This is the pre-peer reviewed version of the following article: [Bello, S., Ríos, C., 1 2 Feijoo, G. and Moreira, M. T. (2018), Comparative evaluation of lignocellulosic 3 biorefinery scenarios under a life-cycle assessment approach. Biofuels, Bioprod. Bioref., 12: 1047-1064. doi:10.1002/bbb.1921], which has been published in final 4 form at [https://onlinelibrary.wiley.com/doi/full/10.1002/bbb.1921]. This article 5 may be used for non-commercial purposes in accordance with Wiley Terms and 6 7 Conditions for Use of Self-Archived Versions. Evaluation of a lignocellulosic biorefinery based on organosolv pulping 8 under a life-cycle assessment approach 9 S. Bello*, C. Ríos, G. Feijoo, M.T. Moreira 10 Department of Chemical Engineering, University of Santiago de Compostela, Santiago 11 12 de Compostela, 15782, Spain *Corresponding author: sara.bello.ould-amer@usc.es 13

14 Abstract

15 The exploitation of lignocellulosic materials with the aim of producing high added value products will potentially counteract concerns such as depletion of fossil resources or the 16 exponential growth of population. With the objective of implementing concepts such as 17 circular economy or process integration, the present study focuses on the assessment of 18 19 an integrated process, based on organosolv fractionation of residual beech woodchips. 20 The Life Cycle Assessment (LCA) methodology and the eco-efficiency concept allow for 21 a holistic analysis of sustainability in terms of environmental approaches of the system. The results show that the pre-treatment of biomass together with the energy demand of 22 23 the process and enzyme production constitute the hotspots of the system. Analyzing the system by means of the ecoefficiency indicator demonstrates that, broadening the multi-24 25 production spectrum of a biorefinery, provides better results when production volume and processing steps are reasonable. 26

- 1 Keywords: biorefinery, lignocellulose, life cycle assessment, furfural, bioethanol, eco-
- 2 efficiency

3 Abbreviations

LCA	Life Cycle Assessment
LCB	Lignocellulosic Biorefinery
SS	Subsystem
WWT	Wastewater treatment
TOPO	Trioctylphosphine oxide
HDPE	High density polyethylene
CC	Climate change
OD	Ozone depletion
TA	Terrestrial acidification
FE	Freshwater eutrophication
ME	Marine eutrophication
HT	Human toxicity
POF	Photochemical oxidant formation
FET	Freshwater ecotoxicity
MET	Marine ecotoxicity
FD	Fossil depletion
ISO	International Organization for
190	Standardization

4

5 **1. Introduction**

6 The exploitation of lignocellulosic materials with the aim of producing high added value 7 products, is a trend that has been ventured in recent years. Nowadays, the world faces 8 major concerns such as depletion of fossil resources, increasing greenhouse gas emissions 9 or the exponential growth of population. Therefore, the premise is to exploit alternative 10 resources, which, in one or another way would positively impact on aspects such as 11 environmental sustainability or circular economy.

According to recent forecasts, the market share of bio-based chemicals is projected to increase from 2 to 22% by 2025.¹ According to this estimate, an increase in large-scale bio-based facilities may be what is expected for the near future, as can be well perceived

15 through current research trends.

First generation biorefineries derive biofuel and co-products mainly from crops or other agricultural raw materials; unfortunately, the use of food crops may generate problems such as rising food prices, net energy losses to greenhouse gas emissions or changes in land use.² The recovery of residual biomass, which is not primarily intended for human consumption, avoids the ongoing *food versus fuel* predicament.

European statistics (2016) show that ethanol from lignocellulosic feedstock represents a
5% share, while crop-based feedstocks such as wheat, corn, sugars and other cereals
represent 32, 31, 24 and 8% respectively.³

9 The objective of this study is the assessment of a well-integrated process, based on organosolv fractionation of residual woodchips incorporated into a second generation 10 11 biorefinery or lignocellulosic biorefinery (LCB). Lignocellulosic feedstock is a promising 12 alternative to starch or sucrose containing materials (first generation biorefineries). Most of the renewable ethanol market is based on feedstocks such as maize, wheat, sugar beet 13 and other cereals. However, the lignocellulosic raw materials present favorable results in 14 15 terms of the output/input energy ratio, lower cost and high ethanol yields, which together with their high availability in locations with temperate and tropical climates, make this 16 raw material potentially advantageous.⁴ 17

It has been demonstrated that one of the critical points in relation to the biorefining process of wood-based raw material is the pre-treatment stage. In fact, it is one of the processing steps with the greatest costs in biorefinery facilities. In the last decade, several technologies have been reported in literature covering a wide range of categories: physical, biological, chemical and physico-chemical pre-treatments. The intended purpose of pretreatment technologies is the efficient fractionation of lignocellulose into its basic components: cellulose, lignin and hemicellulose. After efficient fractionation, the resulting streams should contain high value-added compounds in concentrations that
make purification or recovery economically feasible.⁵

Some pretreatment alternatives include wet oxidation,⁶ steam explosion,⁷ dilute acid pretreatment,⁸ ionic liquid pretreatment,⁹ ozonolysis,¹⁰ biological pretreatment¹¹ or organosolv digestion. As previously stated, this study is focused on a LCB that uses organosolv digestion as the fractionation technique. Authors such as Viel¹² or Laure¹³ have demonstrated the economic viability of organosolv as a fractionation technique in wood biorefineries.

Industrially, some companies have adopted the approach of demonstrating the viability of the biorefining process through pilot and demo scale implementation. Lignol Innovations in Canada¹⁴, has installed a plant facility (Lignol Biorefinery Technology) with a capacity of 100 metric tons/day of dry wood. The demonstration plant constitutes an integrated biorefinery producing ethanol and other added value products such as lignin and furfural, xylose or acetic acid. The Lignol pre-treatment step is an ethanol-based organosolv fractionation.

16 CIMV (Compagnie Industrielle de la Matière Végétale), in France, has developed 17 laboratory and pilot facilities, adequate for processing wheat straw or other agricultural 18 residues as feedstock. Organosolv fractionation using acetic and formic acids¹⁵ allows 19 relatively mild conditions for the pre-treatment of the feedstocks (atmospheric pressure 20 and maximum temperature of 110°C).

Abengoa Bioenergy New Technologies (ABNT) has also developed a demonstration plant in Spain with a capacity to process 70 t/d of feedstock. The plant processes wheat straw along with other agricultural residues. One of the main features is the use of enzymatic hydrolysis together with steam explosion as the biomass pre-treatment
 method¹⁶.

The Fraunhofer-Zentrum für Chemisch-Biotechnologische Prozesse (Fraunhofer CBP) in
Germany has developed a pilot-scale facility that processes up to 70 kg of dry hardwood
per batch. The pretreatment of wood is performed with ethanol based organosolv
fractionation and the main products obtained are glucose, lignin and xylose¹³.

7 Analyzing different case studies, it can be concluded that the viability of second generation biorefineries on a commercial scale is based on a few pillars. On the one hand, 8 9 economic and technical feasibility: the facility must produce benefits in an efficient way 10 and be technologically achievable. In the case of lignocellulosic biorefineries, the multi-11 product approach is favorable to this first premise. On the other hand, if the plant is versatile, the availability of feedstock is not a constraint for production. Therefore, under 12 this assumption, the objective must be to design biorefineries with the capacity to process 13 14 multiple types of raw materials.

Nowadays, the objective is to exploit alternative resources, which would have a positive impact on environmental sustainability and circular economy. The process must therefore show satisfactory environmental performance. The purpose of this study is, therefore, to assess the environmental sustainability of a large-scale simulated biorefinery. Life Cycle Assessment (LCA) is the methodology applied in this study for the evaluation of environmental impacts associated with the process value chain¹⁷.

