

SHAPE-MOTION RELATIONSHIPS OF CENTERING MICROTUBULE ASTERS

Hirokazu Tanimoto¹, Akatsuki Kimura^{2,3,4,*} and Nicolas Minc^{1,*}

Affiliations: ¹ Institut Jacques Monod, 15 rue H el ene Brion, 75205 Paris cedex 13, France

² Department of Genetics, The Graduate University for Advanced Studies (SOKENDAI) Yata
1111, Mishima, Shizuoka 411-8540, Japan

³ National Institute of Genetics, Yata 1111, Mishima 411-8540, Japan

⁴ Institut Curie, CNRS UMR 144, 26 rue d'Ulm, 75248 Paris Cedex 05, France

* Corresponding authors:

Akatsuki Kimura, akkimura@nig.ac.jp ; Nicolas Minc, nicolas.minc@ijm.fr

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ABSTRACT

Although mechanisms that contribute to microtubule (MT) aster positioning have been extensively studied, still little is known on how asters move inside cells to faithfully target a cellular location. Here, we study sperm aster centration in fertilizing sea urchin eggs, as a stereotypical large-scale aster movement with extreme constraints on centering speed and precision. By tracking 3D aster centration dynamics in eggs with manipulated shapes, we show that aster geometry resulting from MT growth and interaction with cell boundaries dictates aster instantaneous directionality, yielding cell shape-dependent centering trajectories. Aster laser surgery and modelling suggest that dynein-dependent MT cytoplasmic pulling forces that scale to MT length function to convert aster geometry into directionality. In contrast, aster speed remains largely independent on aster size, shape or absolute dynein activity, which suggests it may be predominantly determined by aster growth rate rather than MT force amplitude. These studies begin to define the geometrical principles that control aster movements.

INTRODUCTION

Microtubule (MT) asters are animal cells organizational units made of MTs radiating from a centrosome. They orchestrate fundamental processes such as cell polarity, division and embryogenesis (Gilbert, 2010). Asters can grow, shrink and interact with cytoplasmic and surface elements to produce forces that move them to defined cellular locations. Aster forces are exerted at the level of individual MTs and integrated at the aster scale. Single MTs may generate pushing forces by polymerizing against the cell surface (Brito et al., 2005; Laan et al., 2012; Pavin et al., 2012; Tran et al., 2001; Zhao et al., 2012; Zhu et al., 2010), or exert pulling forces from the movement of minus-end directed motors such as dynein bound to cortical or cytoplasmic anchors (Gonczy et al., 1999; Kimura and Kimura, 2011a; Laan et al., 2012; Pavin et al., 2012; Wuhr et al., 2010; Zhu et al., 2010). While much has been learned on the biology and biophysics of aster positioning problems (Kiyomitsu, 2014; McNally, 2013; Minc and Piel, 2012), still little is known on how asters move inside cells.

The centration of sperm asters represents a ubiquitous and stereotypical aster long-range movement. Sperm asters are nucleated around sperm centriole attached to the male pro-nucleus brought inside eggs at fertilization. These asters rapidly assemble from the side of the egg and continuously grow in size while moving to the cell center (Mitchison et al., 2012). Given the atypical large size of eggs and the short time-scale of early embryonic cell cycles, sperm asters must migrate at high speed on the order of several $\mu\text{m}/\text{min}$ and target the cell center with unusual precision. In general, how aster speed and directionality are established is not well understood.

Here, we use quantitative 3D imaging, aster laser surgery, cell manipulation and modelling to understand how aster motion characteristics are determined in fertilizing sea urchin embryos. We provide direct evidence that aster centration is driven by MT length-dependent pulling forces mediated by dynein in the cytoplasm. Our data suggest that aster directionality is determined by aster shape asymmetries, and that its speed is set by its growth rate.

RESULTS AND DISCUSSION

Sperm asters move persistently to the egg center with a constant velocity

To investigate the centration dynamics of sperm asters in sea urchin eggs, we tracked sperm pronuclei which mark aster centers, in 3D with a short time-interval of 10 sec over a full centration periods typically 15-20 min long. This analysis revealed the existence of 3 main phases of motion: (i) a short 2 min long initial phase following sperm penetration with slow speed and no preferential direction; (ii) a centration phase about 6 min long that accounted for ~ 80% of the travelled distance, and during which the aster migrated with persistent orientation toward the egg center and with a constant speed $V = 5.3 \pm 1.2 \mu\text{m}/\text{min}$ ($n=17$ eggs); and (iii) a slowing down phase when the aster reached close to the center (Fig. 1 A-E; Fig. S1 A-E; Video 1). Thus, sperm asters move in a highly persistent manner with near constant speed and orientation during most of their centration period.

Aster centration involves dynein-dependent MT pulling forces exerted in the cytoplasm

As in other systems (Gonczy et al., 1999; Kimura and Onami, 2005; Kimura and Kimura, 2011a; Wuhr et al., 2010), aster movement depended on MTs and dynein. Depolymerization of MTs with 20 μM nocodazole stopped aster migration within 1 min of drug addition. In contrast, depolymerization of F-actin did not affect centration. Inhibition of dynein with 50 μM ciliobrevin D had similar effects as nocodazole (Fig. 1 F-I; Fig. S1 E-G; Video 2). Ciliobrevin D halted minus-end directed lysosome trafficking and affected spindle bipolarity at metaphase, but did not grossly influence MT organization in the aster; suggesting a specific effect of this drug in this system (Fig. S1 H; S2 A-F; Videos 3 and 4).

Dynein may generate pulling forces on MTs. However, aster MT staining revealed a consistent increased MT density at the aster rear close to the cortex, which could be more in agreement with a pushing-based mechanism (Fig. 2 A; Fig. S2 G). To test this directly, we set up an ablation assay to cut a portion of sperm asters and assess the impact on aster movements. We first ablated MTs on the side of asters parallel to their centration direction. Strikingly, 96% of ablated asters (n=28) drifted away from the ablation site with a drift amplitude varying between 2 to 15 μm . The same assay performed in nocodazole-treated eggs did not cause any significant drift, suggesting this effect is caused by MTs (Fig. 2 B-G; Video 5). Ablation of MTs at the aster front caused asters to move backward in 50% of cases (n=10) or to exhibit a transient stop in the other cases, both followed by a rapid recovery to a normal centration motion (Fig. 2 H-K; Video 6). Together these results suggest that MTs generate pulling forces in all direction and that the imbalance of these forces around asters may determine aster directionality.

Next we investigated if MTs and dynein may pull from the cortex (Grill and Hyman, 2005; Kozlowski et al., 2007) or the cytoplasm (Kimura and Onami, 2005; Kimura and Kimura, 2011a; Wuhr et al., 2010), with time-dependent immunostaining of aster growth. In 96% of stained embryos (n=60) at timing before 7 min post fertilization, when asters are already moving at maximum speed, we did not observe any MTs touching the opposite cortex, suggesting that interactions between MTs and the cortex are not required for aster centration. At timing between 7-10 min, when asters begin to slow down, some MTs started to contact the opposite cortex, and after 10-15 min asters had finished centration and filled the whole cytoplasm (Fig. 2 A; Fig. S2 G). Given that dynein has been reported to locate homogeneously in the cytoplasm in fertilizing

sea urchins (Mohri et al., 1976), we conclude that sperm aster centration may be driven by pulling forces mediated by MTs and dynein in the cytoplasm.

Length-dependent forces convert aster geometry into aster directionality

Dynein forces generated in the cytoplasm may be consistent with a length-dependent pulling model, which posits that the amplitude of pulling force on each MT scales to its length (Hamaguchi and Hiramoto, 1986). This model has been used to account for sperm aster centration: MTs at the aster front are longer than at the back and pull more, allowing to propel the aster forward until length equilibrium is reached at the cell center. Accordingly, a simple 3D simulation which assumes that (i) MT pulling forces positively depend on MT length and (ii) a constant MT growth rate in the cytoplasm and no growth at the cell cortex; could recapitulate aster centration in normal spherical eggs (Fig. 3 A-C; Video 9) (Kimura and Onami, 2005; Longoria and Shubeita, 2013).

