

In the following function, we construct the residual needed for time integration of second-order system

$$\mathbf{M}_V \ddot{\mathbf{q}} + \mathbf{C}_V \dot{\mathbf{q}} + \mathbf{F}_V(\mathbf{q}) = \mathbf{V}^T \mathbf{F}_{ext}(t),$$

where  $\mathbf{M}_V := \mathbf{V}^T \mathbf{M} \mathbf{V}$ ,  $\mathbf{C}_V := \mathbf{V}^T \mathbf{C} \mathbf{V}$ ,  $\mathbf{F}_V(\mathbf{q}) := \mathbf{V}^T \mathbf{F}(\mathbf{V} \mathbf{q})$  are reduced operators. We use the reduced residual is defined as

$$\mathbf{r}(\ddot{\mathbf{q}}, \dot{\mathbf{q}}, \mathbf{q}) = \mathbf{M}_V \ddot{\mathbf{q}} + \mathbf{C}_V \dot{\mathbf{q}} + \mathbf{F}_V(\mathbf{q}) - \mathbf{V}^T \mathbf{F}_{ext}(t).$$

A generic Residual function, whose *handle* is passed for performing Implicit Newmark and Generalized-  $\alpha$  nonlinear time integration schemes in this code has the following syntax:

$$[r, drdqdd, drdq, drdq, c0] = \text{Residual}(q, qd, qdd, t);$$

where

$$r = \mathbf{r},$$

$$drdqdd = \frac{\partial \mathbf{r}}{\partial \ddot{\mathbf{q}}},$$

$$drdq = \frac{\partial \mathbf{r}}{\partial \dot{\mathbf{q}}},$$

$$drdq = \frac{\partial \mathbf{r}}{\partial \mathbf{q}},$$

$c0$  = a scalar measure for comparing the residual norm while checking for convergence

The extra arguments:

1. Assembly, which is an instance of ReducedAssembly class
2. Fext, which is a function handle for the external forcing,
3. V is the basis used for Galerkin projection  $\mathbf{V}$  and is a property of the ReducedAssembly Class

are required for computing the residual in this case.

New residual functions that follow the above-mentioned syntax can be written according to user preference. This way, the same time integration class can be used to solve a variety of problems.

Please refer to the Mechanical directory in the examples folder to understand applications and usage.

```
function [ r, drdqdd, drdq, drdq, c0] = residual_reduced_nonlinear( q, qd, qdd, t, Assembly, Fext)
```

In this function, it is assumed that the matrices  $\mathbf{M}_V, \mathbf{C}_V$  for the finite element mesh were precomputed and stored in the DATA property of the Assembly object to avoid unnecessary assembly during each time-step.

```
V = Assembly.V;
M_V = Assembly.DATA.M;
C_V = Assembly.DATA.C;
```

The reduced tangent stiffness  $\mathbf{K}_V = \frac{\partial \mathbf{F}_V}{\partial \mathbf{q}}$  and the reduced internal force  $\mathbf{F}_V$ , however, need to be assembled at each iteration depending on the current state. This assembly is best performed at an element level in its reduced form as

$$\mathbf{K}_V(\mathbf{q}) = \sum_{e=1}^{n_e} \mathbf{V}_e^T \mathbf{K}_e(\mathbf{V}_e \mathbf{q}) \mathbf{V}_e,$$

$$\mathbf{F}_V(\mathbf{q}) = \sum_{e=1}^{n_e} \mathbf{V}_e^T \mathbf{F}_e(\mathbf{V}_e \mathbf{q})$$

We first obtain the full degrees of freedom vector  $\mathbf{u}$  over the mesh from the reduced variables  $\mathbf{q}$  as  $\mathbf{u} = \mathbf{V}\mathbf{q}$ , and then directly assemble the reduced nonlinear operators with the Assembly class method `tangent_stiffness_and_force_modal(u,V)`.

```
u = V*q;  
[K_V, F_V] = Assembly.tangent_stiffness_and_force(u);
```

Residual is computed according to the formula above:

```
F_inertial = M_V * qdd;  
F_damping = C_V * qd;  
F_ext_V = V.'*Fext(t);  
  
r = F_inertial + F_damping + F_V - F_ext_V ;  
  
drdqdd = M_V;  
drdq = C_V;  
drdq = K_V;
```

We use the following measure to compare the norm of the residual  $\mathbf{r}$

$$c0 = \|\mathbf{M}_V \ddot{\mathbf{q}}\| + \|\mathbf{C}_V \dot{\mathbf{q}}\| + \|\mathbf{F}_V(\mathbf{q})\| + \|\mathbf{V}^T \mathbf{F}_{ext}(t)\|$$

```
c0 = norm(F_inertial) + norm(F_damping) + norm(F_V) + norm(F_ext_V);
```

```
end
```