

Active Optical-Based Detuning Circuit for Receiver Endoluminal Coil

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Abstract. In this paper we demonstrate the effectiveness of an active optical detuning circuit for magnetic resonance imaging (MRI) endoluminal receiver coil. Three endoluminal coils prototypes were built: a coil without any detuning circuit, a coil with a galvanic (classic) detuning circuit using a PIN diode, and a coil with an optical detuning circuit using two photodiodes in parallel with a PIN diode. These coils were built and characterized on a laboratory experimental bench. Then, an *in vitro* experiment was performed with a 3.0 T MR system to evaluate the impact of the endoluminal receiver coils in detuned phase on the image uniformity distribution measured using the body coil. Next, the endoluminal coil was used as a receiver coil to compare the signal-to-noise ratio (SNR) distribution based on iso-contour maps. On experimental bench, the results show an increase delay of the switching times (tuned-detuned or detuned-tuned) for optical-detuned coils of about 10 μ s due to the electro-optical circuits, delay still compatible with requirements. When the body coil is used as a transceiver, the SNR uniformity is similar whether the galvanic or the optical detuning circuit is used. Finally, the SNR iso-contours of the different endoluminal coils prototypes are comparable.

Keywords: magnetic resonance imaging, optical detuning, endoluminal coil, fibered sensor, galvanic link, photodiodes.

1. Introduction

Magnetic resonance imaging (MRI) is widely used to diagnose and analyze inflammatory bowel diseases (Geenen *et al* 2007) and to determine rectal cancer stages (Beets *et al* 2013, Dewhurst *et al* 2013, Torkzad *et al* 2010). However, accurate exploration of bowel diseases and detailed information about the colon wall layers, mandatory for proper

management and effective treatment, are still not available. Indeed, despite the huge progresses in radiofrequency (RF) coils, based on the phased array technology with increase of channels (Giusti *et al* 2012), the external MRI coils have remained unable to provide adequate SNR to reach required high spatial resolution images. By comparison several authors have demonstrated that internal coils significantly increase the local SNR and makes possible either to perform fast *in vivo* MR spectroscopy of heart tissues or to obtain high spatial resolution MR images of colon walls in preclinical context (Beuf *et al* 2004, Dorez *et al* 2016, Kantor *et al* 1984, Pilleul *et al* 2005, Ramgolam *et al* 2011).

However, for clinical use, conducting coaxial cables linking the coil (deeply introduced into the patient) to the connecting plug of the MR system may induce safety issues. In fact, the electrical field \vec{E} , accompanying the RF magnetic field \vec{B}_1 , induces currents in the conducting cables at the same frequency that can lead to a strong increase of the local specific absorption rate (SAR) by the tissues (Detti *et al* 2011, Yeung *et al* 2002). Different solutions were proposed to diminish the SAR issue, i.e., coaxial chokes (Ladd *et al* 2000), transformer coupled transmission lines (Weiss *et al* 2005), baluns matching circuits, and traps (Peterson *et al* 2003). These methods do not ensure a total safety for the patient. The use of optical fibers instead of coaxial cables appears as an attractive alternative to solve definitely safety issues. Different solutions have already been explored to ensure an optical connection between MRI and some coils (Fandrey *et al* 2012, Koste *et al* 2005, Memis *et al* 2008, Possanzini *et al* 2011, Yuan *et al* 2007). For example in reference (Possanzini *et al* 2011), the dStreamTM architecture of Philips has introduced a hybrid technique to amplify, filter, and sample the detected nuclear magnetic resonance (NMR) signal to a numerical one to be then converted into an optical signal and transmitted using an optical fiber. In this latter case, the active detuning is classically performed using coaxial cables. Regarding endoluminal coils, whereas the major issue is the optical conversion and transmission of the NMR signal, the optical tuning/detuning is also an important issue to have a fully optical receiver coil. The receiver coil has to be detuned during RF transmit phase to avoid the strong coupling between coils and \vec{B}_1 concentrations close to the receiver coil, which affects the image uniformity and involve again the SAR issues due to E-field concentrations. Thus in the RF-transmission phase, the endoluminal coil should be detuned from the resonance frequency to ensure isolation between transmit and receive coils. PIN diodes are usually used for passive or/and active detuning of the receiver coils. In passive detuning, a crossed pair of fast switching PIN diodes is added to the resonant circuit. When the RF field is transmitted, the induced current alternatively switches one of the diodes within the circuit. Although it is a wireless method, passive detuning is not sufficiently effective because, depending on RF pulses used, the induced current is not always sufficient to activate the PIN diode which can degrade again image uniformity. Moreover, the high conduction losses in fast switching diodes may induce for endoluminal coil considerable heat inside patient's body (Burl *et al* 2005). On the other hand, active detuning can be done by using a PIN diode added to the resonant circuit. The MR system transmits a direct current (DC) to activate the PIN diode