The state of the art with regard to LCB proves that the concept of biorefining is not a novelty in itself. However, the aim of this report is to go beyond general considerations and address the real sustainability of intensive biomass exploitation through LCB. Some authors¹⁸ suggest that a biorefining facility will probably not be limited to the production

of just one high value added bioproduct. Therefore, the aim of this study is to address a
simple hypothesis. If the production scope of a lignocellulosic biorefinery is broadened,
is sustainability really improved?

4 Two illustrative cases have been identified to address the research question. Firstly, the so-called Biorefinery 1.0 was considered as a somewhat conventional biorefinery. This 5 6 facility achieves the pretreatment and conversion of wood into basic products such as 7 glucose, hemicellulose and lignin that do not undergo additional processing. The second 8 case study, Biorefinery 2.0, conveys a somewhat more advanced facility. Consideration was given to the possibility of further conversion to more specialized and higher value-9 10 added bioproducts, such as furfural and bioethanol. For the considered scenarios, material balances will be performed to obtain inventory data based on the project design of an 11 organosolv facility reported by Kautto et al.¹⁹ These data will be used to perform an 12 environmental and economic evaluation to benchmark alternative biorefinery 13 14 configurations.

15 **2. Materials and methods**

16 2.1 Goal and scope

The function of the system under study (LCB) is the use of lignocellulosic biomass to produce bio-products with marketable added value. The aim of the environmental study, performed in accordance with the LCA methodology, is to determine the process subsystems that significantly affect the overall environmental performance of the system. Hence, it is expected that the result of the study will identify the process hotspots in the biorefinery and their root cause.

The functional unit considered was the processing of 1 t/h of hardwood chips in thebiorefinery facility. It seems consistent to select a feedstock-based functional unit, as the

process is characterized by its multiple-output nature. On the other hand, one of the
 objectives of this study is to benchmark two plant schemes. Bearing in mind that each
 biorefinery has distinct outputs, the selection of the raw material input as a functional unit
 ensures consistency throughout the study.

The production scheme was assessed through a cradle-to-gate approach. It is a perspective
that allows us to consider the processes from the production of feedstock up to the plant
gate, that is, the products obtained, ready for the market.

8

2.2 Overview of production system

9 This section is intended to provide a generic description of the production system. To 10 address the research question, several plant configurations were considered through the 11 conception of case studies. The subsystems described below do not necessarily belong to 12 all the case studies. The specificities of the system boundaries regarding each case study 13 are defined in Section 2.3.

The generic system comprises all the process units involved in the ethanol organosolv pulping process, as well as the downstream units for the valorization of pulp and liquor, respectively. The feedstock of the process, as already mentioned, is residual beech woodchips supplied by a sawmill. The plant under assessment has a capacity to process 83.3 t/h of dry wood.

The foreground system includes process units that are the direct object of the present study. To provide meaningful results in terms of the process sections that will be inferred in more environmental loads, the system under study is divided into nine subsystems (SS) described below: SS0.Feedstock, SS1.Organosolv pulping, SS2.Solvent recovery, SS3.Hemicellulose conditioning, SS4.Enzymatic hydrolysis, SS5.Cogeneration unit, SS6.Fermentation to ethanol, SS7.Acetic acid recovery, SS8.Furfural recovery. Fig.1

depicts a block diagram of the plant identifying the system boundaries, subsystems and
main inputs and outputs. Note that the figure addresses the most complete view of the
LCB, including all possible subsystems considered in this study. Specific boundaries of
every case study are reported in Section 2.3.

5

-FIGURE 1-

6 **SS0.Feedstock** comprises forest activities for wood exploitation, sawmill activities and 7 chipping. These process sections and subsystems are implemented within the main subsystem. Feedstock production data have been adapted from other studies. SS0.1 8 includes activities ranging from soil preparation (use of fertilizers) to wood extraction.²⁰ 9 10 SS0.2 includes the sawmilling activities carried out to produce three main products: sawn timber, bark chips and residual wood.²¹ Residual wood is the feedstock considered for the 11 12 purpose of this study. The pre-processing of residual wood to prepare the feedstock for organosolv pulping is considered as SS0.3. Pre-processing activities include chopping of 13 14 wood as physical pre-treatment to obtain woodchips of a suitable size for further processing.²² All the environmental burdens derived from this subsystem were allocated 15 to this residual wood. Fig. 2 depicts the general system configuration considered for SSO. 16

17

-FIGURE 2-

SS1. Organosolv pulping. The process is based on the digestion of wood chips with ethanol (50% v/v) and 1.25% sulfuric acid at 180 °C for 60 min. The pulp is washed with water and ethanol solution and pumped through a screen to the enzymatic hydrolysis stage (SS4). The liquor is further hydrolyzed to obtain sugar monomers. Heat and a fraction of ethanol are recovered prior to SS2 operations.¹⁹ SS2. Solvent recovery. The SS1 liquor is diluted to an ethanol concentration of 15%
 (v/v) and cooled to 50°C to promote lignin precipitation. After lignin precipitation,
 ethanol is recovered by distillation and recycled to SS1.¹⁹

SS3. Hemicellulose conditioning. After solvent recovery, the liquor (sugar solution) is sent to a four-effect evaporation train. Low molecular weight soluble lignin (LMW) is easily separated after evaporation and has no added value so it is burned in the boiler (SS5). The aqueous stream is further subjected to liquid-liquid extraction with furfural, to separate the residual LMW lignin and other organic residues. Lastly, the addition of ammonia allows to adjust pH to 5 before fermentation in SS6.¹⁹

SS4. Enzymatic hydrolysis. Conversion to glucose from cellulose and hemicellulose is feasible through the use of an enzyme cocktail, mainly cellulase with a minor percentage of hemicellulases, allowing a partial conversion of unreacted hemicellulose to hemicellulosic sugars. This process takes place in an enzymatic reactor at 48°C and a residence time of 84 hours.¹⁹ On-site enzyme production is included in this subsystem.^{23,24}

SS5. Electricity and heat cogeneration. This process needs significant energy input. Thus, the operation of a boiler is considered to meet the demands of steam and electricity, using biogas, WWT sludge, bark and all the organic waste from the different subsystems. In this way, it is possible to valorize the different waste streams. The contribution of natural gas as an external energy source is also considered necessary to balance energy demand.¹⁹

SS6. Fermentation to ethanol. The streams from the enzymatic hydrolysis and the diluted hemicellulosic sugar are used as culture medium for the fermentation stage, using *Zymomonas mobilis* as microorganism. In addition, corn liquor and diammonium phosphate are added as nutrient sources. After obtaining a sufficient volume of inoculum,

the main fermenter of the process is operated with culture medium with a composition
similar to that of the inoculum train.¹⁹

SS7. Acetic acid recovery. It is possible to recover the fraction of acids (acetic and
formic) from the condensates obtained in the evaporator train (SS3). For this purpose, a
liquid-liquid extraction (in a mixer-settler column) with triocyphosphine oxide (TOPO)
in undecane is used. Undecane and TOPO are used in a closed circuit, however, for the
purpose of LCA, 1% loses are considered in the circuit. This subsystem includes, as well,
three distillation columns with intermediate decanting steps to separate the acetic acid (at
the bottom of the third column) at 97% purity.¹⁹

SS8. Furfural recovery. As a lateral extraction of the distillation columns used for
ethanol recovery (SS2), a furfural stream is recovered. The side-draw from the distillation
columns is further separated in a decanter, where the aqueous phase is recycled to SS2.
Part of the recovered furfural is used as extraction solvent to recover LMW lignin in SS3;
the rest of the recovered furfural can be commercialized.¹⁹

15 The background system consists of processes that indirectly influence the system, and 16 contribute to environmental impacts. The background systems include the chemical 17 production of ethanol, sulfuric acid and ammonia as well as transport.

18

2.3 Definition of the system boundaries

Alternative approaches were assessed parting from the system layout described above.
Based on the general outline presented in Section 2.2, several hypothetical case studies
have been considered. The case studies differ in terms of the downstream options
considered and the final products obtained. Table 1 provides a summary of the schemes
considered.

