = $C(Qg_i)$

where, ng = Total number of power pool generators

Equivalent reactive power production cost of j^{th} capacitor = $C_{ci}(Qc_i)$

where, $j = 1, 2, \dots, ncap$, as ncap = Total number of capacitors operating in the system

For sake of simplicity cost curves for real power generation are modelled by following quadratic function:

$$C(Pg_i) = a + bPg_i + cPg_i^2$$
(3)

Lamont and Fu [11], introduced reactive power cost based on opportunity cost and used by Dai Y. *et al.*, [8]. The reactive power output of a generator will reduce its real generation capability which can serve at least as spinning reserve and the corresponding implicit financial loss to generator is modeled as an opportunity cost. Therefore, expression of equivalent reactive power generation cost $C(Qg_i)$ is given by (4) as below.

$$C(Qg_{i}) = \left[C(Sg_{i,\max}) - C(\sqrt{Sg_{i,\max}^{2} - Qg_{i}^{2}}) \right] k$$
(4)

where, $Sg_{i,max}$ is the nominal apparent power of the generator *i*; k is the profit rate of active power generation, usually between 5 and 10%. Here we assume $Pg_{i,max} \approx Sg_{i,max}$.

The equivalent reactive production cost for capital investment return of capacitors in (2) can be expressed as their depreciated rate (the life span of capacitors is 15 years) as follows:

$$C(Qc_j) = Qc_j \times \$11600 / MVAr$$

$$\div (15 \times 365 \times 24 \times h)$$

$$= Qc_j \times \$13.24 / (100 \ MVArh)$$
(5)

where, *h* represents the average usage rate of capacitors taken as 2/3. Qc_{j} is in per unit on 100 MVA base. Equation (5) is

a linear cost function with the slope of $dC (Qc_j) / dQc_j =$ \$13.24 /(100 *MVArh*) representing approximately the capacitor investment impacts on reactive pricing.

(6)

The equality constraints are load flow equations:

 $g(V, \delta) = 0$ where

$$g(V,\delta) = \begin{cases} Pg_i - Pd_i - P_i(V,\delta) \implies For each PV\\ and PQ bus except slack bus\\ Qg_i - Qd_i - Q_i(V,\delta) \implies For each PQ\\ bus only \end{cases}$$

 P_i = real power injection into i^{th} bus

 Q_i = reactive power injection into i^{th} bus

$$Pd_i$$
 = real power load on i^{th} bus

 Qd_i = reactive power load on i^{th} bus

 Pg_i = real power generation on i^{th} bus

 Qg_i = reactive power generation on i^{th} bus

The inequality constraints are:

• Real power generation Pg_i at PV buses

$$Pg_{i}^{\min} \leq Pg_{i} \leq Pg_{i}^{\max}$$
⁽⁷⁾

where, Pg_i^{\min} and Pg_i^{\max} are respectively minimum and maximum value of active power generation at i^{th} PV bus.

• Reactive power generation Qg_i at PV buses

$$Qg_{i}^{\min} \leq Qg_{i} \leq Qg_{i}^{\max}$$
(8)

where, Qg_i^{\min} and Qg_i^{\max} are respectively minimum and maximum value of reactive power generation at i^{th} PV bus.

• Reactive power output limit of capacitor

$$0 \le Qc_j \le Qc_j^{\max}$$
(9)

where Qc_j^{max} is maximum value of output of capacitor at j^{th} bus.

• Voltage magnitude V of each PV and PQ bus

$$V_i^{\min} \le V_i \le V_i^{\max}$$
 (10)

where, V_i^{\min} and V_i^{\max} are respectively minimum and maximum voltage at i^{th} bus

• Phase angle
$$\delta$$
 of voltage at all the buses.
 $\delta_i^{\min} \leq \delta_i \leq \delta_i^{\max}$ (11)

where, δ_i^{\min} and δ_i^{\max} are respectively minimum and maximum allowed value of voltage phase angle at i^{th} bus

• Transmission power limit

$$S_{ij} \leq S_{ij}^{\max}$$
 (12)

where, S_{ij}^{max} is the maximum rating of transmission line connecting bus *i* and *j*

Based on the above mathematical model the corresponding Lagrangian function of this optimization problem can be expressed as (13):

$$L = \sum_{i=1}^{ng} [C(Pg_i) + C(Qg_i)] + \sum_{j=1}^{ncap} C(Qc_j) - \sum_{i=1}^{n} \lambda_{pi} [Pg_i - Pd_i - P_i(V, \delta)] - \sum_{i=1}^{n} \lambda_{qi} [Qg_i - Qd_i - Q_i(V, \delta)] + \sum_{i=1}^{ng} \mu_{pi,\min} (Pg_i^{\min} - Pg_i) + \sum_{i=1}^{ng} \mu_{pi,\max} (Pg_i - Pg_i^{\max}) + \sum_{i=1}^{ng} \mu_{qi,\min} (Qg_i^{\min} - Qg_i) + \sum_{i=1}^{ng} \mu_{qi,\max} (Qg_i - Qg_i^{\max}) + \sum_{j=1}^{ncap} \mu_{cj,\max} (Qc_j - Qc_j^{\max}) + \sum_{i=1}^{n} \sum_{j\neq i}^{n} \eta_{ij} (S_{ij} - S_{ij}^{\max}) + \sum_{i=1}^{n} \nu_{i,\min} (V_i^{\min} - V_i) + \sum_{i=1}^{n} \nu_{i,\max} (V_i - V_i^{\max})$$
(13)