when the \vec{B}_1 field is emitted. Hence the low impedance of the PIN diode changes the self-resonant frequency of the coil. This method is faster, more reliable and safer than the passive detuning methods. Conventionally, the DC bias current is provided by the MR system and transmitted using a coaxial cable. For some specific applications, optical active detuning was already carried out. For instance, a safe, reliable and precise catheter tracking was demonstrated for intervention MRI procedures (Weiss *et al* 2004, Wong *et al* 2000). But those studies were not used for imaging and did not require an optical detuning system with high switching performance. Korn *et al* have used optical detuning for coils dedicated to compensate the physiological motion (Korn *et al* 2011). The switching time was not considered as an important parameter. Moreover, the low induced photocurrent (110 μA) in this detuning system would not be sufficient to detune a larger coil. Furthermore, Fandrey *et al* have used a passive technique to detune of the coil and an optical modulator to transmit the RF detected signal to avoid any additional galvanic connection (Fandrey *et al* 2012). In contrast, Memis *et al* have worked with an active optical detuning circuit where a phototransistor associated with a battery instead of a PIN diode (Memis *et al* 2008). This proof of concept was however not suited to MRI applications due to its expected non-magnetic compatibility. Finally, as already mentioned, dStream™ architecture of Philips uses a galvanic active detuning method.

The overall objective of our project is to develop an endoluminal receiver coil devoid of any galvanic connection and excluded from any active component. The fully optical receiver coil has then to ensure two functionalities: the active optical detuning of the coil and the optical transmission of the detected NMR. The optical transmission was validated on an optical bench (Aydé *et al* 2013, Aydé *et al* 2014). In the following, the first functionality of the coil is presented. The optical detuning method was designed to ensure a reliable detuning based on the bias signal provided through optical fiber. After conception, the detuning circuit was associated with a single loop endoluminal coil with conventional NMR signal reception.

The coils and detuning circuits were electrically characterized on a measuring bench before to be compared *in vitro* on a 3.0 T MR system in terms of signal uniformity and SNR.

2. Methods

2.1. Coils Prototypes

A rectangular single loop coil was designed using a 35 μm -thick copper trace (width $w = 5.1$ mm, and length $l = 47$ mm on a FR4 substrate (relative permittivity $\epsilon_r = 4$, thickness $t = 0.8$ mm). Previous *in vivo* works (Armenian *et al* 2004, Beuf *et al* 2004, Pilleul *et al* 2005) have demonstrated that such size and geometry of the loop enable the depiction of bowel abnormalities by imaging the colon wall layers with an adequate penetration depth and a high in-plane spatial resolution. Figure 1 shows the photograph

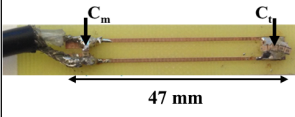
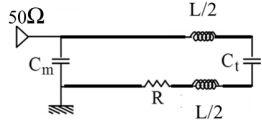
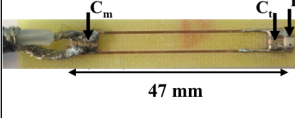
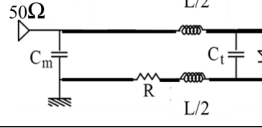
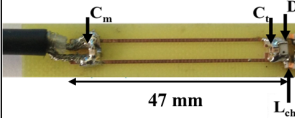
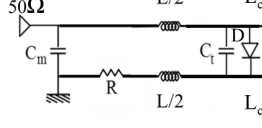
	Coil's prototypes	Electric circuits
Non-detuned coil		
Reference coil		
ODC		

Figure 1. Photographs and electric circuits of the different endoluminal coil prototypes: non-detuned coil, reference coil, and ODC.

and the electric circuit of the different used coils. The endoluminal receiver coils were designed to operate with a discovery MR750 3.0 T MR System (GEHC, Milwaukee, USA). These coils are matched to 50Ω at a 127.73 MHz frequency by using tuning and matching non-magnetic capacitors (American Technical Ceramics (ATC), New York, USA) on the distal and proximal parts of the coil.

A rectangular single loop without detuning circuit was first built. The adjustment of tuning and matching capacitors gives $C_t = 34.4$ pF and $C_m = 203.2$ pF.

The galvanic-detuned coil (reference coil) can be carried out by adding a DH 80055 PIN diode (Temex Ceramics, Pessac, France) to the rectangular coil circuit in the distal part to ensure the detuning of the coil when activated. The tuning and matching capacitor values of this coil are respectively $C_t = 36.3$ pF and $C_m = 190$ pF.

Similarly, the optical-detuned coil (ODC) was built by adding a PIN diode and two photodiodes to the rectangular coil. A silicon S6931-01 photodiode (Hamamatsu Photonics, Japan) was used, with a 6.6 mm^2 photosensitive area. This photodiode is considered as “low-magnetic” based on MR images depicting very negligible local deformation in shape and intensity. Two photodiodes in series were used instead of one to ensure the requested voltage for a PIN diode to operate in direct mode. Tuning and matching capacitor values were 44.4 pF and 206.2 pF respectively. Two choke inductors of $1.2 \mu\text{H}$ (SRT Resistor Technology, Germany) were added between the loop and the two photodiodes to block any alternating currents (AC) from interacting with the detuning circuit during NMR reception phase. When switching from detuning to tuning phase, the response of the coil is slow. Indeed parasitic capacitance of illuminated photodiodes enables photoelectrons to accumulate. Once light is off, these residual charges slowly flow out through the PIN diode which is still weakly biased (under threshold voltage) (Saleh *et al* 2007). Hence, a shunt resistance R_0 of $1.8 \text{ k}\Omega$ was added in parallel to force a rapid discharge of the photodiodes. The switching times from tuning to detuning and