24

<TABLE1>

The simplest considered scenario is a biorefinery with the function of producing the most
basic chemicals feasible to be obtained with minimum downstream processing.
Biorefinery 1.0 produces glucose, hemicellulose and lignin, with a disposition similar to
that studied by Laure et al.¹³ The system boundaries are reduced to six subsystems
presented in Fig. 3.

Biorefinery 2.0 was assessed as shown in Fig. 4. The aim of this biorefinery is to produce
bioethanol, furfural and lignin. This involves the inclusion of the processing steps in
subsystems 6 and 7 for fermentation to ethanol and furfural recovery. Under the scope of
Biorefinery 2.0, two distinct scenarios have been proposed for discussion.

i. Furfural recovery methods (scenarios 2.1-2.4). In Biorefinery 2.0, furfural was
 recovered through distillation.¹⁹ However, the recovery of furfural exclusively by
 distillation is an energy consuming process.

Furfural is the precursor of multiple furan-based biochemicals and biofuels that could 13 14 eventually lead to substitution of the petroleum based counterparts. It is listed as one of the top 30 biomass derived platform compounds by the US. Department of Energy.²⁵ 15 Improving the efficiency of furfural recovery may be a significant aspect given its 16 importance in the market. Nhien et al.²⁶ have proposed an alternative arrangement for the 17 recovery of furfural obtained from lignocellulosic biomass. The process implements a 18 two-step recovery system, combining extraction and distillation. Liquid-liquid extraction 19 20 with three different solvents (toluene, benzene, and butyl chloride) results in two streams: 21 an extract, containing most of the furfural in the feed stream, and a raffinate. The extract 22 was then introduced into a distillation column to separate furfural and the solvent, which was recycled. 23

ii. Acetic acid co-production (scenario 2.5). Acetic acid is usually produced in bulk 1 2 fermentation. The production of acetic acid has not been considered in the Biorefinery 2.0 case study, in view of the very low amount produced from such a common chemical. 3 Therefore, an additional scenario has been considered to allow discussion about the 4 adequacy of implementing acetic acid recovery onto the biorefinery route (Fig. 1). The 5 objective is to assess whether the co-production of acetic acid provides advantageous 6 7 results considering economic and environmental factors.

8

-FIGURE 3-

-FIGURE 4-

9

10

2.4 Life cycle inventory

Life Cycle Inventory (LCI) is the compilation of the dataset for this assessment. In this 11 12 study, basic process data, material balances as well as the biochemical production route considered have been adapted from the simulation of an organosolv process for 13 bioethanol production.¹⁹ Foreground data consists therefore of peer-reviewed literature 14 15 sources (secondary data). The background system components (transport, chemicals, water), have been detailed through the Ecoinvent® database. A summary of data sources 16 considered for inventory collection is presented in Table 2. Tables 3 and 4 display the 17 18 inventories of the foreground systems considered throughout the life cycle assessment.

- <TABLE2> 19 20 <TABLE3> <TABLE4>
- 21
- 22
- 23
- 24
- 25
- 26

1

2.5 Method

The ReCiPe 1.12 hierarchist method²⁷ was used for the selection of characterization
factors. Impact categories at midpoint level were studied. SimaPro 8.02 software was
used for the computational implementation of the inventories.

5 Although all categories of the ReCiPe method were studied, environmental results are 6 presented in terms of the following impact categories: climate change (CC), ozone 7 depletion (OD), terrestrial acidification (TA), freshwater eutrophication (FE), marine 8 eutrophication (ME), human toxicity (HT), photochemical oxidant formation (POF), 9 freshwater ecotoxicity (FET), marine ecotoxicity (MET) and fossil depletion (FD). In 10 analyzing the results of standardization, the above-mentioned impact categories are the 11 most representative of European values.^{28–30}

12 2.6 Allocation

According to the considered disposition of SS0, multiple products are obtained as output of the subsystem (Fig. 2). However, not all wood products are used as input of the organosolv pulping subsystem (SS1). The total environmental impacts do not fully correspond to the residual woodchips used as raw material. Therefore, allocation of impacts to residual woodchips has been applied.

Mass allocation could be considered as a viable option, allocating impacts to co-products
in proportion to the produced volume of each product; volumetric allocation factors are
51% for sawn timber, 13% for bark chips and 36% for residual woodchips.

However, even if all products from SS0 are marketable, they do not have the same economic value. Considering the reference market prices of products from sawmills³¹ the allocation factors are modified to 77% for sawn timber, 14% for bark and 9% for woodchips. Nowadays, residual wood is not as valuable for other applications, as can be

seen through the calculated economic allocation factors. The second allocation method
 better reflects the purpose of finding a niche market for the residual fraction of a sawmill.
 It should be noted that the economic allocation has been considered for SS0.1 and SS0.2,
 but not for SS0.3, since this subsystem only treats residual wood to obtain woodchips.

5

2.7 Assumptions and limitations

The results presented in this study may show some uncertainty arising from assumptions
made due to data gaps. The following are the hypotheses considered throughout the
evaluation as the best possible approximation.

9 i. Transport of woodchips from SS0 to SS1 is the only transport process included. The
10 transport distance has been considered as 100 km, and impacts derived from transport
11 have been assigned to SS1. Lorry freight (16-32 metric tons) was the selected mode of
12 transport. Transport losses of 5% have been considered, with a resulting tonne-kilometre
13 (tkm) value of 105 tonne-kilometre.

14 ii. One of the distinctive characteristics of the considered system is the cogeneration unit 15 (SS5). Cogeneration provides energy and steam to the entire system through the burning of natural gas and process residues in a dual boiler. When a subsystem consumes 16 17 electricity or uses utilities, these are supplied entirely through the cogeneration subsystem. This means that the impacts assigned to SS5 can be divided between 18 subsystems that consume energy. This is relevant for the sake of result interpretation. 19 20 Although a subsystem may not present any direct contribution to impacts, strictly speaking, a fraction of the SS5 impacts would be caused indirectly by the subsystem's 21 22 energy and/or steam consumption.

iii. No infrastructure process was considered in the assessment to assure uniformity ofconditions across all subsystems.

iv. The cogeneration unit of the plant supplies electricity to SS1, SS2, SS3, SS4 (except
for on-site enzyme production), SS6, SS7, SS8. Among these subsystems, SS1 is the main
electricity and steam consumer with a percentage of demand with respect to the total
around 35%. Subsystem 0 includes off-site activities ranging from forestry to wood pretreatment; electricity demands for SS0 are retrieved directly from the grid.

6 **3. Results**

7 The relative contributions to the environmental burdens in each of the selected impact
8 categories are presented below for each studied alternative. The contribution of each
9 process subsystem to each category is shown, allowing the critical points of the process
10 to be discerned.

11

3.1 Environmental performance of Biorefinery 1.0

The characterization results of Biorefinery 1.0 are shown in Figure 5. Analyzing the complete set of environmental results, SS1 can be appointed as the most burdening subsystem; however, there was no major difference with respect to SS4 (enzymatic hydrolysis) or SS5 (cogeneration unit). Nevertheless, SS1 is the largest energy and steam consumer, therefore, it is indirectly responsible for a significant fraction of environmental impacts associated to SS5.

The feedstock subsystem (SS0) presented a considerably uniform distribution of environmental impacts across all categories, with contributions always below 23%. Freshwater eutrophication (23%), marine eutrophication (19%) and climate change (18%) were the groups most affected by wood preparation activities. SS0 contributions were mostly appointed to SS0.2 (sawmill activities). Sawmill activities require high electricity consumption due to the use of machinery; electricity for SS0 is directly retrieved from the grid and not from the cogeneration unit. Other burdens were derived from the use of

lubricant oil for maintenance, plastics for packaging and chemicals for finishing
 operations.

