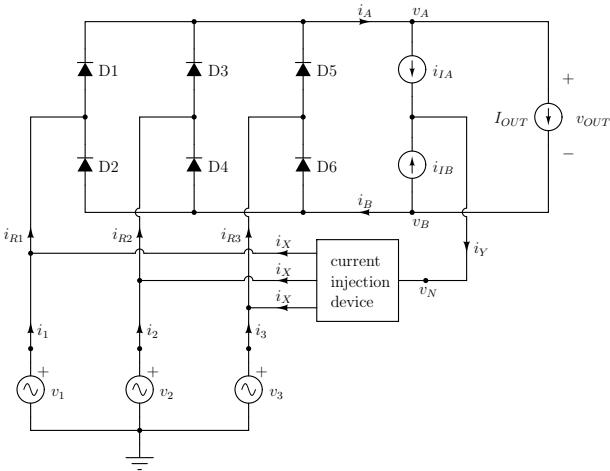


The Third Harmonic Current Injection

1. patch the gaps in the input currents
2. do some shaping

what is this all about?



current injection device

a magnetic device that provides:

$$i_X = \frac{1}{3} i_Y$$

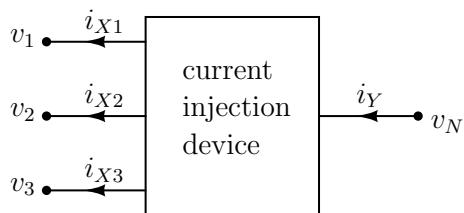
$$v_N = \frac{1}{3} (v_1 + v_2 + v_3) = 0$$

- patching even where not needed ...
- more to be said about the device ...
- hard to put parallel events into a sequence ...
- but, let's take a closer look ...

let's complicate a little bit

some circuit theory ...

8 variables introduced
4 element equations needed
the remaining 4 will be covered by KCL and KVL



$$i_{X1} = \frac{1}{3} i_Y$$

$$i_{X2} = \frac{1}{3} i_Y$$

$$i_{X3} = \frac{1}{3} i_Y$$

$$v_N = \frac{1}{3} (v_1 + v_2 + v_3)$$

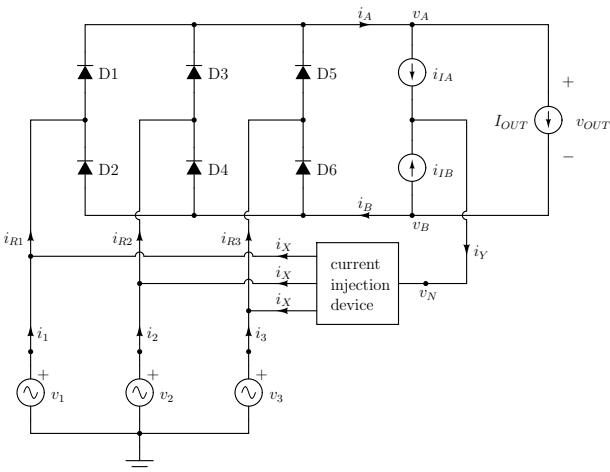
the device is **resistive**, please remember

$$v_N i_Y - v_1 i_1 - v_2 i_2 - v_3 i_3 = 0$$

the device is **non-dissipative**, please remember this

back to the circuit ...

some equations, KCL, ...



$$i_k = i_{Rk} - i_X, \quad k \in \{1, 2, 3\}$$

$$i_X = \frac{1}{3} i_Y$$

$$i_{IA} = i_{IB} = \frac{1}{2} i_Y$$

$$i_A = I_{OUT} + i_{IA} = I_{OUT} + \frac{1}{2} i_Y$$

$$i_B = I_{OUT} - i_{IB} = I_{OUT} - \frac{1}{2} i_Y$$

some equations normalized

j_Y limitations

$$j_X \triangleq \frac{i_X}{I_{OUT}}$$

$$j_k = j_{Rk} - j_X, \quad k \in \{1, 2, 3\}$$

$$j_X = \frac{1}{3} j_Y$$

$$j_{IA} = j_{IB} = \frac{1}{2} j_Y$$

$$j_A = 1 + j_{IA} = 1 + \frac{1}{2} j_Y$$

$$j_B = 1 - j_{IB} = 1 - \frac{1}{2} j_Y$$

for the continuous conduction mode (CCM):

$$j_A > 0 \Rightarrow 1 + \frac{1}{2} j_Y > 0$$

$$j_B > 0 \Rightarrow 1 - \frac{1}{2} j_Y > 0$$

$$-2 < j_Y < 2$$

or

$$-2 I_{OUT} < i_Y < 2 I_{OUT}$$

how to get j_{Rk} , $k \in \{1, 2, 3\}$?