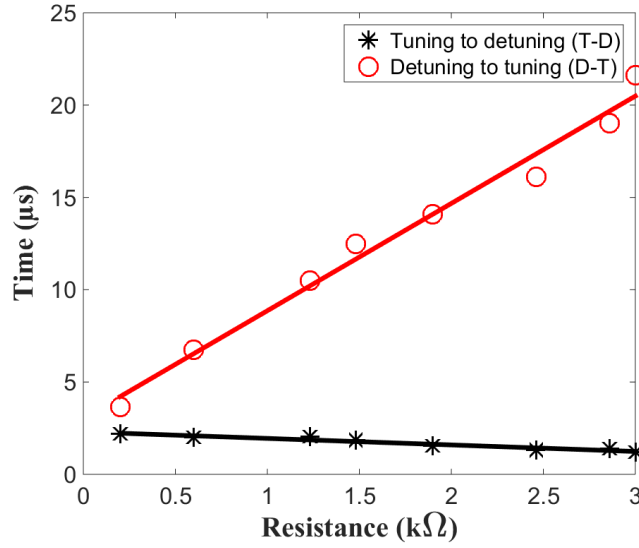


Figure 2. Switching time of the coil for tuning and detuning as a function of resistor-value R_0 .

reciprocally depend effectively on the electro-optical circuits and the added resistance-value. For a high resistance value, the commutation time to tuning mode increases (Figure 2). On the other hand, the resistance should be sufficiently high to have the adequate voltage to activate the PIN diode. Taking these factors into consideration, an appropriate trade off was obtained for a resistance value of 1.8 kΩ.

2.2. Optical Detuning Unit

In order to detune the coil, the two photodiodes added to the coil are illuminated by using two 30 mW fibred modulated laser diodes (Laser Components®, Germany, $\lambda = 650$ nm). The optical detuning system begins when the MR system provides a bias DC current (150 mA) or a negative voltage to respectively detune the coil by turning on the laser diodes or tune the coil back by turning them off. With the connector used for single channel coil, the DC current is provided on the coaxial RF signal cable. A AC-DC filter was first placed to derive the DC bias signal. This DC bias signal was then used to drive the modulation of laser diodes. Given that these laser diodes must be powered and the electronic circuit could contain magnetic components, it was important to place the laser command circuit (including the laser diodes) distant enough from the MR system. To transmit the DC current, a coaxial cable cannot be used; because it is long enough to act as an antenna and depict signal from RF pulses. For this reason our solution was to convert directly the outgoing DC current from the filter to an optical signal using an electrical-to-optical conversion circuit, including an HFBR transmitter (Avago Technologies, 1404, 820 nm, low optical power around 100 μ W). The converted signal is transmitted via a multimode optical fiber (Radiospares, $\emptyset = 0.2$ mm) to the laser command circuit. This latter consists of an optical to electrical converter: an HFBR

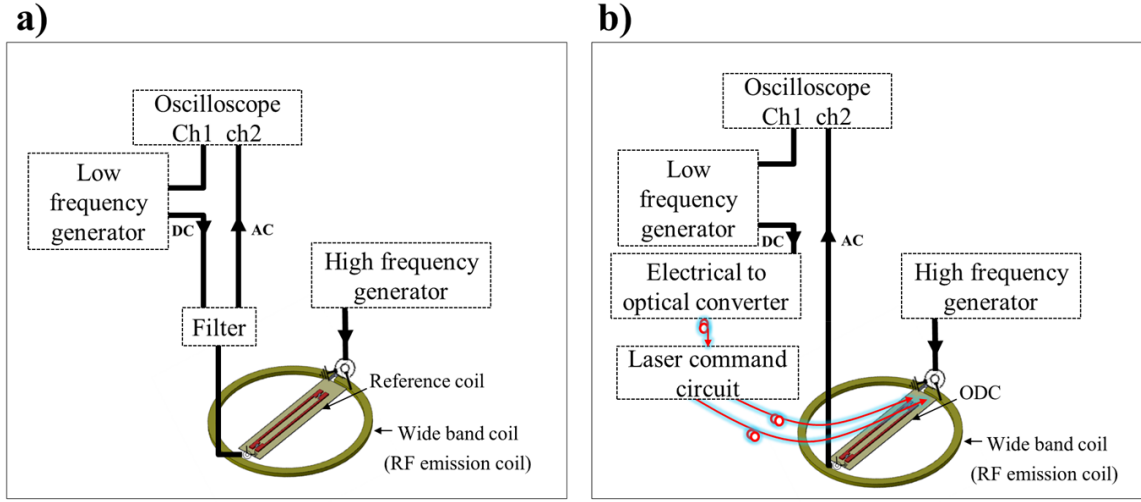


Figure 3. Schematic representation of switching time measurements procedure of an endoluminal coil added to a) a reference circuit and b) an ODC.

receiver (Avago Technologies, 2404, 820 nm) followed by a non-inverting amplifier to modulate the states of the laser diodes and then decouple the coil.

