

Maritime Solar Vortex Platforms for Targeted Precipitation Enhancement:

An Integrated Spectral, Thermodynamic, and Atmospheric Control Approach

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Abstract

Freshwater scarcity in arid coastal regions presents one of the most tractable grand challenges in applied climatology, yet existing intervention technologies — desalination, conventional cloud seeding, and inland solar chimney designs — share a common limitation: they address either the energy side or the moisture side of the precipitation problem, rarely both. This paper proposes a mobile maritime solar vortex platform that resolves this trade-off by deploying a solar-driven convective column system over the open ocean, where boundary layer relative humidity is sufficiently high that the lifting condensation level (LCL) lies within reach of a practical tower structure. Three integrated components are developed: (1) a vertical stacking architecture for convective column intensification, in which staged vortex generators maintain column buoyancy against entrainment dilution and deliver the column to the LCL where latent heat feedback initiates self-sustaining convection; (2) a spectral splitting system in which incident solar radiation is decomposed into infrared thermal forcing for the convective column, visible-band photovoltaic generation for platform power, and ultraviolet concentration for antifouling and water treatment; and (3) a differentiable weather model positioning framework in which gradient-based inversion of a trained atmospheric surrogate identifies optimal platform deployment locations and timing to maximise precipitation delivery to a target inland area. The system is analysed from first principles, with quantitative order-of-magnitude estimates for energy balance and water yield. Key engineering challenges — convective column coherence under wind shear, optical alignment in maritime conditions, and surrogate model fidelity for mesoscale coastal convection — are identified and framed as priorities for staged experimental validation. The proposed system functions as a mechanical convective inhibition (CIN) breaker: its task is not to drive precipitation directly but to deliver sufficient column energy to the LCL that atmospheric conditional instability completes the process. This reframing substantially reduces the required intervention energy relative to prior weather modification proposals.

Keywords: solar vortex; precipitation enhancement; spectral splitting; cloud seeding; atmospheric water harvesting; differentiable weather models; convective inhibition; maritime platforms

1. Introduction

Freshwater scarcity affects more than two billion people and is projected to worsen as climate change intensifies drought frequency and duration across arid and semi-arid zones. Conventional responses fall into two broad categories: supply augmentation through desalination or groundwater extraction, and demand management through efficiency and reuse. Both are necessary but insufficient at the scale required. A third category — atmospheric water harvesting and precipitation enhancement — has received increasing attention, but existing technologies share structural limitations that constrain their impact.

Conventional cloud seeding introduces hygroscopic or glaciogenic aerosols (typically silver iodide) into clouds to enhance precipitation from existing moisture. The technique is well-established and operationally deployed in approximately ten US states and numerous other countries. Its fundamental limitation is that it is moisture-opportunistic: it requires pre-existing cloud cover and sufficient supercooled liquid water content. In genuinely arid regions, where the moisture deficit is most acute, suitable cloud conditions are precisely what is absent. Cloud seeding does not create water; it extracts water that was already going to precipitate, somewhat more efficiently. For severe water scarcity this is insufficient.

Solar chimney designs for precipitation enhancement address the lift side of the problem: by heating a surface collector, they drive a convective updraft that in principle could carry moist air to condensation altitude. The solar chimney concept is well-studied for power generation, but its application to precipitation has a fundamental physical obstacle. In arid regions, the lifting condensation level — the altitude at which rising air cools to its dew point — typically lies 2,500 to 4,000 metres above the surface, depending on temperature and humidity. A mechanically realistic solar tower reaches 200 to 500 metres. The gap between what a tower can deliver and what the atmosphere requires for condensation is approximately an order of magnitude, and bridging it with a single structure is neither technically nor economically feasible.

This paper proposes a system that resolves both limitations simultaneously by changing the deployment context from arid land to the open ocean. Over the ocean, boundary layer relative humidity is typically 75 to 85 percent. At these humidity levels, the LCL drops to 400 to 600 metres — within reach of a practical tower. The moisture problem disappears. The lift problem then becomes the primary engineering challenge, and the vertical stacking architecture proposed here addresses it directly.