To systematically test this hypothesis, we monitored aster centration in defined cell shapes by rapidly pushing freshly fertilized eggs into micro-fabricated wells (Minc et al., 2011). Asters were still able to find the center of shaped eggs, however, they consistently followed a trajectory that highly depended on cell shape and sperm entry point. In axisymmetric situations such as when sperms entered half-way from the side of a rectangle or from the corner of a square, asters migrated straight as expected. However, when sperms entered off-center, asters first migrated perpendicular to the rectangle side, and then exhibited a sharp turn towards a novel direction pointing to the cell center. Similarly, sperm entry close to the corner of elongated rectangle cell

also yielded a concave trajectory, with the position of the turning point depending on shape aspect ratio (Fig. 3 A and B; Video 8). When sperm entry occurred away from the mid-plane, asters exhibited multiple turning points in 3D (Fig. 3 D). Importantly, by altering the boundary conditions in our 3D simulation, we could quantitatively reproduce all experimentally observed aster trajectories including 3D multiple rotations, with no adjusted parameter beside cell shape (Fig. 3 C and E; Video 9). Thus, these results directly demonstrate that asters may interconvert local cell shape sensing into instantaneous directionality through length-dependent MT pulling forces.

Speed determination in growing asters

Although cell shape had a strong influence on aster trajectories, it did not affect aster speed. In all cell shapes assessed, asters migrated with constant speed even when exhibiting turning points in the centration path (Fig. 3 F). Aster speed in shape-manipulated cells was close to the speed measured in round control cells, and did not vary significantly with the length or duration of the centration phase (Fig. 3 G and H). This speed was a little superior but close to the aster growth rate $V_p = 3.8 \mu\text{m}/\text{min}$ estimated from time-dependent immunostaining (Fig. S2 H). In addition, the aster front radius was 5 to 10 μm larger than the rear radius independently of absolute aster size, further indicating that asters may move with a speed similar to their front growth rate (Fig. S2 I). Aster speed also completely recovered in front MT ablation assays (Fig. 2 J and K). Together, these results suggest that aster constant speed is close to aster growth rate and independent of aster size, geometry, or fine-tuned cell-cycle regulation. This finding is unexpected given that the size of asters increases by almost 20-fold during centration (Fig. 2 A). Indeed, a constant centration speed close to aster growth rate has been suggested to be a

signature of MT pushing, rather than pulling (Chambers, 1939; Hamaguchi and Hiramoto, 1980). In what follows, we propose a simple model that explains how length-dependent pulling forces may yield constant aster speed, and exploit this analysis to dissect the generic mechanisms of aster speed determination.

To understand how aster speed is determined, we analyzed a simple 1D model consisting of one MT at the front and one at the rear with respective lengths L_{front} and L_{rear} (Fig. 4 A). Both MTs polymerize with a constant rate V_p in the cytosol and stop polymerization at the cell surface.

Size-dependence of MT pulling force F and drag η are represented by a general scaling form:

$F = aL^\alpha$ and $\eta = bL^\beta$, where a and b are length-independent constants representing dynein density/activity and aster drag, respectively, and α and β are scaling exponents which reflect how forces and drag may scale to MT length (Hays et al., 1982; Minc et al., 2011). Aster speed V is determined by the force balance between MT forces and viscous friction so that:

$$V = \frac{F_{net}}{\eta_{net}} = \frac{a(L_{front}^\alpha - L_{rear}^\alpha)}{b(L_{front}^\beta + L_{rear}^\beta)} \quad (1)$$

By analyzing Eq. 1, we found that a constant speed may arise from either one of the two conditions linking scaling exponents: $\alpha = \beta + 1$ or $\alpha = \beta$ (Materials and methods). This analysis confirmed by 3D simulation suggested that in the first condition $\alpha = \beta + 1$, aster speed may be a positive function of the length *difference* $L_{front} - L_{rear}$ (Eq. 16) (Fig. S3). Initially $V < V_p$, so that front MTs grow faster than at the rear. As a consequence both $L_{front} - L_{rear}$ and V continuously increase. When V reaches V_p , front and rear MTs grow at the same rate V_p and

thus $L_{front} - L_{rear}$ and V become constant, which can be pictured as a treadmilling in MT length front-rear differences. Importantly, in this condition the parameter a/b negatively influences the time τ needed to reach constant speed, but only has a minor impact on the constant speed value (Fig. 4 B and C; Fig. S3). In other words, MT/dynein force amplitude do not affect stationary aster speed, which is determined by aster growth rate. The speed determination in the second condition $\alpha = \beta$ is conceptually different. Aster speed is now determined by the length *ratio* L_{front}/L_{rear} , and the constant speed positively depend on a/b and may take any value between 0 and V_p . (Eq 19) (Fig. 4 D; Fig. S3). Importantly, both conditions give similar centration dynamics in the high force limit: a short acceleration phase and a speed close to aster growth rate, as observed in the experiments. Thus, this analysis suggests that the forces driving aster centration in this system may be relatively high.

Aster speed is largely independent of absolute dynein activity

These two scaling conditions give different centration dynamics for smaller MT/dynein forces. In simulations, a reduction of the force amplitude after asters have reached constant speed $V = V_p$ yielded to a transient aster slowdown followed by a complete speed recovery in the condition $\alpha = \beta + 1$ (Fig. 4 E). In contrast, in the condition $\alpha = \beta$ aster speed remained smaller and did not recover to V_p (Fig. 4 F). To test these predictions experimentally, we rapidly rinsed eggs 5 min after sperm entry with different doses of ciliobrevin D (Fig. S3 E). We found that a concentration of 10 μ M consistently caused asters to stop transiently for a period of ~ 2 min, after which they recovered their initial speed (Fig. 4 G-I). This behavior was observed in 92% of the eggs treated with ciliobrevin D, but only in 13% of eggs rinsed with DMSO. This suggests that

aster speed determination in this system may satisfy the condition $\alpha = \beta + 1$, and is mostly determined by aster growth rate and weakly influenced by the absolute amplitude of MT pulling forces.

Conclusions

In sum, we here systematically test and validate a quantitative model based on length-dependent MT pulling forces as a pure geometrical mechanism determining centering trajectories and speeds of sperm asters. Inhibitor assays, laser ablation and time-lapse immunostaining all provide novel additional evidence supporting that aster centration is driven by dynein pulling directly in the cytoplasm, not at the cortex. Our data on centration trajectories in shape manipulated eggs disentangle aster motion from the polarity set by sperm entry, and demonstrates that asters are able to probe their local geometrical environment to faithfully target the cell center (Fig. 5).

We suggest that sperm asters in sea urchin migrate in a high-force regime. Signatures of this regime are a near symmetric aster shape and a constant speed. Sperm asters in *Xenopus* are also mostly symmetric and move with constant speed (Stewart-Savage and Grey, 1982; Wuhr et al., 2009; Wuhr et al., 2010). In contrast, asters in *C. elegans* exhibit a large asymmetry and long acceleration/deceleration phases, likely reflecting a relatively low-force regime (Kimura and Onami, 2005). Thus, we expect our analysis to be valuable in unifying qualitatively different aster dynamics in various systems.

Our results further constrain the functional form of aster force-size and drag-size dependencies. The relationship $\alpha = \beta + 1$ implies that aster force grows faster than aster drag with its size. In addition, aster trajectories appear to be influenced by the centripetal movement of female pronuclei on the aster, only when the aster is very small (Fig. S2 L and M) (Chambers, 1939; Hamaguchi and Hiramoto, 1980). This suggests that the drag of small asters may be smaller than the drag of large asters, so that $\beta > 0$ and hence $\alpha > 1$; consistent with previous studies suggesting non-linearity in length-dependent pulling forces with $\alpha \sim 3-5$ (Minc et al., 2011). A tentative speculation would be to assume that astral MT forces scale to a local volume around MTs (Kimura and Kimura, 2011b; Minc et al., 2011), so that $\alpha = 3$ and $\beta = 2$; which would imply that aster drag may scale to a local cone-like surface surrounding MTs. Interactions of endomembrane elements such as the ER and other vesicles all along astral MTs could account for such non-linear MT-cytoplasm frictional interactions (Terasaki and Jaffe, 1991). Future work analyzing the relationships between force, motion and geometry of asters *in vivo* will be instrumental to understand further the core spatial organization principles of cells and embryos.

MATERIALS AND METHODS

Sea urchin eggs

Purple sea urchin *Paracentrotus lividus* were obtained from L'Oursine de Ré or the Roscoff Marine station and maintained in large aquarium for several weeks. The aquariums were filled with artificial sea water (ASW) (Instant Ocean, Reef Crystals) and kept at 16°C, with constant oxygenation and water filtering. The ASW was filtered using a 80 µm Nitex mesh (Sefar) and used for all experiments. Gametes were collected by intracoelomic injection of 0.5 M KCl. Sperms were kept at 4°C and used within 1 week. Eggs were rinsed twice, kept at 16°C and used on the day of collection. For live imaging, except for shape manipulation assays, the jelly coat of unfertilized eggs was removed by passing them three times through a 80 µm Nitex mesh, to facilitate egg adhesion on glass dishes.