the input currents

$$j_{R1} = d_1 j_A - d_2 j_B$$

$$j_{R2} = d_3 j_A - d_4 j_B$$

$$j_{R3} = d_5 j_A - d_6 j_B$$

or, in general terms

$$j_{Rk} = d_{2k-1} j_A - d_{2k} j_B$$

for

$$k \in \{1, 2, 3\}$$

plugging in expressions for i_{Rk} and i_X

$$j_k = d_{2k-1} \left(1 + \frac{1}{2} j_Y \right) - d_{2k} \left(1 - \frac{1}{2} j_Y \right) - \frac{1}{3} j_Y$$

there are three cases to be considered:

$$j_k = \begin{cases} 1 + \frac{1}{6} j_Y & \text{for } d_{2k-1} = 1 \text{ and } d_{2k} = 0 \\ -1 + \frac{1}{6} j_Y & \text{for } d_{2k-1} = 0 \text{ and } d_{2k} = 1 \\ -\frac{1}{3} j_Y & \text{for } d_{2k-1} = 0 \text{ and } d_{2k} = 0 \end{cases}$$

some symmetry

more about j_Y

since

$$d_1(\omega_0 t) = d_3 \left(\omega_0 t + \frac{2\pi}{3} \right) = d_5 \left(\omega_0 t + \frac{4\pi}{3} \right)$$

$$d_2(\omega_0 t) = d_4 \left(\omega_0 t + \frac{2\pi}{3} \right) = d_6 \left(\omega_0 t + \frac{4\pi}{3} \right)$$

to have

$$j_1(\omega_0 t) = j_2 \left(\omega_0 t + \frac{2\pi}{3} \right) = j_3 \left(\omega_0 t + \frac{4\pi}{3} \right)$$

we need

$$j_Y(\omega_0 t) = j_Y \left(\omega_0 t + \frac{2\pi}{3} \right) = j_Y \left(\omega_0 t + \frac{4\pi}{3} \right)$$

to get

$$j_Y(\omega_0 t) = j_Y \left(\omega_0 t + \frac{2\pi}{3} \right) = j_Y \left(\omega_0 t + \frac{4\pi}{3} \right)$$

we need

$$j_Y(\omega_0 t) = j_Y \left(\omega_0 t + \frac{2\pi}{3} \right)$$

meaning that j_Y is periodic with $\frac{1}{3} T_0$, i.e. the fundamental frequency of i_Y is $3 f_0$!

thus, **the third-harmonic current injection** is the simplest case

let's assume i_Y

optimization over k and ϕ

$$i_Y = k I_{OUT} \cos(3\omega_0 t - \phi)$$

$$\boxed{j_Y = k \cos(3\omega_0 t - \phi)}$$

range:

1. for the continuous conduction mode $-2 < k < 2$
2. let us assume $-\pi < \phi < \pi$

which couple (k, ϕ) minimizes the THD?

$$j_1 = \begin{cases} 1 + \frac{1}{6} j_Y & \text{for } d_1 = 1 \text{ and } d_2 = 0 \\ -1 + \frac{1}{6} j_Y & \text{for } d_1 = 0 \text{ and } d_2 = 1 \\ -\frac{1}{3} j_Y & \text{for } d_1 = 0 \text{ and } d_2 = 0 \end{cases}$$

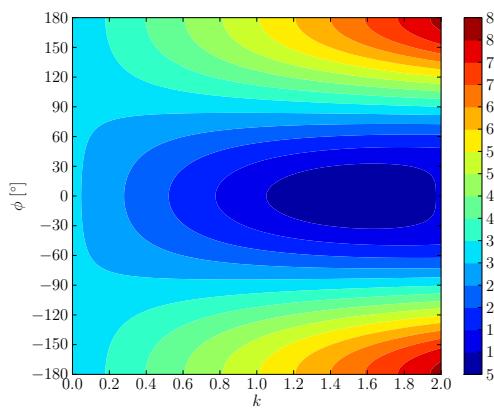
and

$$j_Y = k \cos(3\omega_0 t - \phi)$$

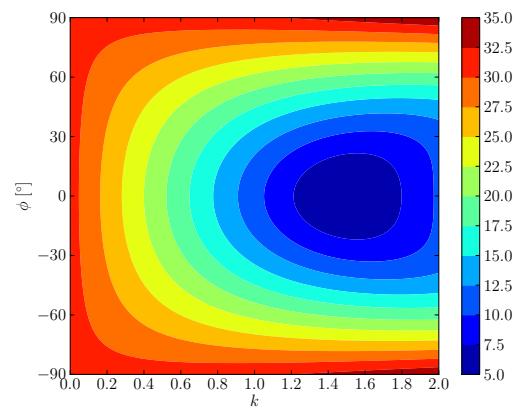
let's go to work!

goal: minimize the THD

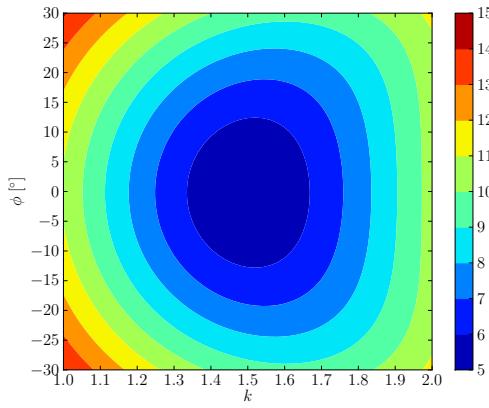
numerical optimization, 1, THD [%]