Three additional integrations distinguish the proposed system from prior solar vortex concepts. First, spectral splitting of incident solar radiation allows the infrared fraction to drive thermal

forcing of the convective column while the visible fraction powers photovoltaic generation for the platform, resolving the energy trade-off inherent in single-mode solar collection. The ultraviolet fraction, typically wasted, is directed to antifouling and water treatment applications that are directly relevant to maritime platform operation. Second, the platform is mobile, allowing deployment to be optimised for precipitation delivery to a specific inland target rather than fixed at a location determined by infrastructure. Third, a differentiable atmospheric surrogate model — specifically, the gradient-based inversion of a trained neural weather model — provides positioning intelligence: given a target precipitation outcome, the model identifies the optimal platform location and deployment window.

The paper is organised as follows. Section 2 develops the physical basis of the system, including the LCL analysis for maritime conditions, the vertical stacking concept, and the latent heat feedback mechanism. Section 3 presents the spectral splitting architecture. Section 4 develops the positioning intelligence framework and its relationship to recent differentiable weather modelling. Section 5 addresses platform design and engineering challenges. Section 6 outlines staged experimental validation pathways. Section 7 presents order-of-magnitude economic analysis. Section 8 addresses governance considerations. Section 9 concludes with priorities for future work.

2. Physical Basis

2.1 The Lifting Condensation Level Problem

The lifting condensation level is the altitude at which an air parcel, lifted dry-adiabatically from the surface, cools to its dew point and condensation begins. It can be estimated from surface temperature T and dew point temperature T_d as:

$$\text{LCL} \approx 125 \times (T - T_d) \text{ [metres]}$$

For representative arid land conditions in the Sahara or Arabian Peninsula in summer — surface temperature 40°C , dew point approximately 5°C at 15 percent relative humidity — the LCL lies at approximately 4,375 metres. At 20 percent relative humidity the dew point rises to approximately 15°C , giving an LCL of approximately 3,125 metres. These figures explain why terrestrial solar chimney proposals for precipitation enhancement, which typically assume towers of 200 to 1,000 metres, fail to close the physical gap.

For maritime conditions the calculation is fundamentally different. At 80 percent relative humidity and a sea surface temperature of 28°C , the dew point is approximately 24°C , giving:

$$\text{LCL} \approx 125 \times (28 - 24) = 500 \text{ metres}$$

This is within reach of a practical tower structure. The entire character of the engineering problem changes: over the ocean, the challenge is not to close a kilometre-scale gap to the LCL

but to optimise the convective column above it. Vertical stacking becomes an intensification strategy rather than a survival requirement.

2.2 Vertical Stacking: The Physical Argument

A solar chimney drives an updraft by creating a temperature differential between heated surface air and the ambient atmosphere. For a buoyant plume rising through a tower of height H with temperature excess ΔT above ambient temperature T_0 , the updraft velocity scales approximately as:

$$w \propto \sqrt{(g \cdot H \cdot \Delta T / T_0)}$$

Once air exits the tower structure, it continues rising as a free buoyant plume. This plume is subject to entrainment of ambient air, which progressively dilutes its buoyancy excess and decelerates the column. Standard buoyant plume theory (Morton, Taylor and Turner, 1956) gives the entrainment rate as proportional to updraft velocity and column perimeter. Qualitatively, narrower columns entrain proportionally more ambient air per unit volume than wider ones, implying that column radius should be maintained rather than allowed to contract as the column rises.

In addition to entrainment, wind shear in the lower to middle troposphere tilts and disrupts free plumes. At moderate shear velocities of 5 to 10 m/s over a few hundred metres, a free plume can be significantly disrupted before reaching condensation altitude. This is the coherence problem: even if the tower delivers a buoyant column to its exit height, there is no guarantee the column survives to the LCL.

The vertical stacking concept addresses both entrainment dilution and shear disruption through staged buoyancy injection. A series of vortex generators, positioned along the intended column trajectory at intervals matched to the local entrainment and shear dissipation rate, re-energises the column before the buoyancy excess from the previous stage has been fully dissipated. Each stage adds sensible heat and momentum, sustaining the column's thermal advantage over ambient air.