Microscopy

Live imaging and laser ablation were performed on a spinning-disk confocal fluorescent microscope (Nikon Ti-Eclipse combined with Yokogawa CSU-X1 spinning-head and Hamamatsu EM-CCD camera) equipped with a 40x oil immersion objective (Nikon Plan Fluor, NA 1.3). The microscope and motorized stage were operated by MetaMorph (Molecular Devices). The microscopy room was air-conditioned and kept at 15~17 degree throughout the experiments. Microtubule immunostaining images were taken with a scanning confocal microscope (Zeiss LSM 780). Either coverslips (VWR, 24*50 mm, thickness No. 1) or glass-bottom dish (MatTek, 50 mm glass bottom dish, thickness No. 1.5) were used for microscopy.

Aster 3D tracking

The male pronucleus at the aster center was stained with Hoechst 33342 (Sigma) at a final concentration of 1 $\mu\text{g/ml}$. The dye was added prior to fertilization and left in the sea water throughout the experiment. Aster 3D centration was monitored by taking time-lapse confocal stack (Fig. S1 A). The acquisition was started just after sperm head penetration (distance between cell cortex and sperm head center smaller than 5 μm) for the experiments presented in Fig. 1, 2 and 4, and at around 4 min after fertilization for the cell-shape manipulation experiments presented in Fig. 3. The tracking period was at least 15 min long to ensure that asters finished centration. Both illumination intensity and exposure time were adjusted to minimize phototoxicity. 15 images with a slice interval of 3 μm were taken at each time-points. The Z stack covered one hemisphere of the eggs and was thus sufficient to monitor the whole centration. Each z-stack took ~8 sec of acquisition and were spaced with an interval of 10 sec or 30 sec. All image analysis were done with a custom code written in Matlab (Mathworks). Aster position in Z was determined by detecting the plane in which the male pro-nucleus was in focus. The XY position in the selected image was then automatically detected. The XY precision was calibrated with immobile sperm heads stuck on coverslip surface and was close to 1 μm . The Z precision was set by the spacing between Z slices, and was around 3 μm . This Z resolution was sufficient to confirm that aster centration trajectory was straight not only in XY but also in XZ and YZ (Fig. S1 B). Aster Z position was smoothed using a cubic spline method. In a subset of cases, small movements of the observation chamber and/or eggs were observed, and were subtracted from the aster motion. Centration dynamics was not affected by the imaging, and in general the first division timing of imaged eggs was within less than 10% different as non-imaged control eggs from the same batch.

Data analysis

Aster travelling distance at time t was defined as $|\vec{X}(t) - \vec{X}(0)|$ where $\vec{X}(t)$ is the aster 3D position at time t , $\vec{X}(0)$ is the initial position, and $|\cdot|$ denotes the norm. For asters with multiple rotations, the trajectory was split into linear paths between rotations, and the travelling distance was defined as the summation of the passed paths and the distance from the last rotating position. For chamber assays, the time delay between fertilization and beginning of the time-lapse was measured for each experiments, and the onset of the travelling distance was defined as the aster speed multiplied by the time delay. The uniform motion phase (phase 2) was manually defined as the linear region in the distance-time curve, and aster constant speed (referred simply as aster speed) was determined by a linear fitting of the curve. Aster instantaneous velocity was defined as $\vec{V}(t) = (\vec{X}(t + \tau_0) - \vec{X}(t)) / \tau_0$ where τ_0 was set to 30 sec. τ_0 is set to 1 min for quantifications of laser ablation experiments, where the induced transient effect has a time-scale of around 2 min. Time-average of aster velocity in phase 2 gave the similar aster constant speed determined with the distant-time curve. In plane orientation of asters was defined as the angle formed by aster in-plane velocity vector and the in-plane line connecting aster initial position and the cell center. The mean squared displacement (MSD) was defined as

$$MSD(\tau_0) = \left\langle \left| \vec{X}(t + \tau_0) - \vec{X}(t) \right|^2 \right\rangle_t, \text{ where } \langle \cdot \rangle_t \text{ denotes time average. Data of 7 min length was}$$

used for MSD analysis, and time 0 is set to be $t=0$ for control, and 2 min after drug addition for inhibitor assays (Fig. S1 E).

Laser ablation

Aster local laser ablation was conducted using a high-power pulsed 355 nm UV laser system (iPulse, Roper Scientific) and a 40x 1.3 NA Plan-Fluor oil objective. The system was operated by the iLas2 software (Roper Scientific). Different ablation conditions were assayed to optimize the laser irradiation protocol. The ablated asters were immediately fixed in situ and the results were judged based on MT immunostaining. The protocol described hereafter was found to be sufficient to significantly reduce both length and density of astral MTs at the ablation line, without damaging the egg (Fig. 2C). Asters migrating in the equatorial plane were selected, and a 25 μm line region situated at 15 μm away from the aster center was irradiated. The irradiated line was parallel to the previous migrating direction, for side-ablation assays, and perpendicular for front-ablation assays. The line consisted of three 350 nm beam lines spaced at an interval of 1 μm . Each single laser irradiation took 7 ms and was iterated 400 times. The ablation was done at three different heights; at the aster center and 5 μm above and below. The total time needed to complete ablation was around 10 sec. For ablation assays, asters migrating mostly in plane were selected and only in plane motion was analyzed.

Pharmacological inhibitors

Inhibitor assays were performed in small glass chambers which allowed a rapid exchange of solutions. The chamber was composed of two clean coverslips and a spacer of 100~150 μm thickness. Using a fluorescence solution, we confirmed that solution exchange was completed within seconds in this chamber. The bottom coverslip was coated with 1% protamine (Sigma), rinsed and dried before chamber assembly. Unfertilized eggs were introduced in chambers and fertilized in situ by introducing a diluted sperm solution. Inhibitors were applied at 3 min post

sperm entry in the experiments presented in Fig. 1 F-I, and at 5 min in the experiments presented in Fig. 4 G-I. All inhibitors were prepared in 100X stock aliquots in DMSO. Latrunculin B (Sigma) was used at a final concentration of 20 μ M. Nocodazole (Sigma) was used at a final concentration at 20 μ M. Ciliobrevin D (Millipore) was used at various final concentrations. Ciliobrevin D inactive analogue (a gift from Dr. Kapoor and Dr. Chen) was used at a final concentration of 50 μ M.

PDMS chamber and operation

Two types of PDMS systems were used in this study: (1) slabs containing egg-sized microwells for cell shape manipulation; (2) flat and wide perfusion channel for immunostaining assays. General procedures for soft-lithography and PDMS molding are described elsewhere (Chang et al., 2014). The PDMS slab used for cell shape manipulation contained typically thousands of rectangular microwells with various aspect ratios. The depth of microwells was around 55 μ m, and the aspect ratio was varied in order to keep the microwell volume roughly equal to the egg volume. The aspect ratio was varied from 1:1 (91*91 μ m) to 4:1 (182*45 μ m). PDMS slabs were activated with a plasma cleaner (Harrick, PDC-002) few minutes before use and covered with ASW. Eggs were fertilized in a falcon tube and a 40 μ L of dense egg solution was placed on a clean cover slip and the PDMS slab was gently applied from the top. The slab was moved down further by removing excess ASW between the cover slip and the PDMS. This procedure took around 3-5 min from sperm addition to the beginning of image acquisitions. The eggs shaped by this method developed through multiple cell divisions in the microwells. For *in situ* immunostaining of eggs in chambers, the PDMS slab was first pierced with a hole at the center to allow for fluid exchange, in a similar manner as described before (Minc et al., 2011). To

flatten eggs in a reproducible manner and force sperm aster centration to occur in 2D in round eggs, we used other custom-made PDMS channels. The channel height was around 70-75 μm , about 10% smaller than the egg diameter. The channel dimension was 25 mm*8 mm. The two extremities of the channels were pierced with holes. Both PDMS slab and cover slip were washed with acetone, isopropanol and water and subsequently air-dried. A drop of 25 μL of unfertilized egg solution was placed on the PDMS channel, and covered with a large cover slip. Edges of the cover slip were pushed onto the PDMS to seal the channel. Eggs were then fertilized *in situ* by introducing sperm solution from the reservoir hole; and fixed and stained through liquid exchange when relevant.