2.3. Experiments

Coils were characterized using a vector network analyzer (VNA) (Agilent Technologies Inc., Santa Clara, CA, USA). The quality factor of each coil is determined from the reflection coefficient $|S_{11}|$ when the coils were loaded with a cylindrical phantom that will be later described in this section. $|S_{11}|$ is studied to assess detuning performance of each coil prototype. Furthermore, the switching time from tuned to detuned state of the coil and reciprocally was measured. The switching times were characterized on an experimental bench as presented in figure 3. A RF magnetic field was generated using a circular wide band RF emission coil excited by a high-frequency generator. The electrical power of the generator was 13 dBm at a frequency of 127.73 MHz. The endoluminal receiver coil, resonating at the same frequency, was located in front of the RF emission coil to detect the magnetic field. The detuning of the reference coil was ensured by a low-frequency signal generator providing a square electrical 0 V/5 V signal. This is equivalent to the decoupling signal from a MR System (Figure 3(a)). A filter was used here to visualize the DC and RF signals separately on the oscilloscope. On the other hand, the optical detuning was ensured by the optical detuning system presented in figure 3(b). The signal received by the endoluminal coils was measured using a numerical 500 MHz oscilloscope (Agilent Technologies Inc., Santa Clara, CA, USA).

In vitro experiments were performed on a 3.0 T MRI. Figures 4(a) and 4(b) show the experimental setup. The coils were inserted into a plastic cylindrical phantom of 11 mm inner diameter, 90 mm outer diameter, and 100 mm-long. The phantom was filled

with a solution of $1.25 \text{ g NiSO}_4 \times 6\text{H}_2\text{O} + 5 \text{ g NaCl}$ per liter of distilled water to mimic the loading conditions of an internal coil inserted in a patient. First, the body coil was used as a transceiver to validate the efficiency of the detuning circuit by comparing the images acquired while using the tuned and the detuned coils. Corresponding images of the phantom without any endoluminal coil were also acquired to provide a basic reference. Two sequences were performed: a fast spin echo (FSE) sequence and a gradient echo sequence (GRE). Imaging parameters for the FSE sequence are $TR/TE = 3275 \text{ ms}/13.3 \text{ ms}$, axial images with a $FOV = 160 \times 160 \text{ mm}^2$, $slice \text{ thickness} = 2 \text{ mm}$, $spacing \text{ between slices} = 0.5 \text{ mm}$, $matrix = 256 \times 256$, $receiver \text{ bandwidth} = 16.67 \text{ kHz}$ or $\pm 8.335 \text{ kHz}$ ($pixel \text{ receiver bandwidth} = 65.11 \text{ Hz/Px}$). Image parameters for the GRE sequence are: $TR/TE = 400 \text{ ms}/8.9 \text{ ms}$, $flip \text{ angle} = 80^\circ$, axial images with a $FOV = 160 \times 160 \text{ mm}^2$, $slice \text{ thickness} = 2 \text{ mm}$, $spacing \text{ between slices} = 0.5 \text{ mm}$, $matrix = 256 \times 256$, $receiver \text{ bandwidth} = 11.90 \text{ kHz}$ or $\pm 5.95 \text{ kHz}$ ($pixel \text{ receiver bandwidth} = 46.48 \text{ Hz/Px}$). The SNR calculation and the registration of the MR images were performed using MATLAB language (Mathworks, Milwaukee, USA). The SNR was determined by the mean of the signal intensity in the entire MR image divided by the mean standard deviation of a region of interest chosen outside the image of the phantom (in the air) which is the noise. For the registration, a self-made MATLAB program was developed to align MR images to a common coordinate system. For the purpose of quantifying the performance of the endoluminal coils in terms of SNR uniformity distribution, the same GRE and FSE sequences were applied, this time, using the endoluminal coil as a receiver. The comparison was done by drawing and identifying some specific SNR iso-contour lines in the images acquired by the different coils. Finally, the local variation of the temperature was measured for both reference coil and ODC used as receivers in the MR experiment. This measurement was performed using the optical fiber temperature system (Opsens, Canada). Fibers tips were mounted to the coil using Teflon rubber, and the whole was immersed in 1.5 % agar-agar gel. For the reference coil, the fibers were placed at the proximal side of the loop, the distal (near the PIN diode), and the middle of the loop. For the ODC, the temperature variation was studied near the PIN diode and the two photodiodes.