The analogy to staged rocket propulsion is instructive but imperfect. In a rocket, each stage fires into vacuum; in the atmosphere, each upper generator sits in the potentially turbulent wake of the generator below. Stage spacing is therefore a critical design variable: stages too far apart allow the column to lose coherence between injections; stages too close produce destructive aerodynamic interference. Determining optimal spacing requires site-specific knowledge of the ambient wind profile and turbulence intensity, and is identified as a primary objective for experimental validation.

One implication of the entrainment analysis concerns horizontal geometry. Since narrower columns entrain proportionally more per unit volume, column radius should be maintained or modestly increased with height. Whether an actively expanding geometry reduces entrainment is

less clear: expansion in a free plume risks flow separation and increased turbulent mixing at the column boundary, potentially counterproductive. Geometry optimisation between stages is treated here as an open design question requiring experimental investigation.

2.3 The Latent Heat Feedback Threshold

The most physically significant feature of the stacked maritime system emerges above the LCL. When rising air reaches saturation and condensation begins, it releases latent heat of approximately 2.5 MJ per kilogram of water condensed. This heat is deposited directly into the rising column, adding buoyancy that the solar collectors did not supply. The column becomes partially self-energising.

The consequence is a threshold nonlinearity. Below the LCL, the system operates as a sensible-heat engine: solar energy in, mechanical uplift out, negligible condensation. Above the LCL, latent heat release accelerates the updraft, which carries more moisture upward, which condenses and releases more heat. Order-of-magnitude estimates suggest latent heat may contribute 30 to 50 percent of column buoyancy above the condensation level, though this figure requires experimental validation.

If the atmosphere above the LCL is conditionally unstable — that is, if the environmental lapse rate exceeds the saturated adiabatic lapse rate — natural convection takes over entirely once the column breaches the LCL, and upper stages of the vortex array become unnecessary. Conditional instability is common in arid-coastal environments with deep convective mixed layers and high sea surface temperatures, particularly during summer months.

This reframes the design objective in a way that substantially reduces the engineering burden. The system is not required to drive precipitation directly from tower base to rainfall: it is required to deliver a coherent, buoyant column to the LCL under realistic wind and shear conditions, at which point atmospheric conditional instability completes the process. The platform functions as a mechanical convective inhibition (CIN) breaker. CIN is the energy barrier that suppresses convective initiation in a potentially unstable atmosphere; the vortex system overcomes it by delivering organised lift to the critical altitude. This is precisely the function performed naturally by orographic lifting, sea-breeze convergence, and frontal boundaries — the platform replicates this function in a controllable, mobile form.

2.4 Energy Balance Estimate

A preliminary energy balance illustrates the order of magnitude of water yield from a maritime deployment. Consider a 1 km² collector operating at 1 kW/m² peak insolation for 10 hours, capturing 10 percent of incident solar energy as useful thermal uplift:

$$\text{Energy available} = 1 \text{ km}^2 \times 1 \text{ kW/m}^2 \times 10 \text{ h} \times 10\% = 3,600 \text{ MJ}$$

Since each kilogram of water condensed requires approximately 2.5 MJ of latent heat, and each millimetre of rainfall over 1 km² corresponds to 10⁶ litres = 10⁶ kg of water:

$$\text{Water yield} \approx 3,600 \text{ MJ} / 2.5 \text{ MJ/kg} = 1,440,000 \text{ kg} \approx 1.4 \text{ mm over } 1 \text{ km}^2$$

This is an upper-bound estimate assuming all captured solar energy goes to latent heat conversion, which overestimates yield — a fraction of energy goes to sensible heating of the column and mechanical work. A more conservative capture efficiency of 5 percent gives approximately 0.7 mm per day. At higher humidity (which reduces latent heat required per unit condensation) and with latent heat feedback included, yields at the upper end of this range are plausible for optimised maritime deployment.

For context, a 50 km² platform array — a large but not implausible offshore installation — would yield 35 to 70 million litres per day at these efficiencies. This is comparable to a mid-sized desalination plant, achieved without the energy penalty of reverse osmosis and with a fundamentally different cost structure.

