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## Colebrook's Flow Friction Explicit Approximations Based on Fixed-Point Iterative Cycles and Symbolic Regression

Dejan Brkić <sup>1,2,\*</sup> and Pavel Praks <sup>1,\*</sup>

- 1 IT4Innovations, VŠB—Technical University of Ostrava, 708 00 Ostrava, Czech Republic
- <sup>2</sup> Research and Development Center "Alfatec", 18000 Niš, Serbia
- \* Correspondence: dejanrgf@tesla.rcub.bg.ac.rs or dejanbrkic0611@gmail.com (D.B.); pavel.praks@vsb.cz or pavel.praks@gmail.com (P.P.)

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Abstract: The logarithmic Colebrook flow friction equation is implicitly given in respect to an unknown flow friction factor. Traditionally, an explicit approximation of the Colebrook equation requires evaluation of computationally demanding transcendental functions, such as logarithmic, exponential, non-integer power, Lambert W and Wright  $\Omega$  functions. Conversely, we herein present several computationally cheap explicit approximations of the Colebrook equation that require only one logarithmic function in the initial stage, whilst for the remaining iterations the cheap Padé approximant of the first order is used instead. Moreover, symbolic regression was used for the development of a novel starting point, which significantly reduces the error of internal iterations compared with the fixed value staring point. Despite the starting point using a simple rational function, it reduces the relative error of the approximation with one internal cycle from 1.81% to 0.156% (i.e., by a factor of 11.6), whereas the relative error of the approximation with two internal cycles is reduced from 0.317% to 0.0259% (i.e., by a factor of 12.24). This error analysis uses a sample with 2 million quasi-Monte Carlo points and the Sobol sequence.

**Keywords:** approximations; iterative procedures; Colebrook equation; Colebrook-White experiment; Darcy friction factor; flow friction; hydraulics; Padé approximants; symbolic regression

### 1. Introduction

The Colebrook equation, Equation (1) [1], is implicitly given in respect to the unknown flow friction factor f, which is captured implicitly in a logarithmic expression in a way that can be expressed explicitly only using special functions such as the Lambert W function or its cognate Wright  $\Omega$  [2–9]. In the latter instance, the Colebrook equation can be solved only numerically using iterative procedures [10] or using specially developed explicit approximations [11–15].

$$\frac{1}{\sqrt{f}} = -2 \cdot \log_{10} \left( \frac{2.51}{Re} \cdot \frac{1}{\sqrt{f}} + \frac{\varepsilon}{3.71} \right),\tag{1}$$

where f is the Darcy flow friction factor (dimensionless), Re is the Reynolds number (dimensionless) and  $\varepsilon$  is the relative roughness of inner pipe surface (dimensionless).

The Colebrook equation has been known since the end of the 1930s and is based on an experiment by Colebrook and White [16] that had been performed a few years earlier using pipes with different inner surface roughness, from smooth to very rough. As the Colebrook equation is empirical [1,16], its accuracy can be disputed [17,18] (e.g., the new Oregon and Princeton experiment related to pipe friction [18]); nevertheless, the equation is widely accepted as a standard and is in common use in the

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design of water and gas pipe networks [19]. It can be also adapted for special cases such as air flow through fuel cells [20], water flow in rivers [21,22] and blood flow in blood vessels [23].

Praks and Brkić [24] recently showed a Newton–Raphson iterative solution of the Colebrook equation based on Padé approximants [25–29]. Based on their solution, one simplified approach and a novel starting point that significantly reduces numerical error will be offered herein.

The simplified method is based on the fixed-point method, a variant of the Newton–Raphson method in which the first derivative of the unknown function is equalized to 1 [30]. In the worst case, the demonstrated iterative procedures need up to seven iterations to reach the final accurate solution [10], whereas in this study the explicit approximations derived from the iterative procedure will have relative errors of up to 1.81% and 0.317% in the case of one internal and two internal iterative steps, respectively. Moreover, when the novel simple rational function  $p_0$  of Equation (2) is used as a starting point, the relative errors are significantly reduced to 0.156% and 0.0259%, respectively. Such small values of the relative error are acceptable for engineering applications, given the empirical nature of the Colebrook equation [17,18].

The approach with Padé approximants offers an iterative procedure in which the repetition of the computationally expensive logarithmic function is avoided [24]. Using only one logarithmic function together with simple rational functions and avoiding computationally expensive functions, such as exponential functions or functions with non-integer powers, the presented method saves the processor time [7–9,12–14], which is essential for effective simulations of large pipe networks [19].

The presented approximations are in a form suitable for computer codes and for application in software packages for everyday engineering use.