3. Results

3.1. Experimental Bench Measurement

The reflection coefficient modulus $|S_{11}|$ as a function of the frequency is measured for each coil prototype in the tuned and detuned modes. The resonance frequency of the three coils is around 127.73 MHz. While the coil detuning, the resonance frequency is shifted except for the non-detuned coil. The quality factor Q of the tuned coils is calculated on tuning mode following the procedure described in reference (Beuf *et al* 2006). The coil without detuning circuit has the highest quality factor ($Q = 74$). The quality factor decreases slightly for both reference coils and ODCs due to the added

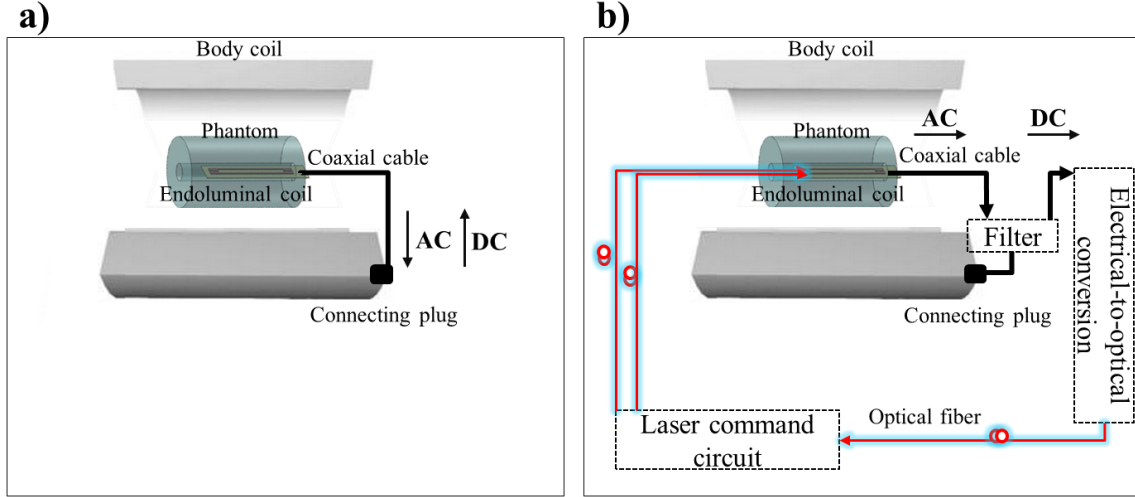


Figure 4. Schematic setups of coil detuning experiments performed on a 3.0 T MR system using an endoluminal coil with a) a galvanic-detuned circuit and b) an optical-detuned circuit.

PIN diode and photodiode components. For the two coil prototypes considered in this work, the quality factors Q are 53 and 55 respectively for the reference coil and ODC. On tuned mode, at 127.73 MHz, $|S_{11}| = -39.33$ dB and $|S_{11}| = -42.96$ dB for coils with optical and galvanic detuning circuits respectively. While on detuned mode, at 127.73 MHz, the reflection coefficient of the coil with optical detuning system is close to 0 dB (-0.70 dB); which is very similar to that of the reference coil (-0.66 dB). This result demonstrates that the current provided by the photodiodes is sufficient to detune the coil. Second, the switching times using the reference coil are fast compared to a typical RF pulse durations (in the order of milliseconds). Precisely, switching to tuning mode takes about 750 ns, and switching back to detuning mode takes about 250 ns. For the ODC, switching time is longer. By adding a resistance, the switching time to tuning state can decrease from approximately 100 μ s to 10 μ s (Figure 5). Using the resistance-value mentioned above in the methods section ($R_0 = 1.8$ k Ω), the switching times for ODC are 13.6 μ s and 1.7 μ s for tuning and detuning respectively.

3.2. In vitro MR Experiments

The MR images acquired to evaluate detuning methods using the body coil as a transceiver are shown in figure 6. For each acquisition, twenty-one axial images were acquired over the entire length z of the loop. The displayed axial signal intensity images and their SNR mapping corresponding to the central image out of stack. With the exception of the coil without detuning circuit, the signal magnitude of the MR images are very comparable with uniform signal distribution. Signal intensity and SNR maps corresponding to the non-detuned coil show clearly the non-uniform signal distribution close to the coil caused by the transmit RF \vec{B}_1 field. The coil detuning is absolutely

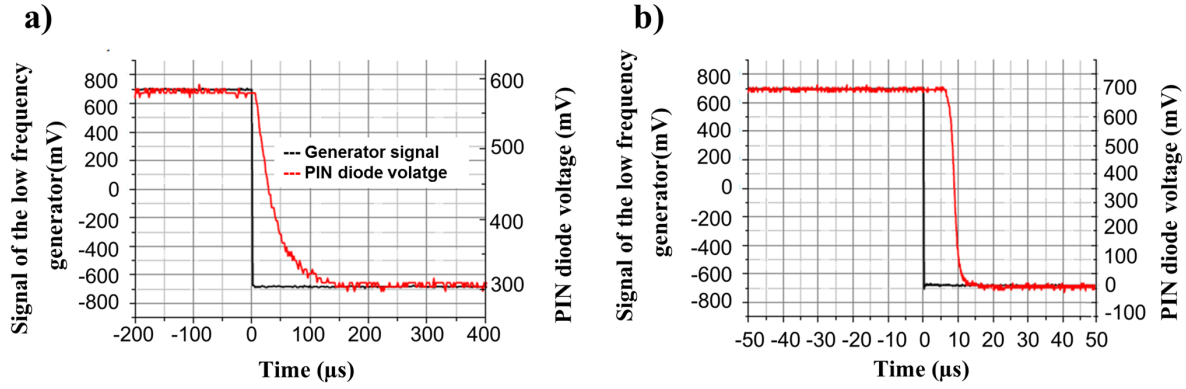


Figure 5. Response time graph showing the evolution of the voltage across the PIN diode versus time for ODC a) without and b) with resistor R_0 .