3. Spectral Splitting Architecture

3.1 The Power-Thermal Trade-off

A maritime platform operating a solar vortex array faces an immediate energy budget problem. The convective column requires high-grade thermal forcing — sustained sensible heating of the air column over the collector area. The platform simultaneously requires electrical power for navigation, positioning, sensor arrays, communications, and the computational load of running atmospheric model inference. A conventional solar thermal approach provides heat but forces a separate photovoltaic installation for electrical power, consuming additional collector area on a platform where footprint is constrained. A conventional photovoltaic approach provides electricity but wastes the thermal opportunity.

Spectral splitting resolves this trade-off by routing different wavelength bands of incident solar radiation to the conversion technology optimised for each band, allowing simultaneous high-efficiency thermal and electrical output from the same collector area.

3.2 Spectral Decomposition

The solar spectrum at sea level distributes approximately as follows:

Ultraviolet (280–400 nm): approximately 5–6 percent of total irradiance

Visible (400–700 nm): approximately 43 percent

Near-infrared (700–1,100 nm): approximately 37 percent

Far-infrared (>1,100 nm): approximately 14 percent

Dichroic mirrors or holographic optical elements can separate these bands with high efficiency before the radiation strikes any absorber. The separated bands are then directed to purpose-optimised receivers.

3.3 Infrared Thermal Pathway

The near-infrared and far-infrared fractions — approximately 51 percent of incident irradiance, or roughly 510 W/m² at peak insolation — are directed to a thermal absorber that heats the air column directly. This thermal forcing drives the convective updraft. Concentrating the IR fraction rather than the full spectrum provides a spectrally cleaner thermal input, which is relevant for condensation surface materials that may degrade faster under visible and UV radiation.

At 1 kW/m² total insolation and 510 W/m² dedicated to thermal forcing, a 1 km² collector delivers approximately 510 MW of thermal input to the column — a substantial forcing that significantly exceeds the energy scales available to conventional cloud seeding operations, which rely on aerosol-mediated microphysical effects rather than direct thermal forcing.

3.4 Visible Photovoltaic Pathway

The visible fraction — approximately 430 W/m² — is directed to high-efficiency multi-junction photovoltaic cells optimised for the visible spectrum. Multi-junction cells achieve efficiencies of 35 to 40 percent on the visible band, compared to 20 to 22 percent for conventional single-junction cells operating on the full spectrum. At 37 percent efficiency on 430 W/m² visible input, electrical output is approximately 160 W/m².

For a 1 km² platform collector, this yields approximately 160 MW of electrical generation — sufficient for all platform operational loads with substantial margin for export via subsea cable or storage as hydrogen or ammonia for transport to shore. The photovoltaic pathway thus transforms the platform from an energy consumer into a potential energy producer, fundamentally altering the economics.

3.5 Ultraviolet Antifouling Pathway

The ultraviolet fraction — approximately 55 W/m² at peak insolation — is concentrated and directed to two applications with direct operational relevance. First, UV irradiation of submerged and splash-zone platform surfaces inhibits biological fouling — the accumulation of algae, barnacles, and biofilm that degrades structural and optical surfaces in marine environments. Antifouling is a persistent maintenance cost for offshore platforms; UV-based antifouling eliminates the need for biocidal coatings and their associated toxicology concerns. Second, concentrated UV provides sterilisation capacity for potable water production from atmospheric condensate collected by the platform, supporting crew operations without chemical treatment.

This application of the UV fraction is notable because it converts what would otherwise be wasted radiation into a direct operational benefit, reducing platform maintenance costs and chemical logistics.

3.6 Far-Infrared Thermoelectric Pathway

The far-infrared fraction may in principle be converted to additional electricity via thermoelectric generators if the temperature differential across the generator is sufficient. Current thermoelectric materials achieve dimensionless figures of merit (ZT) of approximately 2 to 3, limiting conversion efficiency to around 10 to 15 percent at moderate temperature differentials. The thermoelectric pathway is identified as a potential future enhancement but is not relied upon in the core energy balance presented here, as its contribution at current materials performance is modest and its manufacturability at scale remains an open question.

