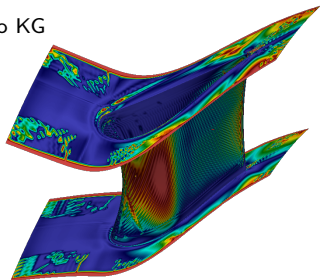
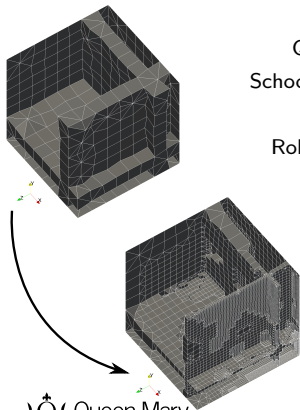


Towards An Output-based Re-meshing for Turbomachinery Applications.

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School of Engineering and Material Science
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Summary

Background, goals and objectives

- Part of AboutFlow project
Adjoint-based optimisation for unsteady and industrial flows.
- This work is an outcome of 3-month secondment at RR.
- Goals and objectives:
 - Implement truncation error and output error estimation procedures in Hydra (RR proprietary code). Use topologically inconsistent geometric multi-grid meshes.
 - Verify implementation using method of manufactured solution (MMS).
 - Perform re-meshing refinement driven by estimated output-based sensor.

Background, goals and objectives

Hydra is a vertex-centred finite volume flow and adjoint solver, using edge-based data structure. Other relevant info for this work:

- 2^{nd} order accurate spatial discretisation (verified using MMS).
- Semi-automatically generated **discrete adjoint solver** (*Tapenade*¹),
- **Geometric multi-grid** solver - reused for truncation error estimation. Multi-grid meshes created using edge-collapsing algorithm.

¹AD tool developed at Inria <http://www-sop.inria.fr/tropics/>

Mesh adaptation - intro

- Error estimation
 - discretisation error (δU) - error in the solution
 - **truncation error** (δR) - imbalance in equations
 - output (objective function) error (δL)
- Adaptation indicator evaluation (scalar, metric)
 - feature-based: uses some form of the discretisation error
 - truncation-based
 - **output-based** - adjoint-weighted truncation error
- Adaptation method/algorithm:
 - **re-meshing**: in this work, use BoxerMesh to re-generate grid respecting regions of the computational domain marked for refinement
 - r-refinement: relocate mesh nodes, keep mesh size constant
 - h-refinement: refine mesh by subdividing cells/edges
 - p-refinement: changing order of discretisation polynomial

Truncation error estimation - intro

Broadly speaking, the truncation error (TE, δR) is the difference between a mathematical model (PDE) and its discrete approximation. TE is commonly estimated using two grids approach, a coarse grid denoted (H) and a fine grid (h).

- In the work of e.g. Venditti and Darmofal [1] [2] [3], Fidkowski [4], TE estimation requires construction of a finer embedded grid h in order to estimate TE on mesh H . The coarse mesh H is used for adaptation.
- As an alternative, for CFD solvers equipped with the **geometric multi-grid**, the truncation error can be estimated in a cheap way without much additional implementation effort. In this approach coarse grid H is used to estimate the error on the fine mesh h . The fine mesh h is used for adaptation. Similar method was presented by Fraysse [5] or Ponsin [6].

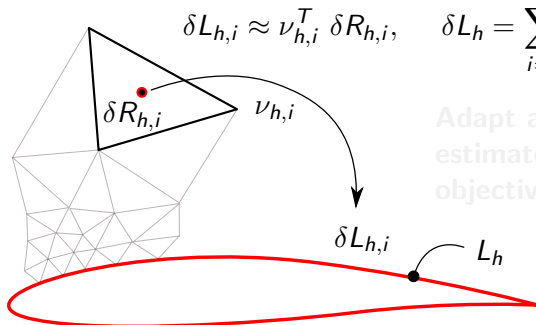
Output error and adjoint variable - intro

Exact objective function (e.g. lift or drag):

$$\tilde{L} = L_h + \delta L_h$$

Error in objective function for discrete space with characteristic size (h) can be estimated as follows (derivation in the conference paper):

$$\delta L_{h,i} \approx \nu_{h,i}^T \delta R_{h,i}, \quad \delta L_h = \sum_{i=1}^N \delta L_{h,i}$$



Adapt a cell only if the estimated error influences the objective function of interest.

