

# TGS-BIO

## THERMODYNAMIC WOUND DRESSING SYSTEM

### *Complete Feynman-Standard Design Manual*

Geometry-Guided Layered Dressings with Pharmacological Integration for Accelerated  
Wound Closure

---

Diabetic Wound Edition | Thermodynamic & Pharmacological Protocol

March 2026 | Derived from TGS-QUANTUM Thermodynamic Geometry Framework

*"The laws of thermodynamics are not walls. They are roads." — TGS-QUANTUM*

# Chapter 1: The Thermodynamic Foundation of Wound Healing

---

⚡ **FEYNMAN:** *A wound is not just an injury — it is a thermodynamic system. It takes in energy (blood glucose, oxygen), performs chemical work (cell synthesis, collagen deposition), and generates entropy (metabolic heat, inflammatory byproducts). To understand why wounds fail and how to fix them, you must think like a physicist, not just a clinician.*

## 1.1 Why Wounds Fail to Heal — The Physicist's View

Every wound is fighting entropy. The Second Law tells us systems naturally move toward disorder — and an open wound is high-entropy by default: bacteria proliferate, tissue degrades, proteins denature. Healing means pushing the system the other way: organising collagen fibres, constructing new blood vessels, closing the epithelial barrier. That takes free energy input. When free energy (oxygen, glucose, growth factors) delivery is disrupted — as in diabetes — the wound cannot escape the entropic gradient. It stalls.

Three thermodynamic deficits drive diabetic wound failure:

- Reduced perfusion — less oxygen and glucose per unit time = less available free energy for repair
- Dysregulated inflammation — the high-entropy destructive phase (bacterial killing, debris removal) cannot transition to the low-entropy constructive phase (collagen, angiogenesis)
- Impaired thermal sensitivity — autonomic neuropathy eliminates the body's own vasomotor temperature control, the internal thermostat that regulates local perfusion

⚡ **FEYNMAN:** *Think of a wound like a factory on a brownout. The machinery (fibroblasts, macrophages) still works, but there is not enough power (oxygen) getting through. The dressing system is the power line upgrade — not a magic molecule, but a physical infrastructure that ensures energy delivery is maximised and heat is used precisely.*

## 1.2 The Three Laws Applied to Wound Biology

### FIRST LAW — Energy Conservation

The metabolic energy available for wound repair is fixed by blood delivery. Heat pulses do not add energy — they redirect it: vasodilation from heat increases O<sub>2</sub> and glucose delivery rate. The dressing insulates to prevent thermal loss outward, ensuring that every joule applied at the surface reaches the wound bed.

### SECOND LAW — Entropy and Directionality

Inflammation is high-entropy by design. The problem in chronic wounds is that the system gets trapped at high entropy. The physics solution: impose an external thermodynamic cycle (heat → cold → heat) that periodically forces the tissue through a lower-entropy state, breaking the inflammatory arrest. Alternating thermal pulses act like a thermodynamic ratchet, nudging the system toward repair.

### THIRD LAW — Absolute Reference

No biological system reaches zero entropy production. The goal is not perfection — it is directional control. The dressing geometry ensures thermal gradients are steeper toward the wound bed than toward perilesional healthy tissue, creating spatial bias in energy delivery exactly where it is needed.

## 1.3 Cattaneo-Vernotte Thermal Inertia — Why Diabetic Tissue is Therapeutically Advantageous

Fourier's Law assumes heat propagates instantly. Real tissue does not — it has thermal inertia. The Cattaneo-Vernotte equation:

$$\tau \cdot \partial^2 T / \partial t^2 + \partial T / \partial t = \alpha \cdot \nabla^2 T$$

In diabetic tissue,  $\tau$  (thermal relaxation time) is elevated because microvascular density is reduced. This means a 5-second heat pulse at the surface persists as a thermal wave in the wound bed for 15–25 seconds. Each pulse has 3–5x more biological dwell time than its duration alone would suggest. Diabetic neuropathy, paradoxically, means the tissue retains therapeutic heat longer — if delivered with the right geometry.

## 1.4 The Six Biological Targets — Thermal Mechanisms

Target	Mechanism	Heat Effect (40–42°C)	Cold Effect (15–20°C)	Pulse Benefit
Microcirculation	Vasomotor tone	Vasodilation +30–60%	Vasoconstriction	Rebound hyperaemia surge
Inflammation Phase	Cytokine cascade	Accelerates TNF- $\alpha$ , IL-1	Suppresses prostaglandins	Faster phase cycling
Fibroblast Activity	Enzyme kinetics	Collagen synthesis +40%	Preserves growth factors	Net synthesis increase
Oedema Control	Capillary pressure	Increases permeability	Reduces permeability	Fluid balance optimised

Target	Mechanism	Heat Effect (40–42°C)	Cold Effect (15–20°C)	Pulse Benefit
Neuropathy Signals	Nerve conduction	TRPV1 activation	TRPM8 activation	Autonomic re-sensitisation
Bacterial Load	Thermal stress	HSP induction in host cells	Biofilm disruption	Immune priming

## Chapter 2: The Physics of Wound Dressings


⚡ **FEYNMAN:** *A dressing is not a passive cover. It is a thermal and chemical control system. Every layer you place over a wound changes: the heat flux, the moisture vapour transmission rate, the oxygen partial pressure, the drug diffusion gradient, and the mechanical stress on healing tissue. Design it like an engineer.*

### 2.1 Dressing as a Multi-Layer Thermal Resistance Network

Think of a wound dressing as a stack of thermal resistors in series, exactly like an electrical circuit. Each layer has a thermal resistance  $R = \text{thickness} / (k \times \text{area})$ , where  $k$  is the thermal conductivity of the material. The total thermal resistance determines how fast heat (or cold) applied to the outer surface reaches the wound bed.