#### 2. A Fixed-Point Iterative Procedure Based on Padé Approximants

The logarithmic function can be accurately approximated in a certain relatively narrow domain using Padé approximants (an approximation of the given function by a rational function of given order) [24]. For example,  $\log_{10}(97)$  can be cheaply approximated knowing that  $\log_{10}(100) = 2$ , and using the fact that  $\log_{10}(97) = \log_{10}\left(\frac{100}{97}\right) = \log_{10}(100) - \log_{10}\left(\frac{100}{97}\right)$ , where  $\frac{100}{97} \approx 1.0309$ , which is close to 1. Consequently,  $\log_{10}(1.0309)$  can be accurately estimated by its Padé approximant at the expansion point x=1. This simple idea can be used for solving the logarithmic-based Colebrook equation. Starting from the initial point  $x_0 = \frac{1}{\sqrt{f_0}} \rightarrow y_0 = \frac{2.51 \cdot x_0}{Re} + \frac{\varepsilon}{3.71}$ , the next value can be calculated as  $x_1 = -2 \cdot \log_{10}(y_0)$ . The pre-computed numerical value  $\zeta$ ;  $\zeta = \log_{10}(y_0)$  should be used in all the following iterations [24]. The next value  $y_1 = \frac{2.51 \cdot x_1}{Re} + \frac{\varepsilon}{3.71}$  and the previous value  $y_0$  should be used as the argument of the Padé approximant  $z_{01} = \frac{y_0}{y_1}$ , where the chosen Padé approximant is  $p_{01} = \frac{z_{01} \cdot (z_{01} + 4) - 5}{4 \cdot z_{01} + 2}$ . Now, the new value  $\log_{10}(y_1) = \zeta + 0.8686 \cdot p_{01}$  should be used for the calculation  $x_1 = -2 \cdot \zeta + 0.8686 \cdot p_{01}$  where  $0.8686 \approx \frac{2}{\ln(10)}$ .

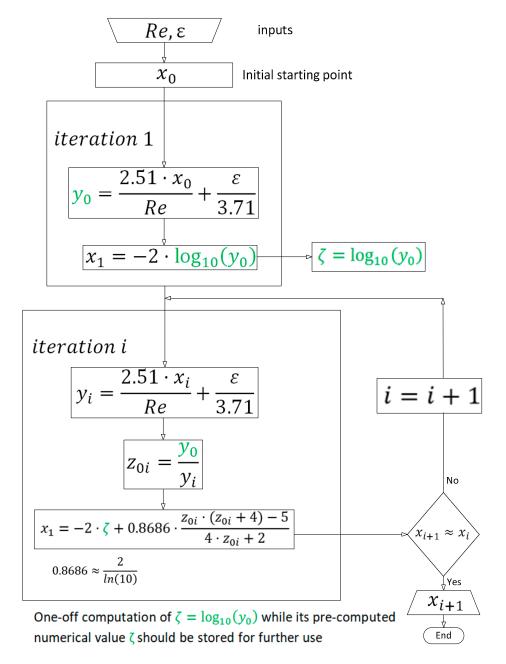
To solve the Colebrook equation using a numerical fixed-point iterative procedure, the steps shown in Figure 1 should be followed. Figure 1 includes a simplified procedure compared with [24], where the Newton–Raphson iterative procedure is used instead of the herein presented fixed-point iterative procedure.

The initial starting point  $x_0 = \frac{1}{\sqrt{f_0}}$  should be chosen from the domain of applicability of the Colebrook equation, which is  $0 < \varepsilon < 0.05$  and  $4000 < Re < 10^8$ . Every initial starting point chosen from this domain will be suitable, but to reduce the required number of iterations, different strategies are offered [10]. We will demonstrate the approach with the fixed-value initial starting point, but also the approach with the starting point given by the rational function:

$$p_0 = x_0 = \frac{1}{\sqrt{f_0}} = \frac{2600 \cdot Re}{657.7 \cdot Re + 214600 \cdot Re \cdot \varepsilon + 12970000} - 13.58 \cdot \varepsilon + \frac{0.0001165 \cdot Re}{0.00002536 \cdot Re + Re \cdot \varepsilon + 105.5} + 4.227$$
 (2)

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Equation (2) was found using the symbolic regression tool Eureqa [31,32] following the approach of Gholamy and Kreinovich [33], in which existing absolute error minimizing software was used to minimize the relative error (various artificial intelligence tools have been used recently for the Colebrook equation, such as symbolic regression [34], novel artificial bee colony programming (ABCP) methods [35], artificial neural networks [36], genetic algorithms [37], etc.). The novel starting point given by Equation (2) has a maximal relative error of only 6.7%, whereas the previous version of the starting point [34] had a maximal relative error of 40%. Thus, we can observe that the approach Gholamy and Kreinovich [33] used was very useful for symbolic regression of the Colebrook equation.