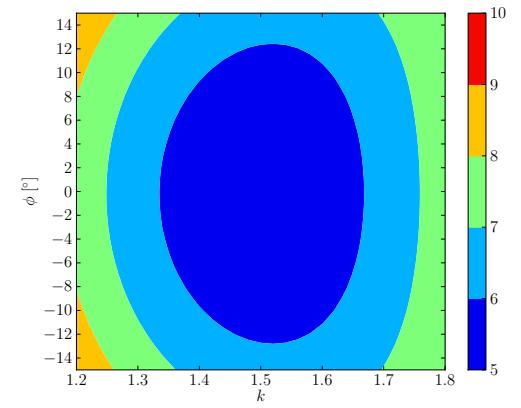
numerical optimization, 2, THD [%]



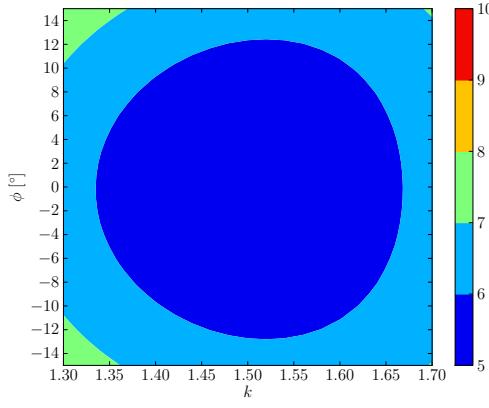
numerical optimization, 3, THD [%]



numerical optimization, 4, THD [%]



numerical optimization, 5, THD [%]



numerical optimization, conclusions

- ▶ improvement possible!
- ▶ $5\% < \text{THD} < 6\%$ achievable
- ▶ $k \approx 1.5, \phi \approx 0$
- ▶ it is promising to continue
- ▶ analytical optimization?
- ▶ circuit?
- ▶ let's continue ...

analytical optimization, start

$$j_1 = \begin{cases} 1 + \frac{1}{6} j_Y & \text{for } d_1 = 1 \text{ and } d_2 = 0 \\ -1 + \frac{1}{6} j_Y & \text{for } d_1 = 0 \text{ and } d_2 = 1 \\ -\frac{1}{3} j_Y & \text{for } d_1 = 0 \text{ and } d_2 = 0 \end{cases}$$

and

$$j_Y = k \cos(3\omega_0 t - \phi)$$

analytical optimization, rms and the fundamental

after lots of work (fortunately, wxMaxima's):

$$\begin{aligned} J_{RMS} &= \frac{\sqrt{k^2 + 24}}{6} \\ J_{1Cm} &= \frac{3k \cos \phi + 48}{8\sqrt{3}\pi} \\ J_{1Sm} &= \frac{3\sqrt{3}k \sin \phi}{8\pi} \\ J_{1RMS} &= \sqrt{\frac{J_{1Cm}^2 + J_{1Sm}^2}{2}} \\ J_{1RMS} &= \frac{\sqrt{768 + 27k^2 + 96k \cos \phi - 24k^2(\cos \phi)^2}}{8\sqrt{2}\pi} \end{aligned}$$

$$THD = \sqrt{\left(\frac{J_{RMS}}{J_{1RMS}}\right)^2 - 1}$$

$$\frac{\partial y(k, \phi)}{\partial k} = 0$$

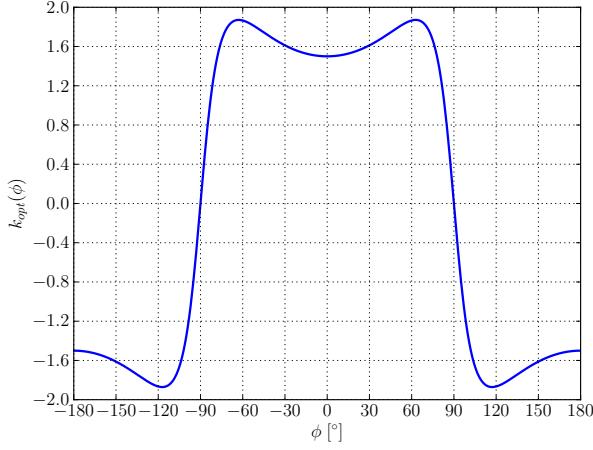
make it simple: to minimize THD is to minimize

$$y(k, \phi) \triangleq \left(\frac{J_{RMS}}{J_{1RMS}}\right)^2$$

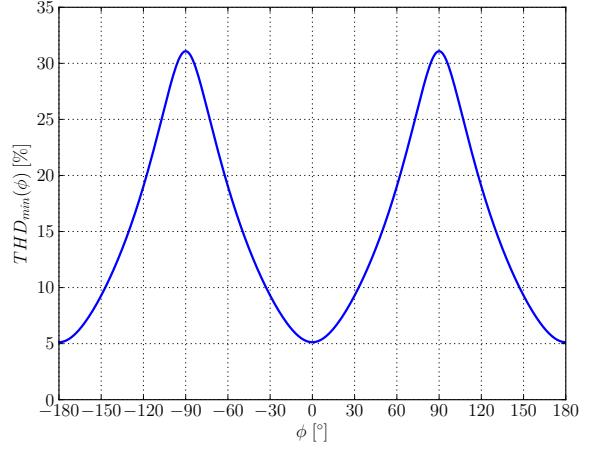
$$k_{opt}(\phi) = \frac{\sqrt{576 (\cos \phi)^4 + 624 (\cos \phi)^2 + 25 - 24 (\cos \phi)^2 - 5}}{4 \cos \phi}$$

$$y(k, \phi) = \frac{2 \pi^2 (16 k^2 + 384 \pi^2)}{6912 + 243 k^2 + 864 k \cos \phi - 216 k^2 (\cos \phi)^2}$$