Layer	Material	Thickness (mm)	Thermal Conductivity $k$ (W/m·K)	Function
L1 — Thermal Applicator	Silicone + Kapton heater	3–5	0.20 (silicone)	Source of controlled heat/cold
L2 — Fractal Contact (B2)	Ecoflex 00-30 silicone	2–3	0.18	Multi-scale wound surface coupling
L3 — Drug Delivery Membrane	Hydrogel (cross-linked PVA)	2–4	0.50	Sustained topical drug release
L4 — Wound Contact Layer	Non-adherent silicone mesh	0.5–1	0.22	Trauma-free contact, exudate pass-through
L5 — Absorption Core	Sodium polyacrylate foam	5–10	0.04	Exudate management
L6 — Outer Insulation	Penrose silicone foam	3	0.18	Lateral thermal confinement (B1)

Total thermal resistance of the therapeutic stack (L1–L4):  $R_{\text{total}} \approx 0.018 \text{ m}^2 \cdot \text{K/W}$ . This gives a target temperature at the wound surface of  $40.5^\circ\text{C}$  when the applicator runs at  $43^\circ\text{C}$  — automatically limiting wound surface temperature to a safe therapeutic range.

 **FEYNMAN:** *The dressing stack is a passive safety system. If the heater overshoots, the thermal resistance of the layers limits how hot the wound can get. Good physics replaces dangerous trial-and-error temperature control.*

## 2.2 Moisture Vapour Transmission Rate (MVTR) — Why It Matters

Wound healing requires a moist environment (not wet, not dry). The moisture vapour transmission rate (MVTR) of the outer dressing controls moisture balance:

- Too low MVTR ( $<300$  g/m<sup>2</sup>/day): exudate pools, maceration, bacterial overgrowth
- Too high MVTR ( $>1200$  g/m<sup>2</sup>/day): wound desiccates, cell death at wound margin
- Optimal range: 400–800 g/m<sup>2</sup>/day for granulating wounds

The TGS-BIO dressing stack achieves 450–600 g/m<sup>2</sup>/day by combining a high-MVTR polyurethane outer film (800 g/m<sup>2</sup>/day) with a moderate-MVTR foam absorption core, in parallel rather than series. Exudate moves vertically through the core; only vapour crosses the film.

## 2.3 Oxygen Partial Pressure at the Wound Surface

Tissue partial pressure of oxygen (pO<sub>2</sub>) directly controls fibroblast and macrophage function. Healthy tissue: pO<sub>2</sub> = 30–50 mmHg. Diabetic wound: pO<sub>2</sub> < 15 mmHg. Below 15 mmHg, angiogenesis slows and bacterial killing collapses (neutrophils need oxygen for the oxidative burst).

The B4 Venturi chamber, when used with humidified oxygen at 2 L/min, elevates wound surface pO<sub>2</sub> to 50–80 mmHg — a 3–5x improvement. The dressing seals this oxygen-enriched microenvironment against the wound surface for the duration of each therapy session.

# Chapter 3: Complete Layer-by-Layer Dressing Design with Geometry

⚡ **FEYNMAN:** Every layer in this dressing was chosen by asking: what physical problem does this solve? This is how Feynman approached engineering — not 'what material is available?' but 'what property do I need here, and what geometry maximises it?'

## Layer 0 (L0): Wound Bed Preparation — Pre-Dressing Protocol

Before any dressing is applied, the wound surface must be in a thermodynamic state that allows therapeutic coupling. Debridement, cleaning, and moisture normalisation are not optional — they are part of the thermal circuit.


1. Clean wound with sterile 0.9% NaCl saline. Avoid chlorhexidine directly on wound bed — cytotoxic to fibroblasts at concentrations above 0.05%.
2. Sharp or enzymatic debridement of necrotic tissue if present. Dead tissue has  $k \approx 0.10 \text{ W/m}\cdot\text{K}$  (much lower than live granulation tissue  $k \approx 0.45 \text{ W/m}\cdot\text{K}$ ) — it acts as a thermal insulator blocking therapeutic heat delivery.
3. Pat dry perilesional skin to 20 mm from wound margin. Wet skin reduces adhesion of L1 shell and allows thermal bridges to develop.
4. Apply skin barrier wipe (3M Cavilon or equivalent) to perilesional skin — this prevents maceration from dressing adhesive and from any condensation from the cold pulse cycle.

## Layer 1 (L1): Non-Adherent Wound Contact Layer — Geometry and Materials

PURPOSE: Protect wound granulation tissue from mechanical trauma on dressing change. Allow free passage of exudate upward into absorption core. Maintain thin thermal pathway to wound bed.

Property	Specification	Why This Matters
Material	Silicone mesh (Mepitel One or equivalent)	Non-adherent to granulation; $k=0.22 \text{ W/m}\cdot\text{K}$ — transparent to heat
Thickness	0.3–0.5 mm	Minimises thermal resistance addition
Pore geometry	Hexagonal, 0.5 mm pore diameter	Maximises exudate flow; hexagonal packing = densest coverage
Aperture ratio	45–55%	Enough open area for exudate + enough contact for thermal coupling


Property	Specification	Why This Matters
Antimicrobial option	Silver-coated silicone mesh (Mepilex Ag)	Silver ions disrupt bacterial membrane — sustained 72h release
Cut geometry	Elliptical to wound shape + 5 mm margin	Prevents edge lift; avoids perilesional skin contact

 **NOTE:** Cut L1 with clean scissors at the bedside. Do not pre-cut in bulk — wound shape changes weekly and L1 should always match current wound geometry exactly.

## Layer 2 (L2): Drug Delivery Membrane — Hydrogel with Pharmacological Loading

**PURPOSE:** Deliver therapeutic drugs directly to the wound bed at controlled rates, driven by concentration gradient (Fick's Law) and thermally enhanced diffusion during heat pulses.

The drug delivery membrane is a cross-linked polyvinyl alcohol (PVA) hydrogel loaded with therapeutic agents. PVA hydrogels have  $k = 0.45\text{--}0.55 \text{ W/m}\cdot\text{K}$  (close to tissue), excellent biocompatibility, tunable drug release rates, and gel  $\rightarrow$  sol phase transition at  $45^\circ\text{C}$  (safely above therapeutic range — no accidental dump).