The term $C(Qc_j)$ will be absent in above equation, if it is not considered as per objective function given by (1). According to the theory of microeconomics, in the above augmented

THE COMPARISON OF OPF BASED NODAL PRICING MODELS							
Literature	OPF problem	Augmented LaGrange function	Expressions of nodal marginal prices				
Baughman & Siddiqi (1991)	$\begin{split} & \underset{i \notin G}{\textit{Minimize}} \sum_{i \notin G} C_i(P_{gi}) \\ & subject to \\ & P_{gi} - Pd_i - \sum_{j \neq N} V_i V_j Y_{ij} \cos(\theta_{ij} + \delta_j - \delta_i) = 0 \\ & Q_{gi} - Qd_i - \sum_{j \neq N} V_i V_j Y_{ij} \sin(\theta_{ij} + \delta_j - \delta_i) = 0 \\ & P_{g_{i,\min}} \leq P_{gi} \leq P_{g_{i,\min}} \\ & Q_{g_{i,\min}} \leq Q_{g_i} \leq Q_{g_{i,\min}} \\ & P_{ij,\min} \leq P_{ij} \leq P_{ij,\max} \\ & V_{i,\min} \leq V_i \leq V_{i,\max} \end{split}$	$\begin{split} & L = \sum_{idG} C_i(Pg_i) \\ & - \sum_{idV} (MCg_i) \bigg[Pg_i - Pd_i - \sum_{jdV} V_i V_j Y_{ij} \cos(\theta_{ij} + \delta_j - \delta_i) \bigg] \\ & - \sum_{idV} (MCg_i) \bigg[Qg_i - Qd_i - \sum_{jdV} V_i V_j Y_{ij} \sin(\theta_{ij} + \delta_j - \delta_i) \bigg] \\ & - \sum_{idV} A_{i,\min}(Pg_j - Pg_{i,\min}) - \sum_{idV} A_{i,\max}(Pg_j - Pg_{i,\max}) \\ & - \sum_{idV} H_{i,\min}(Qg_i - Qg_{i,\min}) - \sum_{idV} A_{i,\max}(Qg_j - Qg_{i,\max}) \\ & + \sum_{idV} \sum_{jdV} H_{ij}(P_{ij} - P_{i,\max}) - \sum_{idV} v_{i,\min}(V_i - V_{i,\min}) \\ & + \sum_{idV} \sum_{jdV} H_{ij}(V_i - V_{i,\max}) \end{split}$	Real power marginal price Load bus $i: \rho_{p_i} = MC_{p_i}$ Generation bus $i: \rho_{p_i} = \frac{\partial C_i(Pg)}{\partial Pg_i} - \lambda_{i,\min} + \lambda_{i,\max}$ Reactive power marginal price Load bus $i: \rho_{Q_i} = MC_{Q_i}$ Generation bus $i: \rho_{Q_i} = -\mu_{i,\min} + \mu_{i,\max}$				
El-Keib &	The P Subproblem	For Real Power Subproblem	At any bus i,				
Ma (1997)	Minimize $\sum_{i=1}^{m} C(P_{Gi})$	$L = \sum_{i=1}^{m} C(P_{Gi}) - \lambda (\sum_{i=1}^{m} P_{Gi} - \sum_{k=1}^{n} P_{Dk} - P_{L})$	Real power marginal price				
	subject to $\sum_{i=1}^{n} P_{Gi} - \sum_{k=1}^{n} P_{Dk} - P_{L} = 0$ $P_{Gi}^{\min} \leq P_{Gi} \leq P_{Gi}^{\max}$ $P_{I} \leq P_{I}^{\max}$ The Q Subproblem <i>Minimize</i> $C_{1}(P_{G1})$ <i>subject</i> to $V_{i}^{\min} \leq V_{i} \leq V_{i}^{\max}$ $Q_{Gi}^{\min} \leq Q_{Gi} \leq Q_{Gi}^{\max}$ $t_{I}^{\min} \leq t_{I} \leq t_{i}^{\max}$	$\begin{split} &\sum_{l=1}^{N} \mu_{l}(P_{l} - P_{l}^{\max}) + \sum_{l=1}^{m} \left\{ \mu_{l}^{\min}(P_{Gl}^{\min} - P_{Gl}) + \mu_{l}^{\max}(P_{Gl} - P_{Gl}^{\max}) \right\} \\ & \text{For Reactive Power Subproblem} \\ & L = C_{1}(P_{Gl}) + \sum_{l=1}^{m} \left\{ v_{PGl}^{\min}(V_{l}^{\min} - V_{l}) + v_{PGl}^{\max}(V_{l} - V_{l}^{\max}) \right\} \\ & + \sum_{k=m+1}^{n} \left\{ v_{POl}^{\min}(V_{l}^{\min} - V_{l}) + v_{PDl}^{\max}(V_{l} - V_{l}^{\max}) \right\} \\ & + \sum_{l=1}^{n} \left\{ v_{QGl}^{\min}(Q_{Gl}^{\min} - Q_{Gl}) + v_{QGl}^{\max}(Q_{Gl} - Q_{Gl}) \right\} \\ & + \sum_{l=1}^{N} \left\{ v_{QGl}^{\min}(t_{l}^{\min} - t_{l}) + v_{rJ}^{\max}(t_{l} - t_{l}^{\max}) \right\} \end{split}$	$\rho_{P_{i}} = \lambda - \lambda \frac{\partial P_{L}}{\partial P_{i}} - \sum_{l=1}^{N_{i}} \mu_{l} \frac{\partial P_{l}}{\partial P_{i}}$ Reactive power marginal price $\rho_{Q} = -\lambda \frac{\partial P_{G_{i}}}{\partial Q} + \sum_{k=m+1}^{n} \mu_{i} \left[-v_{PQ_{i}}^{\min} + v_{PQ_{i}}^{\max} \right] \frac{\partial V_{k}}{\partial Q} - v_{QG_{i}}^{\min} + v_{QG_{i}}^{\max}$				
Choi <i>et</i> <i>al.</i> , (1998)	$\begin{split} & Max \left\{ \sum_{i \in \mathcal{C}} B_i(x_i) - \sum_{j \in \mathcal{G}} C_j(x_j) \right\} \\ & subject to \\ & P_i - \sum_{j \in \mathcal{N}} V_i V_j Y_{ij} \cos(\theta_{ij} + \delta_j - \delta_i) = 0 \\ & Q_i - \sum_{j \in \mathcal{N}} V_i V_j Y_{ij} \sin(\theta_{ij} + \delta_j - \delta_i) = 0 \\ & P_{g,\min} \leq P_g \leq P_{g,\max} \\ & Q_{g,\min} \leq Q_g \leq Q_{g,\max} \\ & P_{c,\min} \leq P_c \leq P_{c,\max} \\ & Q_{c,\min} \leq Q_c \leq Q_{c,\max} \\ & Q_{c,\min} \leq Q_c \leq Q_{c,\max} \\ & Q_c = \frac{\sqrt{1 - pf_c^2}}{pf_c} \times P_c \\ & P_{ij,\min} \leq \delta_i - \delta_j \leq \delta_{ij,\max} \\ & V_{i,\min} \leq V_i \leq V_{i,\max} \end{split}$	$\begin{split} & L = \left\{ \sum_{i,kC} B_i(x_i) - \sum_{j,kG} C_j(x_j) \right\} \\ & + \sum_{i,kC} \lambda_{ijjl} \left[Q_c - \frac{\sqrt{1 - pf_i^2}}{pf_i} \times P_i \right] \\ & + \sum_{i,kC} \lambda_{ijl} [P_i - \sum_{j,kV} V_i Y_{ij} \cos(\theta_{ij} + \delta_j - \delta_i)] \\ & + \sum_{i,kC} \lambda_{ijl} [Q_i - \sum_{j,kV} V_i Y_{ij} \sin(\theta_{ij} + \delta_j - \delta_i)] \\ & - \sum_{i,kG} \mu_{ij,\min}(P_i - P_{i,\min}) + \sum_{i,kG} \mu_{ij,\max}(P_i - P_{i,\max}) \\ & - \sum_{i,kG} \mu_{ij,\min}(Q_i - Q_{i,\min}) + \sum_{i,kV} \mu_{ij,\max}(Q_i - Q_{i,\max}) \\ & - \sum_{i,kV} \sum_{j,kV} \eta_{ij,\min}(P_{ij} - P_{ij,\min}) + \sum_{i,kV} \lambda_{ijV} \eta_{ij,\max}(P_i - P_{ij,\max}) \\ & - \sum_{i,kV} \lambda_{ijV,\min}(V_i - V_{i,\min}) + \sum_{i,kV} \lambda_{ijV,\max}(V_i - V_{i,\max}) \\ & - \sum_{i,kV} \lambda_{ijV,\min}(\delta_i - \delta_{i,\min}) + \sum_{i,kV} \lambda_{ijV,\max}(\delta_i - \delta_{i,\max}) \end{split}$	At any bus i, Real power marginal price $\lambda_{ip} = \frac{\partial \left(\sum_{i \in C} B_i(P_i) - \sum_{j \in G} C_j(P_j) \right)}{\partial P_i}$ $+ \lambda_{ipf} \times \sqrt{\frac{1 - pf_i^2}{pf_i^2}} + \mu_{ip,\min} - \mu_{ip,\max}$ Reactive power marginal price $\lambda_{iq} = -\lambda_{ipf} + \mu_{iq,\min} - \mu_{iq,\max}$				