Immunostaining

Immunostaining was performed using similar procedures as previously (Foe and von Dassow, 2008; Minc et al., 2011). The fixation was performed either in bulk (Fig. 2 A, S1 F), in the flat PDMS perfusion chamber (Fig. 2 C, Fig. S2 G), or in microwells (Fig. S2 J). Fixations in chamber or microwells were done under the microscope to ensure that eggs do not move or change shape during liquid exchange. All experiments followed similar chemicals and timing. Eggs were first fixed for 70 min in 100 mM Hepes (pH 6.9), 50 mM EGTA, 10 mM MgSO_4 , 2% formaldehyde, 0.2% glutaraldehyde, 0.2% Triton X-100, and 400 mM Glucose. Eggs were then rinsed 3X 10 min in PBT and 1X in PBS and placed in 0.1% NaBH_4 in PBS made fresh for 30 min. Eggs were rinsed again with PBS and PBT and blocked in PBT + 5% Goat Serum and 0.1% BSA for 30 min. For MT staining, cells were incubated for 48 hours with a primary anti- α -tubulin antibody, clone DM 1A (Sigma) at 1/8000, rinsed twice in PBS and then for 4 hours with fluorophore-conjugated anti-mouse secondary antibody (Sigma) at 1/750. Aster staining after

laser ablation was done in a PDMS flow chamber, and the fixative was introduced 10 sec after ablation.

Analysis of aster shape

Aster shape was analyzed based on tubulin immunostaining images obtained by confocal microscopy. Live imaging of fluorescently-labeled MTs provided qualitatively similar results (Video 6). The immunostaining was performed in flat flow chambers described above, to force asters to move in the equatorial plane. Aster centration was monitored live, and eggs were fixed *in situ*. Samples in which aster center was largely deviating from the cell equator were discarded from the analysis. Stained eggs were imaged with a point confocal with a slice interval of 0.5 μm and 10 to 15 images around the aster center, and projected to obtain the images presented throughout the manuscript. Aster rear radius was defined as the distance between the male pronucleus and the closest cell cortex, and the front radius was defined as the average MT length at the aster front. More than 10 MTs were analyzed for each asters.

Injection

For the experiments involving live imaging of labeled MTs, HiLyte 488-conjugated tubulin (Cytoskeleton) was microinjected into unfertilized eggs at a final concentration of 1 mg/mL, following previous standard injection protocols (Strickland et al., 2005).

Vesicles tracking

To visualize moving lysosomes, LysoTracker (Molecular Probes) was added at final concentration of 1/10000, 10 min before fertilization. The time-lapse images were analyzed using the Image J plugin Particle Tracker.

Theoretical analysis of the 1D model for aster centration

1D model for MT aster migration

We consider a one dimensional microtubule aster with one MT at the front and one at the back (Fig. 4 A). The two MTs polymerize with a constant rate V_p in the cytoplasm and stop polymerizing when touching the cell cortex. Length-dependencies of each MT force F and drag η are phenomenologically modeled with a general scaling form, so that:

$$F = aL^\alpha, \quad (2)$$

$$\eta = bL^\beta, \quad (3)$$

where L denotes MT length, and a and b are coefficients corresponding to dynein density/activity and MT hydrodynamic friction, respectively. α is a scaling exponent which may represent the nature of dynein-MT interaction (Kimura and Kimura, 2014; Minc et al., 2011). For instance: a homogeneous distribution of dynein motors along MTs would be represented by $\alpha = 1$, while a diffusion-limited dynein-MT interaction in the cytoplasm with limited amount of dynein may correspond to $\alpha = 3$. β is a scaling exponent which characterizes the frictional interaction between aster components and their surrounding environment. For instance if the main contribution to aster drag comes from elements with fixed size such as pronuclei, the aster drag is not expected to depend on aster size (or MT length), so that $\beta = 0$ (Kimura and Onami,

2005; Kimura and Onami, 2007; Shinar et al., 2011) . If the drag of each MTs has a dominant contribution to the overall aster drag, then β may be close to 1 (Longoria and Shubeita, 2013).

Given the polarity of MTs, the net force F_{net} and net resistance η_{net} can be written as:

$$F_{net} = a(L_{front}^{\alpha} - L_{rear}^{\alpha}), \quad (4)$$

$$\eta_{net} = b(L_{front}^{\beta} + L_{rear}^{\beta}). \quad (5)$$

Dynein/MTs forces must be balanced by the frictional force experienced by the aster, and thus aster speed V is determined by its instantaneous shape:

$$V = \frac{F_{net}}{\eta_{net}} = \frac{a L_{front}^{\alpha} - L_{rear}^{\alpha}}{b L_{front}^{\beta} + L_{rear}^{\beta}}. \quad (6)$$

Necessary conditions for aster motion at constant speed

We consider an aster migrating with a constant speed $V = V_C$. Since we assume that free MTs polymerize with a constant rate V_p , the length of the front MT L_{front} is proportional to the time t (aster starts growing at $t=0$), so that:

$$L_{front} = V_p t. \quad (7)$$

The rear MT can freely polymerize with a rate V_p if $V_C \geq V_p$, however its growth is hindered by the cell boundary if $V_C < V_p$. Therefore the length of the rear MT L_{rear} is given by:

$$L_{rear} = \begin{cases} V_p (t - T_0) + L_0 & (V_C \geq V_p) \\ V_C (t - T_0) + L_0 & (V_C < V_p) \end{cases} \quad (8)$$

with L_0 being the rear MT length when aster begins to move at a constant speed. From Eq. 8,

V_C and V_p must then satisfy one of the two relationships below,

(i) $V_C \geq V_p$

$$V_C = \frac{a (V_p t)^\alpha - (V_p t - \delta L)^\alpha}{b (V_p t)^\beta + (V_p t - \delta L)^\beta}. \quad (9)$$

With $\delta L = L_0 - V_p T_0$;

(ii) $V_C < V_p$

$$V_C = \frac{a (V_p t)^\alpha - (V_C t - \delta L)^\alpha}{b (V_p t)^\beta + (V_C t - \delta L)^\beta}. \quad (10)$$

With $\delta L = L_0 - V_C T_0$;

For sufficiently large times, Eqs. 9 and 10 become:

(i) $V_C \geq V_p$

$$V_C \sim t^{\alpha-\beta-1} \quad (11)$$

(ii) $V_C < V_p$

$$V_C \sim t^{\alpha-\beta} \quad (12)$$

Therefore, an aster constant speed motion may be accounted for by either one of these two necessary conditions: $\alpha = \beta + 1$ or $\alpha = \beta$. The first condition encompass a simplified version of a previous stochastic model, with $\alpha = 1$ (average force proportional to MT length) and $\beta = 0$

(constant aster drag) (Kimura and Onami, 2005; Kimura and Onami, 2007). A particular case of the second condition is close to another proposed model incorporating a linear scalable drag so that $\alpha = \beta = 1$ (Longoria and Shubeita, 2013). Below we separately analyze these two conditions to see if they are indeed sufficient to account for constant speed, and to understand how speed is influenced by different parameters.

Analysis 1: $\alpha = \beta + 1$

A simple analytical solution of the 1D model satisfying the scaling condition $\alpha = \beta + 1$ can be obtained in the simplest situation: $(\alpha, \beta) = (1, 0)$ (force proportional to MT length, constant drag coefficient). As we will see below, the aster speed is bounded by the growth rate V_p , so that the aster position X is equal to L_{rear} . Putting Eq. 7 into Eq. 6, the time evolution of aster position is given by:

$$V = \frac{dX}{dt} = \frac{a}{b}(L_{front} - L_{rear}) = \frac{a}{b}(V_p t - X), \quad (13)$$

which yields:

$$V = V_p(1 - e^{-t/\tau}), \quad (14)$$

$$X = V_p t + V_p \tau(e^{-t/\tau} - 1), \quad (15)$$

with $\tau \equiv b/a$. These equations show that aster speed approaches to its growth rate in an exponential manner. An interesting outcome from this result is that the final constant aster speed is determined only by the aster growth rate, and is independent on the force and drag coefficients

a and b . These mechanical parameters however determine the time scale τ needed to reach constant speed.