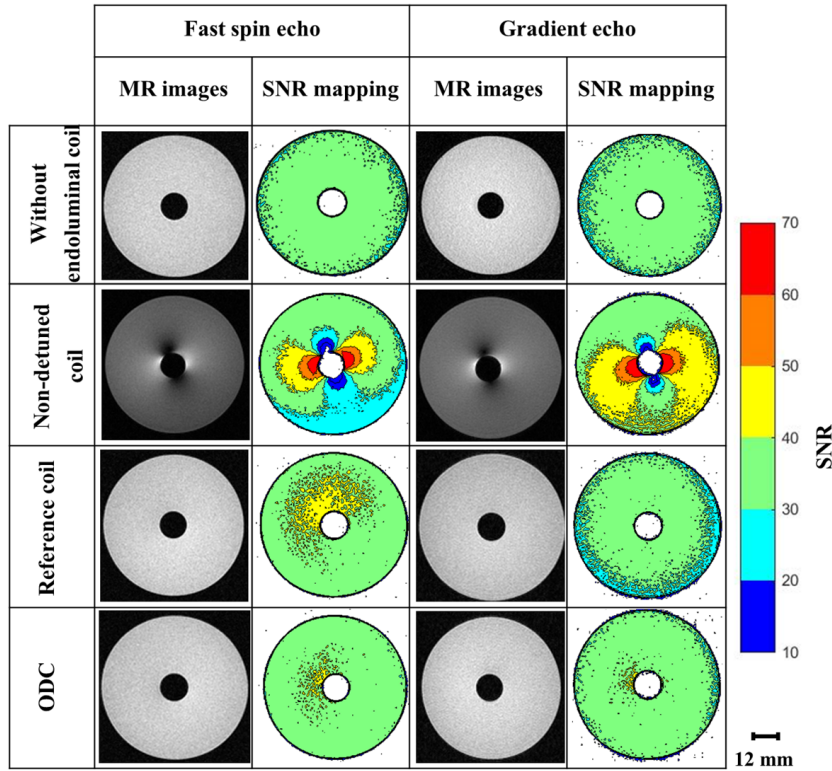


Figure 6. Axial images and SNR mapping of the phantom acquired using FSE and GRE sequence with the body coil used as a transceiver. The three endoluminal coils were located inside the phantom and they were continuously detuned.

mandatory.

The SNR values are ranging between 30 and 40 for the FSE and GRE sequences. For both sequences used, the SNR of MR images taken by the ODC with low-magnetic photodiodes are uniform and very comparable to the image of the phantom without any inserted coil. To study the SNR uniformity along the coil length z , the mean SNR was measured in two square form regions of interest (ROI) of about 100 mm^2 as shown in