3.7 Maritime Optical Alignment Challenges

The principal engineering challenge for maritime spectral splitting is maintaining optical alignment under sea-state conditions. Dichroic mirror arrays or holographic splitters require precise angular alignment to maintain spectral separation. Platform motion in waves introduces dynamic misalignment that conventional land-based concentrating solar systems do not face. Gimballed mounting systems and active alignment correction — analogous to those used in naval optical systems — are technically feasible but add mass and complexity. This is identified as a primary engineering design challenge for the prototype phase, alongside salt spray deposition on optical surfaces and thermal cycling of coatings in the marine environment.

4. Positioning Intelligence: Differentiable Weather Models

4.1 The Actuator Precision Problem in Weather Modification

Prior proposals for gradient-based weather modification have identified the conceptual possibility of inverting differentiable atmospheric models to find minimal initial perturbations that shift a forecast outcome — steering a storm track, modifying precipitation patterns — by running the model gradient backward from a desired future state to required initial conditions. The mathematical operation is physically grounded: adjoint-based sensitivity analysis has been used in operational meteorology for decades to identify where targeted observations most improve forecast accuracy.

The limitation of this approach as a practical weather modification strategy is actuator precision. The perturbations identified by gradient inversion are typically small relative to atmospheric variability, and must be delivered with spatial and temporal precision that existing actuators — surface albedo modification, aerosol injection — cannot achieve. The signal delivered to the atmosphere is comparable to or smaller than natural variability, making reliable attribution and outcome prediction extremely difficult. This is not merely a technical limitation; it is a consequence of operating in the noise.

A maritime solar vortex platform is a fundamentally different class of actuator. It delivers a concentrated, localised thermal forcing — potentially hundreds of megawatts over a defined area — that is large relative to the natural variability of the boundary layer over that location. It is not

a small perturbation to a chaotic system. It is a significant, organised, controllable energy input at a chosen location and time. This changes the character of the optimisation problem.

4.2 Gradient-Based Platform Positioning

Rather than asking 'what atmospheric perturbation produces the desired outcome,' the positioning problem asks a more tractable question: 'given a target precipitation outcome over a specified inland area, what platform deployment location, timing, and forcing intensity maximise the probability of that outcome?'

A trained neural weather model — GraphCast (Lam et al., 2023) or a regional mesoscale surrogate trained on coastal convection data — can be differentiated with respect to the location and timing of a surface thermal forcing anomaly of the magnitude the platform produces. The gradient of the target precipitation metric with respect to platform deployment parameters provides a direction of improvement in the positioning space. Standard gradient-based optimisation over this low-dimensional space — latitude, longitude, deployment time, forcing duration — identifies the optimal deployment scenario.

This is substantially more tractable than full atmospheric state inversion for several reasons. First, the parameter space is small: four to six variables rather than a high-dimensional initial condition field. Second, the forcing is large relative to background variability, so the gradient is operating well above the noise floor. Third, the causal pathway is short and physically interpretable: local maritime convection → moisture-laden air mass advection under prevailing winds → orographic or convergence-driven uplift → inland precipitation. Fourth, the surrogate model can be validated iteratively against real deployments, improving positioning accuracy with operational experience.

4.3 Surrogate Model Fidelity Considerations

A critical caveat applies to surrogate-guided positioning. Neural weather models such as GraphCast are trained on reanalysis data at synoptic to mesoscale resolution. They capture large-scale atmospheric dynamics with high fidelity. The causal pathway from a local maritime thermal forcing to inland precipitation, however, runs through mesoscale to microscale processes — boundary layer convection, sea breeze dynamics, moisture advection — that may be at or below the model's effective resolution.

The gradient computed through the surrogate with respect to a localised surface forcing therefore represents the sensitivity of the surrogate's predictions to that forcing, not necessarily the sensitivity of the real atmosphere. Systematic bias between the two is the primary source of positioning error. A regional mesoscale surrogate — trained specifically on the coastal convection regime of the deployment area at 1 to 3 km resolution — would substantially reduce this bias relative to a global model.

The validation pathway described in Section 6 is designed specifically to characterise and reduce this bias iteratively, by comparing predicted and observed precipitation outcomes across a series of controlled deployments.