**Figure 1.** Algorithm for solving the Colebrook equation using a numerical fixed-point iterative method and Padé polynomials (green letters are for one-off computations).

Calculation of  $\log_{10}(y_0)$  should not be repeated in each iteration, but its numerical value  $\zeta$  should be used in a combination with the Padé approximant in every iteration (with the exception of the first) [24].

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Instead of  $z_{01} = \frac{y_0}{y_1}$ ,  $z_{02} = \frac{y_0}{y_2}$ ,  $z_{03} = \frac{y_0}{y_3}$ , and so on, the adapted chain can be used as  $z_{01} = \frac{y_0}{y_1}$ ,  $z_{12} = \frac{y_1}{y_2}$ ,  $z_{23} = \frac{y_2}{y_3}$ , etc. [24].

The Padé approximant  $\frac{z_{01} \cdot (z_{01}+4)-5}{4 \cdot z_{01}+2}$  used is of the order /1,1/, referring to the polynomial order in the numerator and in the denominator, respectively [24]. As the expansion point z=1 is the root of  $\ln(z)$ , the accuracy of the Padé approximant decreases. For this reason, setting the OrderMode option in the Matlab Padé command to relative compensates for the decreased accuracy. Consequently, the numerator of the Padé approximant of the order /1,1/ includes the polynomial of the second order.

Possible software implementation of developed algorithms is summarized in Section 4.

#### 3. Explicit Approximations Based on Padé Approximants

Two explicit approximations of the Colebrook equation based on the algorithm from Figure 1 will be shown here. The approximation with one internal iterative cycle will be shown in Section 3.1, while the approximation with two internal iterative cycles will be presented in Section 3.2. The iterative procedures are sensitive, depending on the chosen initial starting point [38], and therefore carefully conducted numerical tests are provided separately for the approximation with one and two internal iterative cycles. In both cases, fixed numerical values for the initial starting points are chosen in such a way as to reduce the final maximal relative error over the domain of applicability of the Colebrook equation. Alternatively, the novel rational function, Equation (2), is used as the initial starting point. We show that this alternative approach significantly reduces the relative error of approximations.

In order to perform a deeper analysis of the turbulent flow, the emphasis of this section is on the Reynolds number Re between  $10^4$  and  $10^8$  (the analysis is compatible with [39]). However, the error aggregates in the zone between 4000 and  $10^4$ , where it is still possible that a laminar flow can exist.

### 3.1. Explicit Approximations with One Internal Iterative Cycle

# 3.1.1. An Explicit Approximation with One Internal Iterative Cycle and a Numerical Fix-Value Starting Point

After numerous numerical tests, it is clear that the algorithm from Figure 1 gives the smallest relative error in the domain of applicability of the Colebrook equation for the approximation with one internal cycle, Equation (3), if the initial starting point is set as  $f_0 = 0.022058 \rightarrow x_0 = \frac{1}{\sqrt{f_0}} = 6.73306$  (the numerical value 16.9 of the parameter c in Equation (3) is computed as  $2.51 \times 6.73306$ ). The maximal relative error of Equation (3) is up to 0.79% and its distribution can be seen in Figure 2.

$$\frac{1}{\sqrt{f}} \approx b + 0.8686 \cdot \frac{a \cdot (a+4) - 5}{4 \cdot a + 2} \\
a = \frac{c}{\frac{\varepsilon}{3.71} + \frac{2.51 \cdot b}{Re}} \\
b = -2 \cdot \log_{10}(c) \\
c = \frac{16 \cdot 9}{Re} + \frac{\varepsilon}{3.71}$$
(3)

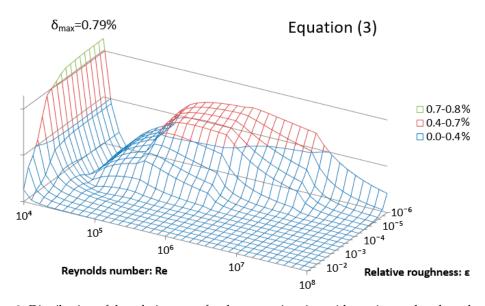
## 3.1.2. An Explicit Approximation with One Internal Iterative Cycle and a Starting Point Given by a Rational Function

Using the rational function  $p_0$ , Equation (2) for the initial starting point  $x_0$  and the proposed approximation, Equation (4) has a maximal relative error of 0.101%. The distribution of its relative error is shown in Figure 3. In comparison with the fixed point version, Equation (3)—the novel staring point—Equation (2) reduces the maximal relative error for one internal iterative cycle by a factor of 7.82 (=0.79%/0.101%).