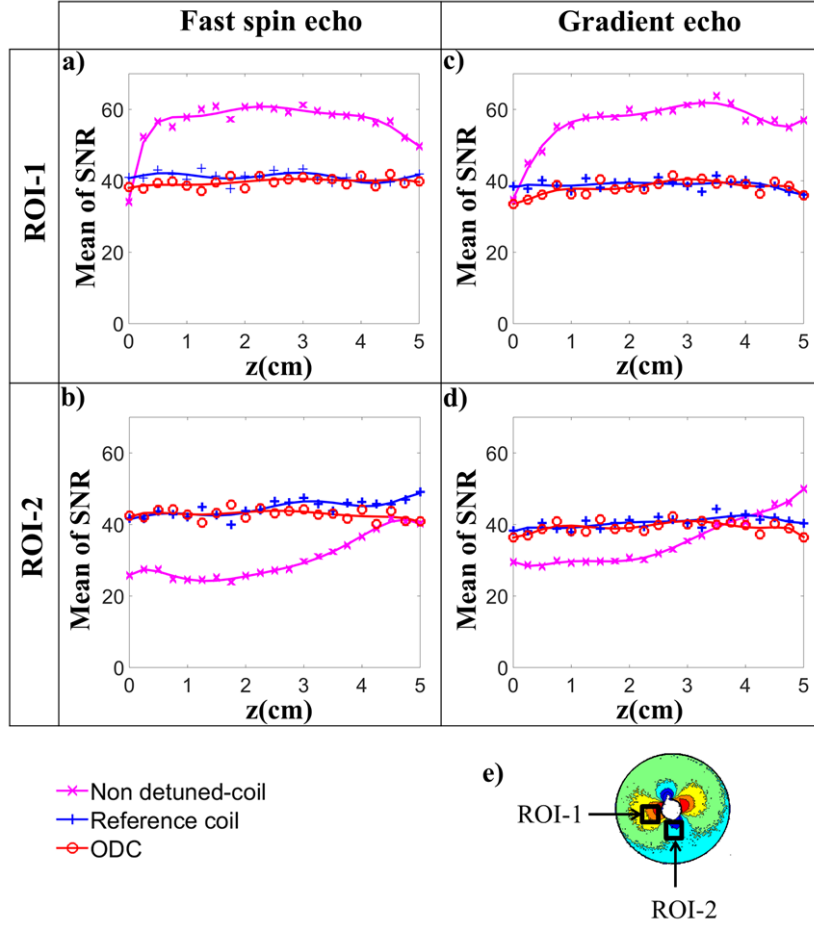


Figure 7. The measured signal-to-noise ratio of two regions of interest (ROI) for twenty-one axial images acquired by the body coil while using three different coils with (a-b) a fast spin echo sequence and (c-d) a gradient echo sequence. e) The choice of the positions of the two regions of interest (ROI-1 and ROI-2) is depending on the hyper and hypo signals presented in the MR image while using a non-detuned coil. The lines present a curve fitting to confirm the minimal variation of the SNR along the reference coil and the ODC.

figure 7. The positions of these two ROIs are identical for each image slice and they were chosen relatively to the positions of hyper and hypo signals of the image acquired while using a non-detuned coil (Figure 7(e)). The SNR uniformity was characterized by comparing the mean SNR of the two ROIs within each image of the stack. For the non-detuned coil, the figures 7(a) and 7(b) and figures 7(c) and 7(d) show that the SNR difference between the two ROI exceeds 30. For all detuned coils, SNR profiles along z for both ROIs are similar for the FSE and GRE sequences. It should be noted that for the ODC, the choice of the photodiode is important. It should have a small-size, a fast response time, and a low-magnetism. Figure 8 exhibits clearly that using magnetic photodiodes induce MR images distortions especially near the location of photodiodes.

The next experiment was done using the body coil as the RF transmitter and the endoluminal coil as a receiver. Given that the intensity of the image taken by a non-

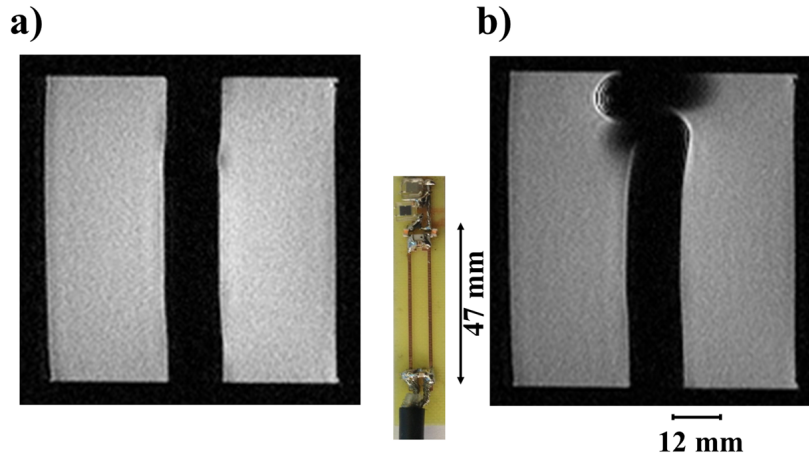


Figure 8. Coronal images of the phantom using a) low-magnetic photodiodes, and b) magnetic photodiodes.

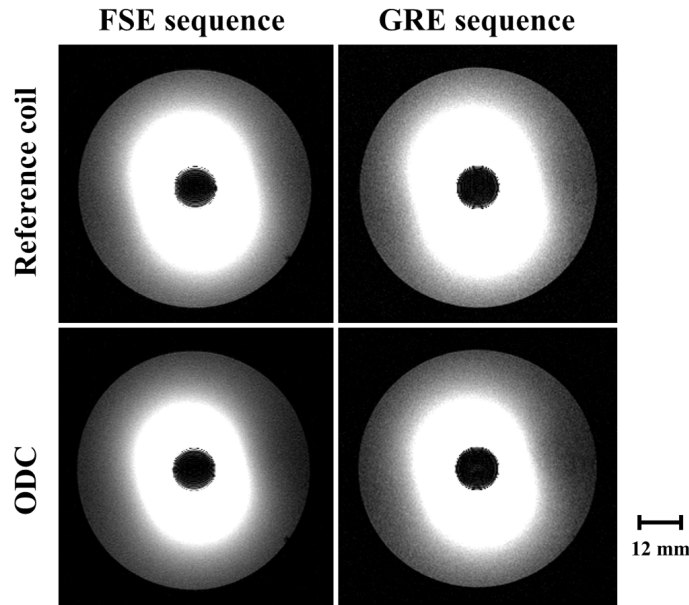


Figure 9. Axial MR images of the phantom acquired by the endoluminal coils.

detuned endoluminal coil is strongly altered by the cross-coil coupling, images were not acquired within these conditions. Images in figure 9 show comparable behavior between coils in terms of intensity and signal uniformity. According to figure 10, SNR iso-contours of the images taken with different coil prototypes are overlapping and this for both FSE and GRE sequences.