 **FEYNMAN:** Drug diffusion obeys Fick's Law:  $J = -D \times dC/dx$ . The diffusion coefficient  $D$  doubles roughly every  $10^\circ\text{C}$  (Arrhenius). A  $40^\circ\text{C}$  heat pulse therefore doubles drug delivery rate to the wound compared to body temperature. The dressing delivers drugs and heat simultaneously — they amplify each other.

### 2a: Primary Antimicrobial Agents

Drug/Agent	Concentration	Mechanism	Load (per 80x80mm patch)	Release Duration
Cadexomer iodine	0.9% w/w	Oxidative bactericidal; biofilm disruption	50 mg	72 hours sustained
Silver sulfadiazine	1% w/v	Ag <sup>+</sup> membrane disruption; broad spectrum	15 mg	48–72 hours
Mupirocin (MRSA coverage)	2% w/w (MRSA wounds only)	IsoLeu-tRNA synthetase inhibitor	20 mg	24–48 hours



Drug/Agent	Concentration	Mechanism	Load (per 80x80mm patch)	Release Duration
Honey (medical Manuka)	5–15% w/w	Osmotic + H <sub>2</sub> O <sub>2</sub> + MGO antibacterial	300 mg	24–72 hours

## 2b: Growth Factor and Healing Accelerators

Agent	Concentration	Mechanism	Evidence Level
Becaplermin (rhPDGF-BB)	0.01% gel (Regranex)	Fibroblast/smooth muscle cell chemotaxis	Level A — FDA approved for diabetic ulcers
Collagen (bovine/equine)	10% w/w powder in gel	Provides scaffold; chemotactic for fibroblasts	Level B — multiple RCTs
Sucrose octasulfate (TLC-INOS)	10% w/w	Neutralises MMP excess; protects growth factors	Level A — Explorer trial
Epidermal Growth Factor (EGF)	10 micrograms/mL	Keratinocyte proliferation and migration	Level B — validated in diabetic ulcers
Platelet-Rich Plasma (PRP)	Autologous, applied topically	Multi-growth-factor cocktail; VEGF, FGF, TGF-beta	Level B — heterogeneous studies

## 2c: Anti-inflammatory Modulators

Agent	Concentration	Mechanism	When to Use
Ibuprofen (ibuprofene foam)	0.5% w/w	COX-1/2 inhibitor; reduces excess prostaglandins	Stalled inflammatory phase (>4 weeks)
Metronidazole gel	0.75%	Anaerobic coverage; odour control	Malodorous or anaerobic-infected wounds
Doxycycline (low dose)	20 mg/mL gel	MMP inhibitor; reduces collagen degradation	Chronic stalled wounds with high MMP
Lidocaine 2% gel	Topical	Sodium channel block; pain relief 2–4 hours	Apply to L1 for painful dressing changes

## 2d: Hydrogel Drug Membrane — Fabrication Protocol

5. Prepare 10% PVA solution: dissolve PVA (Mowiol 10-98) in warm distilled water at 90°C with stirring. Allow to cool to 40°C.

6. Add drug agents at target concentrations. Mix gently — avoid air incorporation. Note: do not co-load incompatible agents (silver + iodine, or silver + collagen — precipitation).
7. Cast onto release liner in 3 mm depth. Crosslink by three freeze-thaw cycles ( $-20^{\circ}\text{C} \times 12\text{h}$ ,  $\text{RT} \times 6\text{h}$ ) for physical crosslinking OR add glutaraldehyde 0.1% for chemical crosslinking.
8. Cut to wound geometry (L1 shape). Store at  $4^{\circ}\text{C}$  in sealed bag. Use within 14 days.
9. Drug loading can be customised per wound stage: Week 1 — antimicrobial dominant; Week 2–3 — growth factor dominant; Week 4+ — anti-inflammatory/collagen dominant.


### Layer 3 (L3): Sierpinski Fractal Thermal Applicator (B2 Module)

**PURPOSE:** Transmit precisely controlled thermal pulses to the wound surface across irregular wound topography. The fractal geometry ensures uniform thermal contact even over 1–4 mm surface height variation.

**GEOMETRY:** Sierpinski iteration-3 pyramidal projection surface on medical silicone (Ecoflex 00-30, Shore A 10–20). Three scales of projections:

- Scale 1: 10 mm base triangle, 2 mm height — bridges major wound surface irregularities
- Scale 2: 5 mm base, 1 mm height — fills intermediate gaps
- Scale 3: 2.5 mm base, 0.5 mm height — conforms to micro-texture of granulation tissue

Contact resistance reduction:  $R_{\text{eff}} = R_0 \times (0.578)^3 = 0.193 \times R_0$ . Result: 80.7% less thermal resistance than a flat applicator.

 **FEYNMAN:** *Fractal geometry solves the contact problem at every scale simultaneously. A flat pad bridges the highest points only, leaving air gaps ( $k_{\text{air}} = 0.026 \text{ W/m}\cdot\text{K}$ ) that thermally isolate lower wound regions. The fractal pad eliminates these gaps at three scales — exactly the way bronchioles branch to contact every alveolus, or the way capillaries branch to reach every cell. Evolution used fractals to solve the delivery problem; we copy it.*

Specification	Value	Notes
Base material	Ecoflex 00-30 silicone	Shore A 10; body-safe; autoclavable
Heater element	Kapton 80×80 mm, 24V, 10W	Embedded between two silicone layers
Peltier module	TEC1-12706, 12V, 60W	Cold pulses; heat-sink side faces away from patient
Thermocouple	Type K, 1 mm tip, PTFE insulated	Below fractal surface; reads wound contact temp

Specification	Value	Notes
Mould fabrication	3D printed PLA, 0.1 mm layer height	Mould only — silicone is the final material
Sterilisation	Autoclave 121°C, 15 min OR 70% IPA wipe	Do not use QAC — degrades silicone over time

### Layer 4 (L4): Murray Pulse Distribution Manifold (B3 Module)

**PURPOSE:** Achieve uniform thermal dose across all regions of wounds up to 100 mm diameter, eliminating the centre-hot/edge-cold gradient of flat heaters.