Simple analytical solution are not available for higher values of the exponents, however for sufficient long time the leading term from Eq. 6, with $\alpha = \beta + 1$, is:

$$V = \frac{a\alpha}{2b}(L_{front} - L_{rear}) \quad (16)$$

This indicates that passed a sufficient time, aster speed in this condition is solely determined by the front-rear length difference $L_{front} - L_{rear}$. Initially both aster speed and the length difference are close to 0. $L_{front} - L_{rear}$ increases in time while aster speed V is smaller than V_p . Since aster speed is a positive function of the length difference, the aster accelerates until the speed reaches V_p . After aster speed has reached V_p , the length difference remains constant (a process similar to a length difference treadmill) and consequently the speed keeps the same value. Therefore, in this condition the aster constant speed V_C is always equal to V_p .

Analysis 2: $\alpha = \beta$

Next we investigate the second condition $\alpha = \beta$. Taking the leading terms in Eq. 10 for large t , we obtain:

$$V_C = \frac{a V_p^\alpha - V_C^\alpha}{b V_p^\alpha + V_C^\alpha}, \quad (17)$$

where $V_C < V_p$. For $\alpha = \beta = 1$, Eq. 17 can be solved and yields:

$$2V_C = -\left(V_p + \frac{a}{b}\right) + \sqrt{\left(V_p + \frac{a}{b}\right)^2 + 4V_p \frac{a}{b}} \quad (18)$$

Equation 18 indicates that V_C can take any value between 0 and V_p and depends strongly on a/b . V_C is a positive function of a/b , and increases linearly with a/b for small a/b and then gradually approach V_p for large a/b .

Speed determination in higher values of the exponents may be qualitatively understood as follows. Equation 17 can be rewritten as:

$$V_C = \frac{a \left(V_p/V_C\right)^\alpha - 1}{b \left(V_p/V_C\right)^\alpha + 1} \quad (19)$$

In addition, $L_{front} = V_p t$, and for large t , $L_{rear} \sim V_C t$. Therefore, in this condition aster speed is determined by the length ratio between front and rear MTs:

$$V_C = \frac{a \left(L_{front}/L_{rear}\right)^\alpha - 1}{b \left(L_{front}/L_{rear}\right)^\alpha + 1} \quad (20)$$

This analysis highlights the conceptual difference in aster constant speed determination in the two scaling conditions. If $\alpha = \beta + 1$, aster speed is determined by the length difference $L_{front} - L_{rear}$, and by the length ratio L_{front}/L_{rear} in the condition $\alpha = \beta$. When speed is determined by the length difference, the final constant speed is always V_p . However, when it is determined by the length ratio, this speed may reach any value between 0 and V_p . The initial aster speed is small and $L_{front}/L_{rear} \sim 1$. Aster then continues accelerating and L_{front}/L_{rear} increases until aster speed reaches V_C determined by Eq. 19. After the aster speed has reached

V_C , front MTs polymerize with V_p whereas rear MT polymerizes with V_C , thus the length ratio $L_{front}/L_{rear} = V_p/V_C$ remains constant. Therefore aster constant speed in this condition can take any value between 0 and V_p , and is strongly influenced by the force parameters a and b .

Numerical 3D simulation for aster centration

We performed 3D numerical simulation to confirm the conclusions from the 1D model analysis. In the simulation, astral MTs are nucleated from a single point centrosome and evenly distributed around the centrosome with a constant angle difference. The number of total MTs, did not influence the simulation results and was set to be 10,000. Initial MT length was set to 0. MTs grew with a constant rate V_p and stopped growing when touching the cell cortex. The contributions of individual MTs to aster force and drag are assumed to be additive. Therefore the aster velocity \vec{V} must satisfy the force balance as:

$$\vec{V} = \frac{\vec{F}_{net}}{\eta_{net}} = \frac{a \sum_i L_i^\alpha \vec{e}_i}{b \sum_i L_i^\beta}, \quad (21)$$

where i is an index corresponding to each MTs and \vec{e} is a unit vector pointing in the direction of MT plus end from the centrosome.

The simulation has four input parameters: MT growth rate V_p , the ratio between force and drag coefficients a/b , and scaling exponents α and β . We fixed V_p at 4 $\mu\text{m}/\text{min}$ (similar to the aster growth rate determined from time-lapse staining of 3.8 $\mu\text{m}/\text{min}$), and varied other parameters as

described below. For the simulations in Fig. 3, we used $(\alpha, \beta) = (1, 0)$, and the force parameter was determined so that the time scale of aster acceleration is the same as the typical duration of T_1 (around 2 min, Fig. 1 C). The aster shape and position were updated every 0.1 sec based on the aster growth rule and Eq. 21. Several time-steps for the simulations were tested, and did not influence the results. Simulations were performed using Matlab (Mathworks).

As inputs, the simulation requires a defined cell geometry and an initial centrosome position. To simulate the centration in normal round eggs, we modeled the egg as a sphere of 90 μm diameter. To simulate cell shape manipulation experiments, the chamber shape was used as a good approximation of actual egg shape and the initial centrosome position was set to be 0.5 μm inside the egg at the site of sperm entry. The height of the chamber was taken as 55 μm as in the experiments, and the initial Z position of the centrosome was the mid-plane, except for analyses like in Fig. 3 G, in which the centrosome started from the bottom surface.

We first performed 3D simulations to test the general condition $\alpha = \beta + 1$, for $(\alpha, \beta) = (1, 0)$ for which analytical solutions are available (Eqs. 14 and 15), and systematically changed the force parameter a/b . The simulations were done for normal spherical cell geometries. The results fully agreed with the outcome of the 1D analytical solution (Fig. S3 A). The aster speed in this simulation approached to V_p in an exponential manner. The time required to establish the final constant speed was negatively correlated with the force amplitudes. We however noted that aster speed slightly exceeded V_p for very high forces, plausibly because of 3D effects. Very similar results were obtained for higher values of the exponents $(\alpha, \beta) = (2, 1)$ and $(3, 2)$ (Fig. S3 A).

Similar validations of the 1D analysis, from 3D simulation were also obtained for the general conditions $\alpha = \beta$. Asters exhibited a constant speed motion with speeds that depended on the force amplitude, a/b . The constant speed was an increasing function of a/b , and was bounded by V_p for high forces. Aster speed also slightly exceeded V_p for very high forces in this scaling condition as well (Fig. S3 B).

To confirm the conceptual difference in speed determinants between the two scaling conditions, we computed aster instantaneous speed at each step of the simulation and plotted it against $L_{front} - L_{rear}$ or L_{front}/L_{rear} for one single simulation run; and represented the result using a density color plots (Fig. S4 C and D). Here L_{front} was defined as the length of the longest MT and L_{rear} as the shortest one. For $\alpha = \beta + 1$, aster speed linearly depended on $L_{front} - L_{rear}$ as expected (Fig. S3 C, left). In contrast aster speed was not uniquely determined by $L_{front} - L_{rear}$ for $\alpha = \beta$ (Fig. S3 D, left). By contrast in the condition $\alpha = \beta$, speed was independent on $L_{front} - L_{rear}$ but exhibited a single localized peak in the density plot of aster speed against L_{front}/L_{rear} , indicating that aster speed is primarily determined by L_{front}/L_{rear} in this condition (Fig. S3 D, right).

Finally, we performed all the above simulations in a 3D rectangular geometry which yielded similar conclusions (Fig. S3 E-H).

Online supplemental material

The supplementary material contains 3 supplementary figures and figure legends, and 10 supplementary videos and video legends. Figure S1 explains 3D imaging method and provides additional quantification of aster centration dynamics, and control experiments of all inhibitor assays presented in Fig 1. Figure S2 provides control experiments of ciliobrevin D, additional time-lapse images of MT aster growth and quantification, dose-dependent effects of ciliobrevin D on aster centration speed, and experiments on the influence of female pronucleus movements on aster motion. Figure S3 includes extended 3D simulation results for general scaling exponents and cell geometry. Video 1 is a time-lapse of MT aster centration in normal condition (corresponding to Fig. 1 A). Video 2 is a time-lapse of aster centration in the presence of various inhibitors (Fig. 1 F and G). Video 3 and 4 are lysosome live imaging in 1% DMSO and 50 μ M ciliobrevin D, respectively (Fig. S1 G-J). Video 5 and 6 are time-lapse of the motions of laser ablated MT aster (Video 5: side ablation, 6: front ablation) (Fig. 2 D and E, Fig. 2 J). Video 7 is a live imaging of a centering MT aster visualized by injecting fluorescent tubulin. Video 8 is a time-lapse of aster centration in a rectangular shaped egg (Fig. 3 A, fifth row). Video 9 is a 3D simulation of aster centration in normal spherical cell geometry and in a rectangular cell geometry. Video 10 is a time-lapse of aster centration in the presence of low dose ciliobrevin D (Fig. 4 G and H).