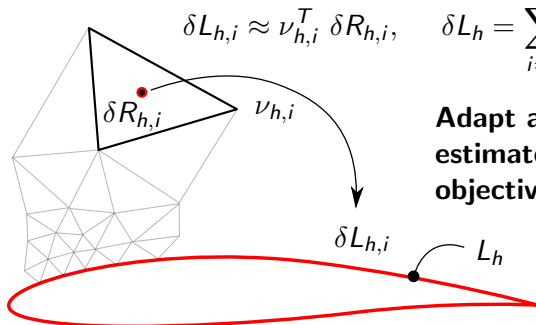
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Error estimation

Introduction

Error estimation

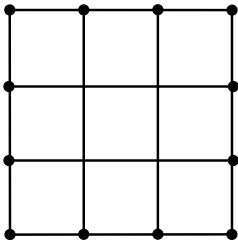
Re-meshing

Results

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Truncation error estimation with multi-grid - procedure

Fine mesh (h)

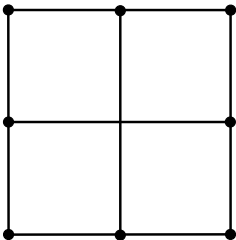


$$U_h \xrightarrow{\mathcal{I}_h^H} U_H^h$$

$$R_h^H \xleftarrow{\mathcal{I}_H^h} R_H(U_H^h)$$

$$\delta R_h = R_h(U_h) - R_h^H$$

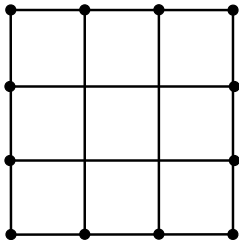
Coarse mesh (H)



1. Solve primal, $R_h(U_h) = 0$
2. Restrict primal solution to the coarse mesh, $U_H^h = \mathcal{I}_h^H U_h$
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Truncation error estimation with multi-grid - procedure

Fine mesh (h)

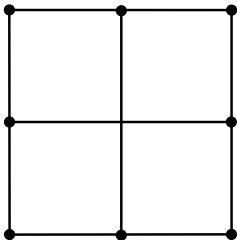


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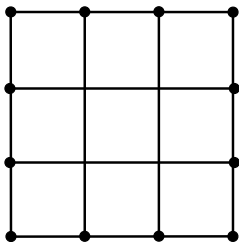
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Truncation error estimation with multi-grid - procedure

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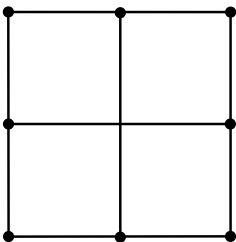


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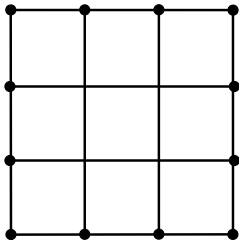
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Truncation error estimation with multi-grid - procedure

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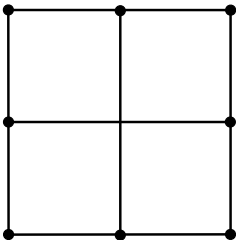


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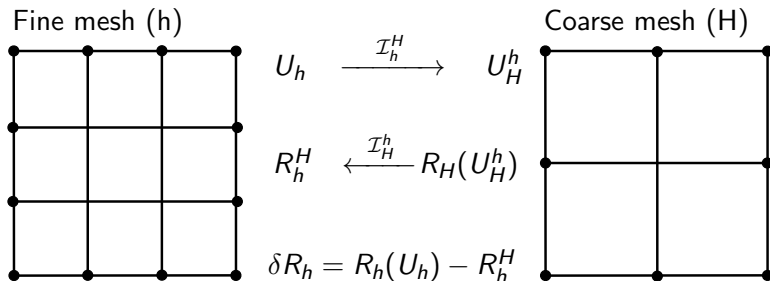
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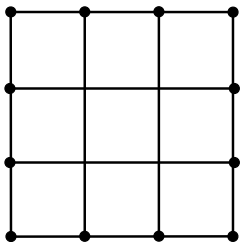
Truncation error estimation with multi-grid - procedure



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Truncation error estimation with multi-grid - procedure

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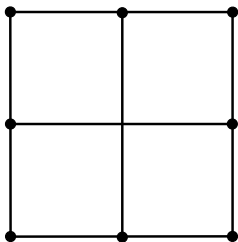


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5. Calculate the truncation error (Note: $R_h(U_h)$ is a remaining fine grid residual, at convergence $R_h(U_h) = 0$).