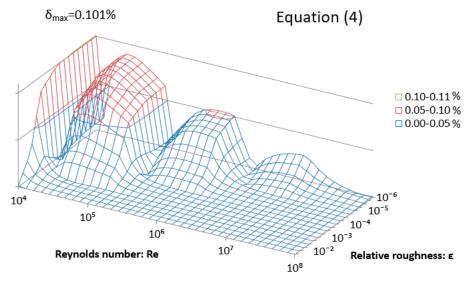
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$$\frac{1}{\sqrt{f}} \approx b + 0.8686 \cdot \frac{a \cdot (a+4) - 5}{4 \cdot a + 2} \\
a = \frac{c}{\frac{\varepsilon}{3.71} + \frac{2.51 \cdot b}{Re}} \\
b = -2 \cdot \log_{10}(c) \\
c = \frac{2.51 \cdot p_o}{Re} + \frac{\varepsilon}{3.71}$$
(4)

where  $p_o$  is from Equation (2).



**Figure 2.** Distribution of the relative error for the approximation with one internal cycle and a fixed starting point.



**Figure 3.** Distribution of the relative error for the approximation with one internal cycle and a starting point given by the rational function  $p_o$ , Equation (2).

### 3.2. Explicit Approximations with Two Internal Iterative Cycles

## 3.2.1. An Explicit Approximation with Two Internal Iterative Cycles and a Fixed Starting Point

The explicit approximation of the Colebrook formula with two internal iterative cycles is given in Equation (5). The numerical fixed value 18.15 of the parameter *c* of Equation (5) depends on the initial starting point, which is carefully chosen to reduce the maximal relative error and corresponds to the

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initial starting point set as  $f_0 = 0.01912468 \rightarrow x_0 = \frac{1}{\sqrt{f_0}} = 7.2310756$ , where  $18.15 \approx 2.51 \times 7.2310756$ . The maximal relative error of Equation (5) is up to 0.172% and its distribution is shown in Figure 4.

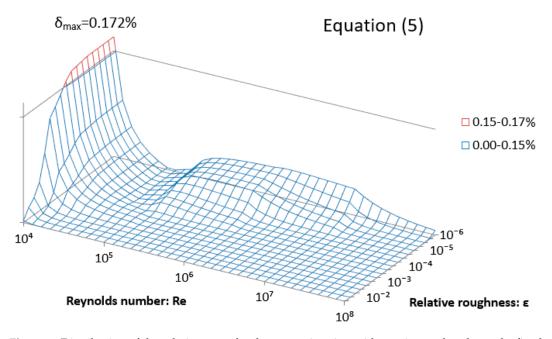
$$\frac{1}{\sqrt{f}} \approx b + 0.8686 \cdot \frac{d \cdot (d+4) - 5}{4 \cdot d + 2}$$

$$a = \frac{c}{\frac{\varepsilon}{3.71} + \frac{2.51 \cdot b}{Re}}$$

$$b = -2 \cdot \log_{10}(c)$$

$$c = \frac{18.15}{Re} + \frac{\varepsilon}{3.71}$$

$$d = \frac{c}{\frac{\varepsilon}{3.71} + \frac{2.51}{Re} \cdot \left(b + 0.8686 \cdot \frac{a \cdot (a+4) - 5}{4 \cdot a + 2}\right)}$$
(5)



**Figure 4.** Distribution of the relative error for the approximation with two internal cycles and a fixed starting point.

## 3.2.2. An Explicit Approximation with Two Internal Iterative Cycles and a Starting Point Given by a Rational Function

The introduction of a starting point given by the rational function Equation (2) instead of a fixed point significantly reduces the relative error from 0.172% in Equation (5) to no more than 0.0154% in Equation 6 (i.e., by a factor of 11.16). Equation (6) presents the new explicit approximation with two internal iterative cycles and a starting point given by the rational function, Equation (2), while the distribution of its relative error is shown in Figure 5.

$$\frac{1}{\sqrt{f}} \approx b + 0.8686 \cdot \frac{d \cdot (d+4) - 5}{4 \cdot d + 2}$$

$$a = \frac{c}{\frac{\varepsilon}{3.71} + \frac{2.51 \cdot b}{Re}}$$

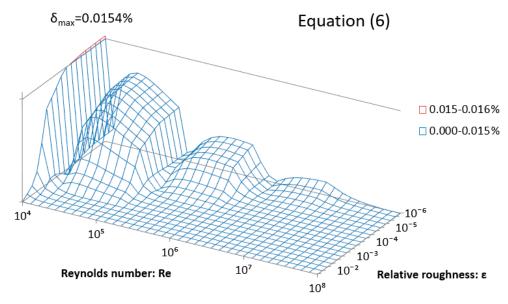
$$b = -2 \cdot \log_{10}(c)$$

$$c = \frac{2.51 \cdot p_0}{Re} + \frac{\varepsilon}{3.71}$$

$$\frac{c}{3.71} + \frac{2.51}{Re} \cdot (b + 0.8686 \cdot \frac{a \cdot (a+4) - 5}{4 \cdot a + 2})$$
(6)

where  $p_o$  is from Equation (2).

