## Passive Resistance Emulation

solved before we started...

Shigeo Masukawa, Shoji Iida
"An Improved Three-Phase Diode Rectifier for Reducing AC Line Current Harmonics"

$7^{\text {th }}$ European Conference on Power Electronics and Applications, EPE'97

pp. 4.227-4.232, Trondheim, Norway, September 1997
initial thoughts ... for a long time . .

- just another multipulse rectifier ...
- from a different (multipulse) world
- which for multi $=12$ provides THD $=15.22 \%$
- all of this is true...
- but there is more ...
- let's study it, first!
$m_{k}$ and $j_{k}, k \in\{1,2,3\}$

- resistance emulation ... since all we need are resistors ...
- switching converter?
- possible, something done, something in progress ...
- requires: auxiliary power supply, control logic, sensors ...
- causes EMI ... which requires filtering ...
- reliability? maintainability?
- is there a simpler way?
- at least, to have some fun ...
- passive resistance emulation!
- "passive" means that there are no controlled switches ...
- neither any control logic ...
- so all the thinking should be done in advance
and they proposed ...

some equations ...

$$
\begin{gathered}
i_{Y}=\frac{1}{n} I_{O U T} \operatorname{sgn}\left(v_{A V}\right) \\
v_{R E}=\frac{1}{n}\left|v_{A V}\right| \\
n_{O P T}=\frac{1}{4 \sqrt{3}-6} \approx 1.0774
\end{gathered}
$$

a closer look at $j_{1}$


how does it work: $j_{Y}$ and $j_{X}$

how does it work: $j_{A}$ and $j_{B}$

voltages at the output...


how does it work: $j_{I A}$ and $j_{I B}$

and the result is ...

the output voltage spectrum ...


current loaded resistance emulator?

emulated resistance? sinusoidal approximation?


is there a way to filter out the higher order harmonics?


some equations ...

$$
\begin{gathered}
v_{R E}=\frac{1}{n}\left|v_{A V}\right| \\
i_{Y}=\frac{1}{n} I_{O U T} \operatorname{sgn}\left(v_{A V}\right)
\end{gathered}
$$

resulting in ...

$$
i_{Y, 1}=\frac{4}{\pi n} I_{\text {OUT }} \cos \left(3 \omega_{0} t\right)
$$

thanks to Professor Robert Warren Erickson and his class Power Electronics 2
topic "Series Resonant Converter"
emulated resistance

$$
R_{E}=\frac{V_{A V, 1}}{I_{Y, 1}}=\frac{3}{64(2-\sqrt{3})} \approx 0.17494
$$

... in this case
there is!

a few hints...

- $3 \omega_{0}=1 / \sqrt{L_{P} C_{P}}$
- $L_{P}$ should be realized as a magnetizing inductance of the transformer ...
- ... which I realized an inductor too late ...
- CIN will do the rest ...
- and there are two resonance constraints to satisfy ...
- thanks, Bob!
- ... and this is not the only time I used the series resonant converter and sinusoidal approximation. . .
resistance emulator, AC side, equivalent circuit


$$
i_{P I T}=\frac{1}{n} I_{O U T} \operatorname{sgn}\left(v_{P}\right)
$$

above $3 \omega_{0}$, really idealized

$m_{k}$ and $j_{k}, k \in\{1,2,3\}$


$$
\begin{gathered}
I_{Y m}=\frac{4}{n \pi} I_{O U T} \\
\frac{3}{2}=\frac{4}{n \pi} \\
n=\frac{8}{3 \pi} \approx 0.84883
\end{gathered}
$$


at $3 \omega_{0}$, somewhat idealized


$$
i_{P I T}=\frac{1}{n} I_{O U T} \operatorname{sgn}\left(v_{P}\right)
$$

$\operatorname{sgn}\left(v_{P}\right)$, not $\operatorname{sgn}\left(v_{A V}\right)$, please remember!
a word (an equation) about $n$
a closer look at $j_{1}$


$j_{Y}$ and $j_{X}$

$j_{A}$ and $j_{B}$

voltages at the output...