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FIGURE LEGENDS

Figure 1. Sperm asters move to the egg center with persistent directionality and constant speed, in a MT and Dynein-dependent manner.

(A) Time-lapse confocal images superimposed with DIC of a male pro-nucleus (white arrowhead) at the center of a sperm MT aster. (B) 3D trajectories of 10 individual asters, and enlarged trajectory of an aster that migrates mostly in-plane. Time is color coded. The centration is subdivided into three phases: an initial penetration phase (P), a rapid centration phase with straight path and constant speed (C), and a final slowing down phase (S). (C) Aster travelling distance and orientation towards the cell center as a function of time, for the sample enlarged in (B). T_1 and T_2 denote the beginning and end of the rapid centration phase. (D and E) Distance- and orientation- time plots of the centration phase of 10 individual asters. Red line; mean, gray section; standard deviation (S.D.). The broken line is a guide for the eyes. (F) Time-lapse images of eggs treated with different inhibitors 3 min after sperm entry. (G) 3D trajectories corresponding to the eggs and conditions from (F). Time is color coded as in (B). (H) Mean aster travelling distance as a function of time with various inhibitors. The gray region indicates the period during which inhibitors are present. Red: DMSO (n=5), blue: 20 μ M Latrunculin B (n=5), green: 20 μ M nocodazole (n=7), purple: 50 μ M ciliobrevin D non active analogue (n=6), orange: 50 μ M ciliobrevin D (n=6). (I) Aster speed computed using distance-time curve between 5 and 7 min. Error bars represent S.D. Scale bars are 50 μ m unless otherwise indicated.

Figure 2. Aster centration is driven by MT-pulling forces in the cytoplasm.

(A) Time-dependent immunostaining of centering MT asters (MT; green, DNA; red). The indicated time is taken in reference with sperm entry by accounting for a mean 3 min delay between sperm addition and sperm entry. (B-G) Aster side photo-ablation. (B) Centering sperm MT asters are ablated parallel to the centration trajectory. A drift in the trajectory towards (away from) the ablation line suggest that MTs are pushing (pulling). (C) In situ MT aster immunostaining performed immediately after laser ablation. The red broken line indicates the line area along which the laser beam was applied. (D and F) Time-lapse (D) and time-projection (E) of a centering aster ablated as indicated. Time 0 is defined as the time when ablation is performed. White arrowhead; male pro-nucleus. (F) Definition of aster velocity and drift following ablation. (G) Aster drift in the indicated conditions (n=10 for control; n=28 for side ablation; n=7 for nocodazole; n=10 for nocodazole + side ablation). (H-K) Aster front ablation. (H) Aster velocity vectors following ablation in the indicated conditions. (I) Aster speeds along the centration path following ablation in the indicated conditions. (J) Distance-time plot of front-ablated aster. (K) Aster velocity along the centration path after ablation (V_2) as a function of the velocity before (V_1). n.s : non-significant; ** Student t-test $p < 10^{-4}$. Error bars represent S.D.

Figure 3. Aster geometry determines aster directionality.

(A) Time-lapses of aster centration in shape-manipulated eggs. (B) Centering trajectories of time-lapse presented in (A). (C) Corresponding numerical simulations. (D) 3D centering trajectory of a sperm aster which exhibit two subsequent turning points (black arrowheads). The plot volume corresponds to a cell quarter and the position $X=Y=Z=0$ marks the cell center. (E) Numerical simulation corresponding to (D). (F) Distance-time plot for the centration trajectory presented in (D), with black arrowheads marking the turning points. (G) Distance-time curves

for 35 centering asters in various cell geometries. Red: shape aspect ratio ≥ 1 , blue: <1 . The black line is an averaged distance-time curve for normal spherical cells. **(H)** Aster speed in different cell geometries. Error bars represent \pm S.D.

Figure 4. Speed determination in growing asters.

(A) One dimensional model of a centering aster. Each MT exert a pulling force F that scale to its length L . The aster moves with a speed V . **(B)** Time-evolution of MT lengths in the model. Note that L_{rear} is equal to aster position in the model. τ_0 and T_2 correspond to the time needed to reach constant speed and to the time at which the front MT contacts the opposite cortex. **(C and D)** 3D simulations for various force parameter values, and for the two scaling conditions linking α and β . **(E and F)** Simulations assessing the impact of abruptly reducing the force amplitude in the two different scaling conditions. The force parameter was decreased by a factor 20 in the simulation at 5 min. **(G)** Confocal time-lapse of a centering aster treated with a low-dose of 10 μ M ciliobrevin D at 5 min post sperm entry. **(H-I)** Aster speed before (V_1) and after (V_2) ciliobrevin D treatment. **(I)** V_2 plotted as a function of V_1 for 7 individual eggs. Broken line marks $V_1=V_2$. Scale bars: 50 μ m.

Figure 5. Aster shape-motion relationships.

(A) Proposed model for how centering MT asters may determine their speed and directionality. Each MT exert a pulling force on the centrosome which scales to MT length. Aster shape asymmetry, which corresponds to the difference between centrosome position and aster geometrical center, is characterized by a unit vector \vec{e} which determines the aster directionality.

Asters migrate with a constant speed which is determined by the growth rate V_p . Therefore, the aster velocity vector can be simply represented $V_p \cdot \vec{e}$. **(B)** These shape-motion relationships enable asters to probe local cell geometry to faithfully find the center in any cell shape.

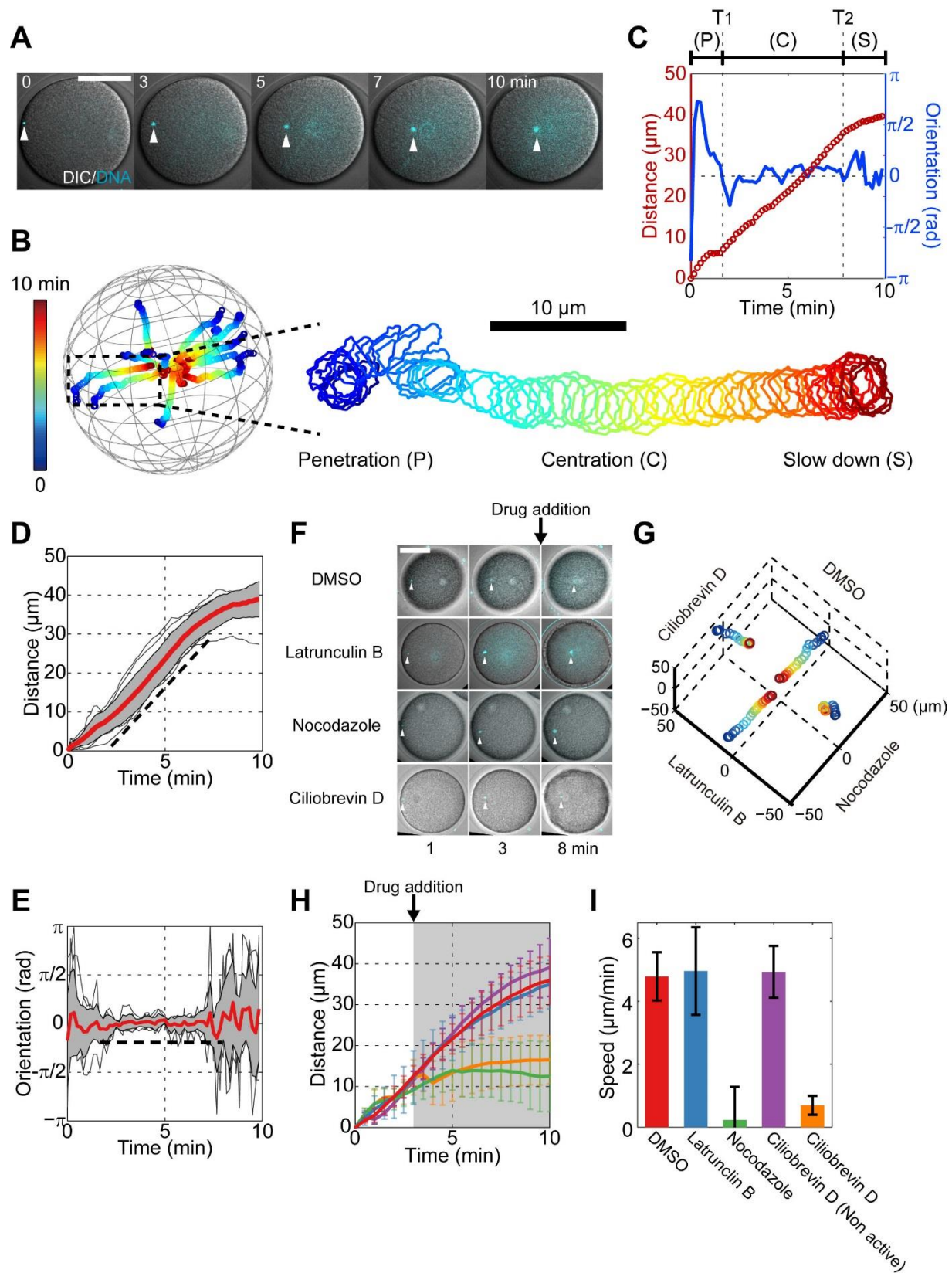


Figure 1 Tanimoto et al.

