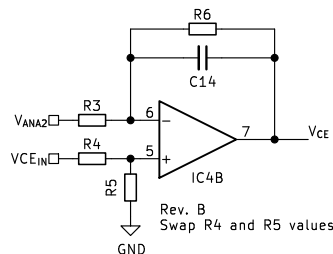


# Voltage translator for potentiostat bias.



Voltage input range 0V to 3.3V, output range -5V to +5V.

$$G = R5 / R4 = R6 / R3 = 3$$

$$V_{ANA2} = 1.65V$$

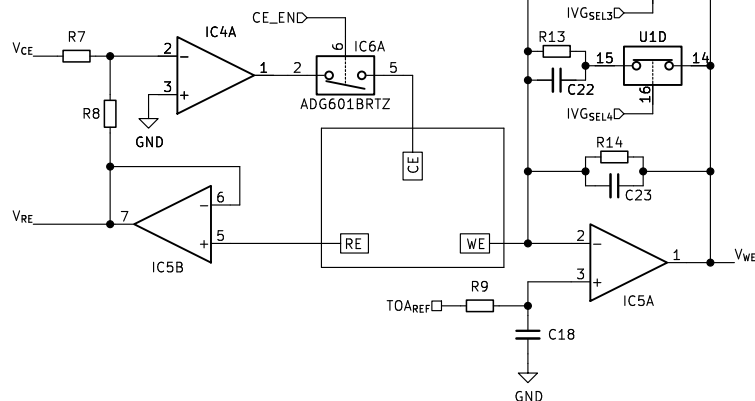
$$V_{CE} = G * (V_{CEIN} - V_{ANA2}) = 3 * (V_{CEIN} - 1.65)$$

C14 is for low pass 10KHz filter.

# POTENTIOSTAT AND I-V CONVERTER

Rev. B  
Changed OPAM for reference OPA2182.  
Changed R7, R8 value to 1K.

TMUX6111 has high switching resistance, grater than 2000hm, but low leakage current. For low I-V gain switch resistance must be into account.  
For low I-V gains TMUX621X and TMUX721X are most suitable due to low switching resistance, aprox 20hm.  
The Leakage current for this series is 10x greater.  
Rev. C add CE switch ADG601BRTZ to detach probe from OPAM.



I-V converter with fractional scale:  
Lower range from -5 to 5uA

Every scale is made of a RC cell, R set current gain and C gives stability.

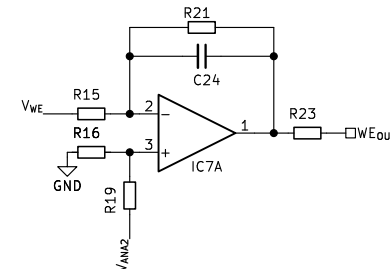
Current gain steps are R14 || (R10 , R11, R12, R13) combination.

R14 = 1M0hm, it gives a gain 1 mV/nA. ADC resolution is :  $3.3 / (2^{12} - 1) = 0.80567\mu V$   
C23 =  $1 / (2 * \pi * Rg * Frq)$ : For Frq = 10KHz lowpass filter C = 16pF  
The OPAM minimum GBW >  $(Ci * C23) / (2 * \pi * R14 * C23^2) = 13667KHz$   
Ci is OPAM input impedance.

The calculus before is made for each I-V switch's RC cell.

TAMPREF output voltage set for zero current.

# Voltage translator for I-V output.



Voltage input range -5V to 5V, output 0V to +3.3V.

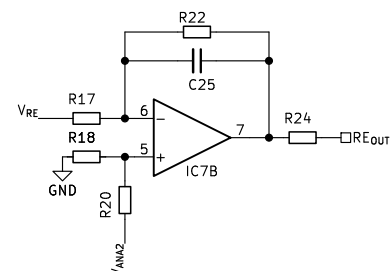
$$G = R21 / R15 = R19 / R16 = 1/3$$

$$V_{ANA2} = 1.65V$$

$$V_{WEout} = V_{ANA2} - G * V_{WE} = 1.65 - (V_{WE} / 3)$$

C24 is for low pass 10KHz filter.

# Voltage translator for VRE output.



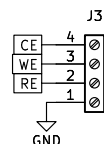
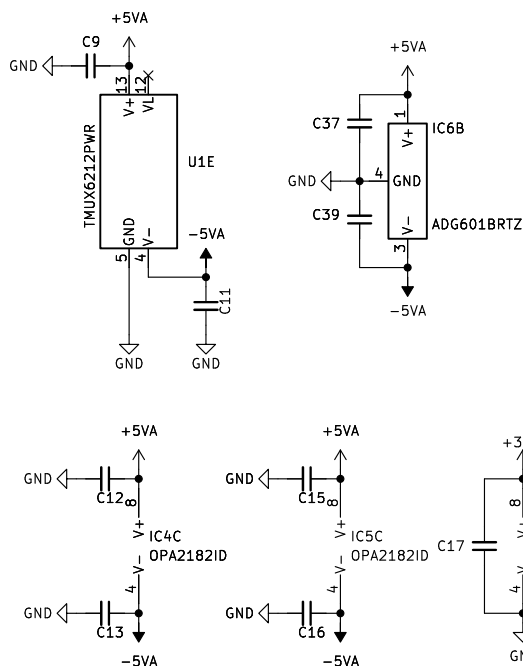
Voltage input range -5V to 5V, output 0V to +3.3V.

$$G = R22 / R17 = R20 / R18 = 1/3$$

$$V_{ANA2} = 1.65V$$

$$V_{REout} = V_{ANA2} - G * V_{RE} = 1.65 - (V_{RE} / 3)$$

C25 is for low pass 10KHz filter.



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