TABLE I

Lagrangian function the marginal prices for real and reactive power on i^{th} bus are λ_{pi} and λ_{qi} respectively, which are taken as the corresponding nodal prices in [3], [5] and [12]. Similar to vector λ , the vectors μ , η and v contain marginal change in cost with respect to the corresponding constraints. The elements of vectors μ , η and v respectively are different than zero only in case that the corresponding constraints are active. The expressions of real and reactive power marginal prices reported in the literature are listed in Table I.

Optimization of either (1) or (2), with power flow relations included as equality constraints (6), inequality constraints (7) to (12) and generation bidding constraints using GA-Fuzzy approach is done. All the line flow limits and control variables e.g. V at PV bus, tap ratio of tap setting transformers and shunt capacitor settings are also taken care in this optimization process. The solution to this optimization problem provides the power pool generations, shunt capacitor settings, transformer tap settings, bus voltages and line flows. GA-Fuzzy approach does not provide Lagrange multipliers required for determination of SRMC during optimization process directly. Therefore, expressions of real and reactive power marginal prices for the proposed nodal pricing model are explained in the next subsection.

B. Expressions of Real and Reactive power marginal prices for nodal transmission pricing model

The optimization problem is solved, if the following equations from (14) to (19) of optimality are satisfied for (13).

$$\frac{\partial L}{\partial Pg_i} = \frac{\partial C_i(Pg_i)}{\partial Pg_i} - \lambda_{pi} = 0 \qquad i = 1, \dots, ng$$

$$\frac{\partial L}{\partial C_i(Qg_i)} = 0 \qquad i = 1, \dots, ng$$
(14)

$$\begin{aligned} \frac{\partial Qg_{i}}{\partial Qg_{i}} &= \frac{1}{\partial Qg_{i}} - \lambda_{qi} = 0 \quad i = 1, \dots, ng \end{aligned} \tag{13} \\ \frac{\partial L}{\partial \delta_{i}} &= \sum_{j=1}^{n} \left[\lambda_{pj} \frac{\partial P_{j}}{\partial \delta_{i}} \right] + \sum_{j=1}^{n} \left[\lambda_{qj} \frac{\partial Q_{j}}{\partial \delta_{i}} \right] = 0 \\ &= \left(\lambda_{ps} \frac{\partial P_{s}}{\partial \delta_{i}} + \sum_{j=1}^{m} \lambda_{qj} \frac{\partial Q_{j}}{\partial \delta_{i}} + \sum_{j=1}^{load} \lambda_{qj} \frac{\partial Q_{j}}{\partial \delta_{i}} \right) + \\ &\left(\lambda_{qs} \frac{\partial Q_{s}}{\partial \delta_{i}} + \sum_{j=1}^{m} \lambda_{qj} \frac{\partial Q_{j}}{\partial \delta_{i}} + \sum_{j=1}^{m} \lambda_{qj} \frac{\partial Q_{j}}{\partial \delta_{i}} \right) + \\ &\left(\sum_{j=1}^{n} \lambda_{pj} \frac{\partial P_{s}}{\partial \delta_{i}} + \lambda_{qs} \frac{\partial Q_{s}}{\partial \delta_{i}} + \sum_{j=1}^{m} \lambda_{qj} \frac{\partial Q_{j}}{\partial \delta_{i}} \right) + \\ &\left(\sum_{j=1}^{n} \lambda_{pj} \frac{\partial P_{j}}{\partial \delta_{i}} + \sum_{j=1}^{m} \lambda_{qj} \frac{\partial Q_{j}}{\partial \delta_{i}} \right) \end{aligned} \tag{16} \end{aligned}$$

$$where \quad i = 1, 2, \dots, (ng + nload) \quad and \quad i \neq s \\ &\frac{\partial L}{\partial V_{i}} = \sum_{j=1}^{n} \left[\lambda_{pj} \frac{\partial P_{j}}{\partial V_{i}} \right] + \sum_{j=1}^{n} \left[\lambda_{qj} \frac{\partial Q_{j}}{\partial V_{i}} \right] + \\ &\left(\lambda_{qs} \frac{\partial Q_{s}}{\partial V_{i}} + \sum_{j=1}^{m} \lambda_{qj} \frac{\partial Q_{j}}{\partial V_{i}} \right) + \\ &\left(\lambda_{qs} \frac{\partial P_{s}}{\partial V_{i}} + \sum_{j=1}^{m} \lambda_{qj} \frac{\partial Q_{s}}{\partial V_{i}} + \sum_{j=1}^{n} \lambda_{qj} \frac{\partial Q_{j}}{\partial V_{i}} \right) + \\ &\left(\sum_{j=1}^{m} \lambda_{pj} \frac{\partial P_{s}}{\partial V_{i}} + \sum_{j=1}^{n} \lambda_{qj} \frac{\partial Q_{j}}{\partial V_{i}} \right) + \\ &\left(\sum_{j=1}^{m} \lambda_{pj} \frac{\partial P_{s}}{\partial V_{i}} + \sum_{j=1}^{n} \lambda_{qj} \frac{\partial Q_{j}}{\partial V_{i}} \right) + \\ &\left(\sum_{j=1}^{m} \lambda_{pj} \frac{\partial P_{s}}{\partial V_{i}} + \sum_{j=1}^{n} \lambda_{qj} \frac{\partial Q_{j}}{\partial V_{i}} \right) \\ &= \left(\lambda_{ps} \frac{\partial P_{s}}{\partial V_{i}} + \lambda_{qs} \frac{\partial Q_{s}}{\partial V_{i}} + \sum_{j=1}^{m} \lambda_{qj} \frac{\partial Q_{j}}{\partial V_{i}} \right) \\ &where \quad i = 1, 2, \dots, nload \qquad and \qquad i \neq s \end{aligned} \tag{17} \\ &\frac{\partial L}{\partial L} \\ &= P_{i}(V, \delta) - Pg_{i} + Pd_{i} = 0 \quad (i = 1, \dots, n) \end{aligned}$$

$$\frac{\partial \lambda_{pi}}{\partial \lambda_{qi}} = Q_i(V,\delta) - Qg_i + Qd_i = 0 \quad (i = 1,...,n)$$
(19)

where n = total no. of buses s = slack bus ng = total no. of generator busesnload = total no. of load buses

nload =total no. of load buses

Equations (16) and (17) can be expressed in matrix form as follows:

$$\begin{bmatrix} \lambda_{ps} \frac{\partial P_s}{\partial \delta_i} + \lambda_{qs} \frac{\partial Q_s}{\partial \delta_i} + \sum_{\substack{j=1\\j\neq s}}^{ng} \lambda_{qj} \frac{\partial Q_j}{\partial \delta_i} & i = 1, \dots (ng + nload) \\ \hline \lambda_{ps} \frac{\partial P_s}{\partial V_i} + \lambda_{qs} \frac{\partial Q_s}{\partial V_i} + \sum_{\substack{j=1\\j\neq s}}^{ng} \lambda_{qj} \frac{\partial Q_j}{\partial V_i} & i = 1, \dots nload \\ \hline \lambda_{ps} \frac{\partial P_s}{\partial \delta_i} & j = 1, \dots (ng + nload) \\ \hline \frac{\partial P_j}{\partial \delta_i} & j = 1, \dots (ng + nload) \\ i & and j \neq s \\ \hline \frac{\partial P_i}{\partial V_i} & j = 1, \dots (ng + nload) \\ i & and j \neq s \\ \hline \frac{\partial P_i}{\partial V_i} & j = 1, \dots (ng + nload) \\ i & and j \neq s \\ \hline \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ i & and j \neq s \\ \hline \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ i & and j \neq s \\ \hline \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ i & and j \neq s \\ \hline \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ i & and j \neq s \\ \hline \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ i & and j \neq s \\ \hline \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ i & and j \neq s \\ \hline \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ i & and j \neq s \\ \hline \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ i & and j \neq s \\ \hline \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ i & and j \neq s \\ \hline \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1, \dots (ng + nload) \\ \frac{\partial Q_j}{\partial V_i} & j = 1,$$

$$\begin{bmatrix} \lambda_{ps} \frac{\partial P_s}{\partial \delta_i} + \lambda_{qs} \frac{\partial Q_s}{\partial \delta_i} + \sum_{\substack{j=1\\j\neq s}}^{ng} \lambda_{qj} \frac{\partial Q_j}{\partial \delta_i} & i = 1, ...(ng + nload) \\ \hline \lambda_{ps} \frac{\partial P_s}{\partial V_i} + \lambda_{qs} \frac{\partial Q_s}{\partial V_i} + \sum_{\substack{j=1\\j\neq s}}^{ng} \lambda_{qj} \frac{\partial Q_j}{\partial V_i} & i = 1, ...nload \\ \end{bmatrix} + \begin{bmatrix} J \\ J \\ \vdots \\ \lambda_{qj} & j = 1, ...(ng + nload) \\ \vdots \\ j \neq s \\ \vdots \\ j \neq s \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ \vdots \\ 0 \end{bmatrix}$$

where, J = Jacobian obtained from Newton Raphson load flow method for final optimized results.

$$\begin{bmatrix} \lambda_{pj} \quad j = 1, \dots (ng + nload) \\ \overline{\lambda_{qj}} \quad j = 1, \dots nload \end{bmatrix} = - \left(\begin{bmatrix} J \\ J \end{bmatrix}^{T} \right) \times \begin{bmatrix} \lambda_{ps} \quad \frac{\partial P_{s}}{\partial \delta_{i}} + \lambda_{qs} \quad \frac{\partial Q_{s}}{\partial \delta_{i}} + \sum_{\substack{j=1\\j \neq s}}^{ng} \lambda_{qj} \quad \frac{\partial Q_{j}}{\partial \delta_{i}} & i = 1, \dots (ng + nload) \end{bmatrix}$$

$$\frac{\lambda_{ps} \quad \frac{\partial P_{s}}{\partial V_{i}} + \lambda_{qs} \quad \frac{\partial Q_{s}}{\partial V_{i}} + \sum_{\substack{j=1\\j \neq s}}^{ng} \lambda_{qj} \quad \frac{\partial Q_{j}}{\partial V_{i}} & i = 1, \dots nload \end{bmatrix}$$

$$(20)$$

Equation (14) can be written for slack bus as:

$$\lambda_{ps} = \frac{\partial C(Pg_s)}{\partial Pg_s}$$
(21)

and (15) can be written for slack and PV buses respectively as:

$$\lambda_{qs} = \frac{\partial C(Qg_s)}{\partial Qg_s}$$
(22)

$$\lambda_{qi} = \frac{\partial C(Qg_i)}{\partial Qg_i} \quad i = 1, \dots, ng$$
⁽²³⁾

Therefore, real (λ_p) and reactive (λ_q) marginal prices for slack bus, PV buses and PQ buses are obtained solving (20)-(23). The above expressions of real and reactive power marginal prices do not include μ , η and v used in (13) as all inequality constraints corresponding to (7) to (12) are taken care in respectively). optimization process.

Short run marginal cost of real power wheeling PWC_{ij} and reactive power wheeling QWC_{ij} for transaction from bus *i* to *j* are calculated by following equations:

$$PWC_{ij} = PW_{ij} \times (\lambda_{pj} - \lambda_{pi})$$

$$QWC_{ij} = QW_{ij} \times (\lambda_{pj} - \lambda_{pi})$$
(24)
(25)

 $QWC_{ij} = QW_{ij} \times (\lambda_{qi} - \lambda_{qi})$ (25) where, PW_{ij} and QW_{ij} are real power and reactive power to be wheeled from bus *i* to *j* respectively.

C. Algorithm for proposed nodal transmission pricing model

Step 1: All system voltages and power pool loads are set to initial conditions. All feasible (scheduled) firm power transactions are added to the system.

Step 2: The optimization of objective function either (1) or (2) is carried out satisfying all constraints (6) to (12) using GA-Fuzzy approach.

Step 3: After the optimization bus voltages, line flows, transformer tap settings (if present in the power system), capacitors reactive supports and power pool generations are obtained.

Step 4: Marginal prices for both real and reactive power at all buses are calculated using (20)-(23).

Step 5: Short run marginal cost of wheeling for bilateral power transactions are calculated using (24) and (25) respectively.

Step 6: The amount to be paid by each demand and amount to be received by each generation company is determined based on marginal cost. Similarly, multilateral power transaction is treated.

Step 7: The marginal network revenue is determined based on total payments and receipts.

IV. COMPUTER TEST RESULTS

A. For 5-bus system

A 5-bus power system [8] is used for computer study. The following four cases are considered to study the impacts of various factors on real and reactive marginal prices.