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**Figure 5.** Distribution of the relative error for the approximation with two internal cycles and a starting point given by the rational function  $p_0$ , Equation (2).

#### 3.3. Further Error Analysis and Comparisons

Table 1 summarize the results of error analysis for 2 million quasi Monte-Carlo points using the Sobol sequence [40,41] related to Equations (3)–(6). The domain for this analysis in respect to the Reynolds number Re is from 4000 to  $10^8$ , while for the sample of 740 points, which was used for Figures 2–5, the domain is from  $10^4$  to  $10^8$ .

**Table 1.** Comparison of maximal relative error (in %) for the first and second iteration without the Padé approximant and with a Padé approximant of the order /1,1/ for the Reynolds number Re from 4000 to  $10^8$ .

Padé Approximant	No		/1,1/	
solution version <sup>1</sup>	$x = x1 + 0.8686*\log(z)$		x = x1 + 0.8686*(z*(z+4) - 5)/(4*z + 2)	
Iteration	1	2	1	2
Fixed starting point	1.81%	-0.317%	1.81%	-0.317%
Starting point by Equation (2)	-0.156%	0.0259%	-0.156%	0.0259%

<sup>&</sup>lt;sup>1</sup> Notation from Matlab codes from Section 4; symbol  $\log(z)$  of the solution update represents the natural logarithm; both Matlab and MS Excel codes are mathematically equivalent: they use the same function, the natural logarithm. In MS Excel, the natural logarithm is expressed by the symbol  $\ln(x)$ , whereas in Matlab, the natural logarithm is expressed by the symbol  $\log(x)$ .

Table 1 shows that iterations using the Padé approximant of the first order  $/1,1/\ln 11(z) = (z^*(z+4) - 5)/(4^*z+2)$  have the same relative error as iterations using the natural logarithm. For the method with one internal cycle (denoted as Iteration 1 in Table 1), the maximal relative error is approximately 1.81% or 0.156%, whereas for the method with two internal cycles (denoted as Iteration 2 in Table 1), the maximal relative error is only 0.317% or 0.0259%. This analysis also shows that the novel starting point given with Equation (2) is very useful.

Compared with analysis performed in MS Excel where 740 points are used, analysis with 2 million quasi Monte-Carlo points using the Sobol sequence detected additional peaks of error, as shown in Table 2. The same value of the maximal error is detected for even 2000 quasi Monte-Carlo points. Thus, this analysis confirms that the Sobol sequence of 2 million quasi Monte-Carlo points sufficiently covers the whole domain. For example, for Equation (6), the largest relative error is detected for the input pair Re = 5263 and  $\varepsilon = 3.1707 \times 10^{-7}$ , which corresponds to the zone with lower Reynolds numbers. Although this input pair is not shown in Figures 2–5, the figures clearly indicate a tendency towards

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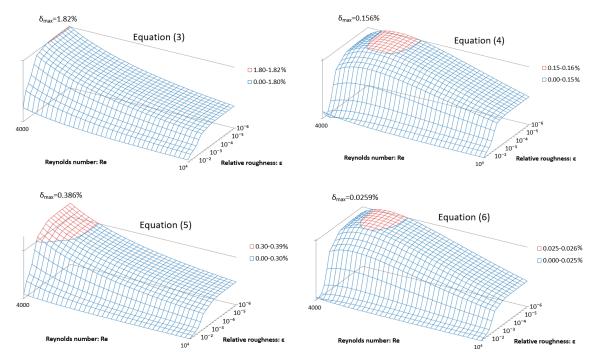
higher relative errors when the Reynolds number Re and the relative roughness of the inner pipe surface  $\varepsilon$  are smaller.

**Table 2.** Analysis of error performed in MS Excel with 740 points compared with analysis from Matlab with 2 million Monte Carlo samples using the Sobol sequence.

Max. Rel. Error %	740 Test Points <sup>1</sup>	2 Million Test Point <sup>2</sup>
Equation (3)	0.79%	1.81%
Equation (4)	0.101%	0.156%
Equation (5)	0.172%	0.317%
Equation (6)	0.0154%	0.0259%

<sup>&</sup>lt;sup>1</sup> Reynolds number *Re* from 10<sup>4</sup> to 10<sup>8</sup>. <sup>2</sup> Reynolds number *Re* from 4000 to 10<sup>8</sup>.