4.4 The Chaos Horizon

Weather prediction degrades rapidly beyond approximately 10 days due to the chaotic nature of atmospheric dynamics, with errors approximately doubling every two days at synoptic scales. Gradient-based positioning is therefore most reliable at short lead times — 24 to 72 hours — where the surrogate's predictive fidelity is highest and the positioning gradient is most meaningful.

This constraint is operationally manageable: a mobile platform can be repositioned within 24 to 72 hours in response to updated model guidance. The system does not require accurate positioning decisions weeks in advance; it requires good short-range positioning decisions, updated as model initialisation improves with incoming observational data. This is analogous to the operational practice of adaptive observation — deploying instruments to locations that will most improve the next forecast cycle — but applied to a precipitation-forcing platform rather than a measurement system.

5. Platform Design and Engineering Challenges

5.1 Platform Concept

The proposed platform is a semi-submersible or ship-borne structure capable of ocean transit and station-keeping in sea states up to approximately Sea State 4 (significant wave height 1.5 to 2.5 metres). The platform carries the solar collector array — spectral splitting optics, IR thermal absorbers, visible PV panels, UV concentrators — along with the primary vortex tower and any staged upper generators. Navigation, positioning, power management, and atmospheric model inference systems are integrated.

Platform scale is determined by the required thermal forcing to achieve convective column coherence under local atmospheric conditions. Order-of-magnitude estimates suggest a collector area of 0.1 to 1 km² is required for meaningful forcing; the lower end is achievable with a large ship-borne installation, the upper end requires a purpose-built semi-submersible platform or an array of coordinated vessels.

5.2 Sea State and Column Coherence

The convective column generated by the platform is a free buoyant plume in the open atmosphere above the collector. Its coherence depends on the ratio of buoyancy forcing to ambient wind shear. Strong solar insolation and high relative humidity — the conditions that maximise precipitation potential — tend to be associated with low-wind, high-pressure regimes

in subtropical maritime environments. This is operationally favourable: the conditions best suited to convective column coherence align with the meteorological conditions most likely to produce precipitation given sufficient lift.

Wind shear disruption of the convective column remains the primary atmospheric engineering challenge. Column coherence can be partially maintained by increasing tower exit velocity — a stronger initial updraft is more resistant to shear tilting — and by selecting deployment windows when forecast wind shear is below a threshold determined by platform-specific column parameters.

5.3 Optical Surface Maintenance

Salt spray deposition on optical surfaces is a chronic problem for maritime solar installations. Salt crystals scatter incident radiation and reduce spectral separation efficiency of dichroic elements. Automated washing systems using condensate collected from the vortex column — a closed-loop water reuse that reduces fresh water logistics — are proposed for routine maintenance. Anti-soiling hydrophilic coatings on glass mirror surfaces, analogous to those used in concentrated solar power plants in dusty environments, should be specified for all optical elements exposed to the marine boundary layer.

Thermal cycling of coatings and structural elements in the marine environment — driven by diurnal solar heating and overnight cooling, compounded by salt-mediated corrosion — requires materials selection appropriate to offshore oil and gas industry standards, which provide an established engineering baseline.

5.4 Power and Propulsion

The photovoltaic pathway generates approximately 160 MW/km² of collector area at peak insolation. Platform propulsion, hotel load, sensor systems, and computing draw an estimated 5 to 15 MW for a large semi-submersible. Surplus electrical generation can be stored as compressed hydrogen via electrolysis for propulsion fuel, eliminating diesel dependence and allowing indefinite range on renewable energy. Nighttime and overcast operation — during which the solar collection system is unavailable — requires either stored energy or conventional backup generation; a hybrid diesel-hydrogen system provides operational flexibility during early deployment phases.

6. Experimental Validation Pathway

Staged validation is essential given the number of unverified physical assumptions in the proposed system. The following four-stage programme is designed to test each major assumption in order of increasing cost and complexity, with each stage providing decision-relevant data for the next.

Stage 1: Laboratory Vortex Chamber

A controlled indoor chamber — 10 to 50 metres in height, with electrically heated base plate, humidity control, and laser Doppler velocimetry — validates the basic vortex dynamics and tests the staged energy injection concept at small scale. Key measurements: updraft velocity profile, entrainment rate as a function of column radius, condensation height as a function of inlet humidity and base temperature, and the contribution of latent heat release to column buoyancy. This stage can be completed within 12 to 18 months at laboratory cost.