Adaptation sensor/indicator

Output error estimation:

$$\delta L_h \approx v_h^T \Big|_{U_h} \delta R_h \quad (1)$$

Solve adjoint on fine mesh:

$$\frac{\partial R}{\partial U} \Big|_{U_h} v_h = \frac{\partial L}{\partial U} \Big|_{U_h} \quad (2)$$

Adaptation indicator (adjoint-weighted truncation error):

$$OS_h = \left| \sum_{i_{eqn}=1}^{N_{eqn}} v_{i_{eqn},h}^T \Big|_{U_h} \delta R_{i_{eqn},h} \right| \quad (3)$$

Re-meshing

Introduction

Error estimation

Re-meshing

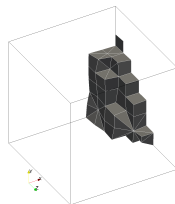
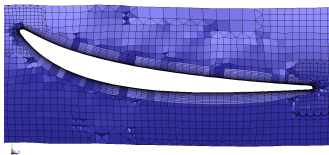
Results

Summary

Basic information

- BoxerMesh² [7] with volume refinement functionality is used for re-meshing. The mesher uses octree cut-cell algorithm to create an initial mesh which is then fitted to the geometry. In the last step a boundary layer is extruded.
- Volume refinement regions are obtained using Paraview. A region is created by group of cells with an adaptation sensor above a specified threshold

Typical Boxer mesh - blade section



Region of cube domain marked for refinement

²<http://www.cambridgeflowsolutions.com/en/products/boxer-mesh/>

Procedure

The procedure for single re-meshing step is as follows:

1. Obtain flow solution (U_h).
2. Estimate truncation error (δR_h).
3. Obtain adjoint solution (ν_h).
4. Evaluate output-based sensor (OS_h).
5. Perform 5 explicit smoothing iterations on obtained sensor (OS_h) to damp unwanted high-frequency modes.
6. Use Paraview to extract mesh region for refinement.
 - Use the 'Threshold' option to mark a region for refinement.
 - Extract surface and output an STL file.
7. Import surface to Boxer and specify new refinement region for octree mesher.
8. Generate a new mesh and re-run the case.

Results

Introduction

Error estimation

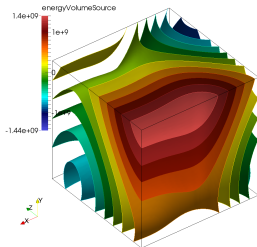
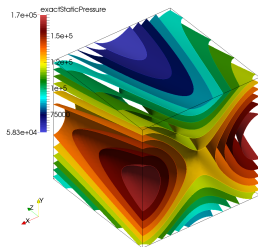
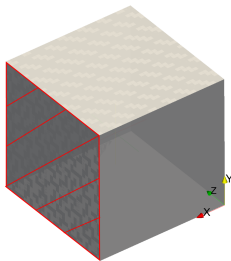
Re-meshing

Results

Summary

Cube test case

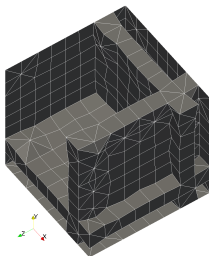
- The simple 3D case with a complex manufactured solution is used for testing - see figures below.
- Compressible, supersonic Euler flow by Roy [8] is used - mix of sine and cosine functions.
- Objective function (L): drag evaluated on the surface marked red on the figure below.



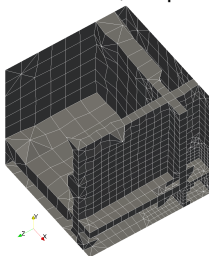
Mesh changes

- Initial mesh: 754 nodes, mixed cell type.
- Two re-meshing steps are performed using an output-based sensor as described in procedure from previous section.
- A non-intuitive and complex refinement structure is obtained.