As shown in Figure 6, additional analysis in MS Excel for the zone  $4000 < Re < 10^4$  shows very good agreement with the results obtained in Matlab.



**Figure 6.** Additional analysis in MS Excel for the zone  $4000 < Re < 10^4$ .

#### 4. Description of Software

The presented approximations were thoroughly tested at IT4Innovations, National Supercomputing Center, VŠB (Technical University of Ostrava, Czech Republic). For simplicity, the codes were expressed in MS Excel format [42] and in Matlab. The Matlab codes also work in GNU Octave, but they can be easily translated in any programming language.

Software codes in MS Excel are given in Supplementary Materials. However, we provide Matlab codes here, in order to support the benchmark study of the Colebrook equation [35] (in addition these Matlab codes are also given in Supplementary Materials).

Equation (3): An explicit approximation with one internal iterative cycle and with a fixed starting point.

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Matlab code:

```
x = 16.9/2.51;
y0 = 2.51*x./R + K./3.71;
x1 = -2*\log 10(y0);
z = y0./((K/3.71) + (2.51*x1./R));
\ln 11 = @(z) (z.*(z+4) - 5)./(4*z+2);
x = x1 + 0.8686*\ln 11(z);
f = 1./x.^2;
```

In the Matlab codes, the Reynolds number Re is noted as R, while the relative roughness of the inner pipe surface  $\varepsilon$  is K.

Equation (4): An explicit approximation with one internal iterative cycle and a rational starting point given by Equation (2).

Matlab code:

For the rational starting point, *x* is given by Equation (2), as follows:

```
x = (2600*R)./(657.7*R + 214600*R.*K + 12970000) - 13.58*K + (0.0001165*R)./(0.00002536*R + R.*K + 105.5) + 4.227;
```

The rest of the Matlab code is unchanged.

Equation (5): An explicit approximation with two internal iterative cycles and a fixed starting point. Matlab code:

```
x = 16.9/2.51;
y0 = 2.51*x./R + K./3.71;
x1 = -2*\log 10(y0);
z = y0./((K/3.71) + (2.51*x1./R));
\ln 11 = @(z) (z.*(z + 4) - 5)./(4*z + 2);
x = x1 + 0.8686*\ln 11(z);
z = y0./((K/3.71) + (2.51*x./R));
x = x1 + 0.8686*\ln 11(z);
f = 1./x.^2;
```

Equation (6): An explicit approximation with two internal iterative cycles and a rational starting point given by Equation (2).

Matlab code:

For the rational starting point, x is given by Equation (2). The rest of the Matlab code is unchanged.

#### 5. Conclusions

This article presents simplified, but still precise algorithms for solving the Colebrook equation based on a fixed-point iterative procedure in which the logarithm is replaced by its Padé approximant in all iterations except the first one [24]. Moreover, a novel simple starting point, which was found by symbolic regression, significantly reduces the error of internal iterations. Consequently, a cheap Padé approximant of the first order is suitable for approximations. Depending on the stopping criteria and number of iterations, this algorithm can solve the Colebrook equation with any desired accuracy. As the computationally expensive logarithmic function is used only in the first step, this algorithm can be used efficiently for simulations of a complex pipe network. This is because the carefully selected Padé approximants can save computational time. For a good balance between efficiency and accuracy [9], two explicit approximations have been demonstrated based on a simplified iterative procedure with a maximal relative error of no more than 1.81% and 0.156% for the variant with one internal iterative cycle, and of no more than 0.317% and 0.0259% for two internal cycles (higher error values are for the fixed initial starting point, while lower error values are for the initial starting point given by the rational function, Equation (2), respectively). The value of the relative error, and also the tendency of

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its distribution, are confirmed by 2 million quasi Monte-Carlo points using the Sobol sequence for  $4000 < Re < 10^8$  and for  $0 < \varepsilon < 0.05$ .

The presented approximations have an acceptable level of accuracy [43], especially in light of the fact that the Colebrook equation is empirical and by its nature not always accurate. We can see that iterations with the cheap Padé approximant of the first order have a nearly identical relative error to iterations with the logarithm. Consequently, the herein presented approximations are favorable, as they do not contain computationally demanding evaluations such as special functions, exponential functions, or non-integer powers.

Supplementary Materials: The following are available online at http://www.mdpi.com/2079-3197/7/3/48/s1.

**Author Contributions:** Conceptualization, D.B. and P.P.; methodology, D.B. and P.P.; writing—original draft preparation, D.B.; writing—review and editing, D.B. and P.P.; data curation, P.P.