$j_{I A}$ and $j_{I B}$

the result...

the output voltage spectrum ...

comparison of $\left|M_{O U T, k}\right|$ to $\left|M_{A B, k}\right| \ldots$

published in ..

Predrag Pejović
"Two Three-Phase High Power Factor Rectifiers that Apply the Third Harmonic Current Injection and Passive Resistance Emulation"

IEEE Transactions on Power Electronics, vol. 15, no. 6, pp. 1228-1240, November 2000
with an overpage fee of more than US\$ 1500 .
voltage loaded resistance emulator ...

voltage loaded resistance emulator ...

ingenious like the cosmological constant.

nice?

- some details not mentioned ...
- VA-ratings of the transformers are low ..
- effects caused by higher order harmonics analyzed ...
- generalized for switching CID ...
- nice result ...
- in theory ...
- well, it works in practice ...
- but there are two resonance constraints ...
- and the circuit is sensitive on leakage of the parallel resonant circuit at $3 \omega_{0} \ldots$
- anything better?


## some equations

$$
\begin{gathered}
v_{R E}=V_{O U T} \operatorname{sgn}\left(i_{Y}\right) \\
V_{R E, 1}=\frac{4}{n \pi} V_{O U T}
\end{gathered}
$$

and it is not dependent on $I_{Y, 1} \ldots$
which is a problem, we cannot control $I_{Y, 1}$ any more
besides, we do not have $V_{O U T}$ available, but $v_{\text {OUT }}$
but, this could (should?) be solved ...
and the solution is ...
the whole circuit ...


- we did not expect too much ...
- just a sort of shallow-DCM converter ...
- with poor control of $I_{Y m} \ldots$
- I did the experiments...
- tired...
- and not particularly motivated ...
- actually, not motivated at all ...
- since we did not expect much ...
- and I connected ...
published in ..

Predrag Pejović, Predrag Božović, Doron Shmilovitz
"Low Harmonic, Three Phase Rectifier that Applies Current Injection and a Passive Resistance Emulator"

IEEE Power Electronics Letters,
vol. 3, no. 3, pp. 96-100, September 2005
which almost cost my student his Ph.D
wither ever got didn't have the IF
though the paper was quite cited
but this was not the administrative requirement
some figures ...
obtained assuming the CCM with

$$
j_{Y}=k \cos \left(3 \omega_{0} t\right)
$$

where

$$
k=1.39
$$

and a value of $n$

$$
n=12.23
$$

don't ask why for a while ...
just $j_{k}, k \in\{1,2,3\}$

now, we can play smart ...

- I was surprised that the results are so good...
- much better than expected...
- even at the first glimpse ...
- after that, I double checked the circuit ...
- but it was too late ...
- the better circuit than intended had already been built
- and it is not that hard to dig when you know where the gold is ...
- ripple of $i_{R E}$ improved the THD ...
- instead of making it worse ...
- wrong assumption ...
- and a serendipity!
- although, it was presented in the paper in a different style
$m_{k}$ and $j_{k}, k \in\{1,2,3\}$



a closer look at $j_{1}$

a closer look at $j_{1}$ and a comparison ...
$j_{Y}$ and $j_{X}$

$j_{I A}$ and $j_{I B}$

power ...

achieved for . .

$$
\begin{gathered}
k_{\text {opt }}=\frac{3\left(\pi^{2}-8\right)}{\pi(2 \pi-5)} \approx 1.39 \\
n_{\text {opt }}=\frac{6\left(\pi^{2}-8\right)}{\pi(16-5 \pi)} \approx 12.23
\end{gathered}
$$

where

$$
T H D_{\min }=\frac{1}{3} \sqrt{\frac{8 \pi^{4}-199 \pi^{2}+360 \pi+54}{15 \pi^{2}-40 \pi-6}} \approx 3.64 \%
$$



$j_{A}$ and $j_{B}$


resistance emulator, AC side ...

at the expense of $\ldots$

$$
\rho_{\text {opt }}=\frac{\sqrt{3}(2 \pi-5)\left(7 \pi^{2}-20 \pi-6\right)}{6\left(\pi^{2}-8\right)^{2}} \approx 0.027063
$$

and

$$
P_{R}=\frac{7 \pi^{2}-20 \pi-6}{4 \pi(2 \pi-5)} \approx 1.5837 \%
$$

which we know from ...

