Circuit Topology Study for Distributed MPPT in Very Large Scale PV Power Plants

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Abstract—In very large scale photovoltaic power plants (VLS-PV), due to partial shading and PV modules mismatching, a single point MPPT is not efficient for all PV modules. Therefore, distributed maximum power point tracking (DMPPT) can be utilized to increase output power capability by increasing the number of converter/inverter units. In this paper, a simple circuit is introduced to achieve DMPPT. Then, the limitations of DC bus voltage, total output power, duty ratio of the different converter choices are discussed. Simulation results also show that the proposed strategy can be utilized to realize seamless transition between soft start mode and steady state operation.

Keywords: DMPPT, Lagrange's Theorem, Sensitivity, Stability, VLS-PV

I. INTRODUCTION

Nowadays, renewable energies are being considered as promising resources to meet the continuously increasing demand of energy and to improve the reliability of electric power systems [1-3]. According to an IEA report, the world's total CO₂ emissions and primary energy demand in 2030 will be twice as much as in 2000. This increasing energy consumption causes serious environmental problems such as global warming and acid rain. To resolve both energy and environmental problems, photovoltaic (PV) solar energy has become a significant and attractive candidate for green power generation in distribution networks [4-7]. However, due to PV's low energy density, to achieve the same megawatt power level as typical power plants do, the Very Large Scale PV (VLS-PV) power plants usually require hundreds of acres of land and hundreds of thousands of PV modules [8].

One example of VLS-PV systems is the solar power plant at Nellis Air Force Base. In this 13.2 MW facility, 72,000 sun power PV modules are installed on 140 acres of land. Fifty-two 250 kW and two 100 kW Xantrex inverters are used to convert the 400 V dc from series-connected PV module groups to 60 Hz low voltage ac. Then, 60 Hz power transformers are used to connect the low voltage output from the inverters to the 12,470 V local distribution lines.

So far, four major megawatt circuit topologies (as shown in Fig. 1) have been proposed for VLS-PV systems [9]:

1. Centralized inverter,

2. String inverter,
3. String inverter with a team concept,
4. Multi-string inverter.

Fig. 1. Major existing megawatt circuit topologies for VLS-PV systems

The centralized inverter, as shown in Fig. 1 (a), seems to be the lowest cost solution for the megawatt PV system. However, there are several major drawbacks to this topology such as mismatch losses due to single maximum power point tracking, low upgradeability, higher power loss caused by reverse current blocking diodes, and very low continuity of service at low irradiation. In the circuit topology with string inverters, shown in Fig. 1(b), mismatch power losses are reduced and diodes between strings are eliminated. Thus, system's efficiency will be increased. The "team concept", as shown in Fig. 1 (c), utilizes a jumper switch between the strings. Therefore, the PV power plants enable to operate continuously at low irradiances. The multi-string inverter, as shown in Fig. 1 (d), has a DC/DC converter for each string that allow the integration of heterogeneous PV strings. This system is also upgradable to a certain extent. Since the DC/DC converters increase the number of control

freedoms in the system, the MPPT, system protection, and ancillary services can be realized with more flexibility. The major disadvantage of this circuit topology is high cost and low reliability because of more power electronics stages are involved. So far, the most popular circuit structure is the string inverter shown in Fig. 1 (b). The Nellis PV 13.2 MW PV power plant is the best example.

To upgrade existing VLS-PV systems such as the one at Nellis Air Force Base to achieve more power and flexibility, DC/DC converters can be added before each inverter to form multi-string inverter as shown in Fig. 1(d). But, this solution may not be cost efficient and reliable. In this paper, a simple and cost efficient circuit is introduced. Then, Lagrange's theorem is utilized to calculate DMPPT. After that, in a case study, this circuit will be compared with other typical circuits for maximum achievable power. At the end, the sensitivity and controllability of different DC/DC converters are analyzed and compared with each others for more flexible and easier control. A seamless transition between a soft start and steady state operation is demonstrated.

II. A SIMPLE AND COST EFFICIENT CIRCUIT TOPOLOGY FOR DMPPT

As shown in Fig. 2, to increase the power handling of existing PV power plants with one converter a time, a DC/DC converter can be added to one string of the string inverter structure.