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#### References

- 1. Colebrook, C.F. Turbulent flow in pipes with particular reference to the transition region between the smooth and rough pipe laws. *J. Inst. Civ. Eng.* **1939**, *11*, 133–156. [CrossRef]
- 2. Corless, R.M.; Gonnet, G.H.; Hare, D.E.; Jeffrey, D.J.; Knuth, D.E. On the LambertW function. *Adv. Comput. Math.* **1996**, *5*, 329–359. [CrossRef]
- 3. Hayes, B. Why W? On the Lambert W function, a candidate for a new elementary function in mathematics. *Am. Sci.* **2005**, *93*, 104–108. [CrossRef]
- 4. Keady, G. Colebrook-White formula for pipe flows. J. Hydraul. Eng. 1998, 124, 96–97. [CrossRef]
- 5. Sonnad, J.R.; Goudar, C.T. Constraints for using Lambert W function-based explicit Colebrook–White equation. *J. Hydraul. Eng.* **2004**, *130*, 929–931. [CrossRef]
- 6. More, A.A. Analytical solutions for the Colebrook and White equation and for pressure drop in ideal gas flow in pipes. *Chem. Eng. Sci.* **2006**, *61*, 5515–5519. [CrossRef]
- 7. Clamond, D. Efficient resolution of the Colebrook equation. *Ind. Eng. Chem. Res.* **2009**, *48*, 3665–3671. [CrossRef]
- 8. Biberg, D. Fast and accurate approximations for the Colebrook equation. *J. Fluids Eng.* **2017**, 139, 031401. [CrossRef]
- 9. Brkić, D.; Praks, P. Accurate and efficient explicit approximations of the Colebrook flow friction equation based on the Wright ω-function. *Mathematics* **2019**, 7, 34. [CrossRef]
- 10. Praks, P.; Brkić, D. Choosing the optimal multi-point iterative method for the Colebrook flow friction equation. *Processes* **2018**, *6*, 130. [CrossRef]
- 11. Zigrang, D.J.; Sylvester, N.D. Explicit approximations to the solution of Colebrook's friction factor equation. *AIChE J.* **1982**, *28*, 514–515. [CrossRef]
- 12. Winning, H.K.; Coole, T. Explicit friction factor accuracy and computational efficiency for turbulent flow in pipes. *Flow Turbul. Combust.* **2013**, *90*, 1–27. [CrossRef]
- 13. Winning, H.K.; Coole, T. Improved method of determining friction factor in pipes. *Int. J. Numer. Methods Heat Fluid Flow* **2015**, 25, 941–949. [CrossRef]
- 14. Vatankhah, A.R. Approximate analytical solutions for the Colebrook equation. *J. Hydraul. Eng.* **2018**, 144, 06018007. [CrossRef]

Computation 2019, 7, 48 11 of 12

15. Pimenta, B.D.; Robaina, A.D.; Peiter, M.X.; Mezzomo, W.; Kirchner, J.H.; Ben, L.H. Performance of explicit approximations of the coefficient of head loss for pressurized conduits. *Rev. Bras. Eng. Agrícola Ambient.* **2018**, 22, 301–307. [CrossRef]