Photochemical oxidant formation was the most impacted category in the organosolv pulping subsystem with a share of 43%. This is mainly due to emissions of volatile organic compounds from road transport of woodchips to the site. The organosolv pulping subsystem (SS1) presented the largest contributions to ozone depletion, terrestrial acidification and human toxicity, with values of 38, 27 and 34% respectively. SS1 was the second major contributor to climate change with 22%. Factors from SS1 responsible of CC were mainly emissions from road transport of woodchips.

10 Solvent recovery and hemicellulose conditioning (SS2 and SS3) did not contribute 11 significantly to the overall environmental impact of the system. Solvent recovery (SS2) 12 caused contributions to impact categories ranging from 1 to 13%. Hemicellulose 13 conditioning presented slightly higher values ranging from 5 to 16%. In general, the 14 contributions to the environmental profile were not significant.

The environmental impacts of SS4 were the result of enzyme production. For this subsystem, eutrophication categories (freshwater and marine) were the most impacted, together with marine ecotoxicity. Surprisingly, the contributions of this subsystem are very comparable to the organosolv pre-treatment. However, it should be noted that the cogeneration unit does not supply the heat and electricity demands, as the on-site cellulase production unit is not present in the plant originally considered. Enzyme production is the only input process into SS4.

For climate change, freshwater ecotoxicity and fossil depletion, SS5 was the most
burdensome subsystem, with a maximum relative contribution of 40% allocated to fossil
depletion. Although SS5 partly uses process residues to burn, it also needs a fresh supply

of natural gas to meet the energetic demand of the plant. On the other hand, CO₂ emissions
 from the boiler also contribute to the overall results.

3

-FIGURE 5_Use Color-

4

3.2 Environmental performance of Biorefinery 2.0

Figure 6 depicts the characterization results of Biorefinery 2.0. The results show the 5 6 impacts for the subsystems in the advanced biorefinery, producing bioethanol, furfural 7 and lignin. Although the furfural recovery subsystem (SS8) was included in the analysis, 8 it showed no environmental impacts. The only input of the furfural recovery subsystem 9 is energy supplied by SS5. As mentioned in Section 2.7, although SS8 did not have direct 10 environmental burdens to any category, one must assume that indirectly, part of the 11 burdens assigned to SS5, were in fact due to energetic consumption in SS8. In general, 12 the environmental profile of the plant has not been greatly affected by the addition of more downstream processing units. 13

The feedstock subsystem (SS0) presented the same results as in Biorefinery 1.0 with very
slight changes and contributions always below 22%. Freshwater eutrophication (22%),
marine eutrophication (17%) and climate change (17%) were the most impacted groups.

For SS1 the profile was once again quite similar to Biorefinery 1.0. Photochemical oxidant formation was the most impacted category in the organosolv pulping subsystem with a share of 39%. Ozone depletion (37%) and human toxicity (33%) categories contributed to SS1 total impacts with values close to POF. SS1 also contributed to emissions due to the use of chemicals (ethanol and sulfuric acid). Organosolv pulping was the greatest contributor among the subsystems in 4 out of 10 impact categories.

Solvent recovery and hemicellulose conditioning (SS2 and SS3) did not greatly contribute
to the overall results. Solvent recovery made contributions to impact categories ranging

from 2 to 12%. Hemicellulose conditioning presented slightly higher values ranging from
 5 to 15%.

Enzymatic hydrolysis (SS4) contributed to overall impacts with significant values. The 3 4 same reasoning as Biorefinery 1.0 can be used. Although the results are comparable to the organosolv pulping subsystem, organosolv does not include its impact contributions 5 6 due to the consumption of electricity, heat and steam. Cellulase production is a highly 7 energy-intensive fermentation process, which, together with the carbon source consumption contribute to the overall results in SS4. Both eutrophication categories 8 presented relevant contributions to the total results (46 and 28% for FE and ME 9 10 respectively) mainly due to water consumption in the fermentation process.

11 The largest contribution to the fossil depletion category was originated in the 12 cogeneration unit (44%), specifically due to the use of natural gas as fuel. The 13 cogeneration subsystem was the main contributor to climate change (33%).

Finally, the fermentation subsystem contributed slightly to the overall environmental results. Contributions to terrestrial acidification (17%) and marine eutrophication (13%) were the major impacts caused by SS6. Overall, the fermentation subsystem was not very significant for the sum of the total impacts. The environmental profile of the plant was not significantly altered due to the ethanol fermentation subsystem.

19

-FIGURE 6_Use Color-

20

3.3 Environmental performance of Biorefinery 2.0 with acetic acid co-production

No significant overall differences were found when analyzing Biorefinery 2.0 and Biorefinery 2.0 with the co-production of acetic acid (Fig. 7). The environmental profile of the overlapping subsystems was maintained, and the only difference was the incorporation of environmental impacts due to SS7. SS7 for acetic acid co-production presents the major contributions to ozone depletion
 (39%) followed by considerable impacts to fossil depletion (23%) and photochemical
 oxidant formation (15%). All contributions to every impact category from SS7 originate
 from the use of chemicals (TOPO and undecane).

5

-FIGURE 7_Use Color-

6

3.4 Comparative assessment of Biorefineries

Comparative assessments for every biorefinery scenario displayed reasonable results
(Fig. 8). The increasing complexity of biorefineries showed a proportional increase of the
environmental impacts for each category. Biorefinery 2.0 with acetic acid co-production
(scenario 2.1) displayed the greatest burdens for all impact categories. In contrast, the
simplest scenario (Biorefinery 1.0) displayed the lowest environmental impacts overall.

According to expectations, when the biorefinery increased its downstream processing steps, the number of equipments, inputs from technosphere, emissions, etc., the environmental impacts were greater. However, this comparative analysis alone is not sufficient to assess whether one scenario is more environmentally efficient than another. Since the function of every biorefinery changed for each scenario, the facilities were not considered comparable and therefore further analysis should be performed.

18

-FIGURE 8 Use Color-

19 *3.5 Comparative assessment of furfural recovery methods*

The comparative assessment for the recovery of furfural with four different alternatives (scenarios 2.1, 2.2, 2.3 and 2.4) is illustrated in Fig. 9. Seven out of ten categories presented higher impacts when considering only distillation. Only climate change, ozone depletion and fossil depletion displayed the hybrid extraction process with toluene as the most unfavorable scenario. These categories (CC, OD and FD) were the most impacted
 because the hybrid alternative uses fossil-based extractants for separation.

3	The extraction-distillation hybrid (for all the solvents studied) presented a better
4	environmental performance than the purification process through distillation, mainly
5	because it consumes less energy. The results showed that the use of benzene for extraction
6	in the hybrid process was the best-case scenario among the alternatives studied. In
7	general, the hybrid separation is more efficient, technologically feasible and
8	environmentally friendly.
9	-FIGURE 9-Use Color-
10	4. Discussion
11	4.1 Eco-efficiency assessment of the considered scenarios

As reported through Sections 3.1 to 3.4, one would assume that the most environmentally sustainable LCB is Biorefinery 1.0. However, the research question is not fully answered through the concluding remarks on the results section. The objective of this study was to perform the holistic sustainability assessment of a Biorefinery and to conclude whether a more complex biorefinery would be more sustainable than a simplistic one.

In accordance with ISO 14045,³² the concept of eco-efficiency acknowledges the consideration of environmental factors along with the value of the system to stakeholders. Considering the economic benefit of each LCB scenario in parallel to the environmental indicators, an in-depth assessment of the concept of sustainability of integrated biorefineries is clearly given. Other studies have concluded the imminent need to integrate issues related to environmental impacts and economic profitability in order to simultaneously evaluate processes and technologies. Quantitative evaluation of the different provisions across both perspectives is highly profitable for stakeholders and
 companies.³³

3 The monetary benefit of each biorefinery according to product sales prices (Table 5) was 4 the selected economic indicator for the assessment of eco-efficiency. When the emission 5 factor is presented per unitary benefit potentially achieved by the biorefinery, the outcome 6 of the assessment is different. In fact, the eco-efficiency indicator is a reliable tool to 7 make comparable two systems which are not. Biorefinery 2.0 attains lower emissions per 8 unitary benefit than Biorefinery 1.0. The eco-efficiency indicator (Table 6) for each impact category is lower for Biorefinery 2.0 in all cases except for ozone depletion and 9 10 terrestrial acidification. Conversely, Biorefinery 2.5 (which includes acetic acid coproduction) does not follow the same trend and is less environmentally sustainable. 11

12

<TABLE5>

<TABLE6>

13

The objectives for optimizing eco-efficiency in a biorefinery are to minimize environmental impacts and maximize economic benefits. Figure 10 is the representation of the eco-efficiency indicator used in this study combining economic benefits with CO₂ emissions. The set of biorefineries evaluated are solutions to the optimization problem; however, the best-case scenario is achieved when the solutions fall in the Q3 quarter of the graph.