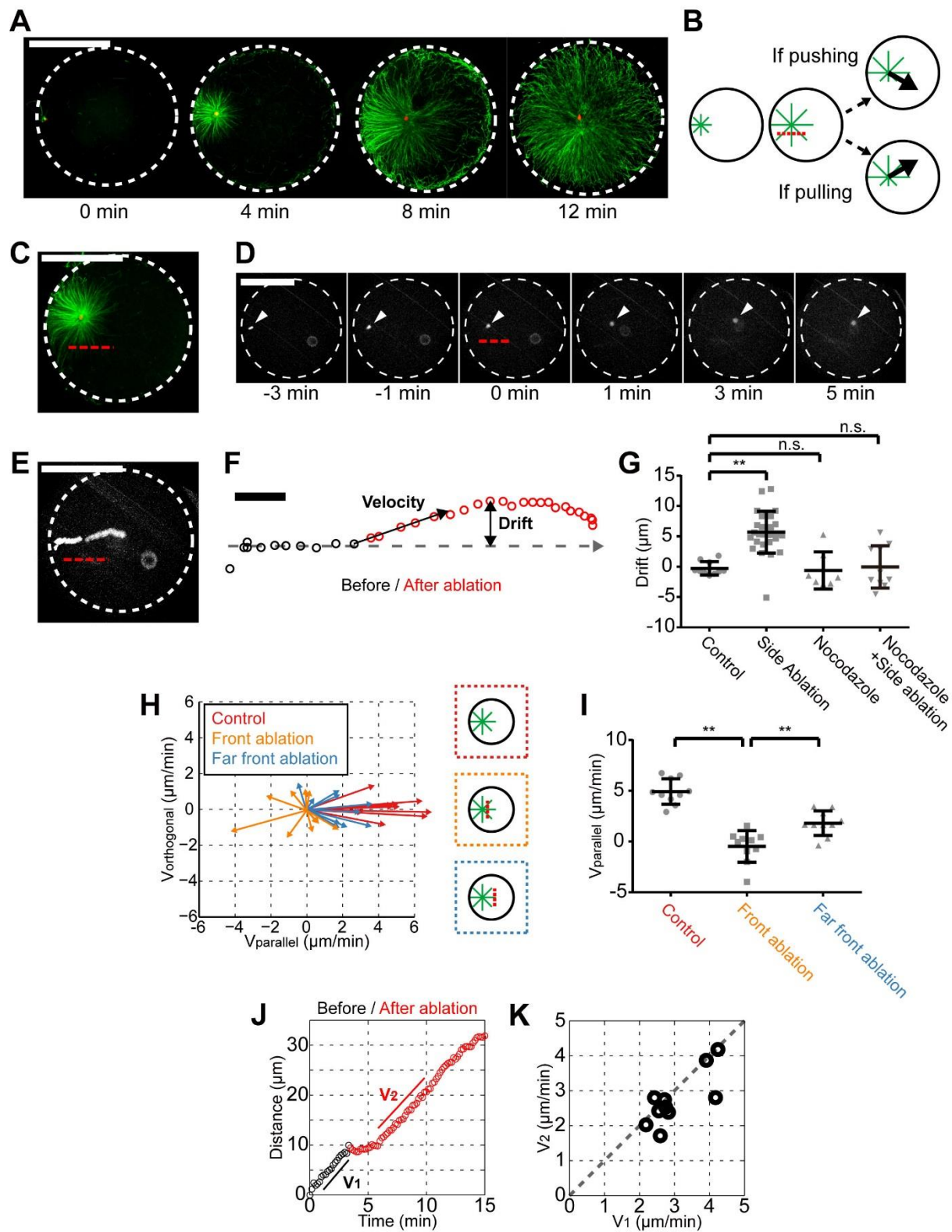


Figure 2 Tanimoto et. al.

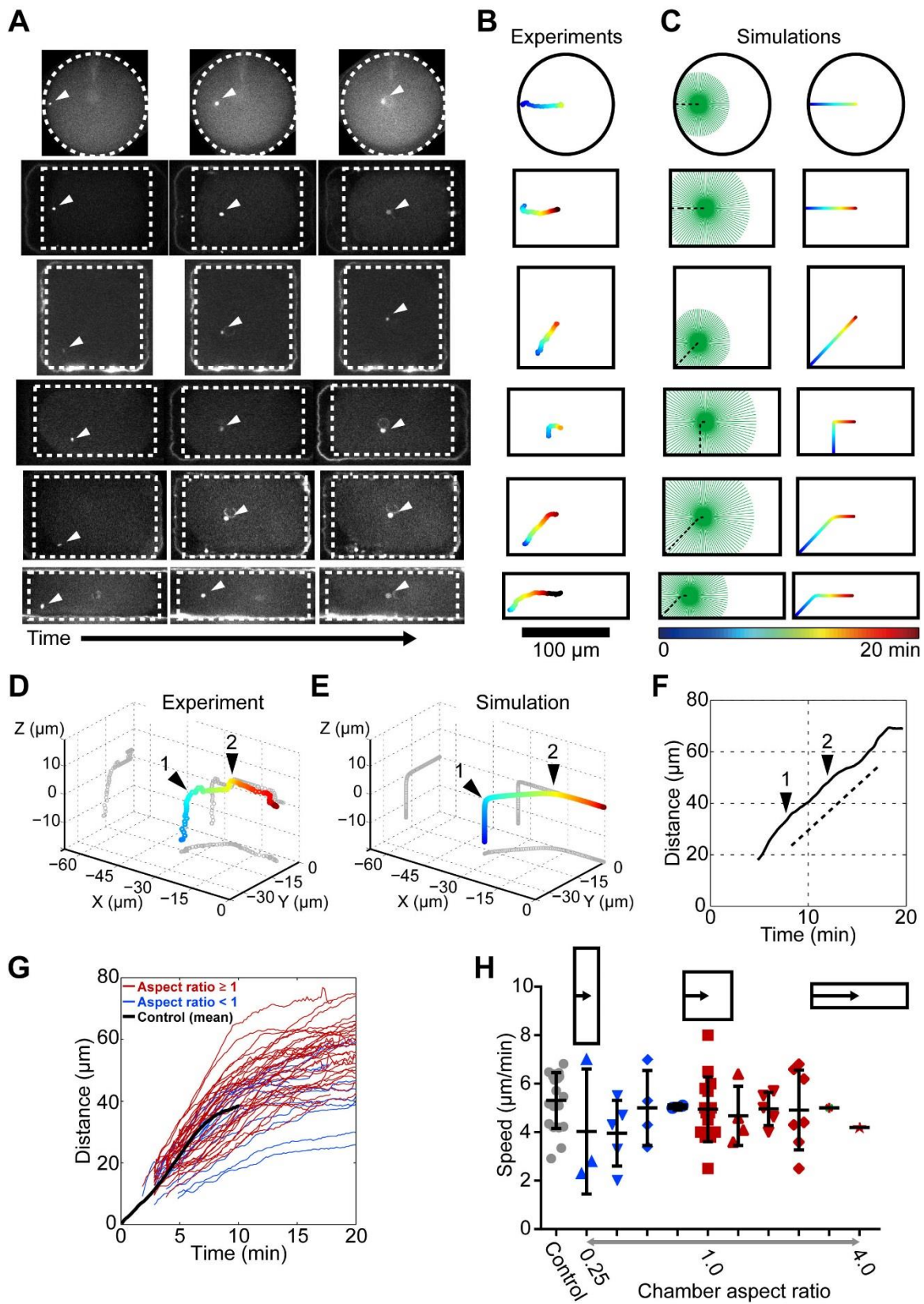


Figure 3 Tanimoto et al.