Stage 2: Coastal Prototype

A small coastal or estuarine installation — collector area of order 100 to 1,000 m², tower height 20 to 50 metres — tests the spectral splitting system, optical alignment under maritime conditions, and salt spray deposition rates under real environmental conditions. The marine atmosphere provides realistic testing conditions for optical surface maintenance protocols. Precipitation enhancement is not expected at this scale; the objective is platform systems validation.

Stage 3: Controlled Maritime Deployment

A larger maritime deployment — collector area 0.1 to 1 km², full vertical stacking array — tests convective column coherence under realistic wind and shear conditions, validates the energy balance estimates, and generates the dataset required to calibrate the regional atmospheric surrogate model. Precipitation outcomes are measured by downstream rain gauge networks and weather radar. Multiple deployments at varying locations, times, and forcing intensities provide the input-output data for surrogate calibration.

Stage 4: Surrogate-Guided Operational Deployment

With a calibrated surrogate model and validated platform system, operational deployments target specific precipitation events over a defined inland area. Platform positioning follows model gradient guidance, updated at 24-hour intervals. Precipitation attribution — separating platform-induced rainfall from natural variability — uses the ensemble forecast framework established during Stage 3 calibration. This stage constitutes a proof of concept for the full integrated system.

7. Economic Analysis

7.1 Cost Comparison with Desalination

Reverse osmosis desalination currently achieves levelised costs of approximately \$0.50 to \$1.20 per cubic metre of produced water, with large plants at the lower end of this range. The proposed system's economic comparison is not straightforward because it produces precipitation over a

catchment area rather than piped water at a defined delivery point; nonetheless, an order-of-magnitude comparison is instructive.

At a water yield of 1 mm per day over a 1 km² platform collector — corresponding to 1,000 cubic metres per day — and assuming capital costs analogous to a combination of offshore wind platform and concentrating solar thermal installation, a rough levelised cost of water lies in the range of \$1.00 to \$3.00 per cubic metre under optimistic assumptions. This is above the lower end of desalination costs but below emergency water supply costs in severely water-stressed regions.

Two factors improve the economics substantially. First, the photovoltaic generation pathway produces electrical revenue estimated at approximately \$10 to \$25 million per year per km² of collector at current wholesale electricity prices, which substantially offsets platform operating costs. Second, precipitation delivered to a catchment recharges groundwater, reduces irrigation costs, and may enable agricultural activities in previously marginal land — benefits that are not captured in a direct cost-per-cubic-metre comparison.

7.2 Revenue Diversification

Beyond water and electricity, the platform generates value across several streams. UV-based antifouling reduces hull maintenance costs. Atmospheric water condensate collected by the platform provides crew potable water without shore-based logistics. Carbon credit revenues from avoided fossil-fuel-based water supply may materialise as voluntary carbon markets develop. In the longer term, if precipitation enhancement contracts are structured similarly to weather insurance — with payments tied to measured outcomes — the platform becomes a financial instrument as well as a physical one.

7.3 Economic Uncertainties

The analysis above carries substantial uncertainty. Capital costs for a novel maritime platform without precedent are difficult to estimate reliably. Water yield projections depend on atmospheric conditions that vary significantly by site and season. The photovoltaic revenue projection assumes continued decline in balance-of-system costs and stable grid connection infrastructure. These uncertainties argue for a staged investment approach — validating physical performance at each stage before committing to full-scale platform construction — rather than large upfront capital deployment.

8. Governance Considerations

8.1 Maritime Jurisdiction

A mobile platform operating in international waters or exclusive economic zones engages a complex legal framework. UNCLOS (United Nations Convention on the Law of the Sea)

governs platform operations beyond territorial waters. Activities constituting 'installations and structures' in the EEZ require coastal state notification and, in some interpretations, consent. Precipitation generated by the platform that falls on coastal state territory raises questions of transboundary resource attribution — questions for which no established legal framework exists.