When the expansion of the biorefinery is specifically performed for specialty bioproducts, the biorefinery is more sustainable. However, the production of bulk chemicals such as acetic acid in this type of facility is not as environmentally sustainable, especially when the production volume is very small. Therefore, the suggestion resulting from the results of the study would be to broaden the multi-production spectrum of the biorefinery only when the production volume and the type of product are reasonable. From an

environmental point of view, an integrated biorefinery is sustainable when the
 intensification of resource demand is not counterproductive.

3

-FIGURE 10-Use Color-

4

4.2 Acetic acid co-production

5 If the sustainability of a biorefinery is variable, then, what biorefinery products should be 6 produced? In the case of acetic acid co-production, for instance, its recovery from the 7 biorefinery route includes the use of TOPO and undecane, chemicals that, although 8 recycled, have high environmental impacts. Therefore, the recovery of acetic acid is not 9 sustainable. In fact, the average production of acetic acid in bulk is a feasible process of 10 fermentation,³⁴ avoiding the use of TOPO and undecane as well as petrochemical 11 production options.

The production of acetic acid through a LCB increases potential revenues as demonstrated in this assessment and in agreement to other studies.^{35,36} However, the negative environmental consequences shift the overall eco-efficiency indicator towards the Q2 quarter (Fig. 10), where economic benefits are high, but so are CO₂ emissions also contribute to climate change.

17 *4.3 Furfural recovery*

One of the outcomes of this study is the need not only to integrate the co-production of various bioproducts but to also optimize existing processes in the biorefinery route. An example would be the recovery of furfural. Recovery of furfural through less energyintensive methods reduces global environmental impacts (Fig. 9), which, in fact, improves the ecoefficiency indicator. For the same production volume of furfural, fewer overall impacts are obtained for the benzene extraction-distillation alternative (Scenario 2.2).

1 This seems relevant in relation to fluctuations of furfural market prices.³⁷ If the process 2 is not fully optimized, a slight variation in the furfural price may change the eco-3 efficiency indicator towards the Q4 quarter (Fig. 10) where overall benefits are not 4 relevant.

5

4.4 Enzyme production

6 The enzymatic hydrolysis considered in the present system under study presents relevant 7 impacts with respect to the biorefinery as a whole. It seems quite unlikely as the impacts of SS4 are derived from on-site enzyme production. Furthermore, enzyme dosage for 8 9 hydrolysis does not constitute a significant amount. However, environmental results are aligned with the cost of enzyme production. Other studies have demonstrated the 10 11 implications that enzyme production has on total costs and emissions for the production of lignocellulosic ethanol.³⁸ The further integration of enzyme production into the 12 biorefinery is expected to result in a reduction of the total impacts aiming for a scenario 13 in which total environmental burdens can be reduced. As in other studies³⁹ enzyme 14 15 production technologies significantly affect environmental impacts and LCA results may be sensitive to changes in this subsystem. 16

17 **5.** Conclusions

Biorefining systems have been studied with the aim of reducing environmental burdens. However, the topic on biorefineries is extensive and varied. Comparison of results with other studies is troublesome. Therefore, the introduction of eco-efficiency and exemplification through different biorefining scenarios is a steppingstone for the optimization of bioproduction.

Data on integrated biorefineries producing multiple bio-based products is scarce. The
evaluation of facilities with primary data should provide an interesting background on the

best configurations towards sustainability of biorefineries. On the other hand, if data
availability is not a constraint, future research should focus on the assessment of a wider
range of biorefinery scenarios.

Finally, regarding the system under study, optimization of LCB hotspots should focus on further integration of enzyme production, optimization of technologies for the manufacture of high value added bioproducts and the optimization of the organosolv pretreatment process. It would be advantageous, as well, to study possibilities of further energy optimization to achieve full integration of the plant.

9 Acknowledgements

This research was supported by the Spanish Government (Ministry of Economy and
Competitiveness) through the ERA-IB2 project 2G-Enzymes (PCIN-2015-031) and the
European project STARProBio (Grant Agreement Number 727740). The authors belong
to the Galician Competitive Research Group GRC2013-032 and to the CRETUS Strategic
Partnership (AGRUP2015/02). All these programmes are co-funded by FEDER (EU).

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1 Tables

Case study	Description	Products	Subsystems included
Biorefinery 1.0	Basic biorefinery	glucose, lignin, hemicellulose	SS0-SS5
Biorefinery 2.0	Advanced biorefinery	ethanol, furfural, lignin	SS0-SS6 and SS8
Scenario 2.1	Distillation for furfural recovery	ethanol, furfural, lignin	SS0-SS6 and SS8
Scenario 2.2	Hybrid extraction- distillation with benzene for furfural recovery	ethanol, furfural, lignin	SS0-SS6 and SS8
Scenario 2.3	Hybrid extraction- distillation with toluene for furfural recovery	ethanol, furfural, lignin	SS0-SS6 and SS
Scenario 2.4	Hybrid extraction- distillation with butyl chloride for furfural recovery	ethanol, furfural, lignin	SS0-SS6 and SS
Scenario 2.5	Implementation of acetic acid co-production	ethanol, furfural, lignin, acetic acid	SSO-SS8

Table 1: Studied scenarios and specification of boundaries

1 Table 2: Summary of data sources

Subsystem	Bibliographic source
SS0. Feedstock	
SS0.1 Forest activities	20
SS0.2 Sawmill	21
SS0.3 Chipping	22
SS1. Organosolv pulping	19
SS2. Solvent recovery	19
SS3. Hemicellulose conditioning	19
SS4. Enzymatic hydrolysis	19
Enzyme production	23, 24
SS5. Cogeneration unit	19
SS6. Fermentation to ethanol	19
SS7. Acetic acid recovery	19
SS8. Furfural recovery	19

SS0.1 Forest activiti	es	
Inputs from technosphere		
Diesel	1.03	kg
N-mineral fertilizer	0.15	kg
Outputs to environment		
N_2	13.54	g
NH ₃	1.85	g
NO _x	2.50	g
SS0.2 Sawmill		
Inputs from process		
Roundwood from SS0.1	0.71	m ³
Inputs from technosphere		
Water	244.38	kg
Lubricating oil	0.09	kg
Steel (packaging)	0.11	kg
Polyethylene (HDPE)	0.16	kg
Inorganic chemicals	22.11	g
(pretreatment)		
Organic chemicals (solvent)	0.66	g
Electricity	19.18	kw
Outputs to environment		
Heat	422.63	MJ
CO_2	30.76	kg
CO	15.67	g
NO _x	34.79	g
Particulates	14.98	g
SO_2	0.82	g
Municipal solid waste	1.50	kg
Outputs to technosphere		
Bark chips	0.10	m ³
Sawn timber	0.41	m^3
SS0.3 Chipping		
Inputs from process		
Residual wood from SS0.1	1.28	m^3
Inputs from technosphere		
Electricity	2.30	kw
Outputs to SS1		
Residual wood chips	1.25	m^3

Table 3: Inventory for feedstock related activities. Inventory is presented with
economic allocation to SS0.1 and SS0.2

- .