Case 1: The objective function has total cost of real and reactive power generations with base loads only i.e. $(\sum_{e \in G} C(Pg_i) + C(Qg_i))$ with base loads).

Case 2: The objective function has total cost of real and reactive power generations and capacitor cost with base loads only i.e $(\sum_{i \in G} [C(Pg_i) + C(Qg_i)] + \sum_{j \in C} C(Qc_j))$ with base loads).

Case 3: The objective function has total cost of real and reactive power generations and capacitor cost. Here base loads with two bilateral transactions of 50 MW each are considered i.e. $(\sum_{i \in G} [C(Pg_i) + C(Qg_i)] + \sum_{j \in C} C(Qc_j)$ with base loads and true hild and true hild and true hild and true hild are true of 50 MW each)

two bilateral transactions of 50 MW each).

Case 4: The objective function has total cost of real and reactive power generations and capacitor cost. Here base loads with two different bilateral power transactions of T1= 80 MW and T2= 50 MW respectively are considered i.e. $\left(\sum_{i \in G} [C(Pg_i) + C(Qg_i)] + \sum_{j \in C} C(Qc_j)\right)$ with base loads and two different bilateral transactions of 80 MW and 50 MW



Fig. 3 Convergence of minimum total cost, maximum fitness and variations of crossover and mutation probabilities using GA-Fuzzy approach for Case-1 and Case-2 for 5 bus system.



Fig. 4 Convergence of minimum total cost, maximum fitness and variations of crossover and mutation probabilities using GA-Fuzzy approach for Case-3 and Case-4 of 5 bus system.

Test results of case 1-4						
	Case-1	Case-2	Case-3	Case-4		
Objective function	$\sum_{i\in G} C(Pg_i)$	$\sum_{i \in G} [C(Pg_i) + C(Qg_i)] +$	$\sum_{i\in G} [C(Pg_i) + C(Qg_i)] +$	$\sum_{i \in G} [C(Pg_i) + C(Qg_i)] +$		
	$+C(Qg_i)$	$\sum_{j \in C} C(Qc_j)$	$\sum_{j \in C} C(Qc_j)$	$\sum_{j \in C} C(Qc_j)$		
	(with base loads)	(with base loads)	(with base loads and bilateral transactions T1 and $T2 = 50$ MW)	(with base loads and bilateral transactions T1=80 MW and T2=50 MW		
$S_{Ci} = P_{Ci} + Q_{Ci}$ (i=1,2)	85.02+0.266j	84.085+4.264j	82.447+8.044j	83.735+5.924j		
(in MW & MVAr)	83.824+13.529j	84.647+16.908j	89.176+18.151j	91.647+24.967j		
Reactive power output of capacitor on bus 4 (MVAr)	47.412	39.305	43.145	49.939		
Total cost	2015.3808 US\$/h	2019.5978 US\$/h	2063.7025 US\$/h	2121.4116 US\$/h		
Marginal price λp of	14.6401	14.5631	14.4256	14.5338		
real power at buses 1-5	14.9536	14.8631	14.9707	15.2524		
(US\$/MW h)	15.4516	15.3570	15.2451	15.5535		
	15.5009	15.4056	15.2607	15.5958		
	15.6571	15.5565	16.0726	16.7446		
Marginal price λp of	0.0019	0.0307	0.0580	0.0427		
real power at buses 1-5	0.0976	0.1222	0.1313	0.1813		
(US\$/MW h)	0.0910	0.1539	0.1617	0.1949		
	0.0383	0.1129	0.1208	0.1512		
	0.3307	0.3673	0.4513	0.5838		

TABLE II

Figures 3 and 4 demonstrate the convergence of minimum total cost, maximum fitness and variations of crossover and mutation probabilities using GA-Fuzzy approach for Case-1 to Case-4.

The results obtained for all the four cases are listed in Table The real power marginal prices at various buses are in the same order for all cases but higher values are obtained at bus 5 for Case 3 and 4. Reactive power marginal prices are $\sim 1/100$ times real power marginal prices for all cases, but from Case 1 to 4 reactive power marginal prices at bus 4 and 5 rise significantly. In Case 1, when the capacitor cost C(Qc) of capacitor connected at bus 4 is neglected, the corresponding reactive power source bus(es) have very little reactive power marginal prices for the free reactive power available locally. When all the reactive power production costs (see Case 2-4) are taken into consideration, the reactive power marginal prices increase noticeably at all buses which send economic signals to electric loads in the form financial incentive to reduce their reactive power demand. Case 4 and 5 are cases of deregulated environment where system becomes more stressed due to bilateral power transactions along with base loads. It is also clear from Table II, reactive power marginal prices increase with greater proportion along with real power marginal prices.

The results obtained from Case-1 and Case-2 are closely matching with Dai Y. et al. [8], as shown in Fig. 5, hence verify Fig. 5 Comparison of real and reactive power marginal prices for 5-bus the determination of real and reactive power marginal prices system using mathematical expressions proposed in section 3.