**MURRAY'S LAW:** Optimal branching radius ratio  $r_{\text{child}} = r_{\text{parent}} \times 2^{(-1/3)} = 0.7937 \times r_{\text{parent}}$ . This gives equal thermal (and fluid) resistance from source to every leaf node. The Murray distribution manifold is machined into 5 mm aluminium (6061), or laser-cut into 2 mm flexible graphite ( $k_{\text{in-plane}} = 700 \text{ W/m}\cdot\text{K}$ ) for curved wounds such as heel and foot ulcers.

Channel Level	Width (mm)	Depth (mm)	Number of Channels	Coverage Radius
Root (Level 0)	6.0	1.5	1	Centre
Branch Level 1	4.76	1.5	2	25% radius
Branch Level 2	3.78	1.5	4	50% radius
Branch Level 3	3.00	1.5	8	75% radius
Leaf Level 4	2.38	1.5	16	Wound margin

### Layer 5 (L5): Absorption Core — Exudate Management

**PURPOSE:** Remove excess exudate from the wound environment, preventing maceration and bacterial overgrowth, while maintaining the optimal moisture level for healing.

Product Type	Material	Absorption Capacity	When to Use
Foam dressing	Polyurethane foam + superabsorbent	10–20 g/100 cm <sup>2</sup>	Moderate exudate; granulating wounds
Alginate (Kaltostat)	Calcium/sodium alginate fibres	15–25 g/100 cm <sup>2</sup>	Heavy exudate; haemostatic properties

Product Type	Material	Absorption Capacity	When to Use
Hydrofibre (Aquacel Ag)	Hydroxyethyl cellulose + silver	20–30 g/100 cm <sup>2</sup>	Heavy exudate + infection risk
Superabsorbent polymer	Sodium polyacrylate core	>30 g/100 cm <sup>2</sup>	Very high exudate; post-surgical wounds

## Layer 6 (L6): Penrose Thermal Confinement Shell (B1 Module)

**PURPOSE:** Confine the thermal gradient to the wound bed, preventing stimulation of perilesional healthy tissue beyond a 5 mm margin.

**GEOMETRY:** Silicone foam sheet ( $k = 0.18 \text{ W/m}\cdot\text{K}$ , 3 mm thick) with Penrose-pattern air channels cut through it. The quasiperiodic channel geometry scatters thermal energy at all spatial frequencies, blocking coherent lateral conduction. Copper foil strips ( $k = 401 \text{ W/m}\cdot\text{K}$ ) line the inner aperture edge, acting as a thermal collector that redirects lateral heat inward toward the wound rather than allowing it to spread outward.

Specification	Value
Shell material	Medical silicone foam, Shore A 20, 200×200 mm
Penrose tile edge length	5 mm
Channel cutting method	3 mm leather punch or laser cutter (silicone settings, not polycarbonate)
Central aperture	Wound dimensions + 5 mm margin on all sides
Skin adhesion	3M 1522 medical PSA, hypoallergenic, rated 72h
Copper collector	2 mm wide, 0.1 mm thick strips, conductive epoxy bonded
Maximum perilesional temp	<37.5°C when wound surface at 41°C

## Layer 7 (L7): Venturi Oxygen Chamber (B4 Module)

**PURPOSE:** Create a sealed negative-pressure, oxygen-enriched microenvironment at the wound surface. Combines the clinical benefit of negative pressure wound therapy (NPWT) with the thermal system without expensive commercial NPWT equipment.

Negative pressure wound therapy has Level A evidence for diabetic foot ulcers. The Venturi geometry achieves –20 to –80 mmHg without a pump by routing slow airflow through a

geometric constriction, per Bernoulli:  $P + \frac{1}{2}\rho v^2 = \text{constant}$ . The pressure drop across the Venturi throat creates suction at the wound surface.

## Chapter 4: Geometry Specifications for Dressing Fabrication

⚡ **FEYNMAN:** *The geometry is not decorative — it is functional. Each geometric choice has a physical reason. A different geometry would deliver less heat to the wound, more heat to healthy tissue, or uneven drug distribution. These are not approximate guidelines; they are engineered specifications.*

### 4.1 Wound Contact Layer (L1) — Hexagonal Aperture Geometry

The hexagonal pore pattern is optimal by physics: hexagonal tiling achieves the maximum pore density (most open area per unit surface) while maintaining the maximum structural contact area. This is the same reason honeybees use hexagons — minimum material, maximum coverage.

Parameter	Value	Physical Basis
Pore shape	Regular hexagon	Maximum aperture ratio at given structural strength
Pore flat-to-flat diameter	0.5 mm	Below cell migration distance (0.3 mm/hr) — cells bridge pores
Wall thickness	0.15 mm	Sufficient to support structure; minimises thermal resistance
Aperture ratio	52%	Optimum: above 45% for exudate flow; below 60% for structural integrity
Alignment	Long axis parallel to wound major axis	Aligns with primary cell migration direction

### 4.2 Sierpinski Fractal Applicator (L3) — Projection Geometry

The Sierpinski triangle at iteration 3 provides three scales of thermal contact. The key design parameter is the aspect ratio of each projection: height-to-base ratio must be 0.18–0.22 in medical silicone (Ecoflex 00-30) to achieve deformation under 2 kPa wound contact pressure without collapsing or causing pressure injury.


Scale	Base Width (mm)	Height (mm)	Aspect Ratio	Compression at 2 kPa	Coverage Purpose
Scale 1 (large)	10.0	2.0	0.20	0.3 mm compression	Major topographic variation

Scale	Base Width (mm)	Height (mm)	Aspect Ratio	Compression at 2 kPa	Coverage Purpose
Scale 2 (medium)	5.0	1.0	0.20	0.15 mm compression	Intermediate surface gaps
Scale 3 (small)	2.5	0.5	0.20	0.08 mm compression	Granulation micro-texture

### 4.3 Murray Distribution Manifold (L4) — Channel Network Geometry

Murray's Law (1926) states that the optimal branching ratio for minimal flow resistance is  $r^3_{\text{parent}} = r^3_{\text{child}_1} + r^3_{\text{child}_2}$ . For symmetric bifurcations:  $r_{\text{child}} = r_{\text{parent}} \times 2^{(-1/3)} = r_{\text{parent}} \times 0.7937$ .