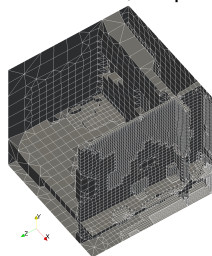
Initial mesh



Re-meshed, step 1



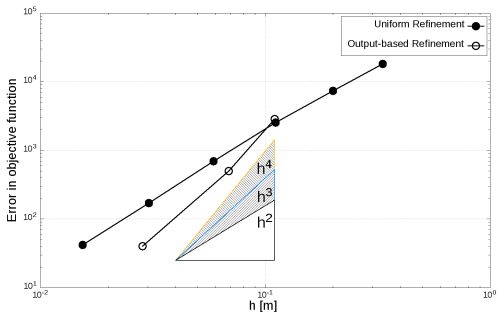
Re-meshed, step 2



Note: coarse grid used for truncation error estimation is not topologically consistent with fine mesh.

Error reduction

- The graph compares drag error reduction wrt characteristic mesh size (h) for uniformly refined vs re-meshed grid.
- Error for a uniformly refined mesh converges with a 2^{nd} slope - as expected for 2^{nd} O discretisation, whereas for a refined grid the error converges with more than an order of magnitude higher slope i.e. between h^3 and h^4 .



Quantitative comparison

Almost and order of magnitude mesh size reduction is obtained for re-meshed grid without affecting cost function accuracy as compared to a uniformly refined case.

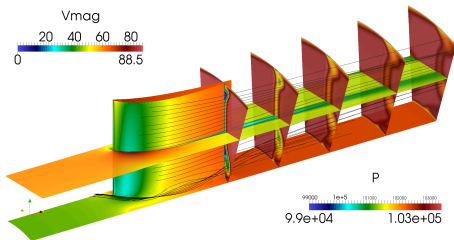
Step	$\delta L/\tilde{L}$ [%]	N_{DoF}^{OS}	N_{DoF}^U	N_{DoF}^{OS} / N_{DoF}^U
0	2.11	754	660	0.87
1	0.37	3082	12100	3.9
2	0.03	43349	335000	7.7

Table: Quantitative comparison of achieved objective accuracy between re-meshed grids using output-based sensor and uniformly refined regular hex meshes. DoF - degrees of freedom, N^{OS} - DoF for output-based refinement, N^U - DoF for corresponding uniformly refined grid.

Note: Uniform refinement was performed for regular all hex mesh, whereas the adaptation was performed on the mixed cell grid type.

TurboLab Stator³ Case from TU Berlin

- The boundary conditions are 42 degrees of swirl angle at the inlet, and outlet static pressure adjusted to keep the mass flow rate at 9.0 kg/s.
- Objective function: pressure loss weighted by mass flow.
- The figure shows static pressure contours on the hub and blade whereas velocity profiles are presented in axial and radial sections. A very strong horseshoe vortex between hub and blade is visualised using streamlines.

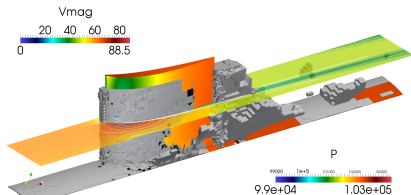


³<http://aboutflow.sems.qmul.ac.uk/events/munich2016/benchmark/testcase3/>

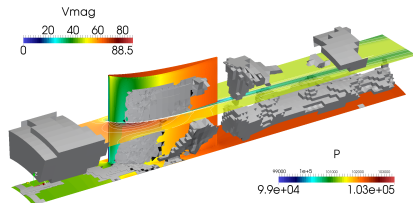
TU Stator

- Comparison of truncation-error-based and output-error-based sensors is presented on the figures (iso-volume).
- Truncation sensor targets for refinement mainly regions of the domain near leading and trailing edges.
- Output sensor marks large cells at the inlet as well as regions of the domain where the strong horseshoe vortex is generated.

Truncation-based sensor



Output-based sensor



Summary

Introduction

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Summary

Conclusion / Future work

- The truncation error estimation methodology using topologically inconsistent fine and coarse meshes was presented. Estimated truncation error was weighted with an adjoint solution to obtain a robust output-based adaptation sensor.
- Re-meshing using Boxer and output-based sensor field was successfully applied to the simple cube test case showing almost an order of magnitude cost function error reduction as compared to the uniformly refined grid.
- More application examples are required including a more realistic turbulent cases e.g. turbine stator in order to investigate how useful is the methodology in practice.
- The key challenge for viscous flows is related to the treatment of boundary layer when performing re-meshing with Boxer.

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