just one waveform

to support one reasoning ...
assuming

$$
j_{Y}=J_{Y} \cos \left(3 \omega_{0} t\right)
$$

to provide that the resistance emulator takes the power

$$
\begin{gathered}
\frac{1}{n} M_{X Y, 1}<M_{A V, 1} \\
\frac{1}{n} \frac{15 \sqrt{3}}{4 \pi}<\frac{3 \sqrt{3}}{8 \pi} \\
n>10
\end{gathered}
$$

and that's why all the diagrams start at $n=10$


- since it started as a serendipity, it continued that way ...
- a close-to-the-best operating point is chosen, somewhere in the CCM
- the waveforms are recorded and analyzed
- the analytical optimum is found
- which is not something I'm gonna bother you with (now)
- but the numerical optimization is easy and fun ...
- and the result had been presented
- but why from $n=10$ ?
- and what is the white area? lack of paint?
and just one spectrum

$$
\begin{gathered}
m_{X Y} \triangleq m_{O U T} \operatorname{sgn}\left(j_{Y}\right) \\
m_{X Y}=\sum_{k=1}^{\infty} M_{X Y, k} \cos \left(3 k \omega_{0} t\right) \\
M_{X Y, k}=\frac{6 \sqrt{3}}{\pi} \frac{6 k \sin \frac{\pi k}{2}-1}{9 k^{2}-1}
\end{gathered}
$$

thus

$$
M_{X Y, 1}=\frac{15 \sqrt{3}}{4 \pi}
$$

and just a short note about $n>6$

- to provide sinusoidal injected current that transfers the power to the resistance emulator we need $n>10$
- but what is the minimum of $n$ to get any $j_{Y}$ ?
- assume that $j_{Y}=0$
- to push $j_{Y}$ we need $n \times m_{A V}>m_{O U T}$
- according to the diagram from the next slide ...
- we need $n>6$
- but that's too much for this presentation
- since it is too irrelevant in practice...
the white area...
- the white area is beyond the DCM limitation
- which comes from two conditions ...
- $j_{A}>0$ and $j_{B}>0$
- any violation in the numerical simulation and the data point gets rejected
- some analytical preparation?

$$
\begin{aligned}
& j_{A}=1-\frac{\left|j_{Y}\right|}{n}+\frac{1}{2} j_{Y}>0 \\
& j_{B}=1-\frac{\left|j_{Y}\right|}{n}-\frac{1}{2} j_{Y}>0
\end{aligned}
$$

which reduces to

$$
\begin{gathered}
\frac{1}{2} j_{Y}>-\left(1-\frac{\left|j_{Y}\right|}{n}\right) \\
\frac{1}{2} j_{Y}<1-\frac{\left|j_{Y}\right|}{n} \\
\frac{\left|j_{Y}\right|}{2}<1-\frac{\left|j_{Y}\right|}{n}
\end{gathered}
$$

the $(k, n)$ plane ...

and the optimum is ...

$$
T H D_{\min }=\frac{1}{9} \sqrt{\frac{61 \pi^{2}-36 \pi-486}{6}} \approx 7.79 \%
$$

and there is more theory, there are more simulations, ...
but we'll stop here.

$$
\begin{aligned}
& \left|j_{Y}\right|<\frac{2 n}{n+2} \\
& J_{Y m}<\frac{2 n}{n+2} \\
& \quad k<\frac{2 n}{n+2}
\end{aligned}
$$

for the CCM
and the thick black line in the next diagram is $k=\frac{2 n}{n+2}$
the DCM, THD (n)

in the CCM ...

the input currents ...

... accompanied with the voltages ...

$j_{1}$ compared to the $3^{\text {rd }}$ harmonic injection case

$j_{I A}$ and $j_{I B}$

$j_{Y}$ and $m_{R E}$


$j_{A}$ and $j_{B}$

$i_{Y}$ and $i_{X}$

power . . .