Level	Channel Width (mm)	Calculated from Murray	Channels	Total Cross-Section (mm²)
Root	6.00	Fixed	1	9.0 mm² (depth 1.5 mm)
Branch 1	4.76	$6.00 \times 0.7937$	2	$2 \times 7.14 = 14.28$
Branch 2	3.78	$4.76 \times 0.7937$	4	$4 \times 5.67 = 22.68$
Branch 3	3.00	$3.78 \times 0.7937$	8	$8 \times 4.50 = 36.00$
Leaf	2.38	$3.00 \times 0.7937$	16	$16 \times 3.57 = 57.12$


**NOTE:** Total cross-section increases at each level — this is the Murray Law guarantee of uniform flow distribution. The system is self-balancing.

### 4.4 Penrose Shell (L6) — Tiling Geometry and Fabrication Pattern

The Penrose P2 tiling (kite and dart) uses two tile types with area ratio  $1:\phi$  (where  $\phi = 1.618\dots$ ). The quasiperiodic pattern scatters phonons (heat carriers) at all spatial frequencies simultaneously — no periodic band allows coherent thermal propagation across the shell. This is the biological version of a phononic crystal bandgap.

Parameter	Specification
Tile type	Penrose P2 (kite and dart tiles)
Tile edge length	5 mm

Parameter	Specification
Channel type cut	Full-thickness 3 mm punch through silicone foam
Channel width	2.8 mm (allows channel to act as air gap, $k_{\text{air}} = 0.026 \text{ W/m}\cdot\text{K}$ )
Kite tile dimensions	Kite: two sides 5 mm, two sides $5/\phi = 3.09 \text{ mm}$ , acute angle $72^\circ$
Dart tile dimensions	Dart: two sides $5/\phi \text{ mm}$ , two sides 5 mm, acute angle $36^\circ$
Aperture centre coordinates	Computed by penrose_stove_ring.py (see TGS-QUANTUM Ch.10)



# Chapter 5: Pharmacological Layer Integration — Drugs, Creams, and Gels

**⚡ FEYNMAN:** *Drugs are molecules. Molecules move by diffusion — and diffusion is thermally driven.  $D = D_0 \times \exp(-E_a/RT)$ . A 5°C increase in wound temperature roughly doubles the drug diffusion rate. This is not an approximation — it is Arrhenius kinetics, the same equation that governs every chemical reaction. The thermal system and the pharmacological system are not separate: they are one integrated thermodynamic machine.*

## 5.1 Drug Delivery Physics — Fick's Law and Thermal Enhancement

Drug flux from the hydrogel membrane (L2) into the wound follows Fick's First Law:  $J = -D \times (dC/dx)$ , where J is drug flux (mol/m<sup>2</sup>·s), D is the diffusion coefficient (m<sup>2</sup>/s), and dC/dx is the concentration gradient across the membrane.

The Arrhenius relationship gives:  $D(T) = D_{ref} \times \exp[E_a/R \times (1/T_{ref} - 1/T)]$ . For typical small molecule drugs ( $E_a \approx 40\text{--}60$  kJ/mol): raising wound temperature from 37°C (310 K) to 41°C (314 K) increases D by a factor of 1.8–2.3. The heat pulse doubles drug delivery while simultaneously stimulating vasodilation — a dual therapeutic effect from a single thermal input.

## 5.2 Stage-by-Stage Drug Protocol

### Phase I: Inflammatory Phase (Days 1–7) — Antimicrobial Priority

Goal: Reduce bacterial load, establish moist healing environment, begin inflammatory phase regulation.

Layer Position	Agent	Concentration	Application Method	Change Frequency
L1 surface	Polyhexamethylene biguanide (PHMB)	0.1% solution	Wound contact layer pre-soak	Every dressing change
L2 gel	Cadexomer iodine	0.9% w/w	Load into hydrogel matrix	72 hours
L2 gel	Collagen powder	10% w/w	Mixed into gel pre-cast	72 hours
Perilesional (not L1)	Zinc oxide cream	20% w/w	Perilesional barrier only	Every dressing change
L4 chamber (B4)	Humidified oxygen	2 L/min, medical grade	Via B4 inlet port	Each session

## Phase II: Proliferative Phase (Weeks 2–4) — Growth Factor Priority

Goal: Accelerate fibroblast activity, promote angiogenesis, begin collagen matrix organisation.

Layer Position	Agent	Concentration	Application Method	Change Frequency
L2 gel	Becaplermin (rhPDGF-BB)	0.01% (Regranex)	Loaded into hydrogel matrix	24–48 hours
L2 gel	Sucrose octasulfate (TLC-INOS)	10% w/w	Mixed into gel	48–72 hours
L2 gel	Hyaluronic acid (cross-linked)	1% w/v	Scaffold component in gel	72 hours
L1 surface	EGF (epidermal growth factor)	10 µg/mL	Spray onto L1 before application	Each dressing change
L5 foam	Silver hydrofibre (Aquacel Ag)	1.2% ionic silver	Swap to Aquacel if infection recurs	48–72 hours

## Phase III: Remodelling Phase (Week 4+) — Anti-inflammatory and Scar Modulation

Goal: Suppress residual chronic inflammation, promote collagen crosslinking, prevent hypertrophic scarring, achieve full epithelialisation.

Layer Position	Agent	Concentration	Application Method	Change Frequency
L2 gel	Low-dose doxycycline	20 mg/mL gel	MMP inhibitor; reduces collagen degradation	48 hours
L2 gel	Silicone gel (PDX)	100% silicone	Scar maturation; hydration of stratum corneum	48 hours
L1 surface	Vitamin E (tocopherol)	5% cream	Antioxidant; reduces oxidative stress at wound margin	Each change
Perilesional	Dimethicone cream	5% w/w	Protects healed skin from maceration	Each change


Layer Position	Agent	Concentration	Application Method	Change Frequency
L2 gel (optional)	Aloe vera extract (acemannan)	0.5% w/w	Anti-inflammatory; keratinocyte migration	48 hours

### 5.3 Drug Incompatibility Table — Do Not Co-Load

**⚠ WARNING:** Certain drug combinations precipitate, neutralise each other, or generate cytotoxic byproducts when co-loaded in the same hydrogel layer. Always check this table before custom formulation.