1	Table 4 : Global inventory for the lignocellulosic biorefinery considering all possible
2	subsystems for the functional unit (1 t/h dry wood chips)

SS1 Pulping		
Inputs from technosphere		
Water (pulping)	3.72	t
Water (washing)	4.56	t
Sulfuric acid	$1.01 \cdot 10^{-2}$	t
Ethanol (pulping)	3.74	t
Transport, freight, lorry (16-32 metric ton)	105	tkm
High pressure steam	1.97	GJ
Electricity (pulping)	7.80.10-2	MWh
SS2 Solvent recovery		
Inputs from technosphere	1.00	
Water (dilution)	1.02	t
Natural gas	$5.40 \cdot 10^{-3}$	t
Low pressure steam	0.77	GJ
Electricity	$6.00 \cdot 10^{-2}$	MWh
Outputs to technosphere		
Lignin	0.16	t
SS3 Hemicellulose condition	oning	
Inputs from technosphere	1	
Furfural (makeup)	$1.92 \cdot 10^{-3}$	t
Ammonia	$6.24 \cdot 10^{-3}$	t
Low pressure steam	0.36	t
High pressure steam	0.21	GJ
	_	
SS4 Enzymatic hydrolys	sis	
Inputs from technosphere	- 00 10 ³	
Enzyme (cellulase)	$7.80 \cdot 10^{-3}$	t
Electricity	$2.04 \cdot 10^{-2}$	MWh
Low pressure steam	$9.12 \cdot 10^{-2}$	GJ
Cellulase production (7.8	kg)	23
Inputs from technosphere		
Corn steep liquor	4.53	kg
Ammonia	0.61	kg
Water	577.74	kg
Nutrients	2.48	kg
Inutrents		
Heat	37.90	MJ
	37.90 81.84	
Heat Electricity		
Heat Electricity Outputs to environment	81.84	MJ 27
Heat Electricity		

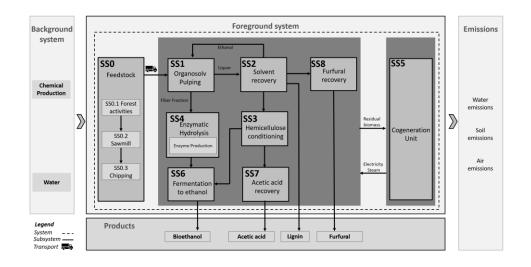
	SS5. Cogeneration un	it	
1	Inputs from technosphere	11	
T	Water	0.68	t
	Sludge (from WWT)	$5.78 \cdot 10^{-2}$	t 2
	Biogas (from WWT)	$4.27 \cdot 10^{-2}$	t t
3	Natural gas	$4.27 \cdot 10^{-2}$ 2.26 \cdot 10^{-2}	t t
	Outputs to environment	2.20.10	ι
4	CO ₂	6.84	lr.a
	_		kg kg 5
	Water (vapor)	108.84	kg ⁵
6	SS6. Fermentation to bioe	thanol	
7	Inputs from technosphere		
7	Water	0.21	t
8	Diammonium phosphate	$1.68 \cdot 10^{-3}$	t
	Corn steep liquor	$1.00 \ 10^{-2}$ $1.27 \cdot 10^{-2}$	t
9	Low pressure steam	1.74	GJ
10	Electricity	$8.40 \cdot 10^{-3}$	MWh
10	Outputs to technosphere	0.40.10	
11	Bioethanol	0.24	+
		0.24	t
12	Water	0.37	t
	Outputs to environment	010 77	1
13	CO_2	218.77	kg
14	O_2	1.44	kg
14	Wastewater	0.0034	m ³
15	SS7. Acetic acid recove	ery	
	Inputs from technosphere		16
	Low pressure steam	0.39	GJ ¹⁶
17	Low pressure steam Electricity	0.39 3.48·10 ⁻²	GJ ¹⁰ MWh
17	-		GJ
17 18	Electricity	$3.48 \cdot 10^{-2}$	GJ MWh
18	Electricity TOPO	3.48·10 ⁻² 3.32	GJ MWh kg
	Electricity TOPO Undecane	3.48·10 ⁻² 3.32 11.93	MWh kg kg
18 19	Electricity TOPO Undecane Outputs to technosphere Acetic acid	3.48·10 ⁻² 3.32	MWh kg kg
18	Electricity TOPO Undecane Outputs to technosphere	3.48·10 ⁻² 3.32 11.93	GJ MWh kg kg t
18 19	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO	3.48 · 10 ⁻² 3.32 11.93 1.56 · 10 ⁻²	GJ MWh kg kg t
18 19 20 21	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane	3.48·10 ⁻² 3.32 11.93 1.56·10 ⁻² 3.32 11.93	GJ MWh kg kg t
18 19 20	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane SS8. Furfural recover	3.48·10 ⁻² 3.32 11.93 1.56·10 ⁻² 3.32 11.93	GJ MWh kg kg t
18 19 20 21	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere	3.48·10 ⁻² 3.32 11.93 1.56·10 ⁻² 3.32 11.93	GJ MWh kg t t kg kg
18 19 20 21 22 23	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam	$3.48 \cdot 10^{-2}$ 3.32 11.93 1.56 \cdot 10^{-2} 3.32 11.93 y 2.40 \cdot 10^{-3}	GJ MWh kg t t kg kg GJ
18 19 20 21 22	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam Electricity	3.48·10 ⁻² 3.32 11.93 1.56·10 ⁻² 3.32 11.93	GJ MWh kg t t kg kg
18 19 20 21 22 23 24	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam Electricity Outputs to technosphere	$3.48 \cdot 10^{-2}$ 3.32 11.93 1.56 \cdot 10^{-2} 3.32 11.93 Y 2.40 \cdot 10^{-3} 2.40 \cdot 10^{-2}	GJ MWh kg t t kg kg GJ MWh
18 19 20 21 22 23	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam Electricity	$3.48 \cdot 10^{-2}$ 3.32 11.93 1.56 \cdot 10^{-2} 3.32 11.93 y 2.40 \cdot 10^{-3}	GJ MWh kg t t kg kg GJ
18 19 20 21 22 23 24	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam Electricity Outputs to technosphere	$3.48 \cdot 10^{-2}$ 3.32 11.93 1.56 \cdot 10^{-2} 3.32 11.93 Y 2.40 \cdot 10^{-3} 2.40 \cdot 10^{-2}	GJ MWh kg t t kg kg GJ MWh
18 19 20 21 22 23 24 25 26	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam Electricity Outputs to technosphere	$3.48 \cdot 10^{-2}$ 3.32 11.93 1.56 \cdot 10^{-2} 3.32 11.93 Y 2.40 \cdot 10^{-3} 2.40 \cdot 10^{-2}	GJ MWh kg t t kg kg GJ MWh
18 19 20 21 22 23 24 25	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam Electricity Outputs to technosphere	$3.48 \cdot 10^{-2}$ 3.32 11.93 1.56 \cdot 10^{-2} 3.32 11.93 Y 2.40 \cdot 10^{-3} 2.40 \cdot 10^{-2}	GJ MWh kg t t kg kg GJ MWh
18 19 20 21 22 23 24 25 26	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam Electricity Outputs to technosphere	$3.48 \cdot 10^{-2}$ 3.32 11.93 1.56 \cdot 10^{-2} 3.32 11.93 Y 2.40 \cdot 10^{-3} 2.40 \cdot 10^{-2}	GJ MWh kg t t kg kg GJ MWh
 18 19 20 21 22 23 24 25 26 27 	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam Electricity Outputs to technosphere	$3.48 \cdot 10^{-2}$ 3.32 11.93 1.56 \cdot 10^{-2} 3.32 11.93 Y 2.40 \cdot 10^{-3} 2.40 \cdot 10^{-2}	GJ MWh kg kg t kg GJ MWh
 18 19 20 21 22 23 24 25 26 27 	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam Electricity Outputs to technosphere	$3.48 \cdot 10^{-2}$ 3.32 11.93 1.56 \cdot 10^{-2} 3.32 11.93 Y 2.40 \cdot 10^{-3} 2.40 \cdot 10^{-2}	GJ MWh kg kg t kg GJ MWh
 18 19 20 21 22 23 24 25 26 27 28 29 	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam Electricity Outputs to technosphere	$3.48 \cdot 10^{-2}$ 3.32 11.93 1.56 \cdot 10^{-2} 3.32 11.93 Y 2.40 \cdot 10^{-3} 2.40 \cdot 10^{-2}	GJ MWh kg kg t kg GJ MWh
 18 19 20 21 22 23 24 25 26 27 28 	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam Electricity Outputs to technosphere	$3.48 \cdot 10^{-2}$ 3.32 11.93 1.56 \cdot 10^{-2} 3.32 11.93 Y 2.40 \cdot 10^{-3} 2.40 \cdot 10^{-2}	GJ MWh kg kg t kg GJ MWh
 18 19 20 21 22 23 24 25 26 27 28 29 	Electricity TOPO Undecane Outputs to technosphere Acetic acid Outputs to environment TOPO Undecane <u>SS8. Furfural recover</u> Inputs from technosphere Low pressure steam Electricity Outputs to technosphere	$3.48 \cdot 10^{-2}$ 3.32 11.93 1.56 \cdot 10^{-2} 3.32 11.93 Y 2.40 \cdot 10^{-3} 2.40 \cdot 10^{-2}	GJ MWh kg kg t kg GJ MWh