Ni	ETWORK R	EVENUE	OBTAINED FOR	CASE	E-3 AND CASE	-4 USING PROPOSED	NODAL TRA	ANSMISSION PRICI	NG MODEL
Bus No.	Real Dema Pd_i (MW	and /)	Revenue (in \$	′h) = λ	$\begin{array}{c} Revenue \ fr\\ h_{\rm pi} \times Pd_i \end{array}$	om base loads Reactive Demand (MVAr)	Qd_i	Revenue (in \$/h	$) = \lambda_{qi} \times Qd_i$
			Case-3		Case-4			Case-3	Case-4
1	0		0		0	0		0	0
2	20		299.414		305.048	9.7		1.27361	1.75861
3	45		686.0295	e	639.9075	22		3.5574	4.2878
4	40		610.428		623.832	19		2.2952	2.8728
5	60		964.356	1	1004.676	29		13.0877	16.9302
	Total		2560.2275	2	573.4635			20.21391	25.84941
				R	evenue from Bi	lateral Transactions			
Transa-	From bu	s i	To bus <i>j</i>		Size	e (MW)		Revenue obtained (in \$/h)	
ction								$= (\lambda_{qi} - \lambda_{pi}) \times Tran$	saction Size
					Case-3	Case-4		Case-3	Case-4
T1	1		5		50	80		82.35	176.864
T2	4		2		50	50		-14.50	-17.17
			Tc	tal				67.85	159.694
	Expenditure for real and reactive power generations								
Bus No.	Pg_i (MW)	Expen	venditure = $\lambda_{pi} \times Pg_i$ (in		Qg_i (N	(IVAr)	Expenditur	$e = \lambda_{qi} \times Qg_i$ (in
				\$/	\$/h)			\$/h)	
	Case-3	Case-4	Case	.3	Case-4	Case-3	Case-4	Case-3	Case-4
1	82.447	83.735	1189.3	474	1216.9877	8.044	5.924	0.4666	0.2529548
2	89.176	91.647	1335.0	271	1397.8367	18.151	24.967	2.3832	4.5265171
	Total		2524.3	745	2614.8244			2.8498	4.7794719
					Summar	y of Results			
S. No.								In (\$/	h)
								Case-3	Case-4
1.			Revenue re	ceived	d from Base Rea	al demand		2560.2275	2573.4635
2.	Revenue received from Base Reactive demand							20.21391	25.84941
3.	Revenue received from Bilateral transactions							67.85	159.694
4.	Expenditure for Real Generation						2524.3745	2614.8244	
5.	Expenditure for Reactive Generation 2.8498 4.77							4.7794719	
6.			Total	Reve	nue (S.No. 1+2	2+3)		2648.29141	2759.00691
7.			Total	Exper	nditure (S.No. 4	4+5)		2527.2243	2619.60387
			Netw	ork R	evenue (S.No. (5-7)		121.06711	139.40304

TABLE III

Table II shows that real and reactive marginal prices at many load buses are higher than at generator buses and reactive marginal prices are smaller than real marginal prices at all the buses. These marginal prices can be used to calculate significant wheeling charges of real and reactive power (marginal network revenue) as difference of revenue received from real and reactive demand and expenditure for real and reactive generation (Table 3). Obviously, in Case-4 network revenue should be more in comparison to Case-3 as total generation exceeds in order to meet the requirement of increased size of bilateral power transaction T1 (= 80 MW) and transmission losses.

B. For IEEE 30-bus system

The proposed pricing model is tested for IEEE 30-bus system data [9], bilateral and multilateral power transactions [13] are presented here. The optimal values of pool generations and shunt capacitor values as obtained through GA-Fuzzy approach alongwith minimum total cost are tabulated in Table IV. The convergence of minimum total cost, maximum fitness and variations of crossover and mutation probabilities using GA-Fuzzy approach for IEEE 30-bus system are demonstrated in figure 6. The results summarized in Table V shows that due to implementation of marginal prices, marginal network revenue of 40.301905 \$/hr is obtained.



Fig. 6 Convergence of minimum total cost, maximum fitness and variations of crossover and mutation probabilities using GA-Fuzzy approach for IEEE 30 bus system (pool loads, bilateral and multilateral transactions)

TABLE IV

OPTIMAL VALUES OF POOL GENERATIONS, SHUNT CAPACITORS AND TOTAL COST FOR IEEE 30-BUS SYSTEM USING GA-FUZZY APPROACH							
Bus No.	Real Generation (MW)	Reactive Generation (MVAr)	Bus No.	Capacitor size (MVAr)			
1	174.961	11.902	10	4.726			
2	47.529	15.599	12	1.967			
5	21.176	36.06	15	4.168			
8	24.51	34.885	17	0.89			
11	12.039	15.297	20	4.618			
13	12.329	21.845	21	4.589			
			23	4.873			
			24	3.513			
			29	0.806			
	Т	otal Real power cost of generators	US 801.82529/h				
	Total	Reactive power cost of generators	US 13.466144/h				
Total capacitors cost			US 3.991976/h				
		Total cost	US 819.28341/h				