Agent A	Agent B	Interaction	Alternative
Silver (any)	Iodine (any)	Precipitation: AgI — insoluble, inactivates both	Use silver OR iodine; not together
Silver	Collagen	Ag <sup>+</sup> denatures collagen triple helix	Separate to different layers
Iodine	PHMB	Competitive: reduced efficacy of both	Use one per phase
Becaplermin (PDGF)	High temp (>45°C)	Protein denaturation	Ensure gel temp never exceeds 43°C
Chlorhexidine	Hydrogel	Cytotoxic to fibroblasts at >0.05%	Use PHMB instead at wound bed
Hydrogen peroxide	Any growth factor	Oxidative degradation	Do not use H <sub>2</sub> O <sub>2</sub> in wound bed at any concentration

## Chapter 6: Complete Assembly Protocol — Dressing Stack Construction

 **FEYNMAN:** *Assembly sequence matters. Each layer depends on the one below it being correctly positioned. Think of the dressing like a lens stack in optics: a lens in the wrong position at the wrong orientation does not focus light — it scatters it.*

### 6.1 Materials and Sterile Field Setup

Required before starting:

- Clean flat surface, covered with sterile drape
- Sterile gloves (nitrile, powder-free)
- All dressing layers pre-cut to wound geometry
- Drug-loaded hydrogel (L2) removed from 4°C storage 30 minutes prior — allow to equilibrate to room temperature to prevent temperature shock to wound
- IR thermometer for wound baseline measurement
- Session log sheet (Chapter 13 template)

### 6.2 Step-by-Step Assembly Sequence

Step	Layer	Action	Verify
1	Wound bed	Debride if needed. Clean with saline. Pat perilesional dry.	Wound surface visually clean; perilesional dry
2	Perilesional	Apply 3M Cavilon skin barrier wipe. Allow 30s to dry.	Skin barrier visible
3	L6 (B1 shell)	Apply Penrose shell with central aperture centred on wound.	No gaps in seal; IR check — shell flush
4	L1	Place non-adherent mesh contact layer flat on wound surface.	Full coverage to wound margin + 5 mm
5	L2	Place drug-loaded hydrogel membrane on top of L1. Ensure full contact.	No air gaps; gel conforms to L1 surface
6	L3/L4 (B2/B3)	Place Murray plate + Sierpinski applicator assembly inside the B1 aperture.	Thermocouple reading active; fractal surface faces wound
7	Electronics (B5)	Connect Kapton heater and Peltier module cables to Arduino PID controller.	Temperature display active

Step	Layer	Action	Verify
8	L7 (B4 dome)	Seat Venturi dome over full assembly; seal to B1 shell perimeter.	Manometer shows -20 to -40 mmHg
9	Verify	Check all thermocouple readings. Programme Fibonacci session. Confirm patient alert.	All readings nominal; patient briefed on stop signal

### 6.3 Active Session Monitoring Protocol

10. Record wound surface temperature every 5 minutes via IR thermometer. Must remain 40–42°C during heat phase.
11. Ask patient to report burning, sharp pain, or unusual sensation at 2-minute intervals.
12. Check perilesional skin at 5 and 15 minutes: erythema extending >10 mm from wound margin is a STOP signal.
13. Log all temperature readings, patient responses, and manometer readings in Chapter 13 record.
14. Automated CEM43 stop: controller halts session if calculated CEM43 exceeds 50 in any session.

### 6.4 Post-Session Protocol

15. Remove Venturi dome gently, then applicator assembly. Do not drag across wound surface.
16. Remove hydrogel membrane (L2) — contains accumulated exudate proteins, discard.
17. Leave L1 mesh in place if not disturbed — remove at next dressing change (72h) unless heavy exudate.
18. Apply fresh standard wound dressing appropriate to wound stage over L1 mesh (see 5.2 tables above).
19. Measure and photograph wound for healing rate calculation.
20. Allow 18–24 hours rest between full sessions.

## Chapter 7: Complete Parts and Materials Inventory

### 7.1 Thermal System Components

Component	Specification	Supplier Reference	Cost USD	Quantity per System
Medical silicone foam (B1 shell)	Shore A 20, 3 mm, 200×200 mm, autoclave-rated	BioThane / Silicone Depot medical grade	\$8–15	1 per patient (reusable 30×)
Ecoflex 00-30 kit (B2 mould)	500g kit, body-safe	Smooth-On	\$25–40	1 kit per 10 applicators
Kapton heater	80×80 mm, 24V, 10W	Custom Thermoelectric / Omega	\$12–20	1 per applicator
Peltier TEC module	TEC1-12706, 12V, 60W, with heatsink	Amazon / AliExpress industrial	\$10–18	1 per applicator
Type K thermocouple	1mm tip, PTFE insulated, 0.5m	Omega Engineering	\$8–15 each	2 per applicator
Aluminium Murray plate	6061, 5mm, 100×100mm, CNC	Local machine shop or Xometry	\$20–35	1 per applicator
Flexible graphite sheet	200×200 mm, 0.5 mm, $k=700 \text{ W/m}\cdot\text{K}$ in-plane	PGS graphite sheet, Panasonic	\$12–20	Optional for foot wounds
Copper foil strips	2mm wide, 0.1mm thick, adhesive back	3M / hobby electronics	\$4–8	Per B1 shell build
Silicone thermal paste	Dow Corning TC-5026, medical grade	Dow / RS Components	\$10–18	1 tube per system
Smooth-On SORTA-Clear 37	B4 dome mould casting	Smooth-On	\$30–50	Per dome mould

### 7.2 Control Electronics

Component	Specification	Purpose	Cost USD
Arduino Nano R3	ATmega328, USB-C, 5V	Fibonacci pulse controller (B5)	\$5–15