$k_{opt}(\phi)$



$THD(k_{opt}(\phi), \phi)$



$THD_{MIN}, k_{OPT}, \phi_{OPT}$

$$THD_{MIN} = \min(THD(k_{opt}(\phi), \phi)) = THD(k_{OPT}, \phi_{OPT})$$

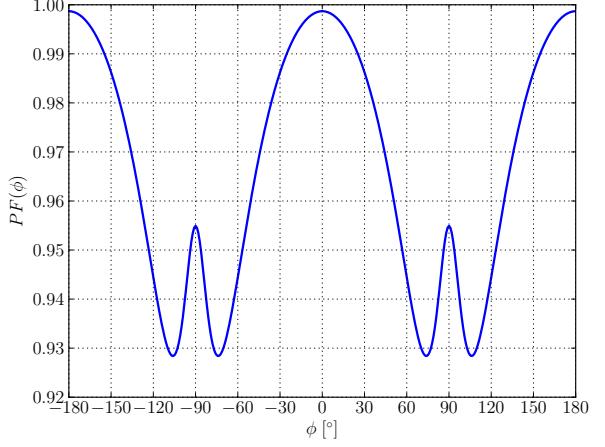
$$\phi_{OPT} = 0$$

$$k_{OPT} = k_{opt}(0) = \frac{3}{2}$$

$$THD_{MIN} = \sqrt{\frac{32 \pi^2}{315} - 1} \approx 5.12 \%$$

and that's all the third harmonic current injection can do

$PF(k_{opt}(\phi), \phi)$



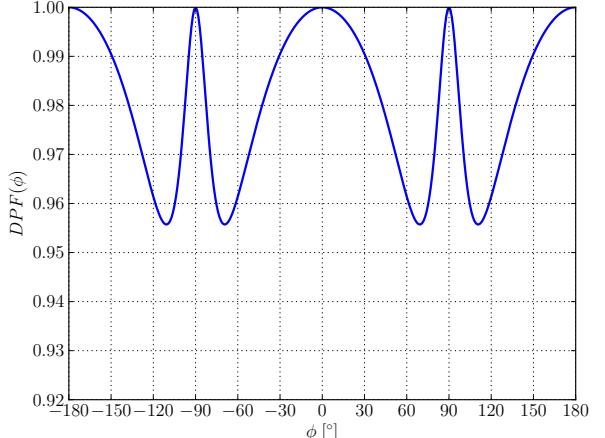
$PF(k_{OPT}, \phi_{OPT})$

$$PF(k, \phi) = \frac{\sqrt{6} (3 k \cos \phi + 48)}{8 \pi \sqrt{k^2 + 24}}$$

$$PF\left(\frac{3}{2}, 0\right) = \frac{3\sqrt{70}}{8\pi} \approx 0.9987$$

we could have optimized $PF(k, \phi)$. . .

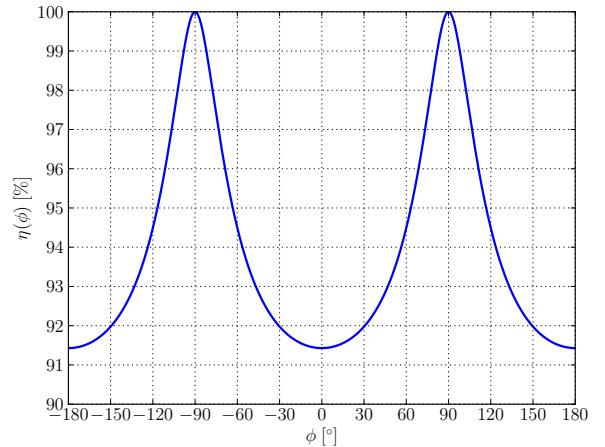
$DPF(k_{opt}(\phi), \phi)$



$DPF(k_{OPT}, \phi_{OPT})$

$$DPF(k, \phi) = \frac{\sqrt{3}(k \cos \phi + 16)}{\sqrt{768 + 27k^2 + 96k \cos \phi - 24k^2 (\cos \phi)^2}}$$