TABLE V

NETWORK REVENUE OBTAINED FOR IEEE 30-BUS SYSTEM USING PROPOSED NODAL TRANSMISSION PRICING MODEL

Revenue from Pool loads							
Bus No.	Real Demand Pd_i	λ_{ni} (\$/MW h)	Revenue $(in \$/h) =$	Reactive Demand Od	λ _{ni} (\$/MVAr	h) Revenue (in $h) =$	
	(MW)	P	$\lambda_{ni} \times Pd_i$	(MVAr)	4. (*	$\lambda_{qi} \times Od_i$	
1	0	3.31921	0	0	0.049762	0	
2	21.7	3.435997	74.56113	12.7	0.042547	0.540345	
3	2.4	3.513915	8.433397	1.2	0.101652	0.121983	
4	7.6	3.570239	27.13382	1.6	0.110167	0.176267	
5	94.2	3.690331	347.6292	19	0.127005	2.413096	
6	0	3.612632	0	0	0.129748	0	
7	22.8	3.66913	83.65617	10.9	0.144936	1.579805	
8	30	3.626385	108.7916	30	0.150447	4.513415	
9	0	3.616505	0	0	0.123827	0	
10	5.8	3.621814	21.00652	2	0.13621	0.27242	
11	0	3.61415	0	0	0.094843	0	
12	11.2	3.599261	40.31173	7.5	0.126418	0.948136	
13	0	3.598323	0	0	0.123478	0	
14	6.2	3.676129	22,792	1.6	0.141555	0.226487	
15	8.2	3.685928	30.22461	2.5	0.134784	0.336961	
16	3.5	3.634265	12.71993	1.8	0.141915	0.255447	
17	9	3.64232	32,78088	5.8	0.143435	0.831922	
18	3.2	3.723113	11.91396	0.9	0.142798	0.128519	
19	9.5	3.728377	35.41958	3.4	0.142602	0.484848	
20	2.2	3.704354	8.149579	0.7	0.13277	0.092939	
21	17.5	3.662132	64.08731	11.2	0.159024	1.78107	
22	0	3.659034	0	0	0.156488	0	
23	3.2	3.722763	11.91284	1.6	0.12908	0.206529	
24	8.7	3.736867	32.51075	6.7	0.158234	1.060166	
25	0	3.746257	0	0	0.152652	0	
26	35	3 822748	13 37962	2.3	0 203776	0 468684	
27	0	3 674906	0	0	0.128106	0	
28	Ő	3.640752	Ő	Ő	0.140059	Ő	
29	2.4	3 783965	9 081516	0.9	0 116025	0 104422	
30	10.6	3.858995	40.90535	1.9	0.147013	0.279325	
Total			1037.401	Total		16.82278	
Revenue from Rilateral Transactions							
From bus <i>i</i>	To bus <i>j</i>	Size (MW)	Revenue obtained	$(in \$/h) = (\lambda_{ni} - \lambda_{ni}) \times '$	Fransaction Size	
9	13	5	/		-0.09091		
22	25	5			0.436115		
		Total			0.345205		
Revenue from Multilateral Transactions							
Bus No.	MW 2	mi (\$/MW h)	Expenditure (\$/h)	Bus No. MV	λ_{ni} (\$/MW h)	Revenue Received (\$/h)	
6	4	3.612632	14.450528	11 2	3.61415	7.2283	
7	2	3 66913	7 33826	13 3	3 598323	10 794969	
	-	2.30710	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	14 1	3,676129	3.676129	
			21.788788		/	21.699398	
			Total = 21.699398 -	21.788788 = -0.08939			

Contd. Table V

Expenditure for Keal and Keacuve power generations							
Bus No.	$Pg_i(MW)$	Expenditure = $\lambda_{pi} \times Pg_i$ (in \$/h)	Qg_i (MVAr)	Expenditure = $\lambda_{qi} \times Qg_i$ (in \$/h)			
1	174.961	580.7323	11.902	0.592267			
2	47.529	163.3095	15.599	0.663691			
5	21.176	78.14645	36.06	4.5798			
8	24.51	88.8827	34.885	5.248344			
11	12.039	43.51075	15.297	1.450813			
13	12.329	44.36372	21.845	2.697377			
	Total	998.9454	Total	15.23229			
Summary of Results							
S. No.			In	(\$/h)			
1.	Reven	ue received from Pool Real demand	103	37.401			
2.	Revenue	e received from Pool Reactive demand	16.	16.82278			
3.	Revenu	e received from Bilateral transactions	0.3	0.345205			
4.	Revenue I	Received from Multilateral Transactions	-0.	-0.08939			
5.	E	xpenditure for Real Generation	998	998.9454			
6.	Exp	benditure for Reactive Generation	15.	15.23229			
7.		Total Revenue	1054	1054.479595			
8.		Total Expenditure	1014	4.17769			
		Marginal Network Revenue	40	301905			

V. CONCLUSION

In this paper new expressions for real and reactive power marginal nodal prices are derived and GA-Fuzzy OPF is used for successful implementation of proposed nodal transmission pricing method. The real power marginal price is usually much higher than the reactive marginal price in non-stressed system (Case-1 and Case-2). Reactive power marginal price is affected by the reactive power production costs of generations and the capital investment cost of capacitors (Case-1 to Case-4). Reactive power marginal prices can be related to the urgency of the reactive power supply and an incentive can be given to improve load power factor and reduce power demand. The proposed nodal transmission pricing model forms a basis to calculate network revenue for bilateral and multilateral power transactions in deregulated power systems (Case-3 and Case-4) to wheel the power between the buses.

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Ashish Saini obtained his Ph.D. in Electrical Engineering from Faculty of Engineering, Dayalbagh Educational Institute, Dayalbagh, Agra, India in 2006. Presently, he is working as Senior Lecturer in Elect. Engg. Dept. at Faculty of Engineering, D.E.I., Dayalbagh, Agra, India. His research interests include applications of artificial intelligence techniques in power system optimization, planning and operation of power systems, power system deregulation, transmission pricing and congestion management. He is a life member of System Society of India, Thiruvananthapurum (India).

A. K. Saxena received his Ph.D. in Electrical Engineering from Faculty of Engineering, Dayalbagh Educational Institute, Dayalbagh, Agra, India in 1994. He is presently working as Professor in Electrical Engineering at Faculty of Engineering, D.E.I., Dayalbagh, Agra, India. His research interests include power system operation and control, security analysis, energy auditing and demand side management. He is a life member of System Society of India, Thiruvananthapurum (India) and member of IEEE.