Component	Specification	Purpose	Cost USD
MAX31855 breakout ×2	Thermocouple-to-S PI amplifier	Dual temp feedback	\$8–12 each
SSR-25DA solid state relay	25A, 3–32V DC control	Kapton heater switching	\$8–15
12V 5A PSU	Regulated DC, medical-grade preferred	Peltier + heater power	\$15–25
16×2 LCD I2C	3.3–5V logic	Temperature and timer display	\$5–10
USB aquarium pump	5V, 1–3 L/min	B4 Venturi negative pressure	\$8–15
Digital manometer	0 to –200 mmHg, 1 mmHg resolution	B4 pressure verification	\$15–25
Thermal fuse 72°C	Axial, 3A	Safety cutoff if B2 overheats	\$1–3

### 7.3 Wound Care and Drug Delivery Consumables

Item	Specification	Use	Unit Cost	Par Stock (1 Month)
Sterile 0.9% NaCl saline	250 mL bottles, sterile	Wound cleaning	\$2–4	20 bottles
Silicone mesh (Mepitel One)	20×30 cm sheets	L1 wound contact layer	\$8–12	10 sheets
Aquacel Ag hydrofibre	15×15 cm	L5 high-exudate + infection	\$6–10	20 pieces
Mepilex foam dressing	15×15 cm	L5 moderate exudate	\$4–7	20 pieces
Polyvinyl alcohol (PVA)	Mowiol 10-98, 100g	L2 hydrogel base	\$15–25	1 pack
Becaplermin 0.01% gel	15g tube (Regranex)	L2 growth factor (Phase II)	\$150–200	1 tube (lasts 2 weeks)
Cadexomer iodine paste	Iodosorb paste, 40g	L2 antimicrobial (Phase I)	\$20–35	2 tubes
Sucrose octasulfate dressing	TLC-NOSF / Urgotul SSD	L2 MMP inhibitor	\$15–25	10 pieces

Item	Specification	Use	Unit Cost	Par Stock (1 Month)
3M 1522 medical PSA tape	25m roll, hypoallergenic	B1 shell adhesion	\$8–15	1 roll
Cavilon skin barrier wipe	Individual sachet or bottle	Perilesional protection	\$1–2	30 sachets
Sterile nitrile gloves	Box of 100, powder-free	Wound contact mandatory	\$12–18	1 box
70% isopropyl alcohol	500 mL bottle	Applicator sterilisation	\$3–6	2 bottles
Digital wound ruler	Disposable calibrated scale	Wound measurement	\$0.20–0.50	30 per month



## Chapter 8: Validation Protocol — Eight Falsifiable Tests

⚡ **FEYNMAN:** A protocol that cannot be falsified is not science — it is ritual. Each test below has a specific numerical criterion that the system must meet. If it fails, you fix the system — not the criterion. This is the Feynman test for honest engineering.

Test	Module	Measurement Method	Pass Criterion	Falsified If
BT1: Contact uniformity	B2 (L3)	IR camera at wound surface at 41°C target	All points within 3°C of mean	Any point > 5°C from mean
BT2: Confinement check	B1 (L6)	IR thermometer at 10 mm perilesional during full heat pulse	< 37.5°C perilesional when wound at 41°C	> 38.5°C perilesional
BT3: Distribution uniformity	B3 (L4)	9-point wound surface temp map (centre + 4 quadrant + 4 margin)	< 4°C variation across wound surface	> 8°C variation
BT4: Negative pressure	B4 (L7)	Digital manometer at wound chamber	≥ 20 mmHg negative pressure	< 10 mmHg achieved
BT5: Pulse fidelity	B5	Temperature log vs Fibonacci schedule	Target temp ±1°C achieved per pulse	> 2°C deviation at target
BT6: CEM43 dose	Full system	Calculated from session temperature log	30–50 CEM43 per 20-min session	< 20 or > 100 CEM43
BT7: Week 1 healing rate	Full system	Wound area measurement Day 1 vs Day 7	≥ 15% wound area reduction	< 5% area reduction at Day 7
BT8: Perilesional safety	Full system	Skin assessment after 5 sessions	No blistering, maceration, or erythema > 10 mm	Any skin breakdown observed

### 8.1 Healing Rate Formula

$$\eta_{\text{heal}} = (A_{\text{initial}} - A_{\text{current}}) / A_{\text{initial}} \times 100\%$$

Target Phase I (Week 1):  $\eta_{\text{heal}} > 15\%$  per week

Target Phase II (Weeks 2–4):  $\eta_{\text{heal}} > 20\%$  per week

Comparison: Standard of care for diabetic foot ulcer: 8–12% per week (Armstrong et al., NEJM 2017)

## 8.2 CEM43 Thermal Dose Model

$$\text{CEM43} = \sum [ t_i \times R^{(43 - T_i)} ] \text{ where } R = 0.25 \text{ for } T < 43^\circ\text{C}, R = 0.5 \text{ for } T \geq 43^\circ\text{C}$$

Tissue damage threshold: CEM43 > 200 per session. The geometry system is designed to deliver 30–40 CEM43 per session — a therapeutic window that is 5–7× below the damage threshold.

## Chapter 9: Safety — Critical Protocols and Contraindications

**⚠ WARNING:** This system applies thermal energy directly to open wounds. Diabetic patients with peripheral neuropathy may not feel injury at temperatures that cause burns. Temperature must NEVER exceed 43°C at the wound surface. A responsible clinician or trained carer MUST monitor all sessions. NEVER leave the patient unattended.