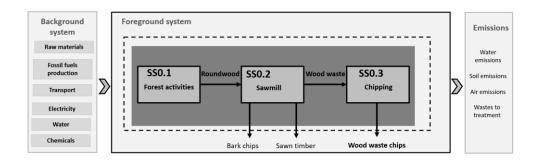
	Product	Average market selling price (€/t)
	Glucose	355.0 ^{23,40}
	Lignin	530.6 ^{41–45}
	Hemicellulose	105.4 46-48
	Bioethanol	830.5 ^{49–53}
	Furfural	865.3 37,54-58
2	Acetic acid	834.2 36,59-61
2		
3		
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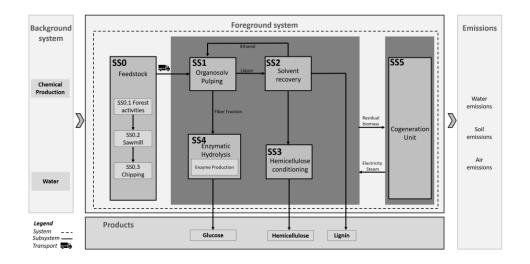
Table 5: Market selling prices of products obtained in the biorefinery configurations

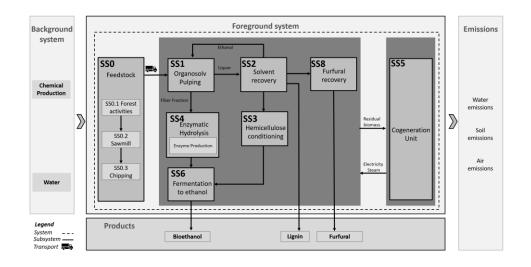
Table 6: Eco-efficiency indicator, calculated for every impact category considered in
 the study and for every biorefinery scenario

CC (kg CO2 eq/€) 0.47 0.42 0.45 OD (kg CFC-11 eq/€) $5.34 \cdot 10^{-8}$ $7.64 \cdot 10^{-8}$ $4.38 \cdot 10^{-8}$ TA (kg SO2 eq/€) $2.32 \cdot 10^{-3}$ $2.41 \cdot 10^{-3}$ $2.62 \cdot 10^{-3}$ FE (kg P eq/€) $9.85 \cdot 10^{-5}$ $8.32 \cdot 10^{-5}$ $8.42 \cdot 10^{-5}$ ME (kg N eq/€) $5.81 \cdot 10^{-5}$ $5.52 \cdot 10^{-5}$ $5.91 \cdot 10^{-5}$ HT (kg 1,4-DB eq/€) $1.26 \cdot 10^{-3}$ $1.13 \cdot 10^{-3}$ 0.097 POF (kg NMVOC/€) $3.04 \cdot 10^{-3}$ $2.64 \cdot 10^{-3}$ $2.75 \cdot 10^{-3}$ FET (kg 1,4-DB eq/€) $2.62 \cdot 10^{-3}$ $2.19 \cdot 10^{-3}$ $2.23 \cdot 10^{-3}$ MET (kg 1,4-DB eq/€) 0.24 0.22 0.28	Eco-efficiency indicator	Biorefinery 1.0	Biorefinery 2.0	Biorefinery 2.
TA (kg SO2 eq/€) $2.32 \cdot 10^{-3}$ $2.41 \cdot 10^{-3}$ $2.62 \cdot 10^{-3}$ FE (kg P eq/€) $9.85 \cdot 10^{-5}$ $8.32 \cdot 10^{-5}$ $8.42 \cdot 10^{-5}$ ME (kg N eq/€) $5.81 \cdot 10^{-5}$ $5.52 \cdot 10^{-5}$ $5.91 \cdot 10^{-5}$ HT (kg 1,4-DB eq/€) $1.26 \cdot 10^{-3}$ $1.13 \cdot 10^{-3}$ 0.097 POF (kg NMVOC/€) $3.04 \cdot 10^{-3}$ $1.13 \cdot 10^{-3}$ $1.30 \cdot 10^{-3}$ FET (kg 1,4-DB eq/€) $3.04 \cdot 10^{-3}$ $2.64 \cdot 10^{-3}$ $2.75 \cdot 10^{-3}$ MET (kg 1,4-DB eq/€) $2.62 \cdot 10^{-3}$ $2.19 \cdot 10^{-3}$ $2.23 \cdot 10^{-3}$	CC (kg CO ₂ eq/€)	0.47	0.42	0.45
FE (kg P eq/€) $9.85 \cdot 10^{-5}$ $8.32 \cdot 10^{-5}$ $8.42 \cdot 10^{-5}$ ME (kg N eq/€) $5.81 \cdot 10^{-5}$ $5.52 \cdot 10^{-5}$ $5.91 \cdot 10^{-5}$ HT (kg 1,4-DB eq/€) $1.26 \cdot 10^{-3}$ $1.13 \cdot 10^{-3}$ 0.097 POF (kg NMVOC/€) $3.04 \cdot 10^{-3}$ $1.13 \cdot 10^{-3}$ $1.30 \cdot 10^{-3}$ FET (kg 1,4-DB eq/€) $3.04 \cdot 10^{-3}$ $2.64 \cdot 10^{-3}$ $2.75 \cdot 10^{-3}$ MET (kg 1,4-DB eq/€) $2.62 \cdot 10^{-3}$ $2.19 \cdot 10^{-3}$ $2.23 \cdot 10^{-3}$	OD (kg CFC-11 eq/€)	5.34·10 ⁻⁸	$7.64 \cdot 10^{-8}$	$4.38 \cdot 10^{-8}$
ME (kg N eq/€) $5.81 \cdot 10^{-5}$ $5.52 \cdot 10^{-5}$ $5.91 \cdot 10^{-5}$ HT (kg 1,4-DB eq/€) $1.26 \cdot 10^{-3}$ $1.13 \cdot 10^{-3}$ 0.097 POF (kg NMVOC/€) $3.04 \cdot 10^{-3}$ $1.13 \cdot 10^{-3}$ $1.30 \cdot 10^{-3}$ FET (kg 1,4-DB eq/€) $3.04 \cdot 10^{-3}$ $2.64 \cdot 10^{-3}$ $2.75 \cdot 10^{-3}$ MET (kg 1,4-DB eq/€) $2.62 \cdot 10^{-3}$ $2.19 \cdot 10^{-3}$ $2.23 \cdot 10^{-3}$	TA (kg SO₂ eq/€)	$2.32 \cdot 10^{-3}$	$2.41 \cdot 10^{-3}$	$2.62 \cdot 10^{-3}$
HT (kg 1,4-DB eq/€) $1.26 \cdot 10^{-3}$ $1.13 \cdot 10^{-3}$ 0.097 POF (kg NMVOC/€) $3.04 \cdot 10^{-3}$ $1.13 \cdot 10^{-3}$ $1.30 \cdot 10^{-3}$ FET (kg 1,4-DB eq/€) $3.04 \cdot 10^{-3}$ $2.64 \cdot 10^{-3}$ $2.75 \cdot 10^{-3}$ MET (kg 1,4-DB eq/€) $2.62 \cdot 10^{-3}$ $2.19 \cdot 10^{-3}$ $2.23 \cdot 10^{-3}$	FE (kg P eq/€)	9.85·10 ⁻⁵	8.32·10 ⁻⁵	$8.42 \cdot 10^{-5}$
POF (kg NMVOC/€) $3.04 \cdot 10^{-3}$ $1.13 \cdot 10^{-3}$ $1.30 \cdot 10^{-3}$ FET (kg 1,4-DB eq/€) $3.04 \cdot 10^{-3}$ $2.64 \cdot 10^{-3}$ $2.75 \cdot 10^{-3}$ MET (kg 1,4-DB eq/€) $2.62 \cdot 10^{-3}$ $2.19 \cdot 10^{-3}$ $2.23 \cdot 10^{-3}$	ME (kg N eq/€)	5.81·10 ⁻⁵	$5.52 \cdot 10^{-5}$	$5.91 \cdot 10^{-5}$
FET (kg 1,4-DB eq/ \in) $3.04 \cdot 10^{-3}$ $2.64 \cdot 10^{-3}$ $2.75 \cdot 10^{-3}$ MET (kg 1,4-DB eq/ \in) $2.62 \cdot 10^{-3}$ $2.19 \cdot 10^{-3}$ $2.23 \cdot 10^{-3}$	HT (kg 1,4-DB eq/€)	1.26·10 ⁻³	$1.13 \cdot 10^{-3}$	0.097
MET (kg 1,4-DB eq/ ϵ) 2.62·10 ⁻³ 2.19·10 ⁻³ 2.23·10 ⁻³	POF (kg NMVOC/€)	$3.04 \cdot 10^{-3}$	$1.13 \cdot 10^{-3}$	$1.30 \cdot 10^{-3}$
	FET (kg 1,4-DB eq/€)	$3.04 \cdot 10^{-3}$	$2.64 \cdot 10^{-3}$	$2.75 \cdot 10^{-3}$
FD (kg oil eq/€) 0.24 0.22 0.28	MET (kg 1,4-DB eq/€)	$2.62 \cdot 10^{-3}$	$2.19 \cdot 10^{-3}$	$2.23 \cdot 10^{-3}$
	FD (kg oil eq/€)	0.24	0.22	0.28