Operating within coastal state territorial waters (12 nautical miles) or EEZ (200 nautical miles) under a bilateral agreement with the state hosting the target precipitation area is the most legally straightforward deployment model for initial operations. This also facilitates coordination with national meteorological services and ground-based monitoring networks.

8.2 Atmospheric Commons

More fundamentally, the atmosphere is a shared resource. Precipitation enhancement in one location could in principle alter moisture availability for downwind regions, though for a maritime platform inducing precipitation from oceanic moisture — moisture that would not otherwise have precipitated over land — the net effect on the continental water budget is additive rather than redistributive. Establishing this distinction empirically, through the surrogate modelling and attribution framework described in Section 4, is an important governance prerequisite.

The governance literature on transboundary weather modification is limited but growing, driven by the increasing commercial deployment of cloud seeding. The 1977 ENMOD Convention prohibits weather modification for hostile purposes; the 1978 WMO statement on weather modification establishes notification principles; but no binding international framework governs commercial precipitation enhancement over the open ocean. This governance gap will need to be addressed as the technology matures, and early engagement with the WMO and relevant treaty bodies is recommended.

8.3 Equity Considerations

Access to the proposed technology will initially be constrained to actors with significant capital and technical capacity — likely national governments or large private entities. If the technology proves effective, equitable access for water-stressed developing nations will require deliberate policy intervention: technology transfer agreements, multilateral financing mechanisms, or open licensing of key system components. The water equity literature consistently identifies governance structures rather than technology as the primary barrier to equitable water access; this system is no exception.

9. Conclusions and Future Work

This paper has proposed a mobile maritime solar vortex platform for targeted precipitation enhancement, integrating three component systems — vertical stacking for convective column

intensification, spectral splitting for thermal and electrical co-generation, and differentiable weather model positioning — that collectively address limitations that have constrained prior weather modification approaches.

The central physical argument is that maritime deployment resolves the moisture availability problem that makes terrestrial solar chimney proposals for precipitation enhancement physically untenable. Over the open ocean, the lifting condensation level lies within reach of a practical tower structure. The vertical stacking concept then addresses column coherence and delivers the column to the LCL, at which point latent heat feedback from condensation makes the column partially self-sustaining. The system functions as a mechanical CIN-breaker, exploiting atmospheric conditional instability rather than fighting it.

Spectral splitting allows simultaneous optimisation of thermal forcing and electrical generation from the same collector footprint, resolving the power-thermal trade-off inherent in single-mode solar collection and potentially transforming the platform into a net electricity exporter. The ultraviolet pathway addresses platform antifouling — a direct operational benefit that converts wasted radiation into maintenance cost reduction.

Gradient-based positioning via differentiable atmospheric surrogates transforms the platform from a fixed weather modification installation into a responsive, optimisable system. The platform is the precision actuator that prior gradient-based weather modification proposals lacked; the surrogate model provides the positioning intelligence that a platform alone cannot supply.

Key claims in this paper that have been subjected to first-principles stress-testing and survive with appropriate caveats are: the LCL analysis for maritime conditions; the staged buoyancy injection concept with explicit acknowledgment of the column coherence challenge; the qualitative entrainment argument for maintaining column radius; and the latent heat feedback threshold effect. Claims that have been identified as requiring experimental validation before being treated as established include: the 30 to 50 percent latent heat buoyancy contribution figure; the specific geometry of optimal stage spacing; and the surrogate model positioning accuracy for the relevant coastal convection regime.

Priorities for future work, in order of urgency, are: laboratory validation of staged vortex dynamics and latent heat feedback; coastal prototype testing of the spectral splitting system under maritime conditions; development and validation of a regional atmospheric surrogate trained on coastal convection data; and design of the attribution framework required to separate platform-induced from natural precipitation in operational deployments.

The system described here does not claim to solve freshwater scarcity. It proposes a physically grounded, experimentally testable mechanism by which solar energy captured over the ocean can be converted to precipitation delivered to coastal arid regions, with a positioning intelligence layer that makes the delivery controllable rather than opportunistic. Whether it closes

economically and scales to policy-relevant impact depends on the experimental validation programme described here and on governance frameworks that do not yet exist. Both are tractable problems. The physics, as developed in this paper, appears to close.

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