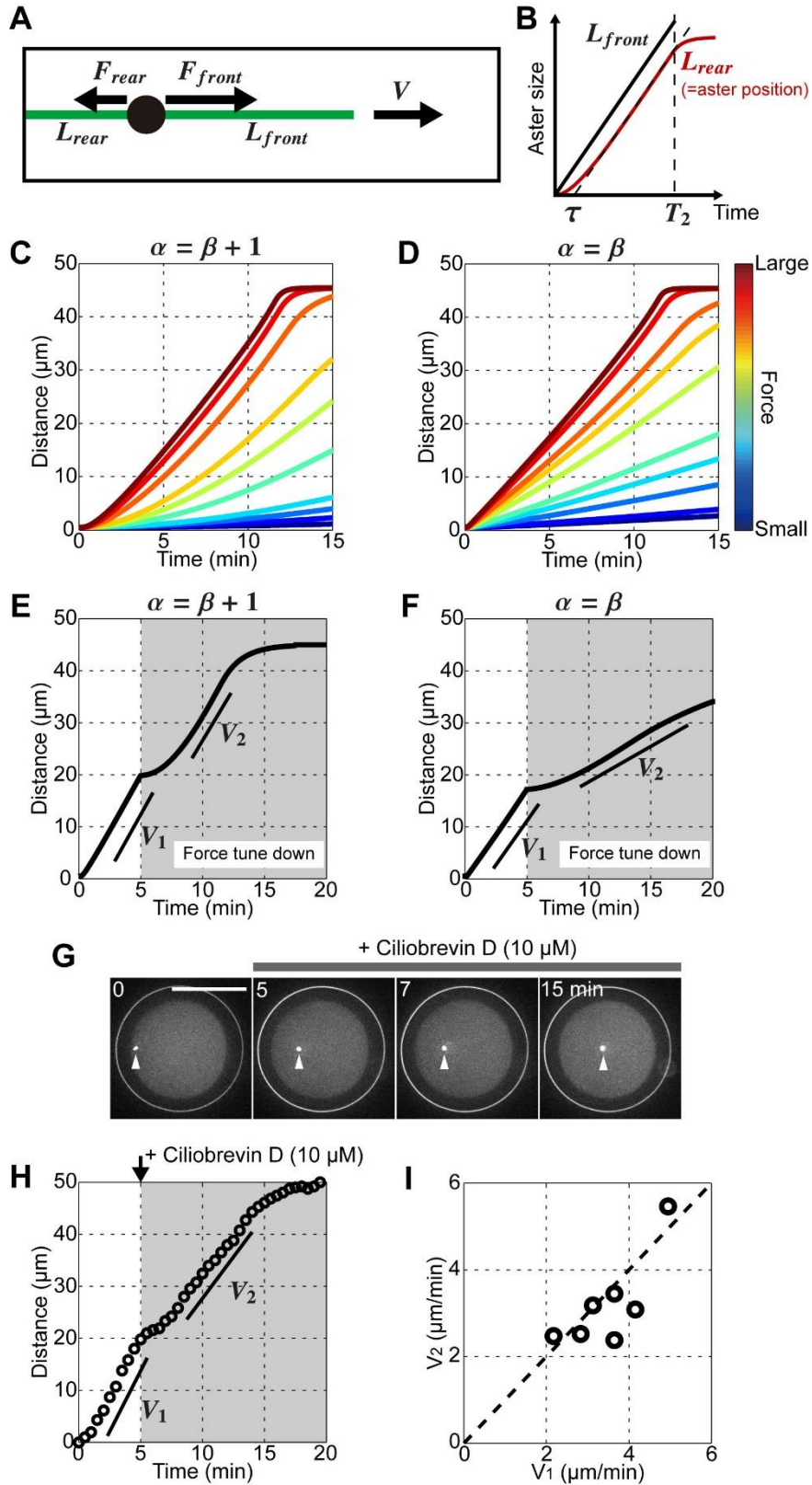
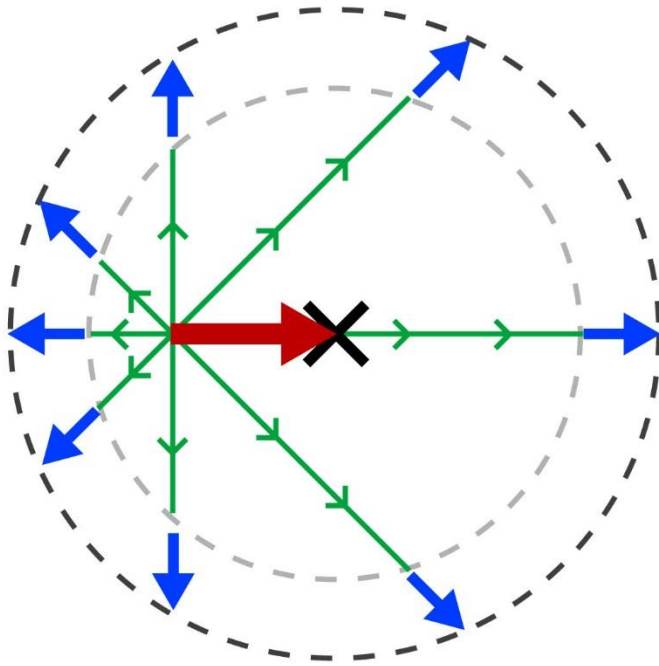


Figure 4 Tanimoto et al.

A

$$\vec{V} = V_p \cdot \vec{e}$$



- ✕ Aster geometric center
- ➔ Shape asymmetry
- ➔ Growth

B

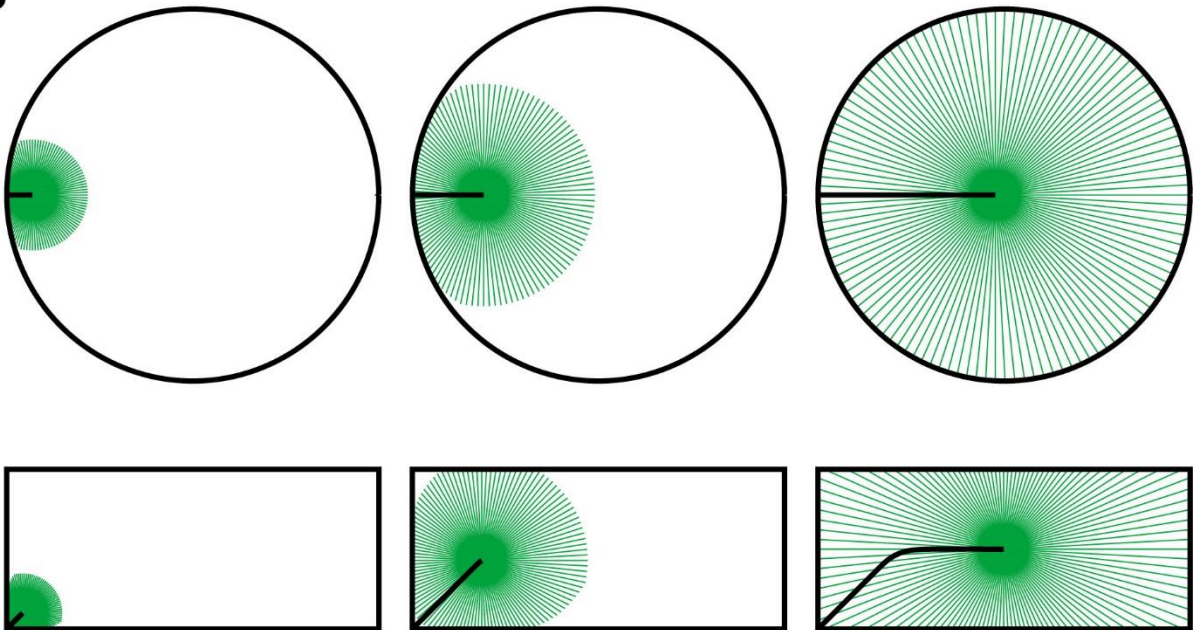


Figure 5 Tanimoto et al.