$$DPF\left(\frac{3}{2}, 0\right) = 1$$



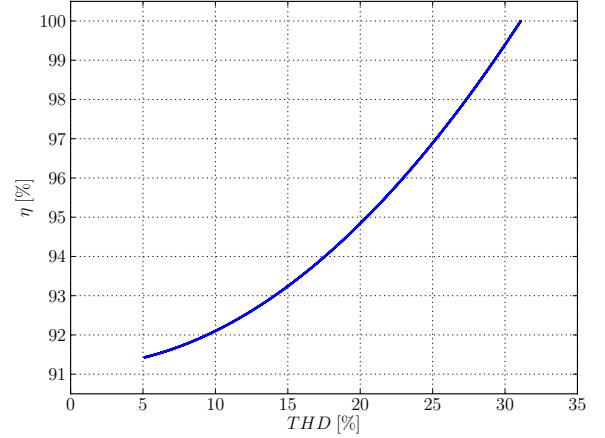
$\eta(k_{OPT}, \phi_{OPT})$

$$\eta(k, \phi) = \frac{48}{3k \cos \phi + 48}$$

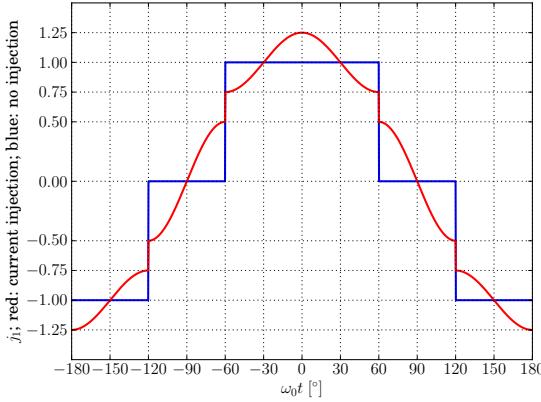
$$\eta\left(\frac{3}{2}, 0\right) = \frac{32}{35} \approx 91.43 \%$$

optimizing $\eta(k, \phi)$?