Finally, the variation of temperature for both the reference coil and ODC was measured during the *in vitro* experiments. For a galvanic detuning of the coil, the elevation of the temperature is around 2.77 °C near the PIN diode owing to the high detuning current emitted (150 mA). In the case of optical detuning, no change in temperature was discerned at the place of the PIN diode, this is due to the low

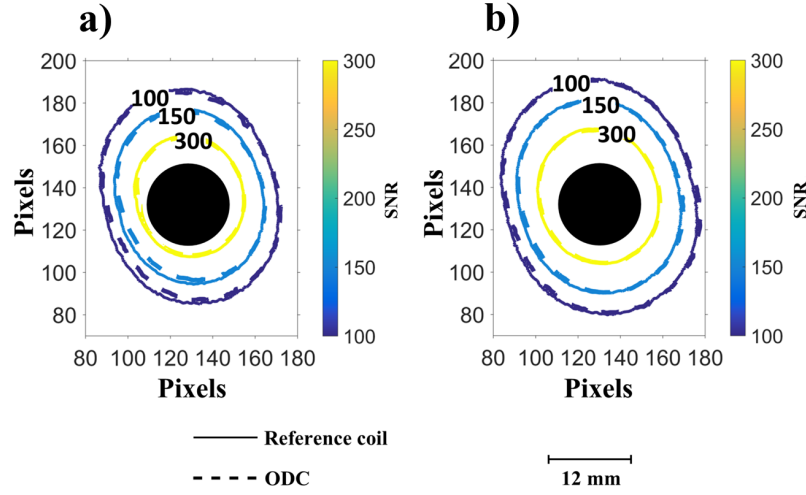


Figure 10. SNR iso-contours of the axial images acquired by the different coils using a) a FSE sequence and b) a GRE sequence.

photocurrent emitted (11 mA) by the photodiodes. And the negligible variation in the temperature ($\Delta T = 0.24$ °C) near the illuminated photodiodes proves that the laser diodes (30 mW, 650 μm) could be used without any potential risks to the imaged person. This result emphasizes that the use of optical detuning without RF induced heating effects could be considered as a safe active detuning mean.

4. Discussion and conclusions

The uniformity of signal intensity of images presented in figure 6 confirms that endoluminal ODC is as efficient as the galvanic-detuned coil (reference coil). The weak point of the ODC can be caused by the relatively low current injected into the PIN diode by the photodiodes. This current is actually around 11 mA which is relatively low compared to the 150 mA injected by the MR system to detune the reference coil. With this low intensity, no elevation of the temperature was recorded using the detuning circuit. But in order to fully ensure patient safety, the developed active detuning system should be associated with an endoluminal coil with a novel optical method of NMR signal transmission (Aydé *et al* 2013, Aydé *et al* 2014). A number of optical systems for NMR signal transmission have already been built (Fandrey *et al* 2012, Koste *et al* 2005, Memis *et al* 2008, Possanzini *et al* 2011, Yuan *et al* 2007). The associated detuning methods were either active and linked to MR console by a coaxial cable, or passive without any connection. In both cases, patient safety is very difficult to ensure for narrow endoluminal coil deeply inserted in the body. Other active optical detuning circuits were proposed for different MR applications (Korn *et al* 2011, Weiss *et al* 2004, Wong *et al* 2000). In the presented work, a PIN diode having very high impedance on blocking mode was used in parallel to tuning capacitor. The PIN diode was activated by two photodiodes being isolated from RF signals by two choke inductors. Using this

detune method, Q factor is not modified compared to that chosen by Weiss *et al* (2004) where a relatively low impedance photodiode non-isolated from the resonant circuit was used instead of the PIN diode. In the latter case, it was however not a real issue due to the pursued objectives of safe catheter tracking. Then an analysis of the behavior of the circuit in the reference (Korn *et al* 2011) shows that the switching time to tuning mode was not evaluated and probably not optimal. This would increase the switching time and limit temporal response of the receiver. With the use of a resistance R_0 , the switching times of our circuit (around ten of μs at the slowest) are still quite small relative to the regular pulse duration (in the range of ms) for most MR imaging sequences including fast and even ultra-fast imaging sequence such as echo-planar imaging. However, our circuit could not be fast enough for very specific sequence such as ultra-short echo time sequences (e.g. UTE). Moreover, in this work, a higher current was provided by the photodiodes to the PIN diode compared to optical detuning system of reference (Korn *et al* 2011) ($11\text{ mA} > 100\text{ }\mu\text{A}$) which is leading to more efficient detuning. Finally, unlike these previous works, our system configuration is suitable for all size of coil or loop. In fact, it can be easily adjusted in order to respond to all detuning applications (coils dimensions, tracking or imaging) by increasing the power of the laser or the radiant sensitive area dimension of the photodiode. It should be notice that *in vivo* studies of optical detuning is not adequate at this stage for several reasons. First, evaluating different detuning performances by comparing subtle changes with variable biological environments is not relevant. Second, keeping in mind that it is a safety issue, it would be unethical to perform this experiment *in vivo*. In conclusion, a novel compact active optical detuning circuit associated to a deported unit was developed and demonstrated with MRI endoluminal coil. The optical detuning circuit was based on the previous work of Korn *et al* (2011). The use of optical detuning was proposed to ensure total the patient safety. This strategy could be more widely developed and adapted in the future with multi-channel array coils. Optical-based detuning circuit associated with signal optical transmission via optical fibers could be the near future (Yuan *et al* 2016).

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