$v_{1}, i_{1}, I_{\text {OUT }} \approx 3 \mathrm{~A}$
$v_{1}, i_{1}, I_{\text {OUT }} \approx 3 \mathrm{~A}$, spectra

$v_{1}, I_{\text {OUT }} \approx 3 \mathrm{~A}$

$v_{2}, i_{2}, I_{\text {OUT }} \approx 3 \mathrm{~A}$, spectra

$v_{3}, i_{3}, I_{\text {OUT }} \approx 3 \mathrm{~A}$


$v_{2}, i_{2}, I_{\text {OUT }} \approx 3 \mathrm{~A}$

$v_{2}, I_{\text {OUT }} \approx 3 \mathrm{~A}$

$v_{3}, i_{3}, I_{\text {OUT }} \approx 3 \mathrm{~A}$, spectra


$v_{\text {OUT }}, i_{\text {OUT }}, I_{\text {OUT }} \approx 3 \mathrm{~A}$, spectra

$v_{1}, i_{1}, I_{\text {OUT }} \approx 6 \mathrm{~A}$, spectra

$v_{2}, i_{2}, I_{\text {OUT }} \approx 6 \mathrm{~A}$


$v_{1}, i_{1}, I_{\text {OUT }} \approx 6 \mathrm{~A}$

$v_{1}, I_{\text {OUT }} \approx 6 \mathrm{~A}$

$v_{2}, i_{2}, I_{\text {OUT }} \approx 6 \mathrm{~A}$, spectra

$v_{2}, I_{\text {OUT }} \approx 6 \mathrm{~A}$

$v_{3}, i_{3}, I_{\text {OUT }} \approx 6 \mathrm{~A}$, spectra

$v_{O U T}, i_{O U T}, I_{O U T} \approx 6 \mathrm{~A}$

experimental results, input, part 1

| $I_{\text {OUT }}[\mathrm{A}]$ | $k$ | $I_{k R M S}[\mathrm{~A}]$ | $V_{k R M S}[\mathrm{~V}]$ | $S[\mathrm{VA}]$ | $P[\mathrm{~W}]$ |
| :---: | :---: | ---: | ---: | ---: | ---: |
| 1 | 1 | 2.64 | 100.09 | 264.21 | 259.49 |
|  | 2 | 2.65 | 99.66 | 264.54 | 260.11 |
|  | 3 | 2.66 | 101.47 | 270.05 | 265.92 |
| 2 | 1 | 5.17 | 96.88 | 501.33 | 499.98 |
|  | 2 | 5.18 | 96.19 | 497.95 | 496.36 |
|  | 3 | 5.19 | 97.28 | 505.32 | 503.87 |

$v_{3}, i_{3}, I_{\text {OUT }} \approx 6 \mathrm{~A}$

$v_{3}, I_{\text {OUT }} \approx 6 \mathrm{~A}$

$v_{\text {OUT }}, i_{\text {OUT }}, I_{\text {OUT }} \approx 6 \mathrm{~A}$, spectra

experimental results, input, part 2

| $I_{\text {OUT }}[\mathrm{A}]$ | $k$ | $P F$ | $T H D\left(i_{k}\right)[\%]$ | $T H D\left(v_{k}\right)[\%]$ |
| :---: | ---: | ---: | ---: | ---: |
| 1 | 1 | 0.9821 | 7.70 | 4.10 |
|  | 2 | 0.9833 | 7.51 | 4.12 |
|  | 3 | 0.9847 | 7.64 | 3.88 |
| 2 | 1 | 0.9973 | 5.40 | 3.92 |
|  | 2 | 0.9968 | 5.91 | 4.22 |
|  | 3 | 0.9971 | 5.47 | 4.05 |

- it seems that's it
- pretty good agreement with the theory
- promising to be applied
- there are more analyses and experimental results presented in the book and in some papers
- but...
conclusions
- resistance emulators analyzed
- current loaded and voltage loaded
- the current loaded one seemed like a better fit ...
- since the adjustment to $I_{O U T}$ is better
- however, the voltage loaded one turned out to be better
- although it was not expected
- simpler, with better $T H D$,
- and its filter should be omitted
- and we are getting close to the end of our story ...
- but there is some more ...
- multipulse operation ...
- and switching resistance emulation ...