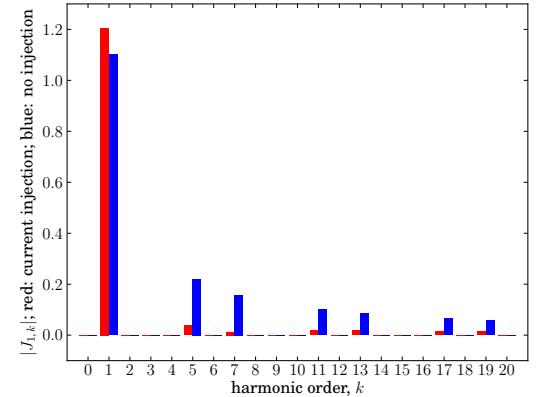
$\eta(THD)$, the tradeoff



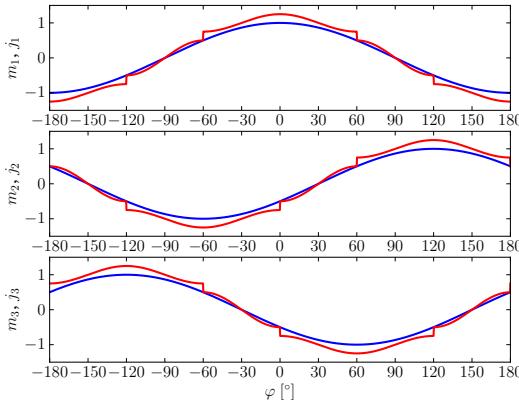
j_1 , with and without injection



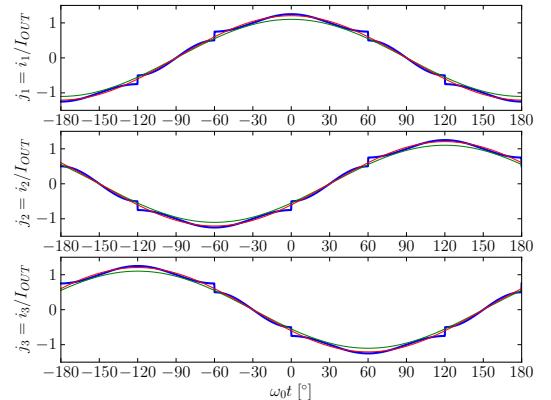
$|J_{1,k}|$, with and without injection



m_k and j_k , $k \in 1, 2, 3$

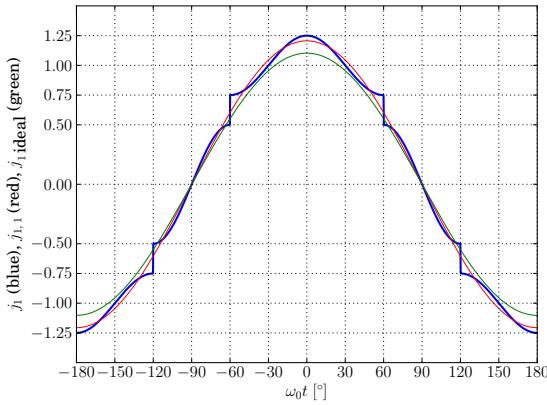


j_k , with ideal waveforms



j_k , with ideal waveforms, a closer look

increase in the amplitude



$$J_{1m} = \frac{35\sqrt{3}}{16\pi} \approx 1.2060$$

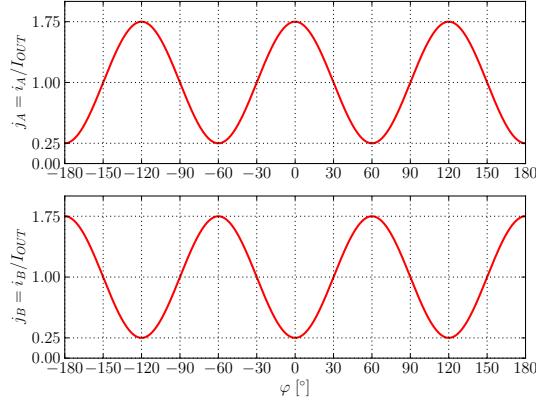
$$J_{1m\text{ideal}} = \frac{2\sqrt{3}}{\pi} \approx 1.1027$$

$$J_{RMS} = \frac{\sqrt{105}}{12} \approx 0.8539$$

$$J_{1RMS} = \frac{35\sqrt{6}}{32\pi} \approx 0.8528$$

$$J_{1RMS\text{ideal}} = \frac{\sqrt{6}}{\pi} \approx 0.77970$$

j_A and j_B



j_A and j_B , mean and rms

$$J_A = \bar{j}_A = \langle j_A \rangle = 1$$

$$J_B = \bar{j}_B = \langle j_B \rangle = 1$$

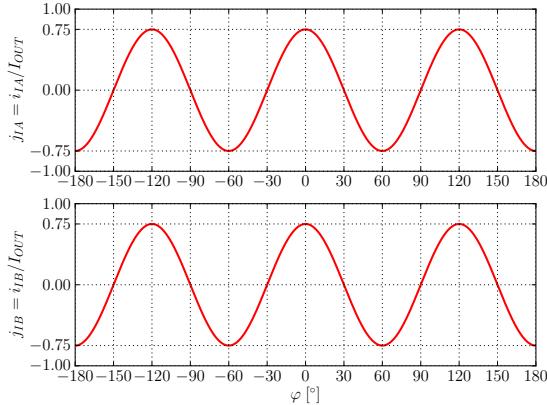
as it was before, but

$$J_{ARMS} = \sqrt{\frac{41}{32}} \approx 1.1319 > 1$$

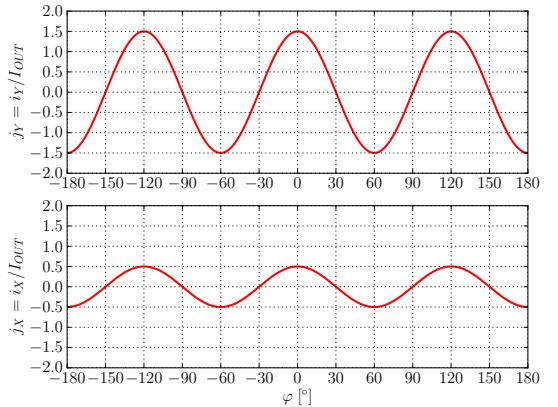
$$J_{BRMS} = \sqrt{\frac{41}{32}} \approx 1.1319 > 1$$

$v_D = V_D + R_D i_D$, somewhat increased losses in the diodes

j_{IA} and j_{IB}

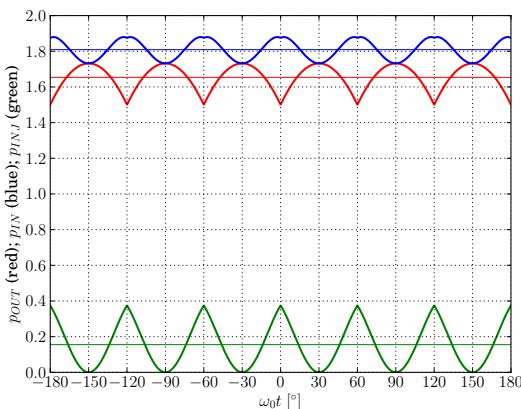


j_Y and j_X



the cost ...

achieved



$$THD = \sqrt{\frac{32\pi^2}{315} - 1} \approx 5.12\%$$

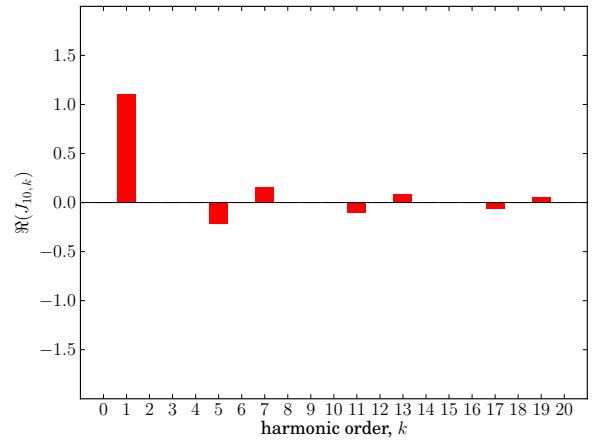
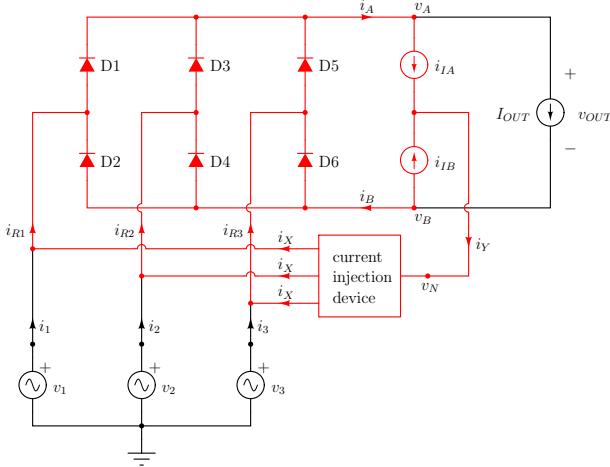
$$PF = \frac{3\sqrt{70}}{8\pi} \approx 0.9987$$