The following equations can be used to describe the dc side voltage of circuit:

$$V_{dc} = V_{PV.1} * f(D) + V_{PV.2} \quad (1)$$

$$f(D) = \frac{I_{PV.1}}{I_{PV.2}}, \quad (2)$$

where, $f(D)$ is the transfer function of DC/DC converters. By control the current of the inverter which is connected to the grid, the total power of the inverter will be determined. Based on this power, with the specific range of modulation indexes and V_{dc} , the current and the related voltage of the PV_2 will be controlled. Then, a desired output voltage of DC/DC converter can be calculated. Through voltage control of the DC/DC converter, the voltage and the current of the first PV will be controlled. This idea is shown in Fig. 3.

To calculate the maximum power, based on Lagrange's theorem, (1) and (2), the following equations can be utilized as constraints:

$$g_1(V_{PV.1}, I_{PV.1}) = 0, \quad g_2(V_{PV.2}, I_{PV.2}) = 0, \quad (3)$$

where, g_1 and g_2 are the dynamic equations of two PVs. As a result, the total power can be derived as follows:

Fig. 2. The circuit topology with one DC/DC converter in VLS-PV systems

Fig. 3. Block diagram of two PV strings control with one DC/DC converter

$$J = V_{pv1} * I_{pv1} + V_{pv2} * I_{pv2} + \lambda_1 * g_1(V_{PV.1}, I_{PV.1}) + \lambda_2 * g_2(V_{PV.2}, I_{PV.2}) + \lambda_3 * (V_{dc} - V_{PV.1} * \frac{I_{PV.1}}{I_{PV.2}} - V_{PV.2}) \quad (4)$$

In this equation, constant coefficients λ_1 , λ_2 and λ_3 are used to make the derivatives of the equations equal zero. To achieve maximum power, the derivative of the total power based on the two PVs' voltages and currents should be zero:

$$\frac{dJ}{dV_{PV.1}} = 0, \quad \frac{dJ}{dI_{PV.1}} = 0, \quad \frac{dJ}{dV_{PV.2}} = 0, \quad \frac{dJ}{dI_{PV.2}} = 0 \quad (5)$$

By using the (1), (2), (3), and (5), the number of non-linear equations will be the same as the number of parameters. Through the use of standard numerical algorithms, such as Newton-Raphson, the PV voltage and current can be calculated and stored in a lookup table that includes irradiation and temperature. Some of the calculated results are shown in the case study part of this paper.

To implement the control algorithm for this circuit, the designed dc bus voltage should be in the reasonable range. The algorithm and modulation index that are utilized for the inverter determine the minimum voltage in the DC bus. If output voltage of inverter is directly connected to the grid, the equivalent modulation index is described by the following equation:

$$Modulation\ Index\ (M) = \frac{\frac{V_{grid} * \sqrt{2}}{\sqrt{3}}}{\frac{V_{dc}}{2}}, \quad (6)$$

Therefore, the minimum dc voltage will be defined by the maximum modulation index:

$$V_{dc}(\min) = \frac{2\sqrt{2} * V_{grid}}{\sqrt{3} * M_{\max}}. \quad (7)$$

The magnitude of dc input current for the inverter is I_{PV2} . Then, based on I_{PV2} and V_{PV2} , the power of PV_1 will be calculated as below:

$$P_{PV1} = (V_{dc} - V_{PV2}) * I_{PV2}. \quad (8)$$

This power should not be more than $MPPT_{PV1}$. Thus, the maximum dc voltage will be determined by the following equations:

$$MPPT(P_1) = (V_{dc}(\max) - V_{PV2}) * I_{PV2} \quad (9)$$

$$V_{dc}(\max) = \frac{MPPT(P_1)}{I_{PV2}} + V_{PV2} \quad (10)$$

Since, the total output power is dictated by dc bus voltage and V_{PV2} , if PV_1 works less than its own maximum power point, it can work on two different points with positive and negative $\frac{dP_{PV1}}{dV_{PV1}}$. This idea is shown in Fig. 4. For the point

“1” with positive derivative, at any disturbance of V_{PV1} , at the same duty ratio of the dc/dc converter, the dc bus will receive positive feedback. But for the point “2”, a possible disturbance of V_{PV1} will result in negative feedback to the dc bus. Thus a more stable working point could be achieved.