- 16. Colebrook, C.; White, C. Experiments with fluid friction in roughened pipes. *Proc. R. Soc. Lond. Ser. A Math. Phys. Sci.* **1937**, *161*, 367–381. [CrossRef]
- 17. Díaz-Damacillo, L.; Plascencia, G. A new six parameter model to estimate the friction factor. *AIChE J.* **2019**, 65, 1144–1148. [CrossRef]
- 18. McKeon, B.J.; Zagarola, M.V.; Smits, A.J. A new friction factor relationship for fully developed pipe flow. *J. Fluid Mech.* **2005**, *538*, 429–443. [CrossRef]
- 19. Ekhtiari, A.; Dassios, I.; Liu, M.; Syron, E. A novel approach to model a gas network. *Appl. Sci.* **2019**, *9*, 1047. [CrossRef]
- 20. Barreras, F.; López, A.M.; Lozano, A.; Barranco, J.E. Experimental study of the pressure drop in the cathode side of air-forced open-cathode proton exchange membrane fuel cells. *Int. J. Hydrogen Energy* **2011**, *36*, 7612–7620. [CrossRef]
- 21. Stubbs, A.; Stoesser, T.; Bockelmann-Evans, B. Developing an approximation of a natural, rough gravel riverbed both physically and numerically. *Geosciences* **2018**, *8*, 449. [CrossRef]
- 22. Möws, R.; Koll, K. Roughness Effect of submerged groyne fields with varying length, groyne distance, and groyne types. *Water* **2019**, *11*, 1253. [CrossRef]
- 23. Mouza, A.A.; Skordia, O.D.; Tzouganatos, I.D.; Paras, S.V. A simplified model for predicting friction factors of laminar blood flow in small-caliber vessels. *Fluids* **2018**, *3*, 75. [CrossRef]
- 24. Praks, P.; Brkić, D. One-log call iterative solution of the Colebrook equation for flow friction based on Padé polynomials. *Energies* **2018**, *11*, 1825. [CrossRef]
- 25. Baker, G.A.; Graves-Morris, P. Padé Approximants, 2nd ed.; Cambridge University Press: Cambridge, UK, 1996.
- 26. Copley, L. Padé Approximants. In *Mathematics for the Physical Sciences*; De Gruyter: Berlin, Germany, 2014; Chapter 7; pp. 163–179. [CrossRef]
- 27. Kalateh Bojdi, Z.; Ahmadi-Asl, S.; Aminataei, A. A new extended Padé approximation and its application. *Adv. Numer. Anal.* **2013**, 2013, 263467. [CrossRef]
- 28. Peker, H.A.; Karaoğlu, O.; Oturanç, G. The differential transformation method and Padé approximant for a form of Blasius equation. *Math. Comput. Appl.* **2011**, *16*, 507–513. [CrossRef]
- 29. Li, S.; Liu, X.; Zhang, X. A few iterative methods by using [1,n]-order Padé approximation of function and the improvements. *Mathematics* **2019**, *7*, 55. [CrossRef]
- 30. Alfaro-Guerra, M.; Guerra-Rojas, R.; Olivares-Gallardo, A. Evaluación experimental de la solución analítica exacta de la ecuación de Colebrook-White (Experimental evaluation of exact analytical solution of the Colebrook-White Equation). *Ingeniería Investigación y Tecnología* **2019**, 20, 1–11. (In Spanish) [CrossRef]
- 31. Dubčáková, R. Eureqa: Software review. Genet. Program. Evol. Mach. 2011, 12, 173–178. [CrossRef]
- 32. Schmidt, M.; Lipson, H. Distilling free-form natural laws from experimental data. *Science* **2009**, 324, 81–85. [CrossRef]
- 33. Gholamy, A.; Kreinovich, V. How to use absolute-error-minimizing software to minimize relative error: Practitioner's guide. *Int. Math. Forum* **2017**, *12*, 763–770. [CrossRef]
- 34. Praks, P.; Brkić, D. Symbolic regression-based genetic approximations of the Colebrook equation for flow friction. *Water* **2018**, *10*, 1175. [CrossRef]
- 35. Gorkemli, B.; Karaboga, D. A quick semantic artificial bee colony programming (qsABCP) for symbolic regression. *Inf. Sci.* **2019**, *502*, 346–362. [CrossRef]
- 36. Brkić, D.; Ćojbašić, Ž. Intelligent flow friction estimation. *Comput. Intell. Neurosci.* **2016**, 2016, 5242596. [CrossRef] [PubMed]
- 37. Brkić, D.; Ćojbašić, Ž. Evolutionary optimization of Colebrook's turbulent flow friction approximations. *Fluids* **2017**, *2*, 15. [CrossRef]
- 38. Praks, P.; Brkić, D. Advanced iterative procedures for solving the implicit Colebrook equation for fluid flow friction. *Adv. Civ. Eng.* **2018**, 2018, 5451034. [CrossRef]
- 39. Brkić, D. Review of explicit approximations to the Colebrook relation for flow friction. *J. Pet. Sci. Eng.* **2011**, 77, 34–48. [CrossRef]

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40. Sobol', I.M.; Turchaninov, V.I.; Levitan, Y.L.; Shukhman, B.V. Quasi-Random Sequence Generators; Distributed by OECD/NEA Data Bank; Keldysh Institute of Applied Mathematics; Russian Academy of Sciences: Moscow, Russia, 1992; Available online: <a href="http://www.oecd-nea.org/tools/abstract/detail/IAEA1260">http://www.oecd-nea.org/tools/abstract/detail/IAEA1260</a> (accessed on 28 August 2019).

- 41. Bratley, P.; Fox, B.L. Algorithm 659: Implementing Sobol's quasirandom sequence generator. *ACM Trans. Math. Softw.* **1988**, *14*, 88–100. [CrossRef]
- 42. Brkić, D. Solution of the implicit Colebrook equation for flow friction using Excel. *Spreadsheets Educ.* **2017**, 10, 4663. Available online: https://sie.scholasticahq.com/article/4663.pdf (accessed on 19 August 2019).
- 43. Pérez-Pupo, J.R.; Navarro-Ojeda, M.N.; Pérez-Guerrero, J.N.; Batista-Zaldívar, M.A. On the explicit expressions for the determination of the friction factor in turbulent regime. *Rev. Mex. Ing. Chim.* **2020**, *19*, 313–334. [CrossRef]



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