$$DPF = 1$$

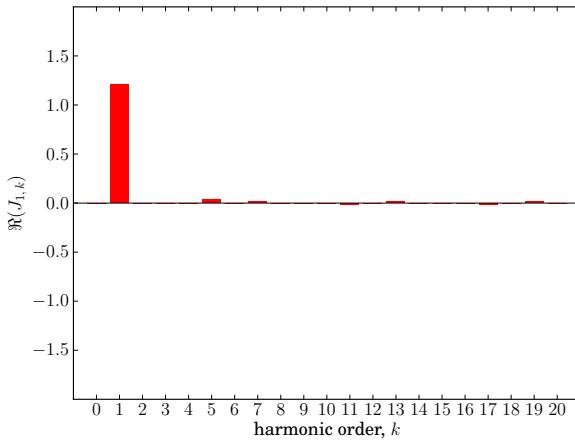
$$\eta = \frac{32}{35} \approx 91.43\%$$

a common misconception ...

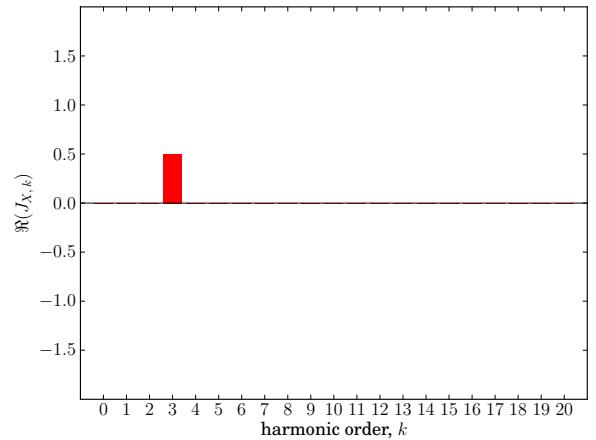
let's walk around, j_{10} , real (cosine) part



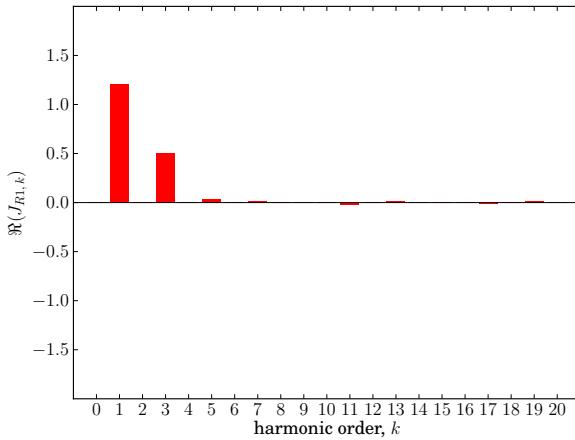
let's walk around, j_1 , real (cosine) part



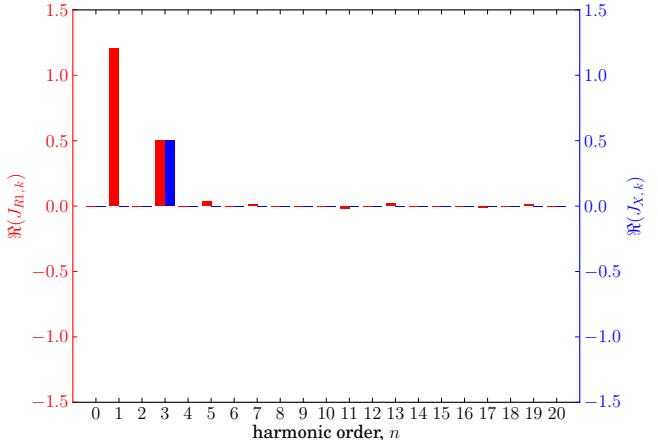
let's walk around, j_X , real (cosine) part