III. CASE STUDY FOR DISTRIBUTED MAXIMUM POWER TRACKING

To analyze maximum achievable power in the circuit, the single dc/dc converter topology is compared with two other cases: no DC/DC converter and two DC/DC converters, as shown in Fig. 5. In this comparison, two PV strings have receive different irradianations. And the total maximum power at the predefined irradiation level is 226 kW. The results of Fig. 5(b) and (c) are listed in Tables 1 and 2 respectively. Then, in Fig. 6, the generated power for these systems is compared with each others.

As shown in the results, when two DC/DC converters are utilized, if V_{dc} is chosen in the range that two converters can switch less than their maximum voltage stress, MPPT always can be achieved for both PVs [4], which is shown in Fig. 6. For the case with one DC/DC converter, in very limited range of V_{dc} , the total achievable power is very close to the summation of MPPT for both PVs. In the case with no

DC/DC converter, there is no compensation on PVs mismatching and the total power is decreased dramatically.

Fig. 4. Two working points for same power in first PV

Fig. 5. Three different circuit topologies for DMPPT in VLS-PV

To analyze the control sensitivity, for the case study with one DC/DC converter, different transfer functions are tested. Then, the change of duty ratio for V_{dc} from 600V to 1000V is calculated and compared with each others. The results are shown in Fig. 7. As shown in this picture, by using $D/(1-D)$ or $(1-D)/D$ transfer function (buck-boost converter), range of

changes for duty ratio will be increased. Then, more flexibility for control and implementation of DC/DC converter can be achieved. It should be noted that for this circuit, the current of second PV string can be higher or lower than the first one. Therefore, buck or boost converter cannot be utilized.

Table. 1: The maximum generated power for two PV strings without dc/dc converter.

Vdc (V)	Vpv1(V)	Vpv2 (V)	Ipv1 (A)	Pmax (Watt) ($\times 10^5$)
	$\times 10^{-2}$			
600	0.016046	6.283953	1.666001	1.045303
650	0.216046	6.283953	1.666000	1.082900
700	0.716045	6.283954	1.665999	1.166199
750	1.216045	6.283954	1.665997	1.249498
800	1.716043	6.283956	1.665992	1.332794
850	2.216019	6.283980	1.665923	1.416034
900	2.715664	6.284335	1.664909	1.498418
950	3.210642	6.289357	1.650527	1.568001
1000	3.664459	6.335540	1.515562	1.515562

Table. 2: The maximum generated power for two PV strings with one dc/dc converter.

Vdc (V)	Vpv1(V)	Vpv2 (V)	Ipv1(A)	Ipv2(A)	$f(D)$	Pmax (Watt) ($\times 10^5$)
	$\times 10^{-2}$					
600	3.558665	4.316569	1.574232	3.327827	0.4730511	1.99669679
650	3.558665	4.806462	1.574232	3.307967	0.4758912	2.15017897
700	3.558665	5.258411	1.574232	3.216698	0.4893939	2.25168895
750	3.558665	5.616699	1.574232	2.974655	0.5292152	2.23099140
800	3.558665	5.868378	1.574232	2.628125	0.5989946	2.10250001
850	3.558665	6.043501	1.574232	2.280550	0.6902863	1.93846786
900	3.558665	6.168876	1.574232	1.978779	0.7955578	1.78090073
950	3.558665	6.261409	1.574232	1.729816	0.9100577	1.64332559
1000	3.558665	6.331636	1.574232	1.527157	1.03082561	1.52715728

Fig. 6. Maximum achievable power for three different cases

IV. SIMULATION RESULTS

The simulation results of circuit topology with one DC/DC converter are shown Fig. 8. The transient of total output power and dc bus voltage is shown for the case that desired dc bus voltages is set at 700 V. The simulated output power verifies the calculated results in Table 2. The simulation

results also show that with the proposed control strategy (Fig. 3), by changing the ac side current command, the one dc/dc converter based system can start from zero output power and have seamless transition between soft start and steady state operation.

Fig. 7. Different DC/DC duty ratio changes based on dc bus voltage.

Fig. 8. Simulation results (a) Dc bus voltage control; (b) Total output power; (c) p_{v2} output voltage; (d) ac side current.

V. CONCLUSION

In this paper, a single DC/DC converter based solution is shown as an addition to the power conditioning circuit topologies for VLS PV power plants. The benefit of this circuit is that it could be used to upgrade the existing systems with one dc/dc converter at a time. A case study is shown in this paper. The study results show that with one more dc/dc converter, the achievable power of the system can be improved significantly. The control strategy of the overall circuit structure and the circuit selections for the added DC/DC converter are also introduced.

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