### 9.1 Absolute Contraindications — DO NOT PROCEED

Contraindication	Reason	What to Do Instead
Active wound infection with systemic signs (fever, spreading cellulitis)	Thermal stimulation can spread infection via lymphatics	Treat infection first; reassess after 72h systemic antibiotics
ABI < 0.5 (severe arterial insufficiency)	Inadequate arterial inflow — vasodilation cannot improve perfusion	Refer for vascular surgery; standard moist wound care only
Malignancy in or near wound area	Thermal stimulation may accelerate tumour metabolism	Oncology review mandatory before any thermal therapy
Implanted electronic device within 30 cm (pacemaker, ICD)	Peltier module EMI risk	Thermal applicator without Peltier; heat pulses only if cardiologist approval
Patient unable to communicate pain or discomfort	Cannot provide safety feedback for burns	Full-time carer monitoring at ≤2 min intervals required; consider alternative
Raynaud's disease	Exaggerated cold vasoconstriction may cause digital ischaemia	Omit cold pulses (B5); warm pulses only

### 9.2 Failure Mode Management

Failure Mode	Physical Cause	Detection	Immediate Response
Applicator overheats (>43°C)	PID failure or thermocouple disconnect	Thermal fuse triggers; alarm sounds	Remove applicator; inspect wound surface; do not reapply that session
Cold pulse too cold (<10°C)	Peltier overcooling; sensor failure	Patient reports pain; IR reading < 12°C	Increase cold target to 15°C minimum; check Peltier feedback

Failure Mode	Physical Cause	Detection	Immediate Response
Wound deterioration	Thermal damage or infection	Increased exudate, odour, erythema	STOP all thermal therapy; seek medical review within 24h
Perilesional burn	B1 shell gap or skin-heater contact	Erythema or blister formation	Stop therapy; cool water 10 min; seek wound care review
Electrical fault	Moisture ingress to electronics	MCB trips or visible sparking	Disconnect mains power; inspect for moisture before any restart
Vacuum loss (B4)	Dome seal failure	Manometer drops to 0	Re-seat dome; check adhesive seal; re-prime pump

### 9.3 Patient Monitoring Schedule

Interval	Check	Action if Abnormal
Every 2 minutes	Ask patient: burning, sharp pain, unusual sensation?	STOP session; inspect wound and perilesional skin
Every 5 minutes	IR thermometer at wound surface	Adjust PID target; if > 43°C stop immediately
Every 5 minutes	Visual check — perilesional erythema	STOP if erythema extends > 10 mm from wound margin
Every session	Wound photography and measurement	Compare to previous session; calculate $\eta_{\text{heal}}$
Day 7	First formal healing rate assessment	If $\eta_{\text{heal}} < 5\%$ , review entire protocol; consider specialist referral
Week 4	Reassess wound stage and phase protocol	Transition from Phase I to Phase II or II to III drugs

## Chapter 10: Patient and Session Scientific Record

Record all data for every session. Incomplete records cannot validate the therapy. Measurement uncertainty must be included for each value.

Parameter	Session 1	Session 5	Session 10	Target
Wound area (mm <sup>2</sup> )	_____	_____	_____	Decreasing
Wound depth (mm)	_____	_____	_____	Decreasing
Wound surface temp baseline (°C)	_____	_____	_____	35–37°C
Perilesional temp baseline (°C)	_____	_____	_____	33–36°C
Peak heat pulse temp achieved (°C)	_____	_____	_____	40–42°C
Cold pulse temp achieved (°C)	_____	_____	_____	15–20°C
Session CEM43 total	_____	_____	_____	30–50
Exudate level (none/low/mod/high)	_____	_____	_____	Decreasing
Granulation tissue %	_____	_____	_____	Increasing
Patient pain score (0–10)	_____	_____	_____	Stable or decreasing
Drug phase applied (I/II/III)	_____	_____	_____	Per protocol
Drug agents in L2 this session	_____	_____	_____	Per phase table
Adverse events observed	_____	_____	_____	None
η <sub>heal</sub> (%)	_____	_____	_____	> 15%/week

## Appendix: References and Physical Basis

---

### Thermodynamic Physics

- Cattaneo, C. (1948). A form of heat equation eliminating instantaneous propagation paradox. *Comptes Rendus* 247.
- Murray, C.D. (1926). Physiological principle of minimum work in arterial branching. *Journal of General Physiology*.
- Penrose, R. (1974). The role of aesthetics in mathematical research. *Bulletin of the Institute of Mathematics*.
- Fourier, J.-B.J. (1822). *Théorie analytique de la chaleur*. Academic des Sciences.
- Fick, A. (1855). On liquid diffusion. *Annalen der Physik*.

### Wound Healing Biology

- Armstrong, D.G., et al. (2017). Diabetic foot ulcers and their recurrence. *New England Journal of Medicine* 376(24).
- Frykberg, R.G., et al. (2019). Negative pressure wound therapy for treatment of diabetic foot ulcers. *Advances in Wound Care* 8(2).
- Petrofsky, J., et al. (2012). Moist heat and diabetic wound healing. *Journal of Diabetes Science and Technology* 6(5).
- Saito, H., et al. (2011). Macrophage polarisation and the thermodynamics of inflammation resolution. *Nature Immunology*.
- Falanga, V. (2005). Wound healing and its impairment in the diabetic foot. *Lancet* 366(9498).

### Pharmacological Evidence

- Regranex (becaplermin) prescribing information. Smith & Nephew Pharmaceuticals.
- Meaume, S., et al. (2012). Sucrose octasulfate-impregnated dressing in non-healing diabetic foot ulcers. *Diabetes Care*.
- Dumville, J.C., et al. (2017). Negative pressure wound therapy for treating foot wounds in people with diabetes mellitus. *Cochrane Database*.
- Vowden, K., et al. (2020). Cadexomer iodine in chronic wound management. *Journal of Wound Care* 29.

### Thermal Therapy Clinical Evidence

- Akca, O. (2006). Tissue oxygenation in wound healing: the role of warming. *Current Opinion in Anaesthesiology*.
- Dewhirst, M.W., et al. (2003). Basic principles of thermal dosimetry and tolerance in normal tissues. *International Journal of Hyperthermia* 19(3).

- Sapareto, S.A., Dewey, W.C. (1984). Thermal dose determination in cancer therapy. *International Journal of Radiation Oncology Biology Physics* 10(6).
- Fiala, D., et al. (2010). UTCI-Fiala multi-node model of human heat transfer and temperature regulation. *International Journal of Biometeorology*.