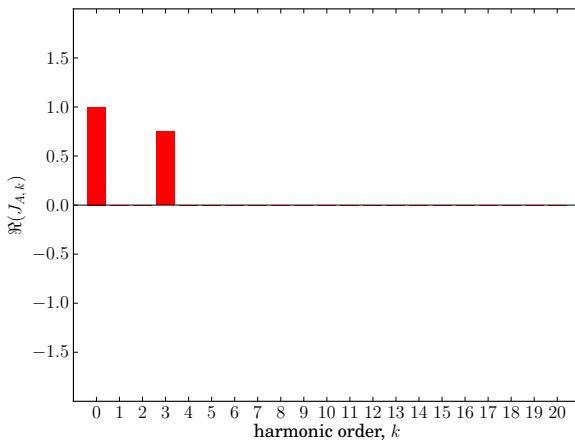
let's walk around, j_{R1} , real (cosine) part



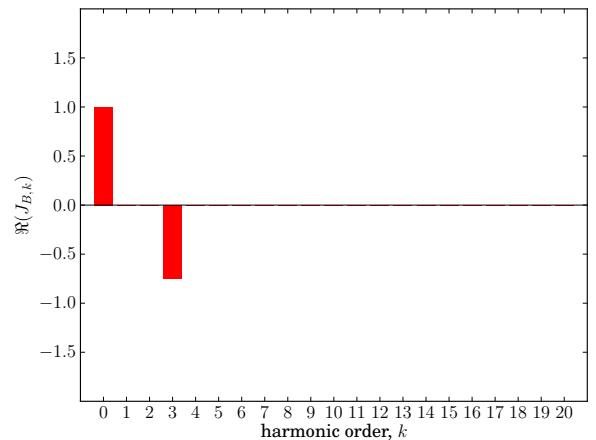
how j_1 is fixed?



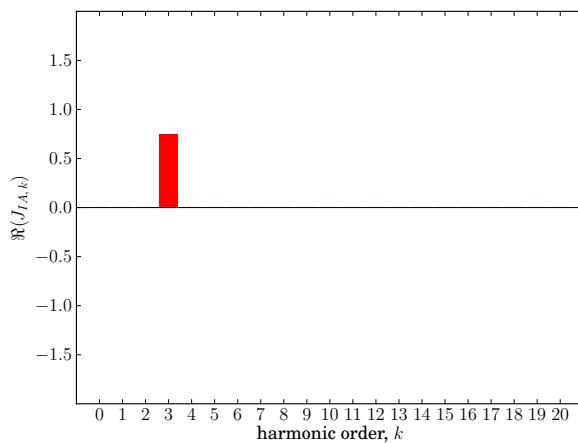
let's walk around, j_A , real (cosine) part



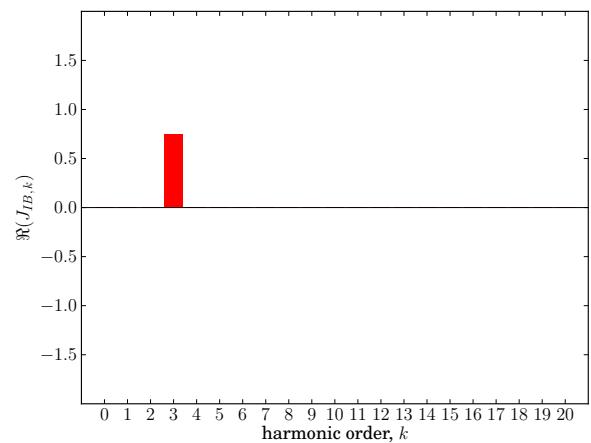
let's walk around, j_B , real (cosine) part



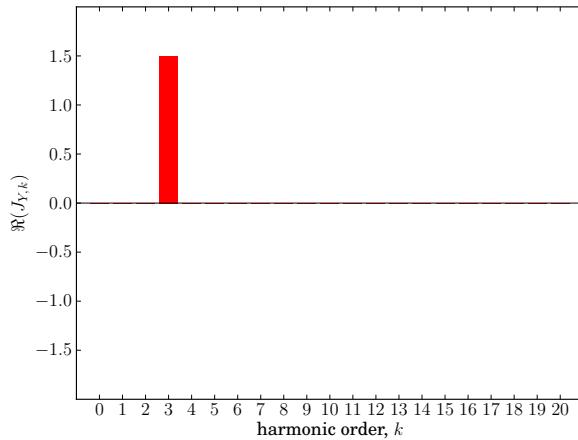
let's walk around, j_{IA} , real (cosine) part



let's walk around, j_{IB} , real (cosine) part



let's walk around, j_Y , real (cosine) part



what the 3rd harmonic current injection is not ...

- ▶ the third harmonic current injection is not a compensation for the third harmonics in the rectifier input currents
- ▶ there were **no** third harmonics in the input currents **before** the injection was applied
- ▶ **neither** there are **any** third harmonics in the input currents **after** the injection was applied
- ▶ the third harmonics circle through and around the diode bridge
- ▶ the diode bridge creates the third harmonics and “consumes” them
- ▶ the diode bridge is a nonlinear system, capable of creating harmonics

“future work”

published in ...

Predrag Pejović, Žarko Janda

“An Analysis of Three Phase Low Harmonic Rectifiers Applying the Third Harmonic Current Injection”

IEEE Transactions on Power Electronics,
vol. 14, no. 3, pp. 397–407, May 1999

but this research was initiated by a comparison of two circuits ...
which is our next topic ...