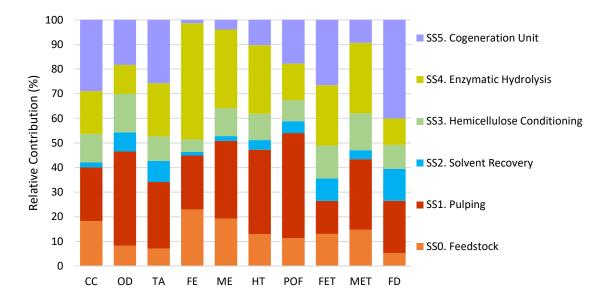




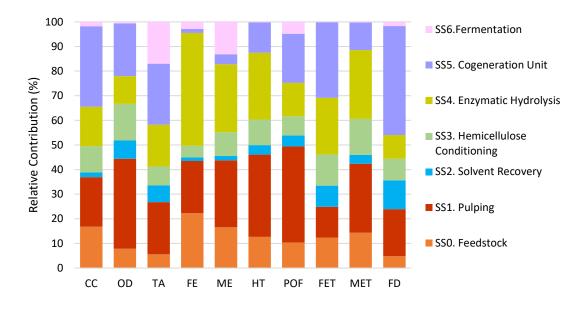




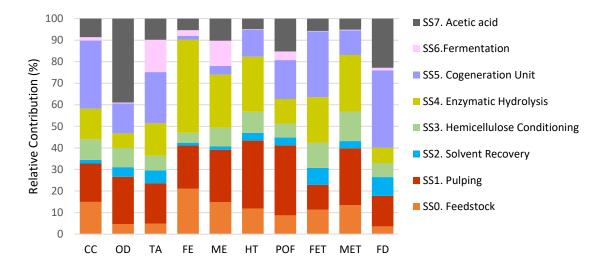


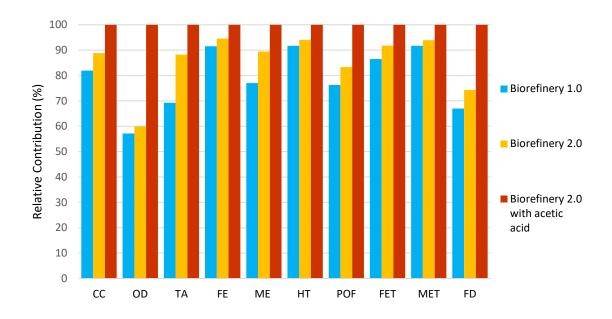


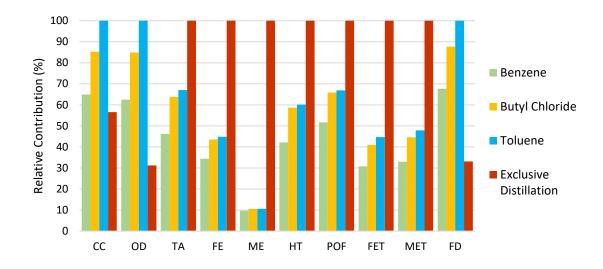


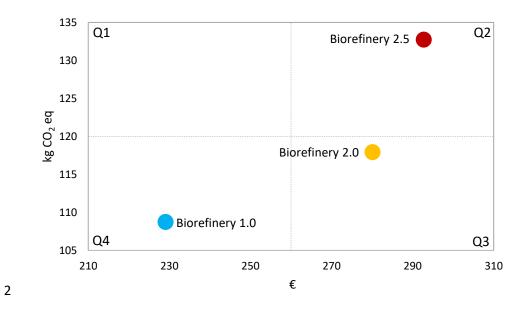












2 **Figure captions**

Figure 1 System boundaries of the lignocellulosic biorefinery for the production of
bioethanol, acetic acid, lignin and furfural. Subsystems (SS) are defined with reference to
process units in the plant.

- 6 **Figure 2** General system configuration SS0. Feedstock
- Figure 3 System boundaries of the lignocellulosic biorefinery for the production of
 glucose, hemicellulose and lignin. Subsystems (SS) and system boundaries defined for
 Biorefinery 1.0

Figure 4 System boundaries of the lignocellulosic biorefinery for the production of
bioethanol, lignin and furfural. Subsystems (SS) and system boundaries defined for
Biorefinery 2.0

Figure 5 Relative contributions (in %) per subsystem in the overall production processof the Biorefinery 1.0

Figure 6 Relative contributions (in %) per subsystem in the overall production processof the Biorefinery 2.0

Figure 7 Relative contributions (in %) per subsystem in the overall production process
of the Biorefinery 2.0 with co-production of acetic acid

- 19 Figure 8 Comparative environmental profiles (in %) for Biorefinery 1.0, Biorefinery 2.0
- 20 and Biorefinery 2.0 with acetic acid co-production
- 21 Figure 9 Comparative environmental profiles (in %) for furfural recovery methods:
- 22 exclusive distillation and hybrid distillation-extraction with benzene, butyl chloride and
- 23 toluene
- Figure 10 Climate change and monetary benefit per functional unit (1 t dry wood /h)